



# Reference manual

## 20-sim 4.3

Windows XP / Vista / 7 / 8

# 20-sim 4.3 Reference Manual

© 2013, Controllab Products B.V.

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## Reference

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# 1 Welcome to 20-sim



This manual describes 20-sim 4.3 in full detail. It is not a getting started manual but intended as a detailed reference to the software. If you are a first time user you are advised to read the Getting Started manual first:

If you are an experienced 20-sim user, you can read the change notes first and then search the topic of your interest.

## 2 What is new in 20-sim?

### General

1. The 20-sim interface has been changed to reflect the new corporate identity. There is now a new logo for 20sim. The about boxes of both 20sim and 3D mechanics are changed.
2. Autosave now also saves simulation experiments.
3. A functionality is added to check for updates online.

### Editor

1. 20-sim 4.3 uses GDI+ for better drawing. The line drawing in the graphic editor is also improved.
2. Auto-sizing of icons for default models is added.
3. Preview of formatting of the text editor for the text box of the graphical editor is now available.
4. Choice list for making connections etc. is now provided. Connection can now be double clicked for selection.
5. Closing Graph Editor also closes the Simulator window. The same is true for loading a new model, this closes the Simulator window as well.
6. Zooming with Alt-mousewheel is now possible.
7. *Save a Copy As* is added as an option for saving a model. It is very helpful for making snapshots of your model.
8. Background Image is added to a model property. Models and sub-models can now have a background picture.

### Simulator

1. It is now possible to move plots and curves among plot windows. All plot windows are listed in a tree at the left window pane.
2. Dragging and dropping of plots and curves within a plot window is now possible.
3. The distribute curves button which was missing in 20-sim 4.2 is back.
4. The right mouse menu on plots now contains additional options for moving plots and more features like analyzing data.
5. The tools option is added to the menu bar of all plot windows.
6. An option to copy all plots altogether from a plot window to clipboard is added.
7. Export of plots to clipboard and bitmap is now possible in both screen resolution and high resolution.

### Library

1. A new implementation has been added to Function table. It is now possible to input table values from a matrix.

2. Unsigned counter support is added to the incremental encoder implementation.

### **Frequency Domain Toolbox**

1. Ctrl-B can now be used as shortcut for Dynamic Error Budgeting.
2. Nyquist plot now always starts scaling on [-2,2] on both axes.
3. Dynamic Error Budgeting: With file input, it now only uses numbers within the range of the file and assumes zero outside. This fixes inconsistencies with different frequency ranges for other inputs.

### **3D Mechanics Editor**

Sensors and Actuator Property window also have break and add connection button.

### **Ccode Generation**

Templates revised e.g. template supports XXDelay, XXInitialFunction and XXStopSimulation

### **Bugfixes and Improvements**

#### **General**

1. Better memory management.
2. Importing old 4.0 models is improved.
3. Better implementation of Table/File for large files.
4. Matlab connection: Better checking on sizes of variables that are communicated.
5. DataFromFile: now always first looks at the model location for the file name.
6. Changes made in plot windows will also trigger a saving option when a model is closed.
7. Exponent notation for numbers now accepts a plus. Example: real R = 1e+029.
8. String parameter that contain a comma (,) are now properly stored and read back from file.
9. In some cases a discrete expression was not calculated in discrete time. Example [a1,a2] = expression; with a1 and a2 scalars could trigger this bug. This is fixed.
10. On some multiple monitor display systems, the menu could appear on the wrong screen
11. Better checking of window positions, plot windows will no longer open outside the windows boundaries.
12. License: Better checking of entered keys, thus preventing typo's.
13. If a user does not have Administrator rights then the possibility to install the license for All Users in the License Activation Wizard is grayed out.

#### **Editor**

1. Right Mouse Menu on tree, Model Properties now really opens the correct level and not on a possible selection.
2. Servo Motor Editor now properly saves a model and library again.

3. Parameter Editor, during editing a value and then clicking on the model tree did not apply the value, this has been fixed.
4. Better synchronization of global parameters.
5. Choosing Plot dialog is now re-sizable, and you can double click to select an entry.
6. Find results now show longer lines before breaking with a ...
7. Auto Causality is now also possible for very large models (>500 bonds).
8. A new default implementation is added for the Integrate-Reset library block to prevent problems with some integration routines like RungeKuttaFehlberg, BDF and MeBDF.

## **Simulator**

1. Some borders are removed for better layout. Also a better theme support for Windows XP is provided.
2. Copy to clipboard now also aligns strip charted plots.
3. Automatic plot variables (variables that end on '\plot') are now automatically added to a new empty plot.
4. Multiple run: redraw is handled properly at the end of each run when needed.
5. Copy Experiment to Clipboard works again.
6. Copy to Clipboard, thickness of box of legend is now properly scaled.

## **Toolboxes**

1. 3D Animation: Crash which was caused during Cut/Delete because of redraw appearing too early is now fixed.
2. Nyquist and Nichols plot properties also show pages for x- and y-axes.
3. Dynamic Error Budgeting: responses are now always independent of the selection of *Show All Outputs*.

## **3D mechanics Editor**

1. View Toggle buttons now really toggle again.
2. Copy/Paste works again.
3. The create and break connection for sensors in 3D mechanics is fixed.

## **Model Processing**

Automatically generated variables for states/rates etc. now always have unique names.

## **3 Requirements**

20-sim only works on computers that will meet the following requirements:

- Operating System: Windows XP, Vista or 7.
- Processor requirements: 20-sim requires a CPU with SSE2 support. Supported: Intel Pentium 4 and above, AMD Athlon x64 and above.
- Available Disk Space: 350 MB.

## 4 Installation

### 4.1 Versions of 20-sim

20-sim is available in three versions: Viewer, Standard and Professional.

- **Viewer/Demonstration version:** This is a freeware version that allows you to load and run models and evaluate the package. Saving of models is not possible in this version.
- **Standard:** This is the standard version of 20-sim. It has no limitations but only includes the Frequency Domain Toolbox.
- **Professional:** This is the full version of 20-sim with all toolboxes.

The table below shows in detail the options that are available in the three versions:

	Viewer	Standard	Professional
Library Models	v*	v	v
3D Mechanics Toolbox	v*	x	v
Animation Toolbox	v*	x	v
Control Toolbox	v*	x	v
Frequency Domain Toolbox	v*	v	v
Mechatronics Toolbox	v*	x	v
Real Time Toolbox	v*	x	v
Time Domain Toolbox	v*	x	v

**v** = included

**v\*** = included but no saving possible

**x** = not included

20-sim is installed, using an Installation Manager that will lock 20-sim to your computer. There are three types of licenses available:

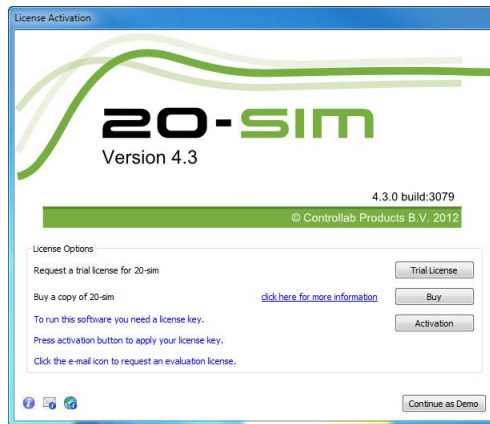
- **Free :** The demonstration version comes with a license that is not locked to your computer. No actions have to be taken after installation of the program.
- **Single License:** A single license locks 20-sim to a specific computer. After installation you have to register to get a valid license.
- **Floating License:** A floating license allows multiple users to work with 20-sim at the same time. After installation you have to register to get a valid license.

## 4.2 Installing 20-sim

20-sim can be downloaded from the website [www.20sim.com](http://www.20sim.com). This is an installation file that will install 20-sim on your computer. The first 4 steps are equal for all users. Depending on the type of license (single, floating) you have to continue differently

1. **Download** and **Install** the 20-sim on you computer.
2. **Start** 20-sim (from the **Windows Start Menu** choose **20-sim 4.3**).

If a valid license of 20-sim was activated before, the program will start automatically. If you have not installed 20-sim before, the *License Activation* dialog will open:

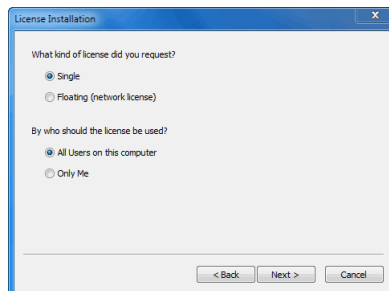


*20-sim 4C 2.0 License Activation Dialog.*

3. If you have a valid license key or license file, press the **Activation** button to enter your license key or browse for the license file.

If you do not yet have a valid license, press the **Trial License** button request an trial license or press the **Buy** button to purchase a license.

4. Select **which kind of license** you have and **who** should use the license.



*License installation dialog.*

### Single License

If you are using a single license, you have to enter a license key or license file.

- On the next dialog, select ***I received a license key by e-mail*** and enter the **key** in the next dialog. When you received a **license file**, you have to enter the **location** of the license file.

You will be asked for confirmation (click **Activate Now**) and activation will be carried out. After a successful activation process the License Information dialog will show the new license (Standard License or Professional License).

## Floating License

### Installing a floating license (Administrator)

If you are using a license that is shared by more users (floating license, also known as concurrent license or server license), you have to enter the received license key and a location on the server (a normal Windows shared folder) first. This location on the server should be accessible to all users and have read/write permission. The floating license will be stored at the selected location.

- On the next dialog, select **First Installation** and then enter the **license key** and the **location on the server** (Windows share).

On the location that you have given, a license file **20sim.lic** will be installed. Remember the location of this file because every new user of 20-sim will need to enter it. You will be asked for confirmation (click **Activate Now**) and activation will be carried out. After a successful activation process the License Information dialog will show the new license (Standard License or Professional License).

### Using a floating license (Other users, Administrator)

If you are using a floating license that was already installed you have to enter the location of the license file.

- On the next dialog, select **Administrator already installed server license** and then enter the **license location**.

After a successful entry of the location of the license location, the License Information dialog will show the new license (Standard License or Professional License).

## 4.3 Uninstalling

You can uninstall 20-sim by clicking the Uninstall command from the 20-sim start menu. Uninstallation of 20-sim *will not deactivate* your license. If you want to move 20-sim to another computer, you have to deactivate your license first before uninstalling.

## 4.4 Deactivation

If you want to move 20-sim to another computer, you have to deactivate your license before uninstalling the program. On the new computer you can then install the program and activate the license. To deactivate your license:

- From the Windows **Start menu** open **20-sim**.
- From the **Help** menu choose **License Activation**.
- Press **the Activation button**.
- Choose **Deactivate Current License**.



You will be asked for confirmation and deactivation will start. After a successful deactivation, your version of 20-sim has turned into the demonstration version. You can now uninstall the software and reinstall it.

## 4.5 Unattended Installation

An unattended installation is an installation that is performed without user interaction during its progress or with no user present at all.

To perform an unattended installation the default 'program files' installation directory run the following command :

```
20-sim-4.3.x.x-win32.exe /S
```

It is possible to set an alternative installation directory by specifying the /D argument. It must be the last parameter used in the command line and must not contain any quotes, even if the path contains spaces. Only absolute paths are supported.

```
20-sim-4.3.x.x-win32.exe /S /D=D:\My Installation Files\20-sim 4.3
```

## 4.6 Matlab

In 20-sim you can exchange data with Matlab / Simulink in various ways:

- Export models as m-files
- Export models as dll-files
- Export a variable to Matlab
- Export a parameter to Matlab
- Pass a variable value to Matlab every simulation step
- Load a variable value from Matlab every simulation step
- Pass a command line string to Matlab every simulation step
- Export linear systems to Matlab
- Import Linear Systems from Matlab

### Troubleshooting

If this fails check if the following three points have been fulfilled.

#### 1. Have the correct version of 20-sim and Matlab

To make a connection with Matlab, make sure you have 20-sim 4.1.3.8 or higher installed and a 32-bit version of Matlab.

The 20-sim Matlab connection makes use of a 32-bit COM component, therefore it is not possible to connect from 20-sim to a 64-bit version of Matlab, which do not provide a 32-bit COM component.

#### 2. Matlab registration in PATH

The standard registration of Matlab in the PATH is the following (assuming Matlab is installed in Program Files):

```
C:\Program Files\MATLAB\R2011b\bin
```

The following path should be added:

*C:\Program Files\MATLAB\R2011b\bin\win32*

In this additional path some important DLL's are present that are necessary to make the connection. for example: libeng.dll. Please check if this DLL is present at this path. If not try to find this DLL in your Matlab installation and add the found path to the PATH environment.

Changing the PATH environment variable can be done in the following manner:

1. From "My Computer", right mouse button: Properties:
2. On Windows 7: choose Advanced Properties and go further as Admin, On Windows XP: you go directly to the System Properties dialog
3. Choose the tab: Advanced
4. Choose: Environment Variables.

### **3. COM-registration**

To make the connection to Matlab, Matlab needs to be registered as a COM-component. This can be done in the following manner from the command line (run: cmd):

*matlab /regserver*

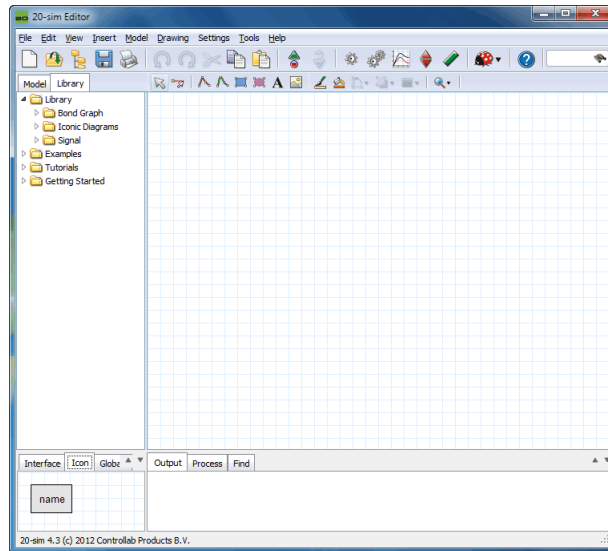
Note: The COM-registration only, is not enough for 20-sim to find the DLL's of Matlab. The second step (setting the PATH variable) must be performed.

## 5 Editor

### 5.1 Introduction

#### Editor

20-sim consists of two main windows and many tools. The first window is the *Editor* and the second is the *Simulator*. The *Editor* is used to enter and edit models. The *Editor* opens automatically when you start 20-sim:



*The 20-sim Editor.*

The *Editor* consists of four parts:

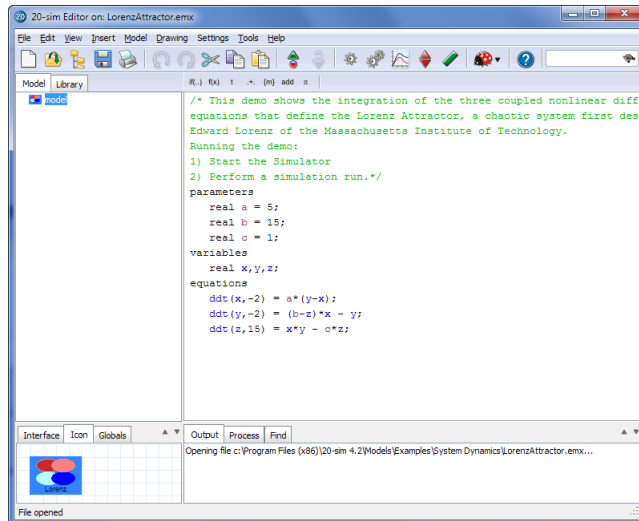
- **Model tab / Library tab:** The Model tab shows the model hierarchy, i.e. the composition of all the elements of the model. The Library tab shows the 20-sim library.
- **Graphical Editor / Equation Editor:** At the lowest level of the hierarchy this editor will show the model equations. In the higher levels this editor will show the graphical parts of your model.
- **Output tab / Process tab / Find tab:** The *Output tab* shows the files that are opened and stored. The *Process tab* shows the compiler messages. The Find tab shows the search results.
- **Interface tab / Icon tab / Globals tab:** The Interface tab shows the interface (inputs, outputs, ports) of a selected model. Double clicking it will open the Interface Editor. The Icon tab shows the icon of a selected model. Double clicking it will open the Icon Editor. The Globals tab will show the global parameters and variables of your model. Double clicking it will open the Global Relations Editor.

#### Using the Editor

The best way to find your way around the Editor is to read the Getting Started manual. It contains a number of topics that will explain the basics of entering equation models, graphical models and run a simulation.

## Equation Editor

Equations models are the models at the lowest level in the model hierarchy. A model without an interface (inputs, output, ports), will have no hierarchy and is thus automatically an equation model. If you have opened an equation model, the right part of the *Editor* shows the *Equation Editor*. In the *Equation Editor* you can enter and edit equation models.



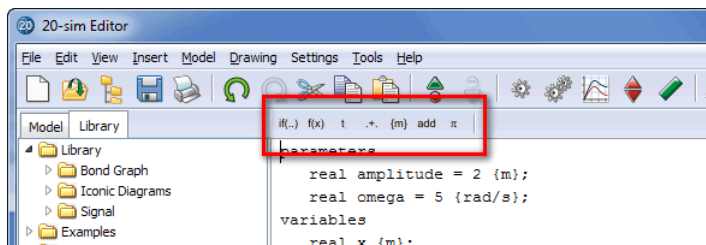
*Equation model with the Equation Editor (right part).*

## Use

Put your mouse in the *Equation Editor* and start typing. If you click on the buttons of the taskbar, sample code is inserted. Read the language reference section to find out more.

## Equation Editor Taskbar

When you select an equation model, the corresponding equations are shown in the *Equation Editor*. A special button bar, called the *taskbar*, is part of the *Equation Editor*. The *taskbar* helps you to enter functions, statements, templates etc.



*The taskbar of the Equation Editor.*



**Statements:** click on this button to insert if-then-else expressions and more.



**Functions:** click on this button to insert functions.



**Specials:** click on this button to insert special functions.



**Operators:** click on this button to insert operators.



**Units:** click on this button to insert quantities and units.



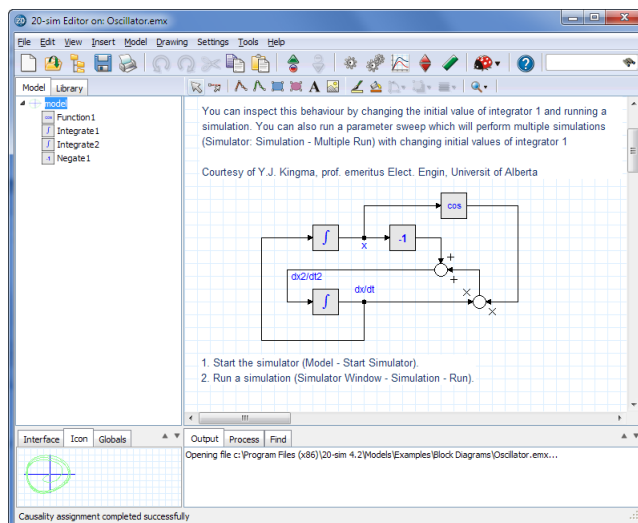
**Declarations:** click on this button to insert declarations of parameters, variables and more.



**Constants:** click on this button to insert predefined constants.

## Graphical Editor

If you have opened a graphical model, the right part of the *Editor* shows the *Graphical Editor*. In the *Graphical Editor* you can enter and edit block diagram models, iconic diagram models and bond graphs.



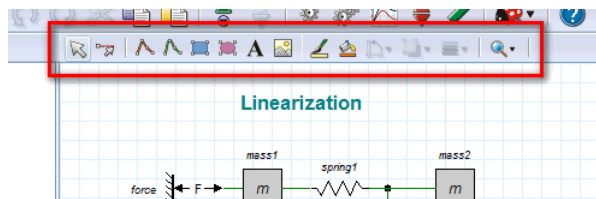
*Graphical model with the Graphical Editor (right part).*

## Use

Select models from the *Model Library* and drag them to the *Graphical Editor*. You can use the buttons of the taskbar, to connect the models and change their position.

## Graphical Editor Taskbar

When you view or enter a graphical model in 20-sim it is shown in the *Graphical Editor*. A special button bar, called the *taskbar*, is part of the *Graphical Editor*. The *taskbar* helps you to select models, connect them and manipulate them. You can also use the taskbar to enter drawing objects. The taskbar is also part of the *Icon Editor*.



*The taskbar of the Graphical Editor.*



**Selection Mode:** Click this button to select models and objects



**Insert Terminals:** (*Icon Editor* only) Click this button to insert terminals.



**Connection Mode:** (*Graphical Editor* only) Click this button create connections between models.



**Line:** Click this button to draw lines.



**Spline:** click this button to draw splines.



**Rectangle:** click this button to draw rectangles.



**Ellipse:** click this button to draw ellipses.



**Text:** click this button insert text.



**Bitmap:** click this button insert bitmaps.



**Line Color:** click this button to set the line color of a selected object.



**Fill Color:** click this button to set the fill color of a selected object.



**Rotate and Mirror:** click this button to rotate or mirror a selected object.



**Arrange and Group:** click this button to group objects, put them to the front etc.



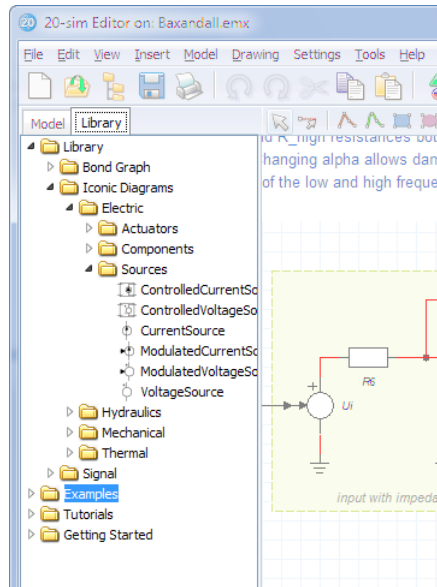
**Line Styles:** click this button to select the line style of selected objects.



**Zoom:** click this button to select the zoom factor.

## Library

In 20-sim, creating models only takes you just a few mouse clicks. By *dragging* an element from the library and *dropping* it in the graphical editor, your model is actually built the same way as you would draw an engineering scheme. 20-sim supports various model representations, such as block diagrams and iconic diagrams. These representations may be combined in one model.



*You can find the library at the left of the Editor.*

The library contains a various sections:

- Bond Graph: bond graph elements
- Iconic Diagrams: Physical components
- Signal: Block diagram elements
- Tutorial: example models that show you how to perform various tasks in 20-sim
- Getting Started: all the models that you need in the lessons of the Getting Started manual.

## Custom libraries

You can create your own model libraries in 20-sim:

1. From the **Tools** menu click **Options - Folders - Library Folders**.
2. Add your **folder**.
3. Give it a useful **name** by clicking **Edit Label**.
4. Click OK to close the dialog.

Then you can add your own library models to the library:

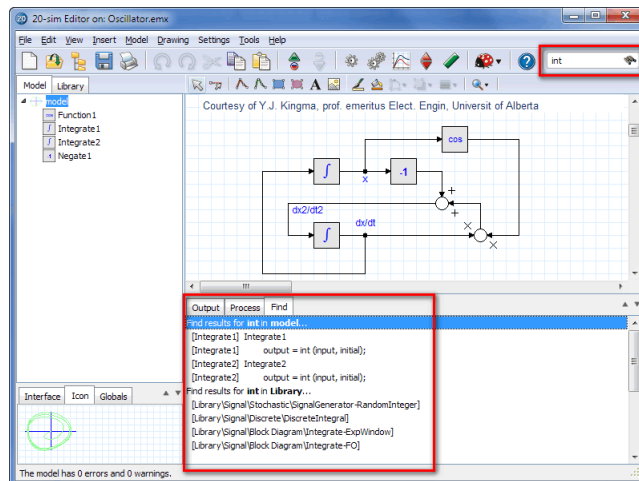
1. Select the **submodel** that you want to store in your library.

- From the **File menu** select **Save Submodel**.
- Store the submodel in your library **folder**.

The next time you start up 20-sim, the library will show the new submodel.

## Find

If you make the *Editor* wide enough, you will see at the top right a *Find box*. You can enter terms here and search them throughout the model. The results are displayed in the *Find tab* at the bottom of the *Editor*.



*Using the Find Box to quickly search the model.*

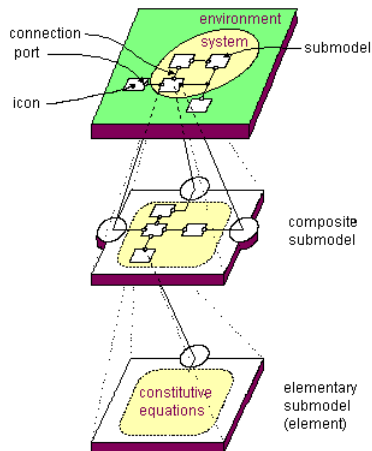
- Scope: The search scope depends on which level of the model you are in. Only the current submodel and all submodels below are searched. Select the top element in the Model Browser (Model tab at the left of the Editor) to search the whole model.
- Library: The 20-sim Library is always searched. The library results are shown below the model search.
- Jump: The Find tab shows the found items with an orange hyperlink. Click on the hyperlink to quickly jump to the corresponding model.
- Find again (F3): Click the F3 button to quickly jump through the found items in the Find tab.
- Menu: You can also start a search from the menu: from the *Edit* menu select *Find*.
- 

## 5.2 Using Models

### Hierarchical Models

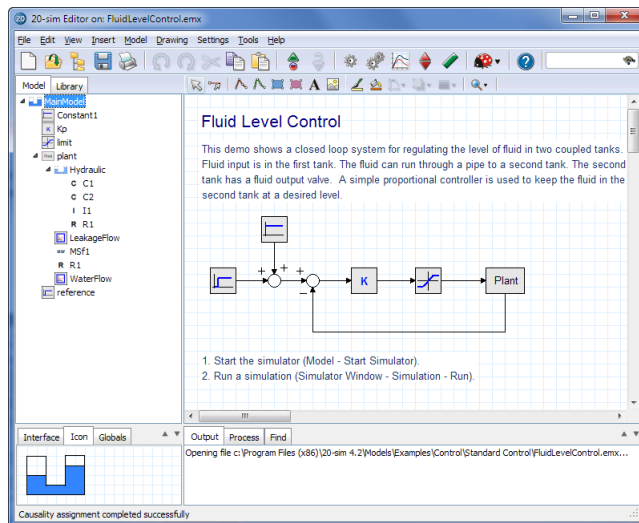
Any *main model* (or system) in 20-sim may be described as a composition of lower level *submodels*. These submodels themselves may again be described as a composition of lower level submodels etc. The lowest level consists of elementary submodels, which do not consist of submodels themselves.







*20-sim supports hierarchic model. The lowest model in the hierarchy is always an equation model.*

You can inspect this in the *Editor*. If you click the *Model* tab at the left of the *Editor*, the *Model Browser* shows complete model hierarchy: a tree like structure showing all the submodels that are used in the model.



*The Model Browser at the left of the Editor shows the complete model hierarchy.*

To travel through the hierarchy, click any model in the tree. You can also select a model in the *Graphical Editor* and click *Go Up*  or *Go Down*  from the *Model* menu.

## Open Models

Models in 20-sim are stored with the extension *.emx*. You can open an existing model in several ways:

1. From the **File menu**, select **Open**.
2. Click the Library tab and from the Library **drag and drop** your model to the *Graphical Editor*.
3. Open a **Windows Explorer**. **Drag and drop** your model to the *Graphical Editor*.

You can open Packed Files with the *Open* dialog by selecting a file with the extension *.emz*.

## Save Models

Models in 20-sim are stored with the extension *.emx*. You can save an existing model in several ways.

1. From the **File menu**, select **Save**: This will save the complete model. If no filename is known a Save dialog is opened.
2. From the **File menu**, select **Save As**: This is essentially the same as the *Save* command but now the *Save* dialog is opened even if a filename is known.
3. From the **File menu**, select **Save a copy As** : This is similar to *Save As* but now a copy of the file is saved instead. This allows the user to keep on working on the model while saving intermediate experiments.
4. From the **File menu**, select **Save Submodel**: This will save the submodel that is selected in your *Graphical Editor*.
5. From the **File menu**, select **Save Encrypted**: This will allow you to store a model using encryption. If a submodel was selected, a menu is opened asking you to store the submodel or the complete model.

Once a model is encrypted, you can not decrypt it anymore! So keep cautious that you always store a non-encrypted original. Encrypted models are useful if you want others to use your 20-sim model, without seeing the underlying equations. If encrypted model is load in 20-sim, the *Go Down* command will does not work on that model.

## Packed Files

To get a simulation running in 20-sim, the data stored in various files may be needed:

- *.emx*: model files
- *.txt*: data files (fileinput)
- *.bmp*: bitmap files (for use in 3D Animation)
- *.dll*: external dll-files (user defined external functions)
- etc.

You can pack all these files into one zip-file, using the **Pack** command from the **File** menu. With this command 20-sim will check all the files that are used and store them into a single zip-file. This option is useful for archiving and sending models by e-mail.

### Pack

1. When the **Pack** command is clicked, a *Save As dialog* appears asking you to enter a name. Always save with the default extension **.emxz** because 20-sim uses this extension to recognize packed files.

After the *Save As* dialog, a *20-sim Pack dialog* appears, showing the collected files. In this dialog you can select the files that should be packed.

2. **Select** the files that should be packed and click the **OK** button.

### Unpack

You can open Packed Files using the *Unpack* command from the *File* menu.

1. When the **Unpack** command is clicked, an *Open dialog* appears asking you open a file. Open a file with the extension **.emxz** because 20-sim uses this extension to recognize packed files.

After the *Open* dialog, a *20-sim Unpack dialog* appears. In this dialog you can see the file that you have selected to unpack and you can choose the method of unpacking.

2. If you want to unpack all files and put them in their original location, select the option **Unpack with full path**.
3. If you want to unpack all files and to a specific directory, select the option **Unpack to directory**.
4. Select **Keep Relative Paths** if you want to keep the original folder structure.

### Insert Models

You can insert submodels from a library using the built in Library tab:

1. Click the Library tab to open the library.
2. Select the submodel that you want to insert and **drag and drop** it in the **Graphical Editor**.

You can also use a file browser:


1. From the File menu, select **Open Browser**. The File Explorer appears.
2. Select the submodel of interest and **drag and drop** it in the **Graphical Editor**.

## Connecting Models

In 20-sim, submodels can be connected using the mouse. When a connection is created it will be displayed using straight lines. When a connection has been made you can change it into a smooth line using the right mouse menu. You can change the color of a connection using the colorbar at the bottom of the Editor. 20-sim supports two types of mouse use. "Tapping Mode" and "Pressing Mode". In the Tapping Mode you click the mouse button (do not keep it pressed but quickly "tap" the button) while making a connection. In the Pressing Mode you keep the mouse button pressed while making a connection.


### Tapping Mode

To connect two submodels using straight lines, you have to:

1. In the toolbar, click  to change to **connection mode**.
2. Put the **mouse pointer** on top of the **first submodel** and **click the left mouse button** (do not keep it pressed but quickly "tap" the button).
3. Drag the **mouse pointer** towards the second submodel (you will see a connection drawn from the first submodel towards the mouse pointer).
4. Put the mouse pointer on top of the **second submodel** and click the **left mouse button** again (do not keep it pressed but quickly "tap" the button).
5. While dragging from the first submodel to the second, you can click the left mouse button (do not keep it pressed but quickly "tap" the button) to create **intermediate points**.


### Pressing Mode

To connect two submodels using straight lines, you have to:



1. In the toolbar, click  to change to **connection mode**.
2. Put the **mouse pointer** on top of the **first submodel** and press **left mouse button** (keep it pressed).
3. Drag the **mouse pointer** towards the second submodel (you will see a connection drawn from the first submodel towards the mouse pointer).
4. Put the mouse pointer on top of the **second submodel** and release the left mouse button.
5. While dragging from the first submodel to the second, you can click the right mouse button to create **intermediate points**.

### Smooth Line

To connect two submodels using a smooth line, you have to:


1. Make a **straight line** connection with **intermediate points**.
2. In the toolbar, click  to change to **selection mode**.
3. **Select** the connection that was created.
4. From the **right mouse** menu select "**smooth line**".

## Tips


- 20-sim will automatically detect which connection has to be made: a signals, a bond or an iconic diagram connection.
- Depending on the physical domain, every connection will have a specific color. You can change these colors in the Units Editor.
- You can toggle between connection mode  and selection mode  by pressing the space bar.

## Implode / Explode

Using the **Implode** command of the **Editor** menu you can quickly create a new submodel out of a set of select submodels.

1. In the toolbar, click  to change to selection mode.
2. Select the the submodels.
3. From the **Edit** menu, click the **Implode** command.

Using the **Explode** command of the **Editor** menu you can quickly open the contents of a selected submodel in the current model layer.

1. In the toolbar, click  to change to selection mode.
2. Select a submodel.
3. From the **Edit** menu, click the **Explode** command.

## Simplify Models

Use the *Simplify Model* command to simplify graphical models according to the following rules:

### Block Diagrams

1. Combining splitters.
2. Combining of multiplications and/or divisions.

### Bond Graphs

1. Eliminating junctions.
2. Melt equal junctions.
3. Eliminating double differences.

### Iconic Diagrams

1. Eliminating nodes.

To simplify a (sub)model, you have to:

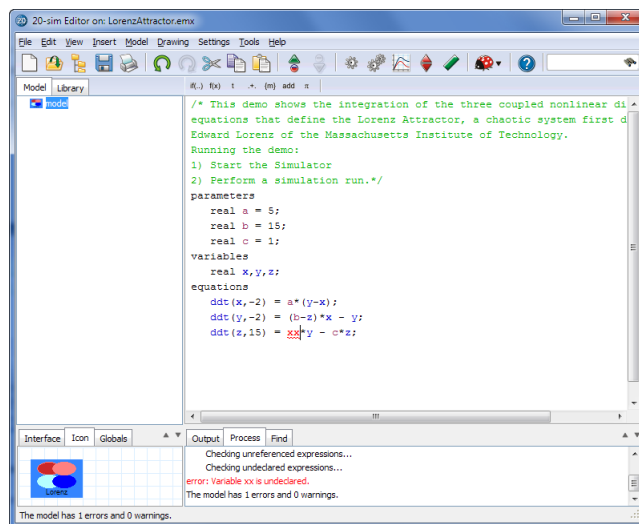
1. Select the complete model or submodel of which you want to simplify.
2. From the **Model** menu select the **Simplify Model** command.

## Check Models

To check a complete model, you have to:

1. From the **Model** menu select the **Check Complete Model** command. Now the complete model will be checked.

If any warnings or errors are found, they are displayed in *Process tab* of the Editor.



*In the Process tab the compiler messages are displayed.*

2. Put your **mouse** on top of an **error message** and click.

20-sim will jump to the part where the error was caused. You can try to solve the error and check again.

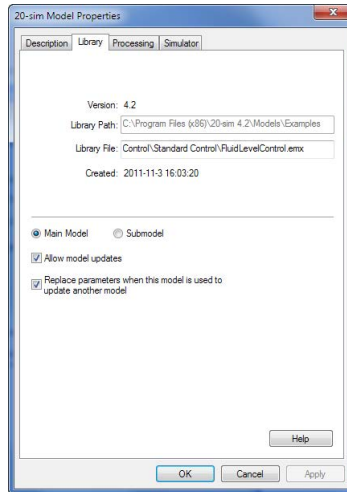
## Model Properties

The properties of 20-sim models are shown in the *Model Properties* dialog. You can open the *Model Properties* in various ways.

- Select the proper model in the Model Browser and then click **Properties** from the **Right Mouse** menu.
- Select the model in the Graphical Editor and then click **Properties** from the **Right Mouse** menu.

- From the **File menu** choose the **Properties** command.
- From the **Settings menu** choose the **Model** command.
- From the **Settings menu** choose the **Submodel** command.

Depending if a *submodel* was selected or a *main model*, various tabs are visible:



*The model properties dialog.*

## Description

In this tab you can enter the name of the submodel and enter various fields to classify a model. The most important elements are:

- **Name:** Enter a unique name for the model.
- **Help Page:** Enter the location of a help page that should be displayed when you click *F1* or *Help*.

## Library

In this tab you can find information on location of the model and some important properties.

- **Version:** The version of 20-sim that was used to create the model.
- **Library Path:** If the model was stored in a known library, the path is shown.
- **Library File:** The relative location of the submodel in the library or the absolute location of the model submodel on your computer.
- **Created:** The date of creation.
- **Main Model / Submodel:** Shows if the model is a main model or submodel.
- **Allow model updates:** Allow the Check for Model Updates command to check if there is an update available for this model.
- **Replace parameters when this model is used to update another model:** If you drag and drop a model from the library on top of an existing model, it will be replaced. Select this option if you want the original parameters to be replaced as well.

## Processing

This tab is only available for main models. 20-sim can operate in two modes: *Debug Mode* and *Fast Mode*. In this tab you can define settings for both modes.

## Warnings/Errors

- *Model contains algebraic variables*: See the section on algebraic loops.
- *Model contains algebraic loops*: See the section on algebraic loops.
- *Algebraic variables solved*: See the section on algebraic loops.
- *Model contains constraint variables*: See the section on constraints.
- *Constraint variables solved*: See the section on constraints.
- *Model contains dependant states*: The model contains differential equations which could not be solved.
- *Dependent states are transformed*: The model contains differential equations which were solved.
- *Output is not used*: Output signals that are not used for connections to other models.
- *Input is not used*: Input signals that are not used for connections to other models (to make such models simulate, a zero input value is applied to all not-connected inputs)
- *Port is not used*: Ports that are not connected.
- *Parameter is not used*: Parameters that are defined but not used.
- *Matrix is assigned a scalar*: A matrix is assigned to a scalar.
- *Variable is not used*: Variables that are defined but not used.
- *Variable Multiple set*: Variables that are assigned a value more than once.
- *Variable is never given a value*: Variables that are never assigned a value.
- *Variable is set but not used*: The variable is assigned a value but never used.
- *Unit Conversion when SI disabled*: Not relevant yet.
- *Unit Conversion when SI enabled*: A unit conversion was found.
- *Unit missing for variable when SI disabled*: Not relevant yet.
- *Quantities Mismatch*: Variables with different quantities are compared.
- *Unit is unknown*: A unit has been used that is not available in the Quantities and Units file.
- *Equations interpreted as code*: Equations can only be valid when interpreted as sequential code. For example when variables are assigned more then once.
- *Possible loss of data at type conversion*: A type conversion has been found that may lead to loss of precision digits.
- *Type conversion found*: A type conversion has been found.
- *Conversion of booleans found*: A type conversions involving booleans has been found.

## Model optimization

- *Transform Dependents States*: Try to solve differential equations.
- *Solve algebraic variables*: Try to analytically solve algebraic loops.
- *Remove Redundant Equations*: Try to remove equations that do not influence model behavior.



- **Optimize Equation Structure:** Try to separate equations into an input section, a dynamic section and an output section.
- **Optimize Static Expressions:** Move expressions with constant output throughout the simulation to the static part of the model equations.
- **Optimize Duplicate Expressions:** Calculate an expression only once and use the result everywhere.
- **Optimize Divisions:** Rewrite divisions as multiplications whenever possible.

## Simulator

This tab is only available for main models. You can set the simulator properties here.

- **Initialize variables at start of simulation:** You can choose to set any variable that was not given a proper value, to zero at the start of a simulation. You can also choose to set the value to NaN to make detection more easy.
- **Calculate Hold Instruction During Initialization:** Calculate an output for hold functions during the initialization of the a simulation.

## General Properties

The general properties of 20-sim models are shown in the *Options* dialog.

- From the **Settings menu** choose the **Options** command.
- From the **Tools menu** choose the **Options** command.

## Editor

- **Fonts:** Enter the default fonts used in graphical models (Editor) and equation models (Equation Editor).
- **Syntax Highlighting Threshold:** Select the number of characters that should be submitted for color syntax highlighting. If this number is too large, the editor may become very slow.

## Plots

You can choose the default settings for a simulation plot in this tab.

- **Default Line Thickness:** Enter the default plot line thickness.

## Folders

You can choose the location of libraries and files in the *Folders tab*.

- **Library Folders:** Enter the library paths and corresponding library names here. The libraries are shown in the Library tab.
- **C-code Folders:** C-code can be generated for various targets. For each target a file targets.ini defines how the C-code should be generated. You can enter the locations of ini-files here.
- **Matlab-Code folders:** 20-sim models can be exported to Matlab. Similar to C-code generation, a file targets.ini defines how the code should be generated. You can enter the locations of ini-files here.
- **Model Template Folders:** You can enter the location of model templates.

## Interface

- *Enable XMLRPC Interface*: 20-sim uses the XMLRPC protocol to communicate with external software. Select this option if you want to enable external communication. The first time that you select this option, the windows firewall may give a warning message.

## Check Energetic Behavior

If you select the **Check Energetic Behaviour** command of the **Model** menu, 20-sim will check the complete model and generate additional variables. The additional variables will only be generated for submodels with powerports:

- power for every power port.
- the net power that flows into the submodel (total sum of all the powers).
- the net energy of the submodel (integrated net power)

This command is the same as Check Complete Model command but will generate extra variables:

- *Sumodelname\port.power*: the net power flow of the port.
- *Sumodelname\summated\_port\_power*: the net power flow into the model.
- *Sumodelname\summated\_port\_energy*: the net energy of the model.

You can inspect these variables during simulation in the Variable Chooser.

## Analyze Causality

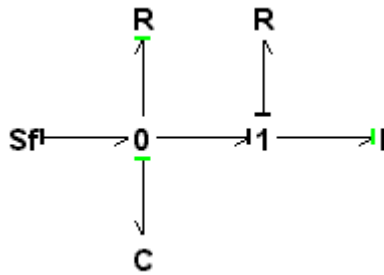
Causal analysis is the procedure to get the model equations correct form. For Bond Graph models this means that the direction of the efforts and flows of the bonds have to be determined. The result of the analysis is displayed by causal strokes (denoted by **|**). For Iconic Diagrams this means that the direction of the across and through variables of the connections have to be determined. The result of the analysis is displayed by causal arrows (denoted by **->**).

To perform causal analysis you have to:

1. From the **Model** menu select the **Analyze Causality** command. Now causality will be assigned in the complete model.

## Bond Graphs

- Causal strokes are shown in Bond Graphs automatically.
- Setting Causality can also be done by hand. Just select a bond and choose Properties from the right mouse menu. A menu pops up in which you can set causality by hand. The corresponding causal stroke is displayed in green (denoted by **|**).



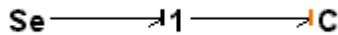
*User defined causality (denoted by |).*

- If 20-sim fails to perform a causal analysis of the model (a **causal conflict**), the corresponding bond is displayed red.



*A causal conflict (denoted by the red bond).*

- Some submodels have a preferred causality. If assignment of the preferred causality is not possible (because of other constraints), the corresponding causal stroke is displayed in orange (denoted by |).

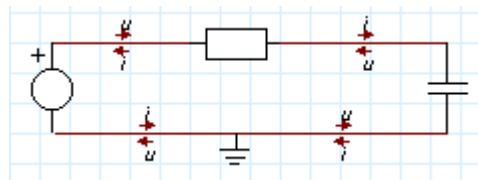


*Preferred causality not assigned (denoted by |).*

- To see the order in which automatic causality assignment has been performed, choose **Causality Info** from the **View** menu.

## Iconic Diagrams

- Causality in Iconic Diagrams is only shown when you select the **Causality Info** command of the **View Menu**.



*Causal Information shown by arrows.*

- If 20-sim fails to perform a causal analysis of the model (a **causal conflict**), the corresponding connection is displayed red.

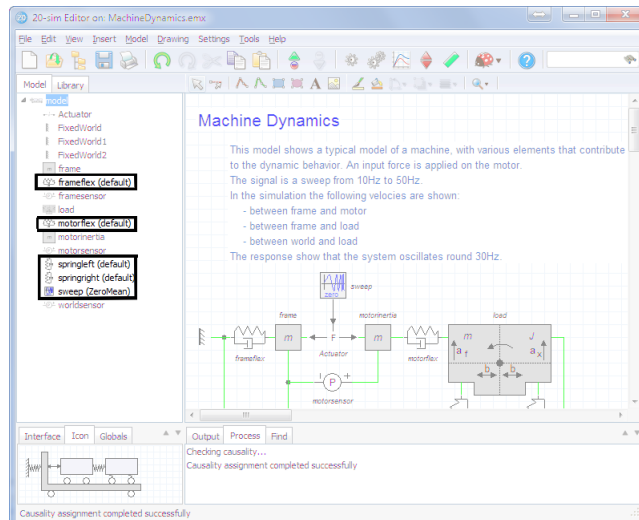
## Implementations

A model may have various implementations. It means that you can combine several versions of a model and store them in one file. If you drag and drop a model with implementations, 20-sim will ask which one to use.

## Example

A fine example of a model with various implementations is the model *MachineDynamics.emx* from the *Examples\1D mechanics* library. This example model has several submodels with implementations:

- SpringDampers
- SignalGenerator-Sweep



*The selected implementation is shown between brackets in the Model Browser.*

When you drag and drop a model with implementation into the *Graphical Editor* you will be asked which implementation to use. In the Model Browser, the chosen implementation is shown between brackets (*Default* and *ZeroMean* in the picture above). If you hover the mouse above a submodel with an implementation, you also see the chosen implementation between brackets. While modeling, you may decide to change the implementation. This can easily be done by selecting the submodel and clicking the right mouse menu. Choose *Implementation* and select the implementation that you want to use.

## Construction

You can make submodels with implementations yourself:

1. **Select** a **submodel**.
2. From the **right mouse** menu choose **Edit Implementation** and **Add New**.
3. Enter the **name** of the implementation and click **OK**.
4. **Store** the submodel using the **Save Submodel** command of the **File** menu.

## Changes

You can change the implementation:

1. **Select** the submodel.
2. From the right mouse menu choose **Edit Implementation** and **select** the **implementation** that you want to change.
3. Make the **changes** that you want in the submodel.
4. **Store** the submodel using the **Save Submodel** command of the **File** menu.

## Continuous-Time and Discrete-Time Models

In 20-sim you can model continuous-time systems, discrete-time systems and combinations of continuous-time systems and discrete-time systems (hybrid) systems. By default, models in 20-sim are continuous-time, and simulated using continuous-time integration methods. However, the program will automatically identify discrete-time parts in a model and simulate them at a fixed rate.

### Continuous-Time

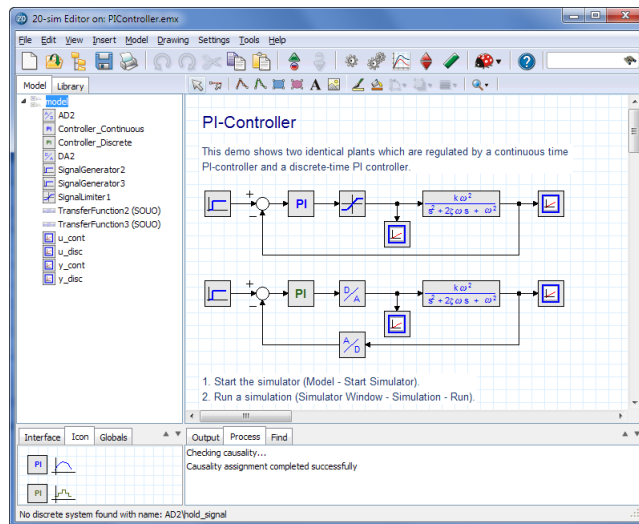
Continuous-time models describe real-world processes. To simulate a continuous-time model, the model will be calculated many steps per second to get a result that is a good representation of the real-world process. If you model a car suspension system, about 100 steps per second might be sufficient to give a good representation of the behaviour of the car. If you model an electronics circuit, 100.000 steps per second might be required. The default integration method in 20-sim will automatically choose the required steps per second.

### Discrete-Time

Discrete-time models describe processes that run on computers at a fixed rate. To simulate a discrete-time model, you only have to indicate the rate at which the model should be calculated. This is called the sample rate or sample frequency. The sample rate of a discrete-time part can be set in the Simulator.

### Mixed Models

In 20-sim you can model in continuous-time and discrete-time. Mixed models containing discrete-time parts and continuous time parts are supported as well. The example below shows a continuous time model of a PI-controlled system at the top. At the bottom the same system is shown with a discrete time controller and a continuous-time system. The discrete-time part is indicated by green input and output lines.



*Discrete-time parts of a model are indicated by green inputs and outputs.*

## Identification of Discrete-Time Parts

In 20-sim every model is continuous-time by default. Discrete-time parts of a model are identified by the occurrence of special functions:

- sample
- hold
- next
- previous
- sampletime

Normally these functions are hidden in the equations that describe a submodel, but 20-sim will automatically recognize that the input or output of such a function should be discrete-time. If the output is discrete-time it is propagated to the next function, which output is then also "*tagged*" as discrete-time, and so on until the whole discrete-time part of a model is identified. A discrete time part of a model is indicated by green inputs and outputs (see previous picture).

## Connection

Continuous-time parts of a model can be connected to discrete-time parts, by using the functions:

- sample: The sample function has a discrete-time input and continuous-time output.
- hold: The hold function has a continuous-time input and a discrete-time output.

You can find these functions for example in the following library models:

- DA.emx (Discrete to Analog Converter)
- AD.emx (Analog to Digital Converter)

- Encoder.emx (Optical Encode)

### Forbidden Functions

In a discrete part of a model, certain functions are not allowed, because they are specifically meant for the use in continuous-time models:

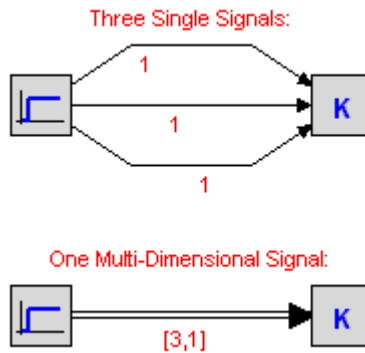
- algebraic
- constraint
- ddt
- dly
- event
- eventdown
- eventup
- frequencyevent
- int
- limint
- tdelay
- timeevent

If you use a library model that contains such a function in a discrete-time part, an error message will be given.

### Working with Multi-Dimensional Models

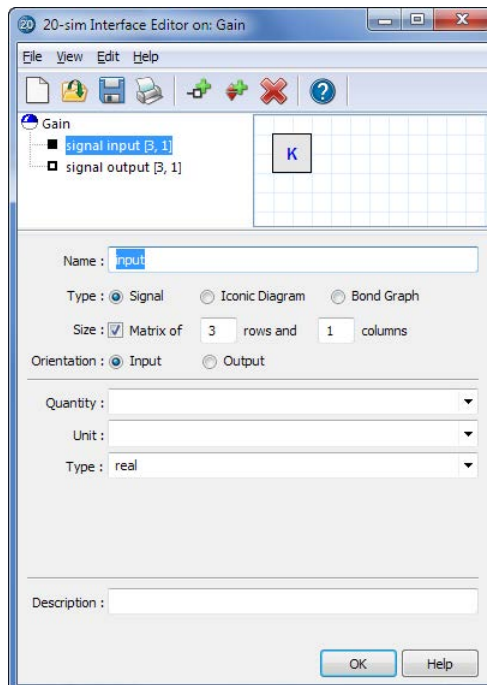
Multi-Dimensional models are models that have connections which are of a size  $[n,m]$  with either  $n$  or  $m$  larger than one. Here  $n$  is the numbers of rows and  $m$  is the numbers of columns. More information on this matrix notation can be found in the topic on matrices and vectors.

The advantage of multidimensional models is shown in the example below. On top two submodels are connected by three (single) signals. The same submodels are also shown below, connected by one multi-dimensional signal of size  $[3,1]$ . If these submodels have to be used a lot, multi-dimensional signals or multi-signals, are easier to use. Multi-dimensional signals, bonds and connections are shown in 2D-sim by double lines.



## The Secret: Multi-Dimensional Ports

The secret of multi-dimensional models is hidden in the model interface. If you open the Interface Editor to inspect an interface, you will notice that each port (signal, iconic diagram or bond graph) has a default **size** (dimension) of 1 (1 Row, 1 Column). By increasing the number of rows and/or columns this size can be increased.



*Definition of Multi-ports: increase the number of rows or columns.*

## The Trick: Automatic Connection

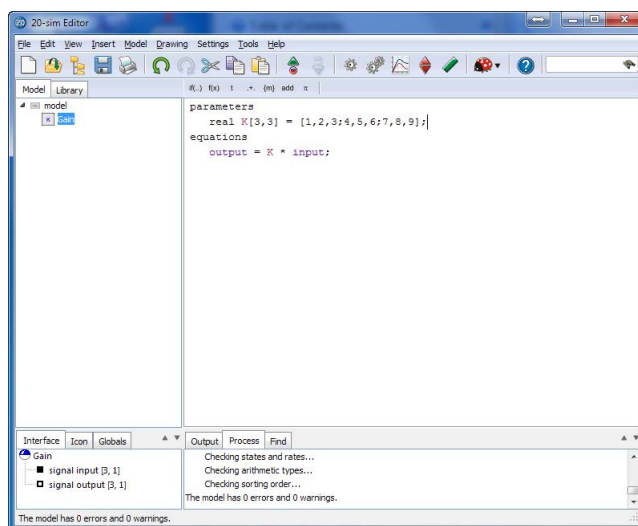


When two submodels are connected, 20-sim will automatically check for the port-sizes and create a connection:

1. If the port-sizes are unequal, an error message will be generated.
2. If both ports have size one, a single signal, bond or connection will be drawn.
3. If both ports have a size larger then one, a multi-signal, multi-bond or multi-connection will be drawn.

## The Finishing Touch: Matrices and Vectors

Behind each multi-dimensional submodel, there are equations in the end. To combine multi-dimensional ports with equations, you can use matrices and vectors. 20-sim has a large connection of matrix and vector functions and operators, to help you define any possible matrix equation. For example the gain model in the picture on top, could have been described as shown below.



*Use the matrix and vector notation to define the model equations.*

## Exporting Models

There are several methods to export 20-sim models.

### Export to previous versions of 20-sim

You can save a model file using the **Save** command or the **Save As** command from the **File** menu. If you want to save part of you model, use the **Save Submodel** command of the **File** menu. A **Save** dialog will be opened in which you can enter the model name and location. At the bottom of the dialog, you can use the **Save As Type** box to select the file type:

- Model files (\*.emx)    Standard 20-sim 4.0 format
- Packed files (\*.emz)    Zipped file including all linked files (e.g. datafiles, dll's, bitmaps etc.)

20-sim	3.6	files Export to 20-sim 3.6 format (* .emx)
Sidops	text	files Save model as text file. (* .txt)

### Export to zip file

You can save a model and all externally linked files into one zip-file, using the **Pack** command of the *File* menu. With the **Unpack** command of the **File** menu, you can open these zip-files.

### Export to Clipboard

From the **File** menu click **Export** and **To File** to export a selected model as a drawing to the clipboard (*Windows Enhanced Metafile* format).

### Export to File

From the **File** menu click **Export** and **To File** to export a selected model as a drawing to a file (*Windows Enhanced Metafile* format).

### Export to HTML

From the **File** menu click **Export** and **To HTML** to export the model, simulations etc. to an HTML file for the use in a word processor.

### Export to Bitmap

From the **File** menu click **Export** and **To Bitmap** to export a selected model as a drawing to a file (*png* format).

### Export to Matlab (m-file)

To export 20-sim models to Matlab, from the *Editor* you have to select the **File** menu and then click **Export to Matlab/Simulink** command. This will open a *Matlab-Code Generation* dialog. You can choose to export a complete model or a submodel. In both cases, three m-files are generated:

- **ModelName.m**: A file containing the model equations and special 20-sim functions. The model equations are directly translated from the equations that are shown with the Show Equations command of the Model menu.
- **ModelName\_run.m**: An example file showing you how to run a simulation with the exported model in 20-sim.
- **ModelName\_print.m**: This file contains a function that is used in the run file.

### Export to Simulink (m-file)

20-sim models are exported to Simulink S-functions. S-functions are block diagram elements of which the internal description can be an *m-file* or a *dll-file*. 20-sim can export both types. M-files can be opened from within Matlab and are therefore more accessible. *Dll-files* are compiled out of C-code, which makes them inaccessible, but a lot faster. Simulink does not support powerports. Therefore the powerports in a 20-sim model are translated to input and output ports.

To export 20-sim models to Simulink with an m-file description, from the *Editor* select the *File* menu and then click *Export to Matlab/Simulink* command. This will open a *Matlab-Code Generation* dialog. You can choose to export a complete model or a submodel. In both cases, two files are generated:

- **ModelName\_.mdl**: The exported 20-sim model based on a m-file that describes the model.

- **ModelName.m**: An m-file that contains the model equations and special 20-sim functions. The model equations are directly translated from the equations that are shown with the Show Equations command of the *Model* menu.

## Export to Simulink (dll-file)

To export 20-sim models to Simulink with an *dll-file* description, from the *Simulator* you have to select the **Tools** menu and then click the **C-code generation** command. This will open the *C-code Generation* dialog where you can choose to export to a Simulink S-function.

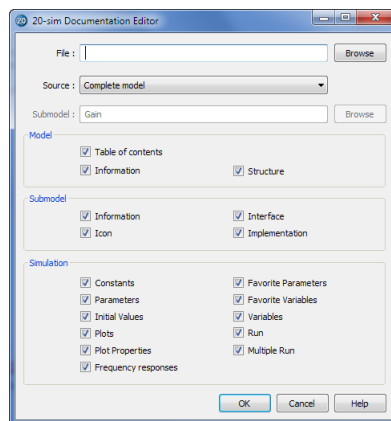
If you select the *OK* button, ANSI C-Code will be generated and compiled into a dll-function. Some files will be generated of which two are needed in Simulink:

- **ModelName\_.mdl**: The exported 20-sim model based on a dll-file that describes the model.
- **ModelName.dll**: A dll-file that contains the model equations and special 20-sim functions. The model equations are directly translated from the equations that are shown with the Show Equations command of the Model menu.

## Documentation Editor

The *Documentation Editor* can be open from the *File* menu in the 20-sim *Editor* by clicking *Document*. The *Document Editor* can be used to generate an html document that can be used for Word Processors and Presentation software.

The *Document Editor* will generate an html document that is fully hyperlinked. From a table of contents you can click to go to the desired part of the document. You can also click in pictures to go to the desired submodels.



*The 20-sim Documentation Editor.*

## General Items

- **File**: Select the output file.
- **Source**: Select the whole model or parts of it.
- **Submodel**: If documentation of a part of the model should be documented, select the desired submodel.

## Model

- *Table of Contents*: Select this option to start the document with a table of contents.
- *Information*: Information on the creation date, user, file location etc.
- *Structure*: The model hierarchy (list of all submodels, their submodels etc.).

## SubModel

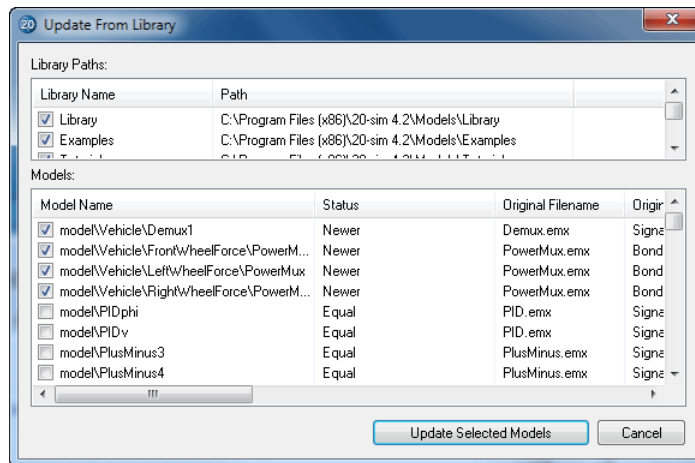
- *Information*: Information on the creation date, user, file location etc.
- *Icon*: The picture of the submodel icon.
- *Interface*: The inputs, outputs and ports.
- *Implementation*: The model implementation with equations at the lowest level.

## Simulation

- *Constants*: List of the constants that are used in the model.
- *Parameters*: List of the parameters that are used in the model.
- *Initial Values*: List of the starting values of the states of the model.
- *Plots*: Show pictures of the plots.
- *Plot Properties*: Show the plot settings.
- *Frequency Response*: Show the frequency responses.
- *Favorite Parameters*: List of the favorite parameters that are used in the model.
- *Favorite Variables*: List of the favorite variables.
- *Variables*: List of the variables.
- *Run*: list of the run settings.
- *Multiple Run*: List of the multiple run settings.

## Check for Model Updates

Most 20-sim models will be built using predefined submodels from a library. You can use the *Check for Model Updates* command of the *Models* menu to see if there are updates of these submodels. A window will open, showing you all the predefined library submodels.



## Items

- **Library Paths:** This part shows the libraries that are included in the search for predefined submodels. You can select or deselect these libraries. You can add your own libraries in the General Properties window.
- **Models:** This part shows all the submodels of which a match has been found in the libraries.
  - **Model Name:** The local name of the submodel.
  - **Status:** Shows if the match is *older*, *equal* or *newer*.
  - **Original Filename:** Original name of the submodel file.
  - **Original Directory:** Original location of the submodel file.
  - **Model Time Stamp:** Time when the used model was saved.
  - **Library Time Stamp:** Time when the library model was saved.

## Note

- The **Check for Model Updates** command will only check the time stamp of a model. If you have changed a submodel, without saving it, the time stamp is not altered.
- To prevent models from being included in the updates check, switch off the Allow model updates option of the Model properties.
- If you are not sure if a submodel should be changed, open the new library submodel in a separate **Editor** first.

## 5.3 Compiling

### Compiling Models

When you enter a model and open the Simulator or when you select the **Check Complete Model** command of the **Model** menu, the model will be compiled. During compilation, 20-sim will perform a number of tasks.

#### Error Checking

- *Type checking*: 20-sim will search for illegal type conversion and possible loss of data.
- *Unit Checking*: Many models in 20-sim use units and quantities. 20-sim will check for a proper use of these units and quantities.

#### Optimizing Model Structure

- *Analyze causality*: determine the causal order of equations.
- *Integral Form*: Equations are changed to integral form as much as possible.
- *Solving differential equations*: Differential equations are solved directly if possible.
- *Solving Algebraic Loops*: Algebraic loops are solved to their analytical solution, where possible.
- *Optimizing Equation Structure*: Some equations have to be calculated only once during each simulation step, because they do not influence the model dynamics. Depending on their relation to the model dynamics (needed for or a result of) these equations are calculated before the model dynamics (input equations) or after the model dynamics (output equations)
- *Remove redundant equations*: A lot of model equations are just assignments like  $\text{var1} = \text{var2}$ , where one variable is already known. 20-sim reduces these equations from the model and maps the unknown variables to known variables.

After these tasks a complete equation model is created, which can be inspected using the **Show Equations** command of the **Model** menu. After the complete equation model has been created the following tasks are applied:

#### Compiling

- *Find the correct order of execution*: All equations will split up into their most simple form and rewritten into the correct order of execution.
- *Interpreter Code*: Create interpreter like code out of the equations. This is low level code that can be understood by the simulation algorithms.
- *Machine Code*: When you have the Built-In compiler option selected, the interpreter code is compiled into platform specific 32-bit machine code. This code uses the full power of native Pentium and 486 instructions. The result is a dramatic increase of simulation speed: 100% to 400 %, depending on the kind of model used!

#### Simulation Code

The resulting code, either interpreter code or machine code, is used in the Simulator to perform simulation runs with and therefore also known as simulation code. As we have learned, the simulation code can be quite different from the original model equations. To denote the function of each original model variable in the simulation code, 20-sim uses the following names:

- independent rate
- independent state
- dependent rate
- dependent state
- algebraic loop in
- algebraic loop out
- interesting variable
- hidden variable

## Causal Form

Equations within 20-sim may be entered in random form. During compilation, 20-sim will automatically try to rewrite equations into a causal form and set them in a correct order. I.e. a form where all output variables are written as function of input variables. Consider for example the following model:

```
variables
  real u,z;
equations
  u = sin(time);
  u = cos(z);
```

Here the (input) variable  $u$  is given by the equation  $u = \sin(\text{time})$ . Consequently the (output) variable  $z$  should be written as a function of  $u$ . This is exactly what 20-sim will try to do while compiling the model into simulation code. I.e. the function  $\cos$  will be inverted and the model will be rewritten to:

```
variables
  real u,z;
equations
  u = sin(time);
  z = arccos(u);
```

Some functions cannot be inverted. Consequently not all equations can be rewritten. 20-sim will report this to the user, during model checking.

## Indifferent Causality

For some models the causal form is not known beforehand. For example the iconic diagram model that describes a damper can be written as:

```
parameters
  real d;
equations
  p.F = d*p.v;
```

Here  $p.F$  denotes the force and  $p.v$  denotes the velocity of the powerport  $p$ . There is no preferred input (force or velocity). This can be explicitly stated, by giving the powerport  $p$  an indifferent causality. During compilation 20-sim will determine whether  $p.F$  or  $p.v$  is the input variable and consequently rewrite the equations.

## Preferred Causality

For some models there is a preferred causal form. For example the iconic diagram model that describes a spring can be written as:

```

parameters
  real k;
equations
  p.F = (1/k)*int(p.v);

```

Here  $p.F$  denotes the force and  $p.v$  denotes the velocity of the powerport  $p$ . The equation is written in integral form which is preferred. Consequently the preferred input is the velocity. Should the force be the input, the equation must be rewritten to a differential form, which is leads to less efficient simulation. This can be explicitly stated, by giving the powerport  $p$  an preferred causality. During compilation 20-sim will try to keep the model in this preferred form. If this is not possible the equations will be rewritten to the less preferred form.

### Fixed Causality

For some models there is only one causal form. For example a simple iconic diagram model that describes coulomb friction can be written as:

```

parameters
  real Rc;
equations
  p.F = Rc*abs(p.v);

```

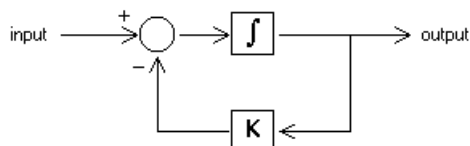
Here  $p.F$  denotes the force and  $p.v$  denotes the velocity of the powerport  $p$ . The equation is cannot be rewritten to a form where  $p.F$  is the input. This can be explicitly stated, by giving the powerport  $p$  an fixed causality. During compilation 20-sim will try to keep the model in this fixed form. If this is not possible an error message will be generated.

### Setting Causality

For some models, the equations are too complex to analyze causality. To help 20-sim, using the right causality, you can set causality for every port in the Interface Editor.

### Integral Form

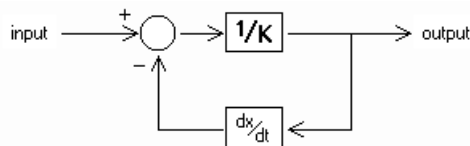
Consider the following first order linear model:



This model can be described by the dynamic equation:

$$\text{output} = \text{int}(\text{input} - K \cdot \text{output})$$

Now look at the following model:



This model can be described by the dynamic equation:

$$\text{output} = (\text{input} - \text{ddt}(\text{output}) / K)$$



Note that we can rewrite this equation as:

$$\text{ddt}(\text{output}) = \text{input} - K * \text{output}$$

or

$$\text{output} = \text{int}(\text{input} - K * \text{output})$$

This is the same equation as the previous model! Apparently, both models are the same! Both models can therefore be described by the dynamic equations:

$$\begin{aligned} \text{ddt}(\text{output}) &= \text{input} - K * \text{output} \\ \text{output} &= \text{int}(\text{input} - K * \text{output}) \end{aligned}$$

We call the first equation the *differential form* (no integrals). The second equation is called the *integral form* (no derivatives). In 20-sim, models can be entered in integral form as well as the differential form.

### Solving Differential Equations

During compilation, 20-sim will automatically try to rewrite equations into the integral form, since this leads to more efficient simulation. Sometimes an integral form cannot be found. Then algorithms will be applied to solve the differential directly. For example an equation like:

$$\text{output} = \text{ddt}(\sin(a * \text{time}))$$

will be replaced by the following equation (applying the chain rule and using the known derivative for the sine function):

$$\text{output} = a * \cos(a * \text{time})$$

Sometimes a differential cannot be solved directly. Then only the Backward-Differentiation Methods can be used for simulation.

### Simulation Code

After compilation simulation code is generated. The equation in integral form:

$$\text{output} = \text{int}(\text{input} - K * \text{output})$$

will be written as:

$$\begin{aligned} \text{independent state} &= \text{output} \\ \text{independent rate} &= \text{input} - K * \text{output} \end{aligned}$$

and can be handled by all integration methods. The equation in differential form:

$$\text{ddt}(\text{output}) = \text{input} - K * \text{output}$$

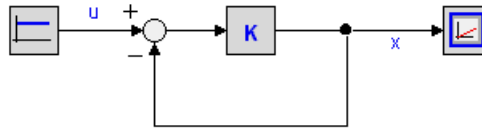
will be written as:

$$\begin{aligned} \text{dependent rate} &= \text{input} - K * \text{output} \\ \text{dependent state} &= \text{output} \end{aligned}$$

and can only be handled by the Backward-Differentiation Methods.

## Algebraic Loops

An algebraic loop in a model is a loop consisting of elements without "memory like" functions. To calculate the variables in this loop, the variable values themselves are needed. Consider the following example of an algebraic loop in an amplifier with negative feedback:



Standard derivation of a simulation model would yield:

$$x = K \cdot (u - x)$$

The variable  $x$  depends on its own value and must be solved by **iteration**. In 20-sim every simulation algorithm is accompanied by an iteration routine. Fortunately 20-sim is able to solve many algebraic loops at equation level. For this model this leads to the analytic solution the system:

$$x = K \cdot u / (1 + K)$$

## Simulating algebraic loops

Although 20-sim contains a sophisticated algorithms to find analytic solutions, the occurrence of unbreakable loops can not always be prevented. The occurrence of algebraic loops may lead to an increase of simulation time, or even stop simulation when iteration fails.

The best solution for these problems is to have a critical look at the model and change the order of calculations in a model. Possible solutions are:

- Algebraic Loops occur when the order of calculations is arbitrary. When an algebraic loop occurs in an equation model or in a set of equation models, you may change the order of calculation by rewriting the equations. The calculation order in bond graph models can be changed by introducing hand-defined causality.
- Introduce 'parasitic' energy storage elements (e.g. a small mass, a small capacitor etc.) to break an algebraic loop. These elements introduce however, large poles in the state equations, which might increase the simulation time considerably.
- Delete elements in the algebraic loop which are not relevant for the model's simulation output (e.g. small dampers, very stiff springs etc.). Care should however be taken, since correct deletions are not always possible and require considerable modeling skill and intuition.
- Combine dual elements. Sometimes elements of the same type can be combined by adding the parameter values (e.g. combining a mass  $m_1$  and a mass  $m_2$  to a mass  $m_1 + m_2$ ). This will in most cases decrease the amount of algebraic loops.

## Order of Execution

Equations within 20-sim may be entered in random form. During compilation, 20-sim will automatically try to rewrite equations into a correct order of execution. I.e. a form where all output variables are written as function of input variables and output variables of previous lines. Consider for example the following equations:

```

variables
    real u,z;
equations
    z = sin(u);
    u = cos(time);

```

Here the (input) variable  $z$  is given as a function of  $u$ . Consequently  $u$  should be calculated first. This is exactly what 20-sim will try to do while compiling the model into simulation code. I.e. the equations will be executed as:

```

u = cos(time);
z = sin(u);

```

### Code Blocks

Equations in a **code block** are not reordered. A code block is a set of equations inside a statement. Suppose we have the following equations:

```

if condition then
    code block 1
    ...
    ...
else
    code block 2
    ...
    ...
end;

```

To prevent incorrect executions of the if-statement, the equations of the code blocks will not be separated. Inside a code-block, equations can are not rewritten into an new order of execution. E.g. the following equations:

```

if time > 10 then
    z = sin(u);
    a = z^2;
    u = cos(time);
end;

```

Will be **not be reordered** and therefore not correctly executed! To get correct code, enter code blocks in a correct order, e.g.:

```

if time > 10 then
    u = cos(time);
    z = sin(u);
    a = z^2;
end;

```

### Prevent Order Changes

To make all equations a code block you can use the code section. E.g.

```

parameters
    real y = 8;
variables
    real x1, x2, x3;
code
    x1 = time;
    x2 = sin(time);
    x3 = y*x1;

```

## Integration Steps

Some integration algorithms do more calculations before generating the next output value. These calculations are called minor steps, the output generation is called a major step. During a minor step, all model equations are executed. In most cases you will not notice this because only the results of the major step are shown in the simulator. There are however, exceptions. The next topic will discuss this in more detail.

## Integration Steps

Some integration methods do more calculations before generating the next output value. These calculations are called **minor steps**, the output generation is called a **major step**.

integration method	minor steps
Euler	0
Backward Euler	variable
Adams-Bashford 2	0
Runge Kutta 2	1
Runge-Kutta 4	3
Runge Kutta Dormand Prince 8	variable
Runge-Kutta-Fehlberg	variable
Vode Adams	variable
Backward Differentiation Formula (BDF)	variable
Modified Backward Differentiation Formula (MBDF)	variable

## Execution of Equations

During a minor step, all model equations are executed. In most cases you will not notice this because only the results of the major step are shown in the simulator. There is one exception. If you use equations like

```

variables          real y;
initialequations  y = 0;
equations          y = y + 1;

```

you will find that the value of  $y$  depends on the integration method that is used. The reason is obvious once you realize that the equations are executed during minor steps. If you use a *Runge Kutta 2* integration method, there is one minor step during which  $y$  is increased and one major step during which  $y$  is increased again!

## Major

To prevent an equation from being calculated during minor steps, you can use the predefined variable **major**. This variable will return the boolean *false* when calculations are performed for a minor step and will return *true* when calculations are performed during a major step. The *major* variable is used for example in the library model *Amplitude Sensor*:

```

parameters        real initial = 0.0;
variables          real prev, peak;
initialequations  peak = initial;
                  prev = 0;
                  output = initial;
code              if major then
                  peak = max([abs(input), peak]);
                  if (input > 0 and prev < 0) or (input < 0 and prev > 0) then
                      output = peak;
                      peak = 0;
                  end;
                  prev = input;
                  end;

```

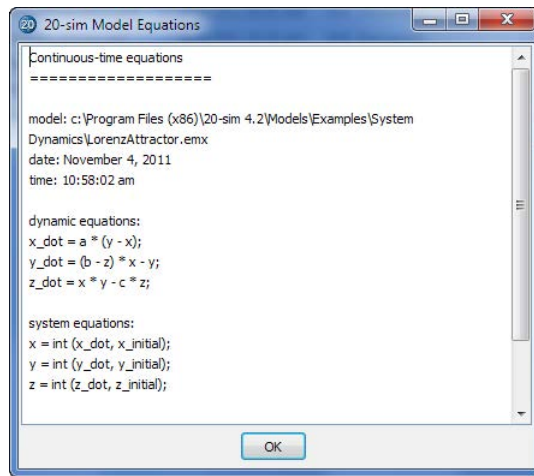
Note that the initial values are set in the *initialequations* section, because we do not want the variables to be set to zero at every integration step. Instead of an *equations* section, a *code* section is used to prevent 20-sim from rewriting the equations in a different order.

## Show Equations

During processing a complete set of equations is generated for each model. To inspect these equations or copy them for use in other programs, you have to:

1. From the **Model menu** select the **Check Complete Model** command.
2. From the **Model menu** select the **Show Equations** command.

Now a window is popped up showing all the model equations.

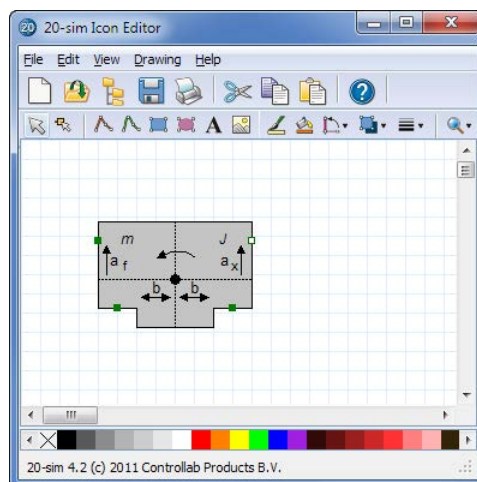


*The model equations after compiling.*

## 5.4 Icon Editor

### Icon Editor

The *Icon Editor* is a vector oriented drawing editor that can be used to create custom made icons for any 20-sim model. You can also use the *Icon Editor* to change the appearance of existing models.



*The 20-sim Icon Editor can be used to create custom made model icons.*

### Open

1. In the **Editor** select the **model** that you want to give a new appearance.

2. From the **Tools menu** select **Icon Editor**,
3. or from the **right mouse menu** select **Edit Icon**,
4. or at the bottom left of the Editor click the **Icon tab** and in the Icon tab **double click**.

## Use

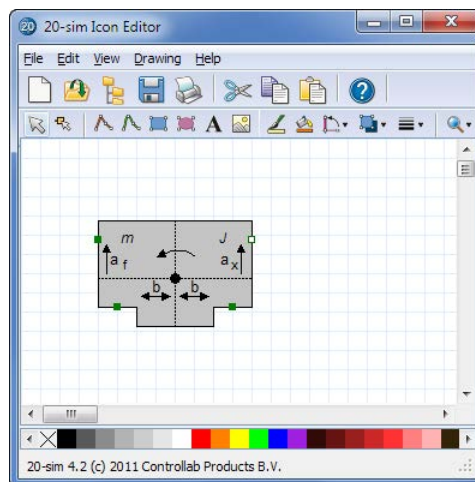
1. Use the **taskbar buttons** or the menu commands to insert objects and edit these objects.
2. If you are satisfied with the icon, insert the **terminals**.
3. From the Icon Editor **menu**, select **File** and **Update**.
4. **Close** the Icon Editor.

## Terminals

Most submodels will contain ports (i.e. an input signal, an output signal or a power port). If you are creating submodel icons, you want to indicate the connection points of these ports. These connection points are called *terminals*. In the *Icon Editor* you can define the position of the terminals.

1. In the taskbar click the **Terminal button** .
2. Click with the **mouse** pointer on the position where you want to **insert a terminal**.

If you have multiple inputs, outputs or ports, a menu will open to ask you which input, output or port should be selected.

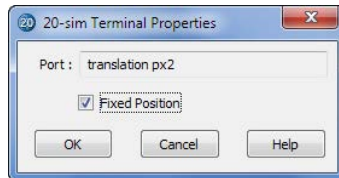


*The inputs, outputs and ports are indicate by small rectangles.*

The terminals are visible in the drawing as small rectangles.

3. You can **select a terminal** and from the **right mouse** menu click **Properties**.

This will open the *Terminal Properties* showing the name of the input, output or port and the option to fixate the position. With a fixed position, the connections will start or end exactly at the position of the terminal. Without a fixed position, the connections will point to the center of the icon and start or end at the border of the icon.



*You can give a terminal a fixed position.*

## 5.5 Global Relations Editor

### Introduction

If you want to share parameter values or variable values between submodels, you can use signals from one submodel to the others. This is not always desired and it will increase the effort that you have to make in connecting submodels.

Using globals is an alternative for sharing values. By defining a parameter or variable global, we can instruct 20-sim that a parameter or variable value is shared between submodels.

### Using Globals

If you want to share parameters or variables between submodels, you have to:

1. Add the **keyword global** to definition of the parameter or variable.
2. Define the scope of the globals, i.e. which models share the same parameters and variables?

### Global Parameters and Variables

Global parameters and variables are defined using the keyword **global**. In equation models, this keyword is added after the definition of the data type in the Equation Editor:

```
parameters
  real global par1 = 100 {Hz};
  real global par2 ;
variables
  real global var1;
  real global var2;
..
..
```



Parameters can only be assigned a value once. The same goes for variables. Only one submodel must define their value using an equation. If parameters or variables are assigned more than once, 20-sim will generate an error.

### Example

The best way to describe the use of global parameters and variables is by an example model. You can find this model in the 20-sim demonstration library (*Demo\Tips And Tricks\Global Parameters and Variables.emx*). The model exists of three submodels. In the first submodel two global parameters (*f* and *A*) are assigned and one variable (*sinewave*). The variable is assigned a value in the equations section and connected with the output (*out1*).

```
submodel1

parameters
    real global f = 100 {Hz};
    real global A = 1 {none};
variables
    real global sinewave;
equations
    sinewave = A*sin(f*2*pi*time);
    out1 = sinewave;
```

In the second submodel, the two global parameters are used to connect them with two outputs (*out1* and *out2*).

```
submodel 2

parameters
    real global f {Hz};
    real global A {none};
variables
    real global sinewave;
equations
    out1 = f;
    out2 = A;
```

In the third submodel, the global variable is connected with an output (*out1*).

```
submodel 3

variables
    real global sinewave;
equations
    out1 = sinewave;
```

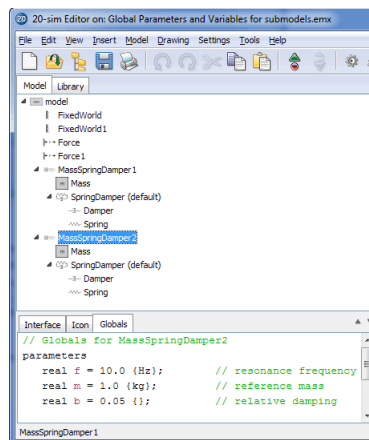
To prevent conflicts global parameters may be assigned a default value only once. The same goes for global variables: they may be assigned a value in the equation section only once.

## Scope

Global parameters and variables are defined using the **keyword *global***. In equation models, this keyword is added after the definition of the data type in the Equation Editor. In 20-sim we can define which submodels share the same parameter or variable. This is called the **scope** of this parameter or variable.

### Part of the Model

You can set the scope by using the Global Relations Editor. In this editor you can enter parameters or variables. All global parameters or variables **that are defined in submodels lower in the hierarchy**, share the same value.



*Setting the scope of global parameters with the Global Relations Editor.*

The image above shows an example. In the model hierarchy we see the submodel *MassSpringDamper2* selected. The Globals Relations Editor, shows three parameters:  $f$ ,  $m$  and  $b$ . If these parameters exist in the submodels lower in the hierarchy (*Mass*, *SpringDamper*, *Damper*, *Spring*), and use the keyword *global*, they share the same value. Submodels higher in the hierarchy, can never share these parameter values.

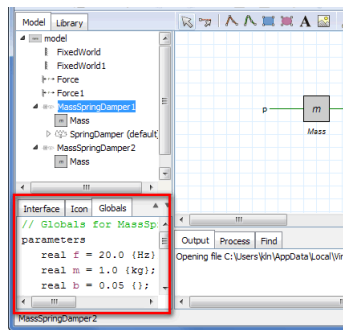
### Whole Model

If no parameter or variable is defined using the Global Relations Editor, the scope is the whole model. I.e. global parameters and variables are shared across the whole model.

## Global Relations Editor

The *Global Relations Editor* is used to restrict the scope of global parameters and variables. You can find the *Global Relations Editor* at the lower left of the *Editor* by selecting the *Globals* tab.

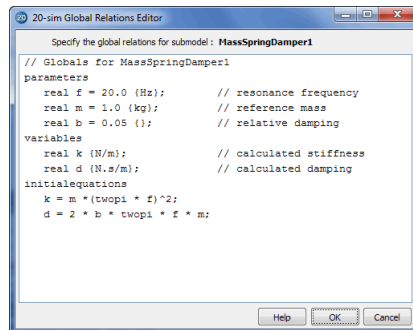
1. In the **Editor**, go to the **Model Hierarchy** at the left and **select** the **submodel**, you want to add global parameters or variables for.
2. Select the **Globals tab** at the lower left of the Editor.



Select the **Globals** tab, put your mouse pointer on top and click **Edit Global Relations**.

- Put your **mouse pointer** in the middle of the tab. From the **right mouse menu** select **Edit Global Relations**.

This will open the Global Relations Editor. You can use this editor to enter parameters, variables and equations.



Use the **Global Relations Editor** to enter parameters, variables and equations.

You can enter parameters, variables and equations here just like in the Equations Editor. The parameters and variables will only be useful if they are used in submodels lower in the hierarchy as globals.

### Example

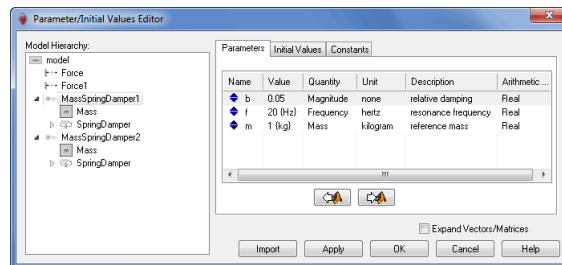
The best way to describe the use of the Global Relations Editor is by an example model. You can find this model in the 20-sim demonstration library (*Demo\Tips And Tricks\Global Parameters and Variables for submodels.emx*). This model shows two mass-spring-dampers with shared parameters and variables.

- In the **Editor**, go to the **Model Hierarchy** at the left and **select** the submodel *MassSpringDamper1*.
- Select the **Globals tab** at the lower left of the Editor.

- Put your **mouse pointer** in the middle of the tab. From the **right mouse menu** select **Edit Global Relations**.

Now you will see the Global Relations Editor, as shown in the previous figure. Three parameters are defined:  $f$ ,  $m$  and  $b$ . The parameter  $m$  is use in the submodel *Mass* lower in the hierarchy. The variable  $k$  is used in the submodel *Spring* lower in the hierarchy. The parameter  $d$  is use in the submodel *Damper* lower in the hierarchy.

- Now open the *Parameters Editor*.



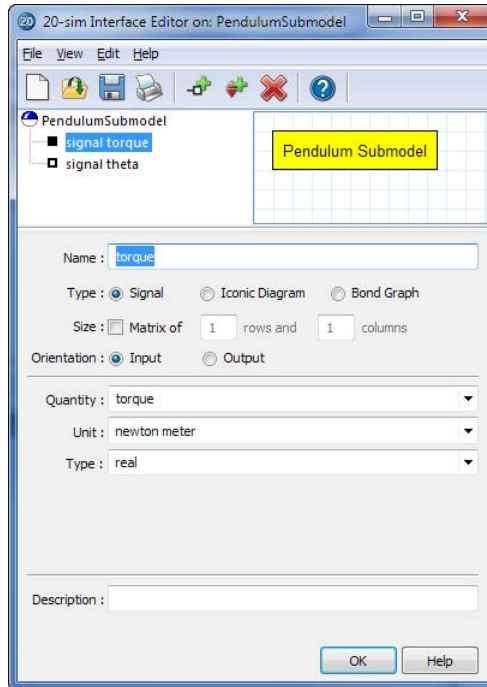
*Parameters that are shared can be set at the top model.*

You will see that it contains the parameters  $f$ ,  $m$  and  $b$  at the level of the model *MassSpringDamper1*. This allows us to duplicate this model and use a second mass-spring-damper model with different parameters.

## 5.6 Interface Editor

### Interface Editor

The *Interface Editor* can be used to define the interface, i.e. the input signals, output signals and power ports of a submodel.



*The 20-sim Interface Editor can be used to define the model interface.*

### Open

1. In the **Editor** select the model of which you want to change the interface.
2. From the **Tools menu** select **Interface Editor**,
3. or from the **right mouse menu** select **Edit Interface**,
4. or at the bottom right of the Editor click the **Interface tab** and in the Interface tab **double click**.

### Use

1. Use the **Edit menu** to add ports to the list.
2. Select a port from the list and change its **properties** (make it an input signal, output signals and power ports etc.)

3. From the **Interface Editor menu**, select **File** and **Update**.
4. **Close** the Interface Editor.

## Port Properties

From the *Edit* menu select *Add Port*. A new port will now be added to the list. If you select the port in the list you can change its properties

- *Name*: Enter the name of the port.
- *Type*: Select the port-type: Signal, Iconic Diagram or Bond Graph.

## Signal

- *Size*: If the signal is multi-dimensional, enter the number of rows and columns.
- *Orientation*: Choose input signal or output signal.
- *Quantity*: If the signal represents a physical quantity, you can choose the quantity from a predefined list.
- *Unit*: If the signal represents a physical quantity, you can choose the corresponding unit from a predefined list.
- *Type*: The default type of a signal is a real number. Choose out of *real*, *integer* or *boolean*.

## Iconic Diagram

- *Size*: If the port is multi-dimensional, enter the number of rows and columns.
- *Orientation*: Choose an input or output orientation for the port.
- *Domain*: Choose the physical domain of the port. The most general domain is power. Depending on your choice you will see the two variables (Across and Through) associated with the port.
- *Causality*: Select the causality of the port.
- *Separate High/Low Terminals*: You may choose this option for models with a velocity difference, voltage difference etc.
- *Any Number of Terminals*: You may choose this option for models with a variable number of connections.

## Bond Graph Port

- *Size*: If the port is multi-dimensional, enter the number of rows and columns.
- *Orientation*: Choose an input or output orientation for the port.
- *Domain*: Choose the physical domain of the port. The most general domain is power. Depending on your choice you will see the two variables (Effort and Flow) associated with the port.
- *Causality*: Select the causality of the port.

## Orientation

In the *Interface Editor* you can set the orientation of a ports. In the *Editor* this orientation can be made visible by setting the **Orientation Info** command from the **View** menu. Depending on the type of port the orientation has a different meaning.

- **Signals:** For signals the orientation indicates the direction of the associated variable : input or output.
- **Bond Graphs:** The orientation of a bond graph port is the direction of the half arrow at the end of a bond. It indicates the direction of the positive power flow.
- **Iconic Diagrams:** The orientation of an iconic diagram port also indicates the direction of the positive power flow.

If you select the top of the list in the Interface Editor, you can choose the *Port Relations tab* to set multiple port relations:

- **Equal / Not equal:** The equal and not equal restrictions can be used to specify that a port p1 must have the same or opposite orientation as port p2.

## Causality

A powerport (i.e. iconic diagram port or bond graph port) is always characterized by two variables. One of these variables should be an input and one of these variables should be an output. The choice of input and output variable is called causality. In the *Interface Editor* you can set the causality of the various ports of a submodel. In the *Editor* this causality can be made visible by setting the **Causality Info** command from the **View** menu.

- **Fixed out:** The fixed out causality restriction indicates that one of the two variables is always an output variable.
- **Preferred out:** *The preferred out causality restrictions indicate that one of the two variables is preferably an output variable.*
- **Indifferent:** A powerport with an indifferent causality restriction can have both variables as output.

If you select the top of the list in the *Interface Editor*, you can choose the *Port Relations tab* to set multiple port restrictions:

- **Equal / Not equal:** The equal and not equal restrictions can be used to specify that a powerport p1 must have the same or opposite causality as powerport p2. This is denoted as p1 equal p2 and p1 notequal p2 respectively.
- **One\_out:** The restriction One\_out should only be used for bond graph ports. It is used to indicate that at a one or zero junction, only one bond may have an effort out causality.
- **One\_in:** The constraint restriction One\_in should only be used for bond graph ports. It is used to indicate that at a one or zero junction, only one bond may have an effort in causality.

## Ports with more than one Terminal

By default, an iconic diagram port is a port where power can be exchanged between a component and its environment in terms of an *across* variable and a *through* variable. Such a port is represented by one terminal (connection point). However, there are two special cases where it is desirable to define an iconic diagram port that has more than one terminal.

### Separate High / Low Terminals

Consider, as an example, an mechanical spring. The power that flows into such a component is uniquely determined by the velocity difference between the two terminals of the component and the common force that acts upon both ends. Because of this one could say that there is one port, whose power is determined by one *across* value (the velocity difference) and one *through* value (the common force), but is represented by two terminals. To support this, 20-sim allows you to define a special type of iconic diagram port by indicating that it has *Separate High / Low Terminals*. The two terminals of the connection are named *high* and *low*. If the port is named *p*, the formal equations are:

**fixed in orientation:**

$$\begin{aligned} p.F &= p\_high.F = p\_low.F \\ p.v &= p\_high.v - p\_low.v \end{aligned}$$

**fixed out orientation:**

$$\begin{aligned} p.F &= p\_high.F = p\_low.F \\ p.v &= -p\_high.v + p\_low.v \end{aligned}$$

In 20-sim these equations are automatically derived.

### Any Number of Terminals

Consider, as an example, a mass. A characteristic of this component is that you can connect many springs and dampers to it. Implicitly, one expects that the net force (i.e., the summation of the forces applied by the connected components) will be applied to the mass, and that it will have a single velocity. To support this, 20-sim allows you to define a special type of iconic diagram port by indicating the kind to be *Any Number of Terminals*. The terminals of the connection are named *1*, *2*, *3* etc.. If the port is named *p*, the formal equations are:

**fixed in orientation:**

$$\begin{aligned} p.v &= p1.v = p2.v = p3.v = ..... \\ p.F &= sign1*p1.F + sign1*p2.F + sign1*p3.F + .... \end{aligned}$$

**fixed out orientation:**

$$\begin{aligned} p.v &= p1.v = p2.v = p3.v = ..... \\ p.F &= -sign1*p1.F - sign1*p2.F - sign1*p3.F - .... \end{aligned}$$

with

*sign = 1 when p1 has a fixed in orientation etc.*

*sign = -1 when p2 has a fixed out orientation etc.*

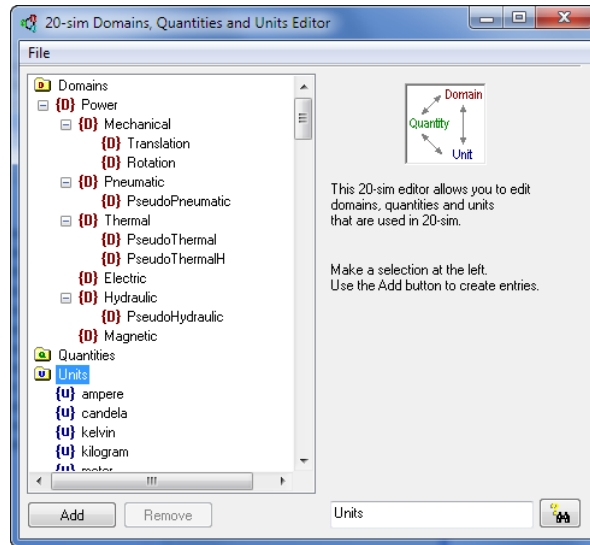
In 20-sim these equations are automatically derived.



## 5.7 Domains, Quantities and Units


### Domains, Quantities and Units Editor

At various modeling levels you can use information on physical domains, quantities and units. This information is stored in the file *QuantitiesAndUnits.ini* in the 20-sim bin directory. To edit this information you can use the *Domains, Quantities and Units Editor*. When opened, the editor automatically reads the file *QuantitiesAndUnits.ini*. When closed the editor asks you where to store the file. Note that any changes made become effective after 20-sim has been restarted.



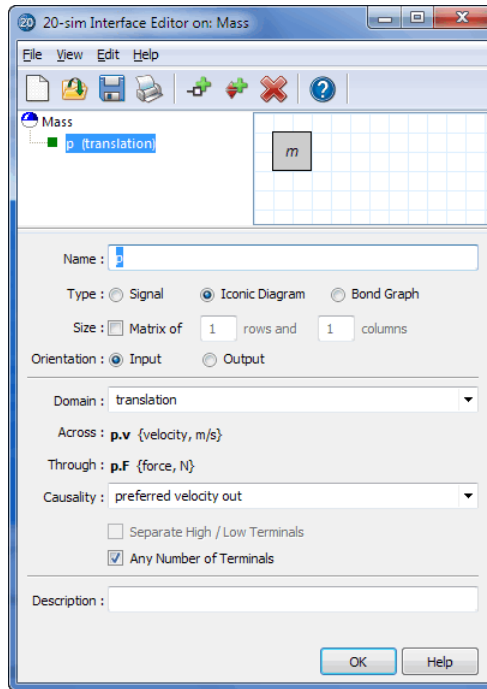
The Domains, Quantities and Units Editor.

You can start the *Domains, Quantities and Units Editor* by selecting the **Units Editor** command from the **Tools** menu. In the editor a tree-like structure is shown indicating the available Domains, Quantities and Units.

1. You can select every items in the tree for editing.
2. Use the **Add** or **Delete** button to add new items or delete existing item.
3. Use the **Find button**  to find items in the tree.

### Domains

In the Interface Editor every powerport (Iconic Diagram or Bond Graph) can be assigned a physical domain. 20-sim will use this information to prevent that ports of different physical domains may be connected. More popular: in this way you can never connect a translation model to an electric component.



*Use the Interface Editor to assign a physical domain to a port.*

In the *Interface Editor* you can select the physical domain that you want to assign to a port. The editor will show the corresponding port variables and the notation that should be used in the model equations.

The tables below show the available domains and their respective port variables.

#### **power domain**

Power  
Mechanical  
Translation  
Rotation  
Pneumatic  
Thermal  
Electric  
Hydraulic  
Magnetic

#### **across**

across  
velocity  
velocity  
angular velocity  
pressure  
temperature  
voltage  
pressure  
magnetomotoric force

#### **through**

through  
force  
force  
torque  
air flow  
entropy flow  
current  
volume flow  
magnetic flux

For the power domains the variables multiply to **power**. There are also some domains defined where the variables do not multiply to power. These are called **pseudo domains**. The following pseudo domains are defined.

<b>pseudo domain</b>	<b>across</b>	<b>through</b>
Pseudo Pneumatic	pressure	mass flow
PseudoThermal	temperature	heat flow
PseudoThermalH	temperature	enthalpy flow
PseudoHydraulic	pressure	mass flow

You can enter new (pseudo) domains in the Domains, Quantities and Units Editor. If the port is defined as a bond graph port, effort and flow are used to indicate the domain variables. The corresponding tables are shown below.

<b>power domain</b>	<b>effort</b>	<b>flow</b>
Power	effort	flow
Mechanical	force	velocity
Translation	force	velocity
Rotation	torque	am
Pneumatic	pressure	angular velocity
Thermal	temperature	air flow
Electric	voltage	entropy flow
Hydraulic	pressure	current
Magnetic	magnetomotoric force	volume flow
		magnetic flux

<b>pseudo domain</b>	<b>effort</b>	<b>flow</b>
Pseudo Pneumatic	pressure	mass flow
PseudoThermal	temperature	heat flow
PseudoThermalH	temperature	enthalpy flow
PseudoHydraulic	pressure	mass flow

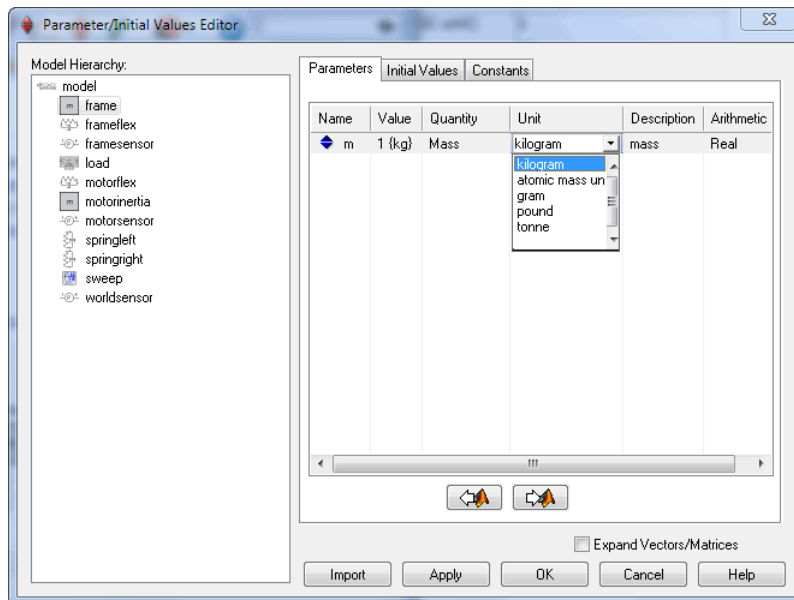
## Quantities and Units

In 20-sim, to every constant, parameter and variable a quantity may be assigned. Well known quantities are for example position, velocity, time and energy. 20-sim will use these quantities to check the validity of (basic) equations. The value of a quantity can be expressed in a specific unit. The quantity time can for example be expressed in the unit second or in the unit minute:

<b>quantity</b>	<b>unit</b>	<b>multiplication to SI unit</b>
Time	second (SI unit)	1
	minute	60

	hour	3600
	day	31556926.08
Position	meter (SI unit)	1
	foot	0.3048
	inch	0.0254
	yard	0.9144

In 20-sim a quantity can be expressed in every desired unit. To prevent **conversion** problems, internal calculations are always performed in standard SI-units. Therefore non-SI units are stored with a **multiplication** factor. When a variable has a unit, the unit can also have common engineering **prefixes**. For example, a parameter  $m$  {kg} with a value of 0.1 can be selected in the *Parameters / Initial Values Editor*. If you click on the unit, you can select other units to enter the mass.



*You can use the units in the Parameters / Initial Values Editor to select a desired unit.*

You can enter new quantities and units in the Domains, Quantities and Units Editor.

## Editing Domains

You can edit existing domains or add new domains in the *Domains, Quantities and Units Editor*. In the Domains section you can add new domains or edit existing domains. Each domain has several edit fields:

- **Domain name:** If you click on a selected domain in the tree, you can edit the name.
- **Description:** Enter a description of the domain.
- **Quantities:** You can enter quantities of these variables in the quantities section.
- **Mechanical Domain:** Select this button if your domain is part of the mechanical domain.
- **Pseudo Domain:** Select this button if your domain is a pseudo domain.
- **Color:** Double-click the color box to change the color of a domain.

In some domains the integrated effort/flow variables and differentiated effort/flow variables are of a specific quantity. You can enter these quantities in the according edit fields. For some domains these values have no meaning and you can leave the edit fields blank.

## Editing Quantities

You can edit existing quantities or add new quantities in the *Domains, Quantities and Units Editor*. In the Quantities section you can add new quantities or edit existing quantities. Each quantity has several edit fields:

- **Quantity name:** If you click on a selected quantity in the tree, you can edit the name.
- **Description:** Enter a description of the quantity.
- **Variable name:** This name is used for display purposes. For example if one of the variables of a port p has the quantity length it will be denoted as p.x.
- **SI Symbol:** Enter the official SI-symbol here. Enter combinations as nominator/denominator (e.g. Electric Resistance:  $\text{kg.m}^2/\text{A}^2.\text{s}^3$ )
- **Units:** Every quantity can be expressed in several unique units (i.e. a unit can be assigned to one quantity only). You can enter new units here or edit existing units that belong to the selected quantity.
- **Unit Symbol:** For display purposes every unit has a specific symbol. It is shown here in a read-only field.

A quantity can have an alias name. Enter this alias as a subentry of the main quantity. This alias name refers to the main quantity and therefore to the same associated units.

## Editing Units

You can edit existing units or add new units in the *Domains, Quantities and Units Editor*. In the Units section you can add new units or edit existing units. Each unit has several edit fields:

- **Unit name:** If you click on a selected unit in the tree, you can edit the name.
- **Description:** Enter a description of the unit.
- **Quantity:** Choose the quantity to which the unit should be associated. A unit can be associated to one quantity only.
- **Symbol:** For display purposes every unit has a specific symbol.
- **Multiplications:** A quantity can be expressed in several units. To prevent conversion problems, internal calculations are always performed in standard SI-units. Therefore non-SI units are stored with a multiplication factor. You can enter the multiplication factor here.

- *Allow Symbol Prefixes:* Some units can be expressed with symbol prefixes. Select the check box to allow the use of prefixes. 20-sim supports the following prefixes:

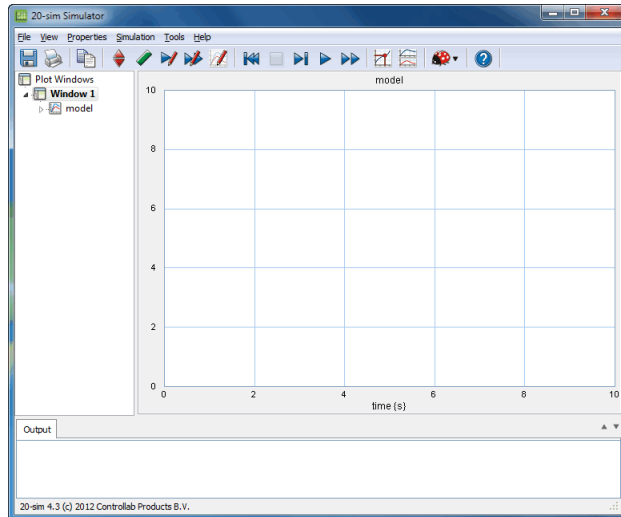
<b>prefix</b>	<b>symbol</b>	<b>value</b>
femto	f	$10^{-15}$
pico	p	$10^{-12}$
nano	n	$10^{-9}$
micro	u	$10^{-6}$
milli	m	$10^{-3}$
kilo	k	$10^3$
mega	M	$10^6$
giga	G	$10^9$
tera	T	$10^{12}$

## 6 Simulator

### 6.1 Introduction

#### Simulator

20-sim consists of two main windows and many tools. The first window is the *Editor* and the second is the *Simulator*. The *Editor* is used to enter and edit models. The *Simulator* is used to simulate and analyze the models. The Simulator is opened in the *Editor* by clicking the *Start Simulator* button from the *Model* menu.



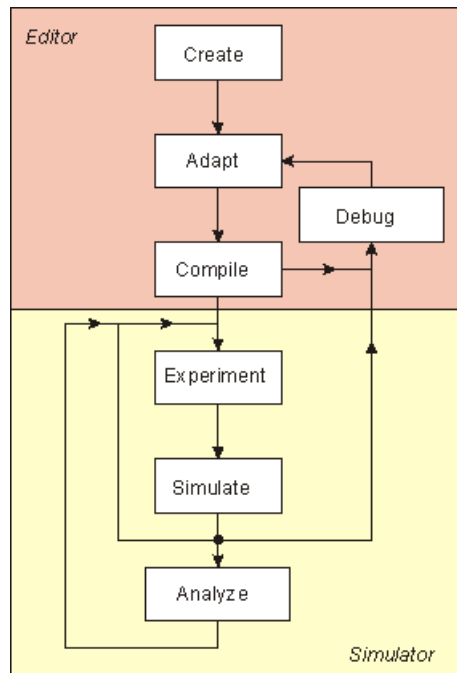
*The Simulator is used to carry out simulations, show the results and analyze them.*

The *Simulator* consists of two parts:

- *Simulation Plot*: This is the graph in the middle. Here the simulation results are shown.
- *Output tab*: The *Output tab* shows warnings and messages.

#### Simulation

A modeling and simulation session in 20-sim can be visualized by the diagram shown below.



*Modeling and Simulation in 20-sim.*

## Compiling/Debugging

After the model has been successfully entered, it must be checked and compiled to generate simulation code. This is done in 20-sim automatically when you open the *Simulator* or when you check a model. In some cases the model contains errors which have to be solved by adapting the model. Errors in 20-sim are presented in the *Process tab* at the bottom of the *Editor*.

## Settings

After a successful compilation of a model that is created in the Editor you can open the Simulator. In the Simulator you have to enter specific settings:

- Parameters / Initial Values.
- Run Properties.
- Plot Properties.

## Running

After the settings have been entered you can run the simulation.

## Plotting

Simulation results can be shown in 20-sim as:

- Numerical Plots:
  - Time Domain (default)
  - Frequency Domain (FFT Analysis & Linearization)
- Animation in a Graphical Model



- 3D Animation

### **Debugging**

If you experience problems during simulation you have to resolve them in a debugging session.

### **Analysis**

After a successful simulation you can analyze your model using various tools:

- Parameter Sweeps
- Curve Fitting
- Optimization
- Sensitivity Analysis
- Monte Carlo Analysis
- Variation Analysis
- FFT Analysis
- Linearization

### **Message Log**

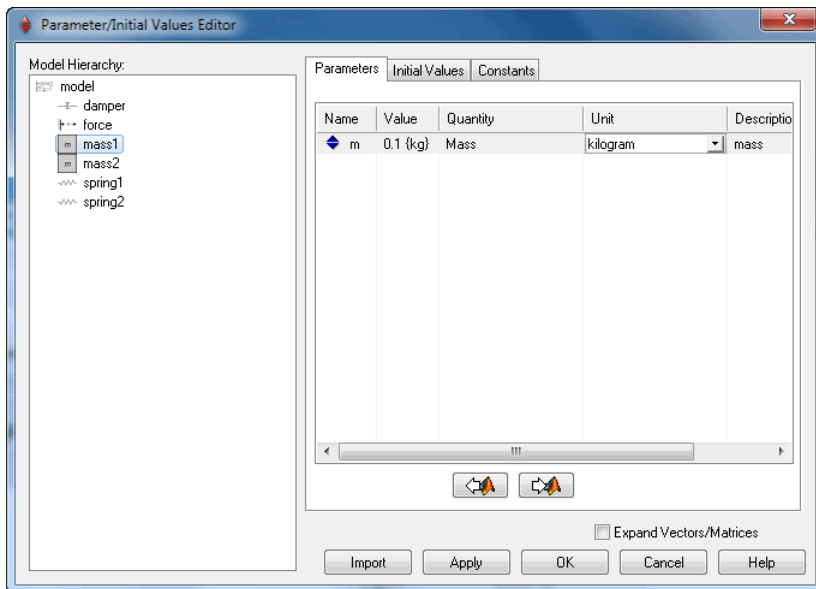
The bottom of the Simulator shows a tab named *Output*. This tab contains the *Message Log* which shows all the messages, warnings and errors, that are generated during a simulation.

## 6.2 Running a Simulation

### Parameters and Initial Values

The *Parameters/Initial Values Editor* is used to edit the constants, parameters and initial values of a model. Parameters and initial values can be changed during simulation, constants cannot be changed. To open the Parameters/Initial Values Editor, you have to:

1. From the **Properties** menu select the **Parameters** command.



*The Parameters/Initial Values Editor.*

The parameter items (Name, Value, Quantity, Unit, Description, Kind, Arithmetic Type, Value) of the *parameters* and *initial values* are listed in right part of the window. The list of parameters and initial values that is displayed depends on the selected submodel in the left part of this window.

### Items

- **Model Hierarchy:** The left part displays the complete model hierarchy. At each level of the hierarchy, submodels can be selected. The right part of the window then shows the parameters and initial values of that submodel. To see all parameters and initial values, select the top level of the hierarchy, i.e. the main model listed on top.
- **Parameters and Initial Values:** The order of the parameters or initial values in the list depends on the order in which the submodels were originally entered in the Editor. Click on the name box to make the order to alphabetical. Drag the name box to change the width of the parameters list.
- **Value:** You can change the default value of a parameter or initial value in the value list. Select the parameter or initial value (mouse) and enter the desired value. Use the Enter key to quickly run through a list of parameters.

- **Unit:** If available, select the desired Unit from the drop down list.
- **From Matlab / To Matlab:** Use the buttons to import or exports parameter values from or to Matlab.
- **Import:** Use this button to import the parameter values from another model.

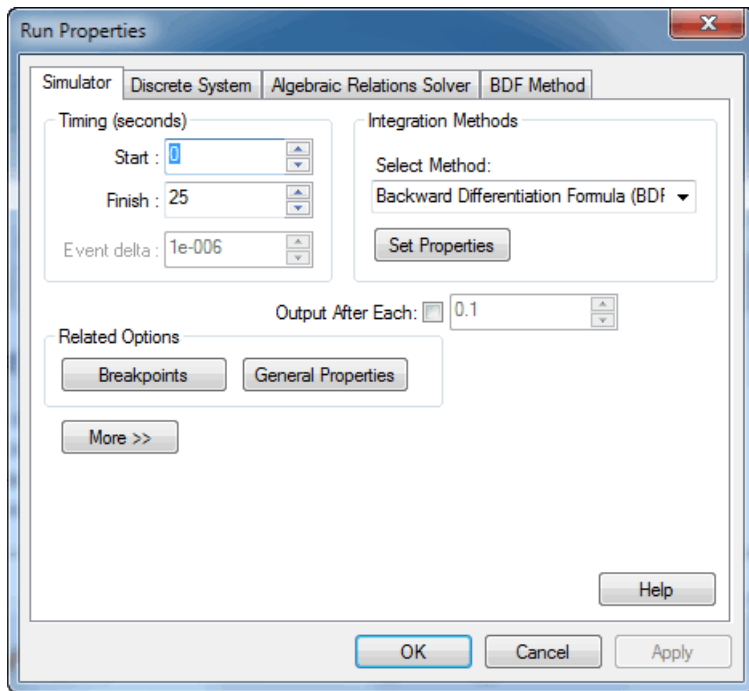
### Note

- All equations in 20-sim are calculated using standard SI-units. You can however enter parameters, using whatever Unit you like. In the *Parameters/Initial Values Editor*, you can change the unit using the little drop down list next to the *Value* box.
- The description of a parameter can be specified in the parameters part of the equation description of a model.
- To see a global parameter, select the top level of the hierarchy, i.e. the main model listed on top.
- Hidden parameters are not visible in the Variables Chooser.

### Run Properties

The *Run Properties Editor* can be used to choose the *integration method* used for simulation. An integration method is the algorithm that calculates the model equations during each simulation and generates the output values for the simulation plots. The default integration method is the Backward Differentiation Formula (BDF). To open the Run Properties Editor, you have to:

1. From the **Properties** menu select the **Run** command.



*The Run Properties Editor.*

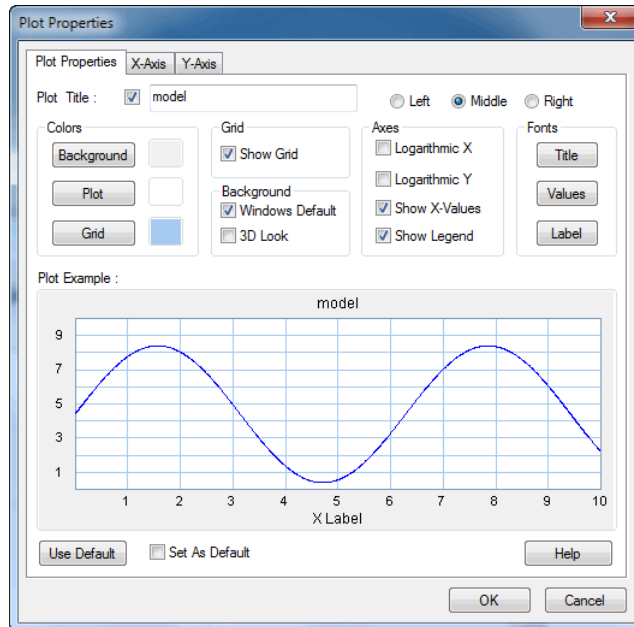
Initially, the fields in the Run Properties Editor contain default values if no experiment was loaded. Two or more tabs can be selected:

- **Simulator:** This tab shows the general simulation settings.
- **Discrete Systems:** This tab is only visible when discrete systems are part of your model. It contains the settings for the sample frequency.
- **Algebraic Relations Solver:** This tab is only visible when your model contains algebraic loops that could not be solved during processing.
- **Integration Method:** The last tab contains the specific settings for the selected integration method.

## Plot Properties

The Plot Properties Editor can be used to enter the plot specifications. To open the Plot Properties Editor, you have to:

1. From the **Properties** menu select the **Plot** command.



*The Plot Properties Editor.*

The editor shows three tabs which can be used to set the properties of the plot and the x and y variables.

### Plot Properties Tab

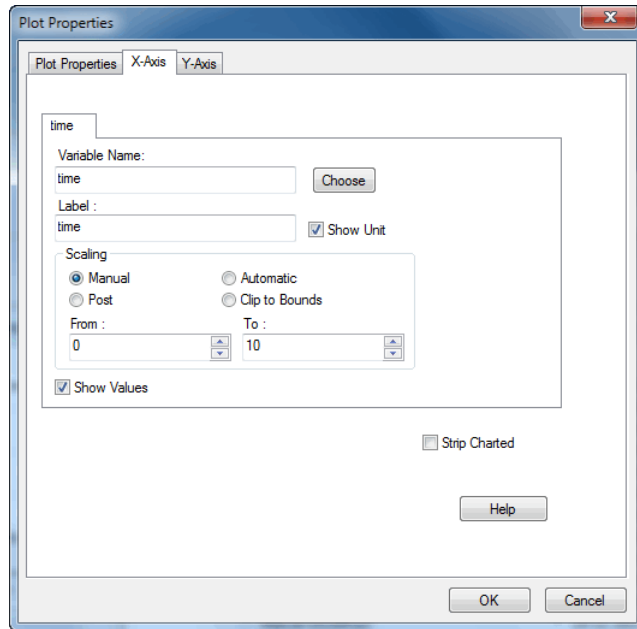
The *Plot Properties Tab* shows the general settings that accompany a plot. A preview is shown in the lower part of the tab.

- **Plot Title:** Select this option to add a title to the plot. In the text box you can type the desired title. Use the radio buttons to display the title to the left, in the middle or to the right of the plot.
- **Colors:** Click the Background, Plot and Grid buttons to select the background, plot and grid colors.
- **Grid:** Select this option to show the grid.
- **Background**
  - *Windows Default:* Select this option to get the default Windows background.
  - *3D Look:* Select this option to get a plot with 3D Look (sunken edges).
- **Axes:**
  - Select the options *Logarithmic X* and *Logarithmic Y* to show logarithmic plots.

- **Show X-Values:** Use this option to show or hide the X-axis values.
- **Show Legend:** Use this option to show to show a legend.
- **Fonts:** Click the *Title*, *Values* and *Labels* buttons to select the font options for the title, values and labels.

### X-Axis Tab

The *X-Axis Tab* can be used to specify the variable plotted along the X-axis.



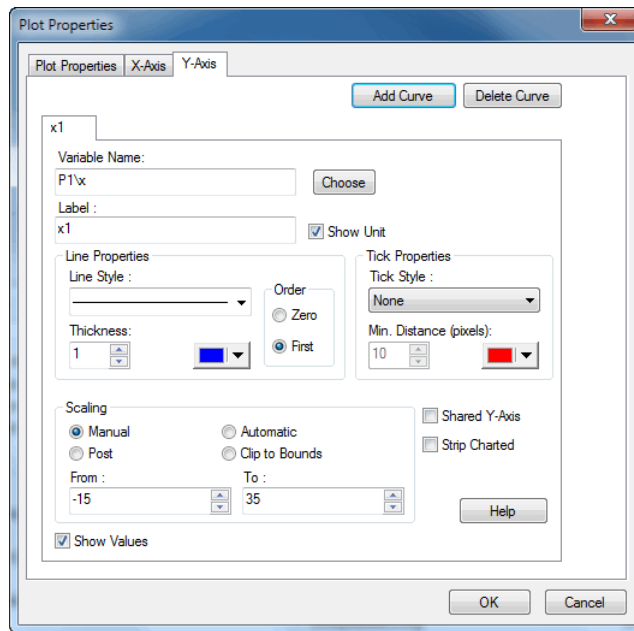
*The X-Axis tab of the Plot Properties Editor.*

- **Variable Name:** Either time or one of the dynamic variables of the model can be chosen as the X-axis variable. Click the button on the right (Choose) to open the Variable Chooser and select the desired variable.
- **Label:** Enter the label that should be printed below the X-axis.
- **Show Unit:** Select this option to display the unit of the chosen variable.
- **Scaling**
  - **Manual:** Fix the scale of the X-axis by selecting a minimum and maximum value in the From and To boxes.
  - **Post:** During the simulation run, the scale for the variable along the axis is fixed. When the run is finished or has been interrupted by the user, the minimal and maximal scale values are automatically updated and the plot is redrawn to make sure all calculated points are displayed.
  - **Automatic:** When a variable reaches the end of the scale, during simulation, the the minimal and maximal scale values are automatically updated and the plot is redrawn to make sure all calculated points are displayed.

- **Clip to Bounds:** When a variable reaches the end of the scale, during simulation, the the minimal and maximal scale values are automatically updated and the plot is redrawn to make sure all calculated points are displayed. When the run is finished or has been interrupted by the user, the minimal and maximal scale values are automatically updated to show the plot at maximum scope.
- **Show Values:** Use this option to show or hide the X-axis values.

### Y-Axis Tab

The *Y-Axis Tab* is used to specify the curves that should be shown in the plot. For each selected curve, a tab is shown, displaying the settings of that curve.



*The Y-Axis tab of the Plot Properties Editor.*

### Curves

- **Add Curve:** Add a new tab to specify a new curve to be displayed in the plot.
- **Delete Curve:** Delete the selected tab. As a result, the curve specified in the tab will not be displayed in the plot, and the settings are lost.
- **Variable Name:** Use this box to connect a variable to a curve. One of the dynamic variables of the model can be selected. Click the button on the right (Choose) to open the Variable Chooser and select the desired variable.
- **Label:** Enter the name of the curve. This label is also printed next to the the Y-axis.
- **Show Unit:** Select this option to display the unit of the chosen variable.

- **Line Properties**
  - *Line Style*: Select the desired line style of the curve.
  - *Thickness*: Select the desired line thickness of the curve.
  - *Color*: Select the desired line color of the curve.
  - *Order*: In the plot a line is drawn from plot point to plot point. You can choose the line to be of two orders of interpolation:
    - Zero: the line consists only of horizontal and vertical parts.
    - First: the line consists of straight parts.
- **Tick Style Properties**
  - *Tick Style*: Each calculated point of a curve, can be displayed by a special marker. Select here the desired marker.
  - *Min. Distance (pixels)*: To prevent markers from being drawn on top of each other, you can set the minimum distance between markers. Points that are too close to a previous marker are not drawn with a marker.
  - *Color*: Select the marker.
- **Scaling**: Scaling can be selected for each curve individually or combined for all curves.
  - *Shared Y Axes*: Select this option to use one Y-axis scale for all curves.
  - *Strip Charted*: Select this option to display each curve in a separate plot.
  - *Manual*: Fix the scale of the variable by selecting a minimum and maximum value in the From and To boxes.
  - *Post*: During the simulation run, the scale for the variable along the axis is fixed. When the run is finished or has been interrupted by the user, the minimal and maximal scale values are automatically updated and the plot is redrawn to make sure all calculated points are displayed.
  - *Automatic*: When a variable reaches the end of the scale, during simulation, the the minimal and maximal scale values are automatically updated and the plot is redrawn to make sure all calculated points are displayed.
  - *Clip to Bounds*: When a variable reaches the end of the scale, during simulation, the the minimal and maximal scale values are automatically updated and the plot is redrawn to make sure all calculated points are displayed. When the run is finished or has been interrupted by the user, the minimal and maximal scale values are automatically updated to show the plot at maximum scope.
  - *Show Values*: Select or de-select this option to show or hide the name and scale of a curve.
- **Separate X-Axis**: If you want another x-axis than specified in the X-axis tab, click the Choose button to select the desired variable.



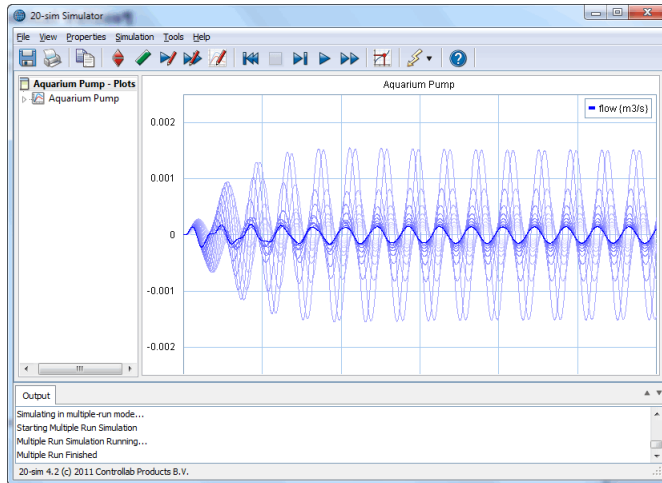
## Running a Simulation

After specification of the Parameters/Initial Values, the Run Properties and Plot Properties you can start a simulation run by choosing the appropriate command from the *Simulation* menu.

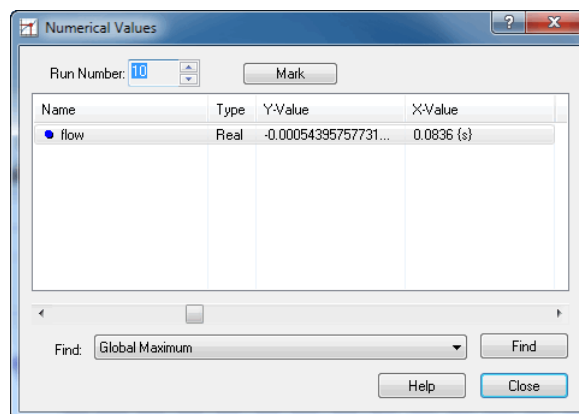
- **Run:** Select the Run command to start or continue a simulation run. Once a run is started, the Stop command becomes active. The run can be interrupted by selecting this command.
- **Stop:** Use the Stop command to interrupt a simulation. Once a simulation has stopped it can be continued by selecting the Start Simulation command.
- **Clear**
  - **All Runs:** Select the Clear All Runs command to clear all runs that were performed, from the graphical screen and from the computer memory.
  - **Last Run:** Select the Clear Last Run command to clear the run that was performed last, from the graphical screen and from memory.
  - **Previous Runs:** Select the Clear Previous Runs command to clear all runs, but the last, from the graphical screen and from memory.
- **One Step:** Use the One Step command to calculate one new simulation point. Using this command repeatedly, allows you to run a simulation step by step.
- **Brute Force:** Using the Brute Force command, curves are displayed after complete calculation of a simulation run. This saves time (re)drawing curves during calculations and therefore considerably speeds up simulation.
- **Multiple Run:** Select the Multiple Run command to start multiple runs needed for the *Time Domain Toolbox*. Runs can be interrupted by selecting the Stop command.
- **Replay**
  - **3D Animation:** Any 3D Animation that was performed during a simulation run, can be quickly replayed using this option.
  - **Real Time 3D Animation:** Any 3D animation that was performed during a simulation run, can be replayed in real time (i.e. frames are skipped if necessary) using this option.
  - **Read Datafile:** Use the Read Data File command to read previously stored simulation runs from file.
- **Copy States:** With the Copy States command the current independent state variables can be imported as new initial values. Current state variables are the state variables at the end of a simulation run or at the point where a simulation run was interrupted.

## Numerical Values

In every simulation plot you can inspect the numerical values by selecting the *Numerical Values* command of the *View* menu. The *Numerical Values* window, can also be popped up by double clicking the left mouse button, while pointing the mouse at a curve in the plot.



The Numerical Values window will pop up and display the numerical values of all plotted variables as a function of time. The last variable shown is always the X-axis variable (usually time).



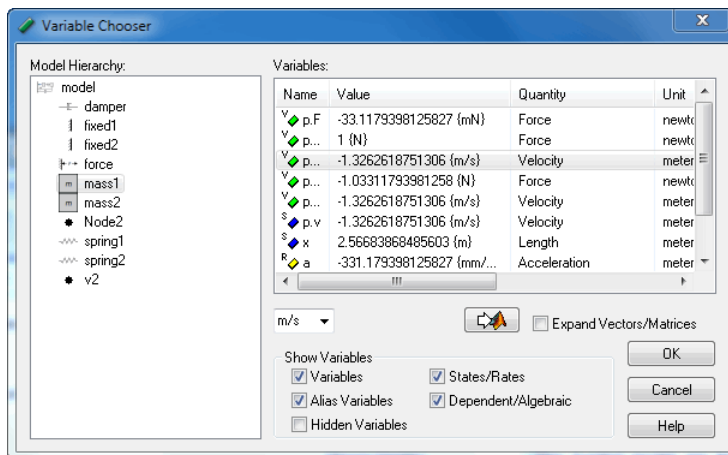
*The Numerical Values window.*

- **Run Number:** The run number indicates the run of which the numerical values are shown. The highest number indicates the last run simulated. Lower numbers are used for previous runs. To select another run number, type in the number of interest or point in the plot at the curve of interest. In the simulation plot, previous runs are shown with fading colors.

- **List:** The list shows all variables that are shown in the plot and their corresponding X-values and Y-values. The variable that is currently selected is pointed out by an arrow in the plot.
- **Scroll-bar:** Use the scroll-bar to change the selected x-axis variable value (usually time).
- **Find:** With the Find button, the global maximum etc. of the selected variable can be found. The following functions can be selected:
  - *Global Maximum*
  - *Global Minimum*
  - *Next Local Maximum*
  - *Next Local Minimum*
  - *Previous Local Maximum*
  - *Previous Local Minimum*
- **Mark:** Click the *Mark* button to store the set of numerical values. If you drag the scroll-bar to find a new set of values, the relative changes will be displayed as well as a first order derivative.

## Variable Chooser

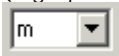

The Variable Chooser can be used to select and inspect any dynamic variable of the loaded model. The names, kinds, types, values, quantities, units and descriptions of the variables of the loaded model are listed in right part of the window. The list of dynamic variables displayed, depends on the selected (sub)model in the left part of this window. The left part displays the complete model hierarchy.



The Variable Chooser shows all variables of a model.

## Items

- **Model Hierarchy:** The model hierarchy shows several keys:

- **Model:** At each level of the hierarchy, submodels can be selected and inspected. The right part of the window then shows the variables that are part of that submodel. To see all variables including time, select the top level of the hierarchy, i.e. the main model listed on top. Click on one of the variable items (Name, Value, Quantity, Unit, Description, Kind, Arithmetic Type, Value) to order the variables alphabetically.
- **Input Probes/Output Probes:** In the Frequency Response dialog pairs of input variables and output variables can be selected for linearization. If input variables have been selected they are shown under the input probes key. If output variables have been selected they are shown under the output probes key.
- **Favorites:** variables that are used a lot can be added to the favorites key for easy use.
- **Variables:** Select the desired variable from the list (use your mouse pointer), select the desired Unit from the drop down list and click OK to close the window.
- **Unit Selection:** If a quantity was assigned to the selected variable with multiple units (e.g. position -> m , mm , inch , etc.) you can switch units by the unit selection  at the bottom of the variable list.
- **Expand Vectors/Matrices:** Select complete vectors and matrices or only their elements.
- **To Matlab:** Use the  button to export a variable value to Matlab. You will be asked to enter a Matlab variable. Data will be exchanged between this Matlab variable and the variable that is selected in 20-sim.
- **Show Variables:** Select the specific kind of variables (Variables, States/Rates, Dependent/Algebraic) that should be displayed in the Variables list.

## Actions

If you select a variable in the list and use the right mouse menu several actions can be performed:

- **Add to Favorites:** add the selected variable to the favorites list.
- **Add to Input Probes:** Add the variable to the list of inputs for linearization. This list is used in the Frequency Response dialog.
- **Add to Output Probes:** Add the variable to the list of outputs for linearization. This list is used in the Frequency Response dialog.
- **Copy:** copy the variable value to clipboard.
- **Copy with Unit:** copy the variable value and corresponding value to clipboard.
- **Copy Specified:** Specify the items that should be copied and then copy to clipboard.



## Tips

1. All equations in 20-sim are calculated using standard SI-units. You can however display the results, using whatever Unit you like. In the *Variable Chooser*, you can change the unit using the little drop down list just above the *Show Variables* section.
2. To see global variables, select the top level of the hierarchy, i.e. the main model listed on top.

3. To quickly find some variables out of the list, add the keyword interesting in the equation description. In the Variables list, de-select States, Rates, Algebraic Loops, Dependent States and Dependent Rates. Then only the interesting variables are shown.
4. When using large models, opening the Variable Chooser may take some time. Use the General Properties window to set the maximum number of variables that should be shown.
5. To hide variables from the list, add the keyword hidden in the equation description. Hidden variables are not visible in the *Variable Chooser*.

## Debugging

20-sim has various tool to help you to pinpoint and resolve problems that may occur during a simulation.


- **Switch to Debug Mode:** 20-sim is operating in *Debug Mode* when you see the *Debug Mode button* . If your *Simulator* or *Editor* is in *Fast Mode*  click on the button to change to *Debug Mode*.
- **Recompile your model:** In the editor select *Check Complete Model* from the *Model* menu. This will recompile your model in *Debug* mode and show a maximum of warnings. If any warning looks suspicious, solve this first.
- **Breakpoints:** Set breakpoints to monitor time or conditions between variables.
- **Run to the breakpoint:** Use the *Run* command from the *Simulation* menu to run the simulation to a breakpoint. As soon as the breakpoint has been reached, the simulation will halt. The *Output tab* at the bottom of the Simulator will display which breakpoint was active.
- **Simulate Step-by-Step:** Use the command *One Step* from the *Simulation* menu to simulate do one simulation step for the complete model.
- **Inspect the Results:** After each step, open the Variable Chooser to inspect the various variables of the model. You can also switch to the *Editor* to inspect results at model level:
  - **Submodels:** Select a specific submodel and choose *parameters* or *variables* to inspect the parameters and variables of that submodel.
  - **Equation submodels:** Put the mouse pointer on top of an equation and point to a variable or parameter of interest. A box will appear, showing the numerical value associated with that variable or parameter.

### parameters

**real** initial = 0;

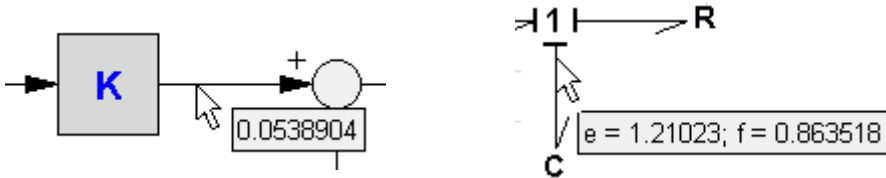
### equations

**output** := **hold** (**input**, initial);

 135.156

*Use the mouse pointer to inspect numerical values.*

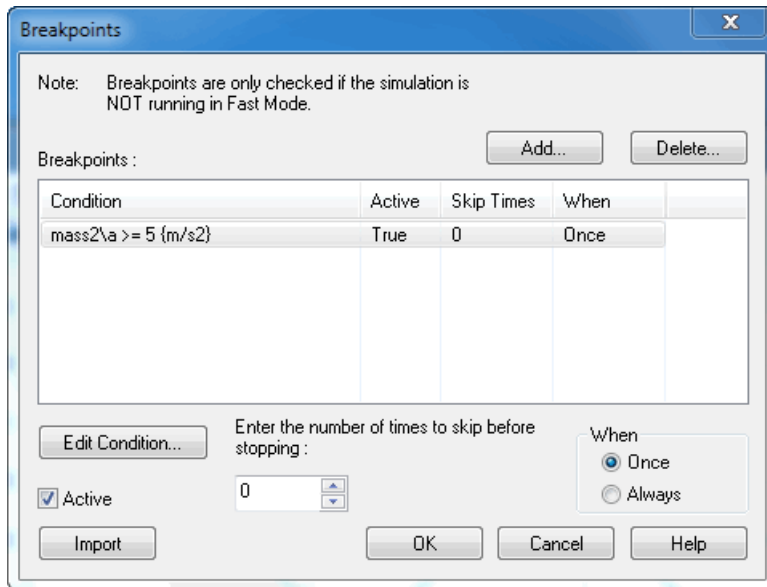
- Graphical submodels: Put the mouse pointer on top of a signal, bond or connection. A box will appear, showing the numerical value associated with that signal, bond or connection.



*Use the mouse pointer to inspect numerical values.*

## Breakpoints

20-sim allows you define stops in a simulation called breakpoints. You can set breakpoints using the Breakpoint Editor. This editor can be opened by selecting the *Breakpoints* command from the *Properties* menu in the Simulator.



*Setting Breakpoints.*

You can run a simulation from breakpoint to breakpoint, using the *Continue* command from the *Simulation* menu.

Breakpoints are useful when problems occur during simulation. By defining an appropriate breakpoint and using the *Run* command, you can run a simulation until the point where the problem occurs. You can continue the simulation using single steps or just running it again.

## Items

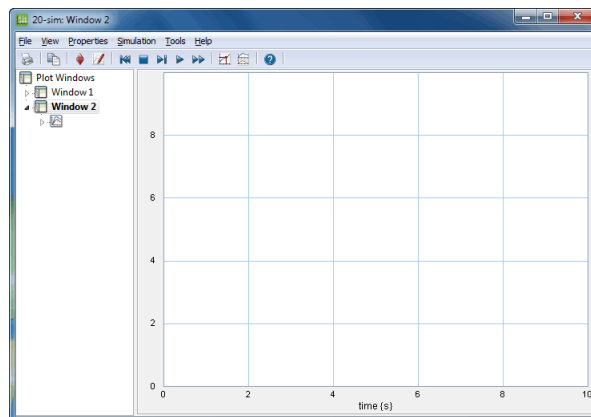
- **Add/Delete:** Use the Add and Delete buttons to add or delete breakpoints. When you add a breakpoint, an editor will be opened to enter the breakpoint conditions.
- **Breakpoints:** The Breakpoints list shows the entered breakpoints.
- **Enter the ... skip before stopping:** A breakpoint may occur more than once before it should stop the simulation run. Enter here the number of times to skip the breakpoint.
- **When:** A breakpoint may occur more than once during a simulation run. With this option you can select the breakpoint to be active only once or always.
- **Active:** Use this option to make a breakpoint effective or not.
- **Edit Condition:** When a breakpoint is selected in the breakpoints list, you can edit it, using the Edit Condition button. This will open an editor which helps you to enter the breakpoint condition.
- **Import:** Import breakpoints from another model.

## Note

Breakpoints are only active when 20-sim is operating in *Debug Mode!*

## New Simulation Plot

You can open additional plots by selecting the *New Plot Window* command from the *View* menu of the simulator.

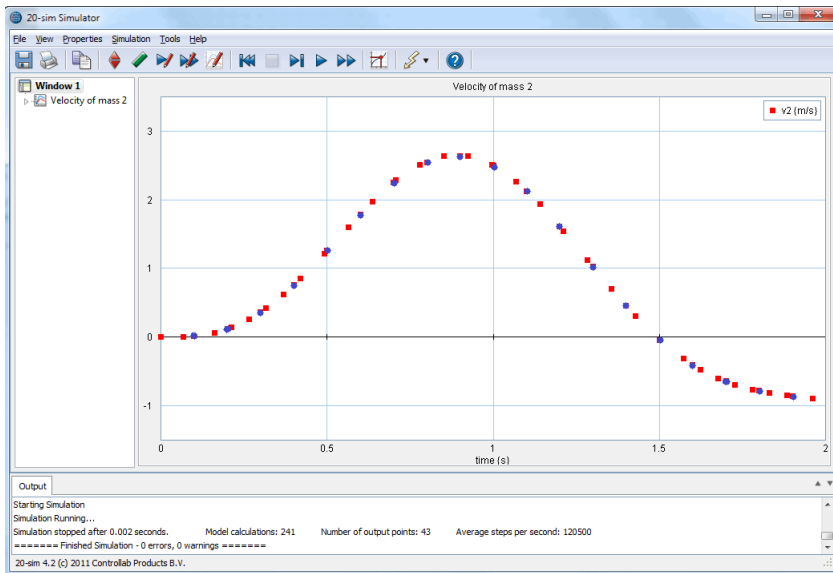


*You can open additional plots in 20-sim.*

Every plot will have a menu bar and buttons to allow you to enter the settings for the plot and running a simulation.

## Resample Curves

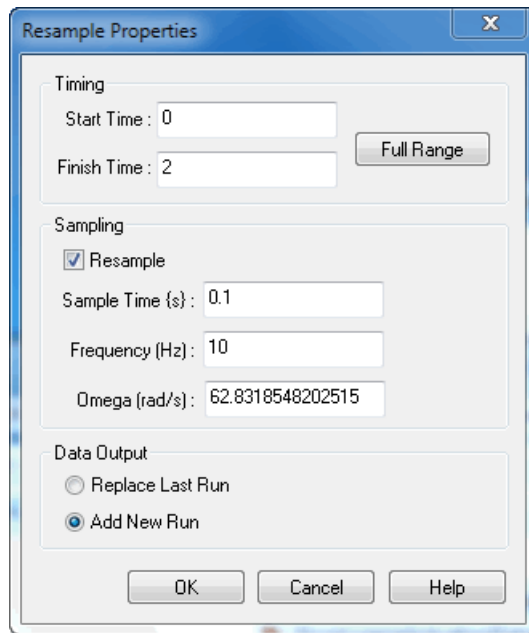
Select the *Resample Curves* command from the *View* menu to sample a simulation run with a fixed sample time. This is useful if you want to use your simulation results in other programs that need data with a fixed time step. An example is given below where a curve (red dots) is shown that is simulated with a variable step integration method. Resampling with a sample time of 0.1 s will result in a curve with only the blue dots.



*Use the Resample Curves command to get equidistant timing in the plot.*

Selection of the *Resample Curves* command of the *View* menu pops up the *Resample Curves dialog*. You can enter the amount of data that you want to resample and the sample time or frequency.





*The Resample Curves dialog.*

### Note

To get simulation data with a fixed time step, using a fixed step integration method is not enough, because this data may contain additional steps generated by time or state events. **Only the Resample Curves command will guarantee fixed time step data!**

### Copy States

To get the same model behavior, compared to the end of the previous run, we have to copy the states of a model to the initial values.

When you use the **Copy States** command of the **Simulation** menu, 20-sim overwrites the initial values of the functions ddt, int, limint and resint with their current output states. This can be done at the end of a simulation run or at any point where a simulation run was interrupted.

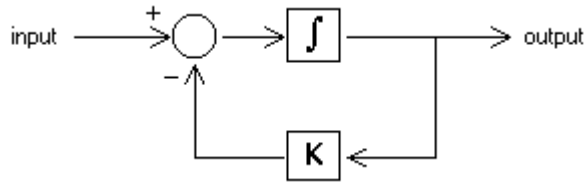
### Tip

For some models, behavior at some operating point or "steady state" is of interest. Use the **Copy States** command to create simulation that directly starts at working level:

1. Run a simulation from  $t = 0$  [s] until the operating point is reached. Use the **Copy States** command to store the states as new initial values. Now save the experiment using some special name.
2. Now each time you open this experiment, simulations directly start at operating point.

### States

Consider the following first order linear model:



This model can be described by the dynamic equation:

$$\text{output} = \text{int}(0) + \text{int}(f(\text{input}, \text{output}))$$

with:

$$\text{int}(0) = \text{the initial value of the integral}$$

$$f(\text{input}, \text{output}) = \text{input} - K \cdot \text{output}$$

In more general terms this equation can also be described as:

$$\text{state} = \text{int}(0) + \text{int}(\text{rate})$$

$$\text{rate} = f(\text{input}, \text{state})$$

When we start to simulate this model at  $t = 0$  [s] the value of the integral is zero. The state is therefore equal to the initial value  $\text{int}(0)$ :

$$\text{state}(0) = \text{int}(0)$$

At the end of a simulation, the integral may be unequal to zero. The state is therefore equal to:

$$\text{state}(\text{end}) = \text{int}(0) + \text{int}(\text{rate}(\text{end})).$$

In other words, the value of the state is *characteristic* for the behavior of the model. To start a new simulation with the *same behavior*, we have to change the initial value to:

$$\text{int}(0) = \text{state}(\text{end})$$

This is valid for all dynamic models: The states of a model are characteristic for its behavior. To get the same behavior, compared to the end of a previous run, we have to copy the states to the initial values.

## Exporting Simulations

There are several methods to export simulation results:

1. Export Plot to Clipboard or File.
2. Export Experiment To Clipboard.
3. Export Data to File.

### Export to Clipboard or File

From the *File* menu, you can choose *Export Plot To MetaFile* or *Export Plot To Clipboard* to export a drawing of the simulation plot.

### Export Experiment To Clipboard.

From the *File* menu, you can choose *Export Experiment To Clipboard* to export all plot settings. A dialog will be opened asking you to specify the settings that should be copied. You can select:

- Parameters
- Initial Values
- Plot Specifications
- Run Specifications
- Multiple Run Specifications
- Export Data Specifications
- BreakPoints

### Export Data to File

From the *File* menu, you can choose *Save Data To File* to export the plotted values to a data file. A file dialog window will pop up asking you to enter a filename. You can choose from the following file formats:

- Comma Separated File (\*.csv): This is the default format and can be used for exporting data to spreadsheet programs such as Microsoft Excel or Open Office Calc.
- 20-sim data file (\*.n): This is the standard 20-sim format.
- Data Files (\*.dat): The standard ANSI format for data files.

### Tip

You can use the *Export Data To File* command to store simulation results of time consuming simulations. For later use you can use the *Import From Data File* command to read the result from file.

### Importing Simulations

There are several methods to import simulation results:

1. Import experiment.
2. Import simulation data.

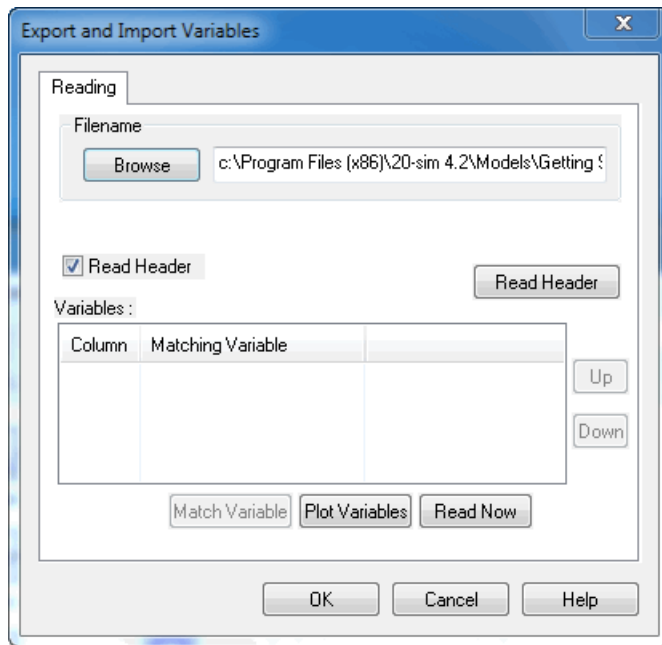
### Export Plot Settings

From the *File* menu, you can choose *Import Experiment* to import the simulation settings from another model. The setting contain all the necessary information that you need to define a simulation:

- parameters
- run porperties
- plot properties
- ...

### Import Data File

From the *File* menu, you can choose *Import Data From File* to import a previously saved simulation plot. A window will pop up allowing you to specify the filename and variables that should be plotted.



*Import data from file.*

If the file contains a header describing the variables inside, they will be shown in the variables dialog.

- **Filename:** You can select an existing filename using the browse button or type one. Data can be read as text file or as binary format.
- **Read Header:** Select this button if you want extra information (variable names etc.) to be read from the data file.
- **Variables:** The variables box shows the number of columns that were found in the data file. Each column must be matched with a variable that is shown in the plot. Click with the mouse on a column number to select it. Then click the Match Variable button. This opens a Variable Chooser in which you can select a variable. When a header was used when storing the data file, this matching is done automatically.
- **Match Variable:** Use this button to select a matching variable for each column in the variables box.
- **Plot Variables:** Use the Delete button to delete a selected variable
- **Plot Variables:** Use this button to put the same variables as shown in the plot into the columns of the variables box.
- **Up/Down:** Use the Up and Down buttons to change the order of the variables shown in the list.

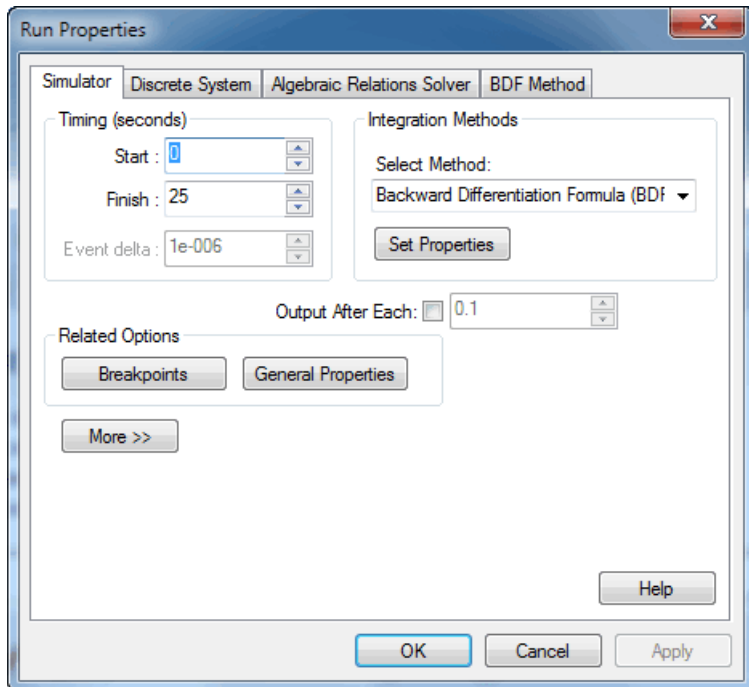
### Tip

You can use the *Export Data To File* command to store simulation results of time consuming simulations. For later use you can use the *Import From Data File* command to read the result from file.

## 6.3 Run Properties

### Simulator Tab

The Simulator tab is the first tab of the *Run Properties Editor*. This tab shows the general simulation settings:



The 20-sim Run Properties.

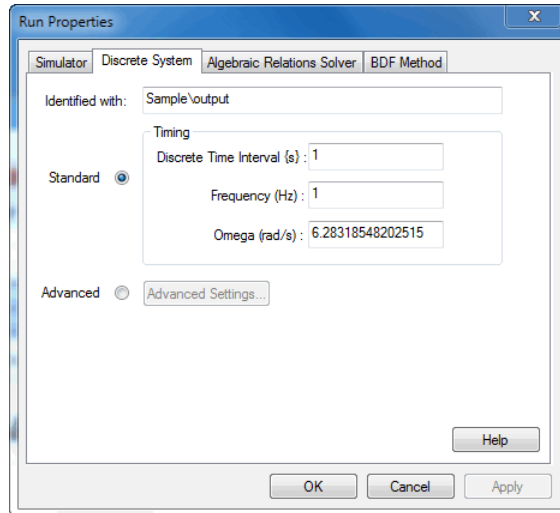
### Items

- *Timing (seconds)*:
  - *Start*: the start time of a simulation run (default: 0)
  - *Finish*: the finish time of a simulation run (default: 10)
  - *Event delta*: the accuracy for spotting state events. This option can only be selected if a model contains state events.
- *Integration Methods*: 8 numerical integration methods are available, each with its own parameters. The parameters can be changed by clicking the Set Properties button or selecting the tab on top of the editor.
  - Euler

- Backward Euler
- Adams-Bashford 2
- Runge Kutta 2
- Runge-Kutta 4
- Runge Kutta Dormand Prince 8
- Runge-Kutta-Fehlberg
- Vode Adams
- Backward Differentiation Formula (BDF)
- Modified Backward Differentiation Formula (MBDF)
- *Output After Each*: This is the plot interval. Use this option to generate output only after each equidistant time interval has passed. For each interval, the exact simulation point is used (if available) or the nearest point is used (if not available, for example when using variable step algorithms).
- *Related Options*
  - *BreakPoints*: Click this button to open the Breakpoints Editor.
  - *General Properties*: Click this button to open the General Properties Editor.
  - *More*: Click this button to set advanced options:
    - *Endless*: Select this option if you do not want the simulation to stop.
    - *Attempting Real-Time simulation*: Select this option if you want the simulation to run as fast as the real time. You can choose the option *Catch up with lost time* and set the *Maximum allowed lost time*.

## Discrete System Tab

The Run Properties Editor can be used to edit the sample frequency of a discrete-time system in the model. 20-sim automatically detects the existence of discrete systems in a model. For each discrete system, one extra tab (Discrete System) is shown in the *Run Properties Editor*.



*The Discrete Systems tab.*

## Items

- *Identified with:* Each discrete system in a model is assigned a unique identifier. 20-sim detects discrete systems by looking for discrete functions and variables:

1. sample
2. hold
3. next
4. previous
5. sampletime

When a function has been found, the elements of the corresponding discrete system are identified by propagation of the equations. In order of appearance in the model, the discrete system is assigned a unique identifier:

1. sample -> the variable that is assigned to the output of the sample function.
2. hold -> the variable that is assigned to the output of the hold function.
3. previous -> the discrete state corresponding with the previous function.
4. next -> the discrete state corresponding with the next function.
5. sampletime -> the variable that is equal to the sampletime.

- **Timing (Standard):** Each discrete system has a default sample frequency of 1 Hz. You can change this frequency to any desired value:
  - **Discrete Time Interval (s):** The sample interval (in s) of the discrete system
  - **Frequency (Hz):** The sample frequency (in Hz) of the discrete system.
- **Timing (Advanced):** For discrete-time control loops that interact with physical continuous-time systems through sensors (analog to digital) and actuators (digital to analog) the specific timing is important. Click the Advanced button to specify this timing.

## Advanced Discrete System Settings

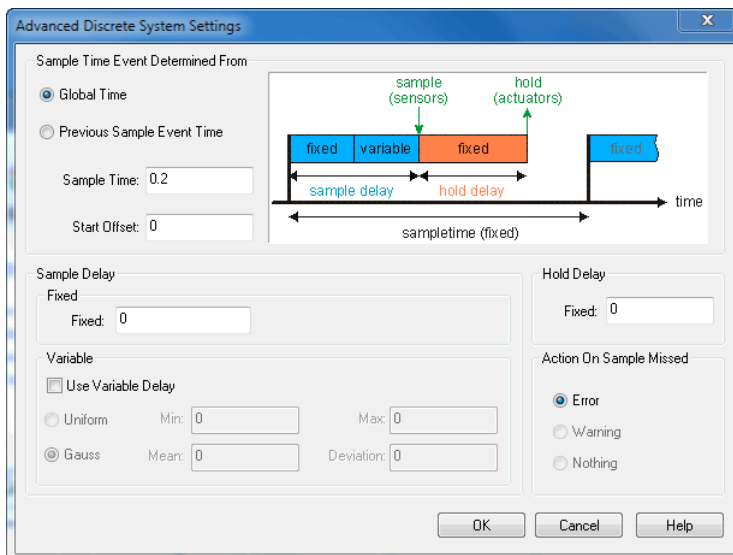
The *Advanced Discrete System Settings* dialog can be used to set the timing for discrete-time control loops that interact with physical continuous-time systems through sensors (analog to digital) and actuators (digital to analog). You can open the dialog by:

1. In the Simulator from the **Properties** menu, click **Run** to open the Run Properties Editor.
2. Select the **Discrete System tab** and click the **Advanced Settings** button.

In the *Advanced Discrete System Settings* dialog you can specify the timing of control loops with a fixed *sampletime* (click *Global Time*) and control loops with a variable *sampletime* (click *Previous Sample Event Time*).

## Fixed Sampletime

When you click the **Global Time** option the following window appears.



*Advanced settings for discrete systems.*



The window shows the timing diagram for a fixed *sampletime* control loop. The loop starts with a clock interrupt from a timer. It will take some time before the interrupt is handled and generally some calculations are performed before the sensor signals (*sample*) are read. This delay is represented by the *sample delay* which is divided in a fixed time and a variable time part. The control loop will proceed and perform the necessary calculations to generate the actuator output (*hold*). These calculations will take some time, which is represented by the fixed time *hold delay*. After this action the control loop will come to a halt until the next clock interrupt is generated.

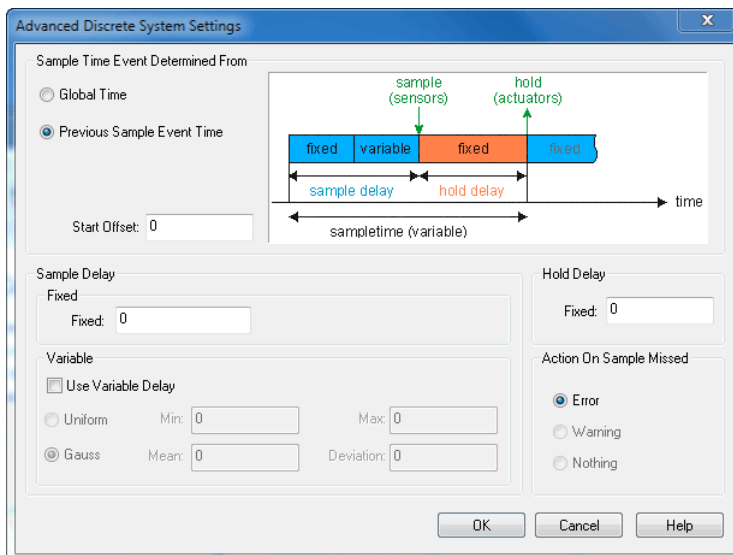
If the control loop is properly designed it will know the task it is performing when a clock interrupt is getting in. E.g. if it is still calculating the actuator outputs when clock interrupt is getting in, an error will be generated, specifying that the sampletime is too small to perform all necessary calculations.

## Items

- *Sample Delay*:
  - *Fixed*: Enter the fixed sample delay here.
  - *Variable*: Enter the variable delay here. You can choose from two distributions:
    - *Uniform*: The delay is uniformly distributed between the given minimum and maximum.
    - *Gaussian*: The delay has a given mean and standard deviation.
- *Hold Delay*: Enter the fixed hold delay here.
- *Action on Sample Missed*: An error will be generated when the total delay is larger than the sampletime or when the total delay is negative.

## Variable Sampletime

When you click the **Previous Sample Event Time** option the following window appears.



*Variable sample time.*

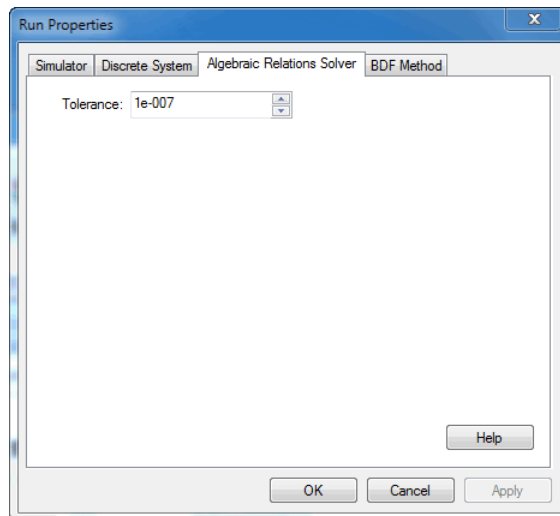
The window above shows the timing diagram for a variable sampletime control loop. It performs the same tasks as a fixed sampletime control loop, but will start the next loop as soon as the previous loop was finished. The variable sampletime control loop does not use a clock interrupt!

### Items

- *Sample Delay:*
  - *Fixed:* Enter the fixed sample delay here.
  - *Variable:* Enter the variable delay here. You can chose from two distributions:
    - *Uniform:* The delay is uniformly distributed between the given minimum and maximum.
    - *Gaussian:* The delay has a given mean and standard deviation.
- *Hold Delay:* Enter the fixed hold delay here.
- *Action on Sample Missed:* Only an error will be generated when the total delay is negative.

### Algebraic Relations Solver Tab

The *Algebraic Relations Solver tab* of the Run Properties Editor is visible when your model contains algebraic loops that could not be solved during processing. In the tab, you can specify the tolerance of the algebraic solver algorithm. For each model evaluation, this solver tries to solve the algebraic loop relations, while standard integration algorithms, such as Euler, can be use to evaluate the model equations.



*The Algebraic Relations Solver tab.*

### Euler

This is the explicit Euler method. It is a single-step explicit method, which needs one model calculation per time step. The size of the time step is fixed. This simulation algorithm requires 1 parameter to be specified:

- *Step Size:* the step time of the integration algorithm (default: 0.01).

## Backward Euler

This is a combination of the implicit Backward Euler method and the explicit Forward Euler method. It is a single-step implicit method, which needs one model calculation per time step. With the parameter alpha the combination is defined:

alpha combination		
-1	100% Forward Euler	explicit
0	50% Forward Euler, 50 % Backward Euler	explicit
1	100% Backward Euler	implicit

- *Step Size*: the step time of the integration algorithm (default: 0.01).
- *Relative Tolerance*: Relative tolerance for the rootfinding in the Backward Euler method.
- *Alpha*: Choose between Forward Euler (alpha = -1), Trapezoidal (alpha = 0) and Backward Euler (alpha = 1).

## Adams-Bashford

This is the trapezoidal rule. It is a single-step explicit method, which needs only two model calculations per time step. The size of the time step is fixed. This simulation algorithm requires 1 parameter to be specified:

- *Step Size*: the step time of the integration algorithm (default: 0.1).

## Runge Kutta 2

This is an explicit single-step second-order derivatives method which needs 2 model calculations per time step. It is the simple form of the classical Runge-Kutta method. The size of the time step is fixed. This simulation algorithm requires 1 parameter to be specified:

- *Step Size*: the step time of the integration algorithm (default: 0.01).

## Runge-Kutta 4

This is an explicit single-step fourth-order derivatives method which needs 4 model calculations per time step. It is the classical Runge-Kutta method. The size of the time step is fixed. This simulation algorithm requires 1 parameter to be specified:

- *Step Size*: the step time of the integration algorithm (default: 0.01).

## Runge-Kutta-Fehlberg

This is an explicit variable-step 4/5-order derivatives method, primarily designed to solve non-stiff and mildly stiff differential equations. Because the method has very low overhead costs, it will usually result in the least expensive integration when solving problems requiring a modest amount of accuracy and having equations that are not costly to evaluate. This simulation algorithm has 4 parameters:

- *Integration Error* (required)
  - *Absolute*: The absolute integration error, valid for every state variable (default: 1e-6).
  - *Relative*: The relative integration error, valid for every state variable (default: 1e-6).
- *Step Size* (not required)

- *Initial*: The step size for the first simulation step (default: 0.01).
- *Maximum*: The maximum size of a simulation step (default: 1).

### Runge Kutta Dormand Prince 8

This is an explicit variable-step 8-order derivatives method, primarily designed to solve non-stiff and stiff differential equations. This simulation algorithm has 4 parameters:

- *Integration Error* (required)
  - *Absolute*: The absolute integration error, valid for every state variable (default: 1e-6).
  - *Relative*: The relative integration error, valid for every state variable (default: 1e-6).
- *Step Size* (not required)
  - *Initial*: The step size for the first simulation step (default: 0.01).
  - *Maximum*: The maximum size of a simulation step (default: 1).

### Vode Adams

This is the explicit variable-step stiff integration algorithm of Cohen and Hindmarsh. This method is specially suited for explicit models that combine high and low frequency vibrations with little damping (so called "stiff" models). This simulation algorithm has 4 parameters:

- *Integration Error* (required)
  - *Absolute*: The absolute integration error, valid for every state variable (default: 1e-6).
  - *Relative*: The relative integration error, valid for every state variable (default: 1e-6).
- *Maximum Step Size* (not required): The maximum size of a simulation step (default: 1).
- *Multistep Method* (required): The variable step integration method that is used. A BDF method is default and best suited for stiff systems.
- *Iteration Type* (required): The method used for iteration loops (algebraic relations). The Newton method is default and best suited for stiff systems.

### Backward Differentiation Formula (BDF)

This is an implicit multi-step variable-order first-order derivatives method. It is Gear's backward differentiation formula, which is up to fifth order, so 1 to 5 model calculations are needed per time step. The code of the Dassl library is used. It is suitable for models having derivative causalities and/or algebraic loops. This simulation algorithm has 4 parameters:

- *Integration Error* (required)
  - *Absolute*: The absolute integration error, valid for every state variable (default: 1e-5).
  - *Relative*: The relative integration error, valid for every state variable (default: 1e-5).
- *Step Size* (not required)
  - *Initial*: The step size for the first simulation step (default: 0.1).
  - *Maximum*: The maximum size of a simulation step (default: 1).

**Note**

- Undamped models are not simulated properly with this method.
- The default values are suitable for problems with time constants of order of magnitude of 0.1 to 1. Initial Step Size and Maximal Step Size influence the behavior of the method and should be tuned with care.

**Modified Backward Differentiation Formula (MBDF)**

This is an implicit multi-step variable-order first-order derivatives method. It is Gear's backward differentiation formula, which is up to fifth order, so 1 to 5 model calculations are needed per time step. The code of the Dassl library is used. It is suitable for models having derivative causalities and/or algebraic loops. The MBDF allows the use of constraint variables when proper initial values are used.

This simulation algorithm has 4 parameters:

- *Integration Error* (required)
  - *Absolute*: The absolute integration error, valid for every state variable (default: 1e-5).
  - *Relative*: The relative integration error, valid for every state variable (default: 1e-5).
- *Step Size* (not required)
  - *Initial*: The step size for the first simulation step (default: 0.1).
  - *Maximum*: The maximum size of a simulation step (default: 1).

**Note**

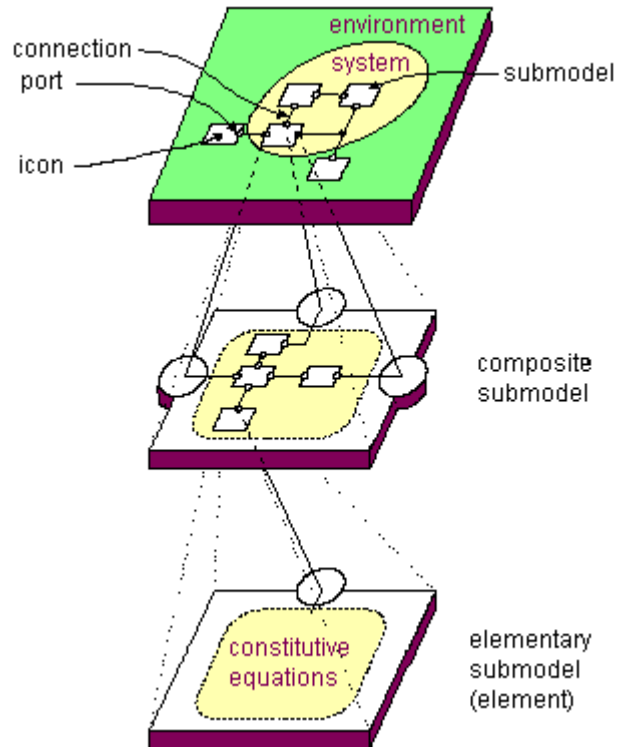
- This is the only method that supports the use of the constraint function.
- The MeBDFi method cannot handle constraints that do not influence the model. Therefore 20-sim will check at the beginning of the simulation if constraints have been properly defined. The constraints that do not influence the model are set to zero automatically. If you do not want to use this check, deselect the **Smart Constraint Solving** option.
- Undamped models are not simulated properly with this method.
- The default values are suitable for problems with time constants of order of magnitude of 0.1 to 1. Initial Step Size and Maximal Step Size influence the behavior of the method and should be tuned with care.

## 7 Language Reference

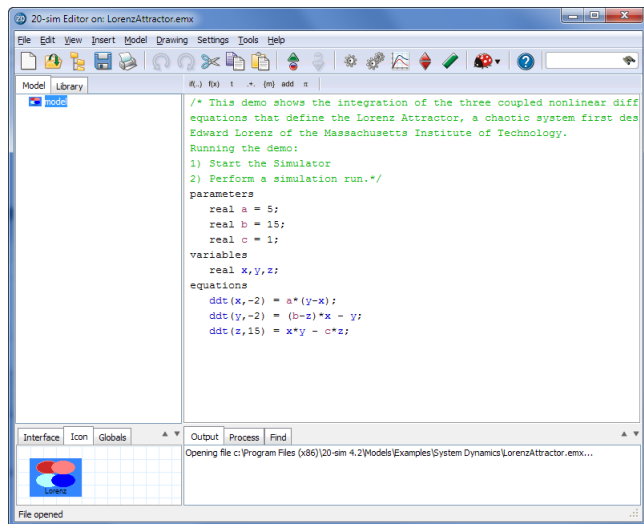
### 7.1 Introduction

#### Language Reference

Every (sub)model has an implementation. This can be a composition of lower level submodels, which themselves are composed of lower level submodels etc. At the bottom of this hierarchy the submodels consist of a set of mathematical equations (equation submodel). These submodels are therefore known as *equation submodels*.



All equations used in 20-sim are described in the language *SIDOPS+*. A simple equation model written in *SIDOPS+* is shown below:



You will find out that in most cases the *SIDOPS+* language is equal to standard mathematical notation. Regardless of your modeling background, you can learn quickly to build your own equation models. 20-sim comes with over 80 built-in functions that do most of the work for you. To learn more about equation models, have a look at the following sections:

1. Model Layout
2. Keywords ( Constants, Parameters, Variables, Equations )
3. Data Types
4. Operators
5. Functions
6. Statements

## Model Layout

The general layout of an equation model is:

*constants*

*// enter your constants here, for a description see constants*

*parameters*

*// enter your parameters here, for a description see parameters*

*variables*

*// enter your variables here, for a description see variables*

*initialequations*

*// enter your initial equations here, for a description see initialequations*

*code*

```

// enter your equations here, for a description see code
equations
// enter your equations here, for a description see equations
finalequations
// enter your final equations here, for a description see finalequations

```

Only the *equations* section is required. The other sections are optional.

## Equations

The body of an equation model consists of the keywords *initialequations*, *code*, *equations* and *finalequations*, each followed by one or more equations. Equations are relations between variables indicated by an equal (=) sign:

```

y = x + 1;
z + y = sin(time*2*pi*f);
g = ddt(g + z, g_initial);

```

An equation can be combination of operators, functions, powerports variables, inputs, outputs, constants, parameters and variables. Equations in 20-sim follow the standard mathematical notation.

## Rules

The following rules must be obeyed when specifying equations:

1. An equation may span more than one line but must always be finished by a semicolon (;)
2. Parentheses may be used to indicate grouping as in ordinary mathematical notation, e.g.  
 $u = \sin(\text{time} * f * 2 * 3.1415 + (a + b) / c);$
4. Extensions like .e or .f are used to indicate the effort and the flow variables of powerports. These extensions are not allowed for any other type of identifier (i.e. inputs, outputs, constants, parameters or variables).
5. 20-sim has some predefined variables which have a special meaning.
6. Each variable must be assigned a value exactly once.
7. Errors are shown automatically after checking in the Process tab. Double clicking on the error text will make 20-sim jump to the error, which is then colored red.

## Execution

1. Equations within 20-sim may be entered in random form. During compilation, 20-sim will automatically try to rewrite equations into a correct order of execution.
2. Some integration algorithms do more calculations before generating the next output value. These calculations are called minor steps, the output generation is called a major step. During a minor step, all model equations are executed. In most cases you will not notice this because only the results of the major step are shown in the simulator, but in some cases this may cause unwanted results.



## Equation Sections

In 20-sim equations can be divided in four sections: *initialequations*, *equations*, *code* and *finalequations*.

### Initialequations

The *initialequations* section should contain all equations that should be calculated before the simulation run. The equations are calculated once. The equations in this section form a code block, i.e. the equations themselves and the order of the equations are not rewritten during compilation and executed sequentially. The results of the *initialequations* section are not shown in the simulator plots and can therefore not be inspected in the Numerical Values window!

### Example

The *initialequations* section is used in the library model *Spring Damper (stiffness)*:

```
parameters
  real k = 10.0 {N/m};
  real m = 1.0 {kg};
  real b = 0.05 {};
variables
  real x {m};
  real d {damping,N.s/m};
initialequations
  d = 2*b*sqrt(k*m);
equations
  x = int (p.v);
  p.F = k * x + d*p.v;
```

As you can see in the *initialequations* section the damping *d* is calculated out of the relative damping *b*, mass *m* and stiffness *k*.

### Equations

The *equations* section contains all standard equations. They do not have to be entered in a sequential form. They are rewritten during compilation to get the correct order of execution. The resulting code is calculated every simulation step. You can see the use of the *equations* section in the example above.

### Code

The *code* section contains a code block. A code block contains all equations that must be calculated sequentially, i.e. the equations themselves and the order of the equations are not rewritten during compilation. The resulting sequential code is calculated every simulation step.

### Example

The *code* section is used in the library model *Spring Damper (stiffness)*:

```

parameters
    real initial = 0.0;
variables
    real prev, peak;
initialequations
    peak = initial;
    prev = 0;
    output = initial;
code
    if major then
        peak = max([abs(input), peak]);
        if (input > 0 and prev < 0) or (input < 0 and prev > 0) then
            output = peak;
            peak = 0;
        end;
        prev = input;
    end;

```

## Finalequations

The *finalequations* section should contain all equations that should be calculated after a simulation run. The equations are calculated once. The equations in this section form a code block, i.e. the equations themselves and the order of the equations are not rewritten during compilation and executed sequentially. The results of the *finalequations* section are not shown in the simulator plots and can therefore not be inspected in the Numerical Values window!

## Example

The *finalequations* section is used in the library model *DoMatlab-Final*:

```

parameters
    string command = "";
finalequations
    // send the command to the workspace
    doMatlab (command);

```

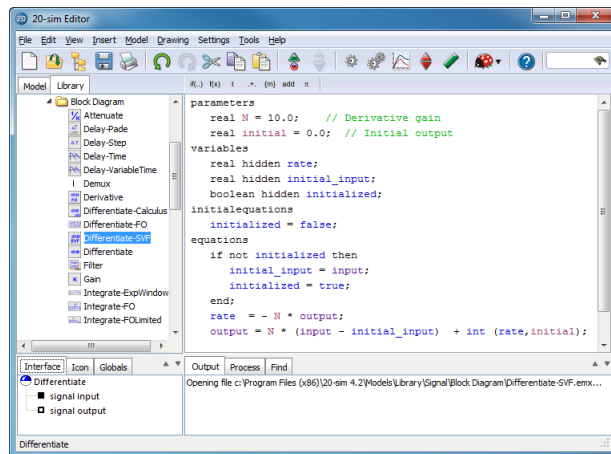
As you see you can give the parameter *command* any value, which is then exported to Matlab at the end of the simulation run.

## Using Port Names

To use port variables in equations, you must use the port names that are defined in the *Interface Editor*.

## Signal Ports

For signal ports, you can directly use the port names. The example below, shows the library model *Differentiate-SVF.emx*. In the *Interface Editor*, two ports are defined with the names *input* and *output*. In the equations these names are used.

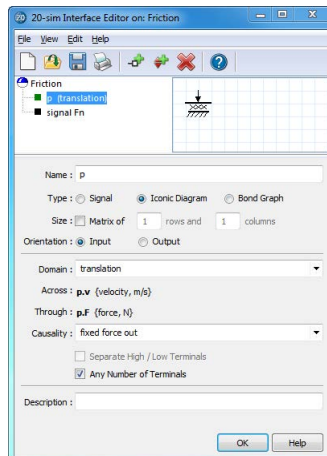


The *Interface* tab shows the contents of the *Interface Editor*.

## Power ports

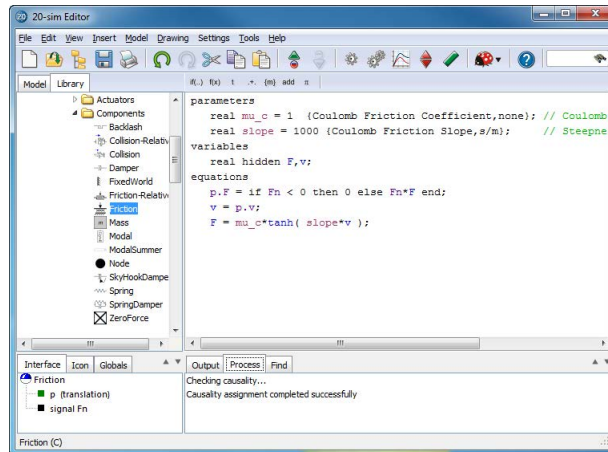
Power ports describe the flow of power and are always characterized by two variables. For bond graph ports the extensions *.e* and *.f* are used to indicate these variables. For iconic diagram ports many aliases are known. You can use these variables in equations by typing the port name followed by a dot and the extension.

You can always find the correct extensions by opening the *Interface Editor* and selecting a port. The example below, shows the library model *Friction.emx*. In the *Interface Editor*, one power port is defined with the name *p*. As shown, the correct description of both variables is *p.v* and *p.F*.



Double clicking in the *Interface* tab will open the *Interface Editor*.

The equation description of this model (see below) shows the use of the variables *p.v* and *p.F*.



*In the equations the port variables  $p.F$  and  $p.v$  are used.*

## Reserved Words

While entering equations, the 20-sim Editor will automatically detect reserved words. You can recognize reserved words, because they will be shown with a different color:

element	color
keywords	<b>black</b>
data types	<b>black</b>
functions	<b>blue</b>
statements	<b>black</b>
predefined variables	<b>blue</b>

20-sim knows the following reserved words:

- , \* , .\* , ./ , .^ , / , ^ , + , < , <= , <> , == , > , >= , abs , adjoint , Adjoint , algebraic , and , antisym , arccos , arccosh , arcsin , arcsinh , arctan , arctanh , atan2 , boolean , by , ceil , code , collect , columns , constants , constraint , cos , cosh , cross , data , ddt , delta , det , diag , direct , discrete , div , dll , dlldynamic , dly , do , doMatlab , effortincausality , else , end , equal , equations , event , eventdown , eventup , exp , exp10 , exp2 , export , externals , eye , false , finalequations , first , floor , flowincausality , for , frequencyevent , from , fromMatlab , gauss , global , hidden , hold , homogeneous , if , import , initialequations , inner , int , integer , interesting , inverse , inverseH , limint , limit , log , log10 , log2 , major , max , min , mod , msum , mul , next , nonlinear , norm , norminf , not , or , parameters , previous , ramp , ran , random , real , repeat , resint , resint , return , round , rows , sample , sampletime , sign , sin , sinh , skew , sqr , sqrt , step , stopsimulation , string , sum , sym , table , tan , tanh , tdelay , then , tilde , time , timeevent , to , toMatlab , trace , transpose , true , trunc , type , types , until , variables , warning , while , xor

## White Space

Like C and other programming languages, 20-sim does not recognize white space (spaces and tabs, carriage returns) except in a string. We recommend that you use white space to make your model easier to follow. For example, the following model is dense and difficult to read:

```
variables
  real y,u;
equations
  y = step(1);
  u = -step(1);
  if time > 5 then y = -ramp(1); u = ramp(1);
  else y = ramp(1); u = -ramp(1); end;
```

Adding white space with indentation makes the same code much easier to read:

```
variables
  real y;
  real u;
equations
  y = step(1);
  u = -step(1);

  if time > 5 then
    y = -ramp(1);
    u = ramp(1);
  else
    y = ramp(1);
    u = -ramp(1);
  end;
```

## Writing Comments

20-sim gives you several options to create comments in a model. You can use each option add explanatory text to your model or to exclude ("comment out") certain parts of your model for testing and debugging purposes.

### Block Quotes ("...")

You can enclose a block of text between quotes (""). This method makes it easy to write a comment over multiple lines:

```
"This is a line of sample code that shows you how to
use the 20-sim comments"
```

### Programming (/\*...\*/)

You can enclose a block of text between the constructs /\* and \*/. This method is used often in programming and also allows to write a comment over multiple lines:

```
/*This is a line of sample code that shows you how to
use the 20-sim comments*/
```

### Single Line Comment (//...)

A option often used in programming is to insert // into a line. The compiler ignores everything to the right of the double slashes on that line only.

```
// This is a line of sample code showing the
// 20-sim comments.
```

You can begin comments anywhere in a model. 20-sim will automatically recognize comments and color it green.

## State and Time Events

Normally an integration algorithm uses a fixed time step or a variable step, depending only on the model dynamics. In some cases, the algorithm is forced to perform calculations at a specific time.

### Time Events

The most simple form of forced calculation is calculation at a specific time. This is called a *time event*. The following functions cause time events.

function	description
timeevent	Forces the integration algorithm perform a calculation at a specific time.
frequencyevent	Forces the integration algorithm perform a calculation at a specific frequency.
sample , hold, next, previous	These functions introduce a discrete system in a model. A discrete system forces the integration algorithm to perform calculations every sampletime.

### State Events

Sometimes the integration algorithm must iterate to find the next calculation step. This is called a *state event*. The following functions cause state events.

function	description
event	Forces the integration algorithm to find the exact point where the input crosses zero.
eventup	Forces the integration algorithm to find the exact point where the input crosses zero from a negative to a positive value.
eventdown	Forces the integration algorithm to find the exact point where the input crosses zero from a positive to a negative value.
limint	Forces the integration algorithm to find the exact point where the output become larger or smaller than the minimum and maximum parameters.
resint	Forces the integration algorithm to find the exact point where the input becomes zero.

To find the exact point where simulation should be performed iteration is used. The accuracy of the iteration can be set by the event delta parameter in the Run Properties window.

## 7.2 Keywords

### Keywords

Before the actual equations, three sections can be entered denoted by the keywords *constants*, *parameters* and *variables*. This is shown in the example below:

```
constants
    real basefrequency = 60;
    real pi = 3.14159265;
parameters
    real amplitude = 1;
variables
    real plot;
equations
    plot = amplitude * sin (basefrequency*2*pi * time);
```

The order of appearance of these sections must always be: (1) constants, (2) parameters and (3) variables. The sections are optional. If you do not use constants parameters or variables, these sections may be omitted.

### Constants

Constants are symbolic representations of numerical quantities that do not change during or in between simulation runs. Constants must be defined in 20-sim, using the constants keyword. After the keyword, lines with constant declarations can be entered. Every line must be finished by a semicolon (;). An example is given below:

```
constants
    real V = 1 {volume, m3};           // the volume of barrel 1
    real hidden D = 0.5 {length, m};   // the length of part 1
    ...
```

### Types

20-sim currently supports four types of constants: *boolean*, *integer*, *real* and *string*. These types must be specified explicitly. The use of the type real is shown in the example above.

## Hidden

To prevent users from inspecting constants, the keyword *hidden* can be applied. This keyword should follow the data type.

## Constant names

Constant names can consist of characters and underscores. A constant name must always start with a character. Constant names are case-sensitive. No reserved words may be used for constants. If a reserved word is used, an error message will pop-up while checking the model. In the example above the names *V* and *D* are used.

## Constant Values

It is advised to assign every constant a value. Otherwise 20-sim will assign a default value (0, false or an empty string), which can easily lead to misinterpretations. Unlike parameter values, constant values cannot be overridden in the Simulator.

## Quantity and Unit

If a constant is known to represent a physical value, you can define the corresponding quantity and unit. 20-sim will use this information to do a unit check on equations. The use of quantities and units is optional. In the example above the quantities volume and *length* are used with the units *m3* and *m*.

## Example



*constants*

```
real pi = 3.14159265359;
real two pi = 6.28318530718;
integer i = 10 {length,m};           // vehicle length
integer j = 1 {time,s};
```

*constants*

```
string filename = 'data.txt';
integer i = 1;
real state = 0.0;
boolean t = true, f = false;
```

## Tip

- You can easily enter constants by using the Add button  in the *Equation Editor Taskbar*.
- You can easily select quantities and units by using the Units button  of the *Equation Editor Taskbar*.

## Predefined Constants

Some constants in 20-sim have a predefined value. These constants do not have to be declared in the *constants* section of a model. You can add your own predefined constants in the file *Constants.ini* in the 20-sim bin-directory.

### Standard

pi	3.1415926535897932384626433832795
exp1	2.71828182845904523536028747135266
twopi	6.28318530717958647692528676655901
sqrt2	1.41421356237309504880168872420969



log2 0.6931471805599453094172321214581766

### Physics

g_n	9.80665 {m/s <sup>2</sup> }	Standard acceleration of gravity
G	66.7259e-12 {N.m <sup>2</sup> /kg <sup>2</sup> }	Newtonian constant of gravitation
c_0	299.792458e6 {m/s}	Speed of light (vacuum)
mu_0	1.2566370614359172953850 573533118e-6 {H/m}	Permeability (vacuum)
epsilon_0	8.854188e-12 {F/m}	Permittivity (vacuum)
h	6.6260755e-34 {J.s}	Planck constant
m_p	2.17671e-08 {kg}	Planck mass
l_p	1.61605e-35 {m}	Planck length
t_p	5.39056e-44 {s}	Planck time
e	1.60217733e-19 {C}	Elementary charge
R_H	25812.8056 {Ohm}	Quantized Hall resistance
mu_B	9.2740154e-24 {J/T}	Bohr magneton
mu_N	5.0507866e-27 {J/T}	Nuclear magneton
Ry	10973731.534 {1/m}	Rydberg constant
a_0	5.29177249e-11 {m}	Bohr radius
N_A	6.0221367e+23 {1/mol}	Avagadro constant
m_u	1.6605402e-27 {kg}	Atomic mass constant
F	96485.309 {C/mol}	Fraday constant
k	1.380658e-23 {J/K}	Boltzmann constant
sigma	5.67051e-08 {W/m <sup>2</sup> .K <sup>4</sup> }	Stefan-Boltzmann constant
b	0.002897756 {m.K}	Wien constant
R	8.31451 {J/mol.K}	Molar gas constant
V_m	0.0224141 {m <sup>3</sup> /mol}	Molar volume (ideal gas)
n_0	2.686763e+25 {1/m <sup>3</sup> }	Loschmidt constant
m_e	9.1093897e-31 {kg}	Electron mass
m_p	1.6726231e-27 {kg}	Proton mass
m_n	1.6749286e-27 {kg}	Neutron mass

### Conversion Constants

eV	1.60217733e-19 {J}&#9;	Electron volt
u	1.6605402e-27 {kg}	Atomic mass unit
atm	101325 {Pa}	Standard atmosphere
deg	0.0174532925199432957692 369076848861 {rad}	Angular degree

### Parameters

Parameters are symbolic representations of numerical quantities which can only be changed after simulation has been stopped. They can therefore be changed in between of simulation runs, or after the user has (temporarily) stopped the simulation.

Parameters must be defined in 20-sim, using the `parameters` keyword. After the keyword, lines with parameter declarations can be entered. Every line must be finished by a semicolon (;) and may be followed by comment with a description of the parameter. An example is given below:

```
parameters
  real V = 1 {volume, m3};           // the volume of barrel 1
  real hidden D = 0.5 {length, m}; // the length of part 1
  ...
```

## Types

20-sim currently supports four types of parameters: *boolean*, integer, real and string. These types must be specified explicitly. The use of the type *real* is shown in the example above.

## Hidden

To prevent users from inspecting parameters or decreasing the list of parameters, the keyword *hidden* can be applied. This keyword should follow the data type.

## Global

To use the same parameter in other submodels, the keyword *global* can be applied. This keyword should follow the data type.

## Parameter Names

Parameter names can consist of characters and underscores. A parameter name must always start with a character. Parameter names are case-sensitive. No reserved words may be used for parameters. If a reserved word is used, an error message will pop-up while checking the model. In the example above the names *V* and *D* are used.

## Parameter Values

Parameters can be assigned *default* values. These values can be overridden in the Simulator using the Parameters command.

## Quantity and Unit

If a parameter is known to represent a physical value, you can define the corresponding quantity and unit. 20-sim will use this information to do a unit check on equations. The use of quantities and units is optional. In the example above the quantities *volume* and *length* are used with the units *m3* and *m*.

## Comment

If comment is added at the end of the parameter declaration, it is shown in the Variable Chooser to facilitate the selection between variables.

## Example



```

parameters
  real p1 = 12, p2, state = 1.1;
  integer i = 10 {length,m};           // vehicle length
  integer j = 1 {time,s};

parameters
  string filename = 'data.txt';        // This comment appears as a description in the
Parameters/Initial values editor.
  integer i = 1;                       // Just a parameter
  real state;                          // Initial velocity [m/s]
  boolean t = true;                    // T = true

```

## Tip

- You can easily enter parameters by using the Add button  in the *Equation Editor Taskbar*.
- You can easily select quantities and units by using the Units button  of the *Equation Editor Taskbar*.

## Variables

Variables are symbolic representations of numerical quantities that may change during simulation runs. Variables must be defined in 20-sim, using the variables keyword. After the keyword, lines with variable declarations can be entered. Every line must be finished by a semicolon (;). An example is given below:

```

variables
  real interesting V {volume, m3};      // the volume of barrel 1
  real hidden D {length, m};           // the length of part 1
  ...

```

## Types

20-sim currently supports four types of variables: *boolean*, *integer*, *real* and *string*. These types must be specified explicitly. The use of the type real is shown in the example above.

## Interesting

By adding the keyword *interesting* after the variable type, a variable will be given special focus in the Variable Chooser. The Variable Chooser shows the complete list of variables of a model and is used to select variables for plotting. The keyword *interesting* is shown in the variable list, making it easier to find variables of special interest.

## Hidden

To prevent users from inspecting variables or decreasing the list of variables, the keyword *hidden* can be applied. This keyword should follow the data type.

## Global

To use the same variable in other submodels, the keyword *global* can be applied. This keyword should follow the data type.

## Variable Names

Variable names can consist of characters and underscores. A variable name must always start with a character. Variable names are case-sensitive. No reserved words may be used for variables. If a reserved word is used, an error message will pop-up while checking the model.

## Variable Values

Variables cannot be assigned default values.

## Quantity and Unit

If a variable is known to represent a physical value, you can define the corresponding quantity and unit. 20-sim will use this information to do a unit check on equations. The use of quantities and units is optional. In the example above the quantities *volume* and *length* are used with the units *m3* and *m*.

## Comment

If comment is added at the end of the variable declaration, it is shown in the *Variable Chooser* to facilitate the selection between variables.

## Predefined Variables

20-sim has some predefined variables which have a special meaning.

### Example

```
variables
  real interesting p1,p2,state;
  integer i;
  integer j;
```

```
variables
  string filename;
  integer interesting i;
  real interesting state;
  boolean t,f;
```

## Predefined Variables

Some variables in 20-sim have a predefined value. These variables do not have to be declared in the *variables* section of a model.

### time

The variable *time* is equal to the simulated time. It can for example be used in functions such as:

```
u = sin(time*f*2*3.1415);
```

### sampletime

The variable *sampletime* is equal to the sampletime. It is only meaningful when it is used in an equation model that is part of a discrete loop in your model. 20-sim will automatically detect, which loop the model belongs to and assign the proper value to the variable *sampletime*.

### random

The variable *random* will yield a random variable uniformly distributed in the interval  $[-1,1]$ . E.g.:

```
u = random;
```

### **true**

The variable *true* will return the boolean value true.

### **false**

The variable *false* will return the boolean value false.

### **major**

Some integration algorithms, will perform model calculations at one or more intermediate points before calculating the next output value. To prevent equations being calculated, at these intermediate steps, you can use the variable *major*. This variable will return the boolean *false* when calculations are performed for an intermediate step and will return *true* when calculations are performed for the output values.

### **Example**

```
....
if major then
    sim_steps = sim_steps + 1;    // this equation is not evaluated at intermediate
    points
end;
....
```

## **Global Parameters and Variables**

Global parameters and variables are defined using the keyword **global**. In equation models, this keyword is added after the definition of the data type in the Equation Editor:

```
parameters
    real global par1 = 100 {Hz};
    real global par2 ;
variables
    real global var1;
    real global var2;
..
..
```

Parameters can only be assigned a value once. The same goes for variables. Only one submodel must defined their value using an equation. If parameters or variables are assigned more than once, 20-sim will generate an error.

### **Example**

The best way to describe the use of global parameters and variables is by an example model. You can find this model in the 20-sim demonstration library (*Demo\Tips And Tricks\Global Parameters and Variables.emx*). The model exists of three submodels. In the first submodel two global parameters (*f* and *A*) are assigned and one variable (*sinewave*). The variable is assigned a value in the equations section and connected with the output (*out1*).

*submodel1*

*parameters*

*real global f = 100 {Hz};*

*real global A = 1 {none};*

*variables*

*real global sinewave;*

*equations*

*sinewave = A\*sin(f\*2\*pi\*time);*

*out1 = sinewave;*

In the second submodel, the two global parameters are use to connect them with two outputs (*out1* and *out2*).

*submodel 2*

*parameters*

*real global f {Hz};*

*real global A {none};*

*variables*

*real global sinewave;*

*equations*

*out1 = f;*

*out2 = A;*

In the third submodel, the global variable is connected with an output (*out1*).

*submodel 3*

*variables*

*real global sinewave;*

*equations*

*out1 = sinewave;*

To prevent conflicts global parameters may be assigned a default value only once. The same goes for global variables: they may be assigned a value in the equation section only once.

## 7.3 Types

### Data Types

For all parameters, variables, initial conditions etc. 20-sim supports the following data types:

1. Boolean
2. Integer
3. Real
4. String

The declaration of data types can be done in the *constants*, *parameters* and *variables* sections of the model. E.g.:

```

parameters
  real a = 1
  integer B[2,2];
variables
  string c;
  boolean yesno;

```

Declaration of data types in equations is not allowed. E.g.:

```

real v = sin(t*a + b); // This is not allowed!

```

## Hidden

To prevent users from inspecting variables, parameters or constants (e.g. for encrypted models) or decreasing the list of parameters and variables, the keyword *hidden* can be applied. This keyword should follow the data type. For example:

```

parameters
  real hidden a = 1
  integer hidden B[2,2];
variables
  string hidden c;
  boolean hidden yesno;

```

## Interesting

To allow for a quick selection of variables in the Variable Chooser, the keyword *interesting* can be applied for variables. This keyword should follow the data type. For example:

```

parameters
  real a = 1
  integer B[2,2];
variables
  string interesting c;
  boolean interesting yesno;

```

Interesting variables are shown, even when all options are deselected in the Variable Chooser. This makes it possible to quickly select variables out of a large list.

## Boolean

Either *true* (1) or *false* (0). Variables of this type should not be used to store any other values. Like C++, 20-sim evaluates non-zero values as true; only the value of zero is evaluated as false. Normally, the value of one is used to indicate true.

## Examples

```

boolean a;
boolean b = true;
boolean c = false;
boolean D[2,2] = [true,true,false,false];
a = b and c;

```

## Limitations

When used in standard functions, booleans are treated as reals with value 0 or 1. An equation like:

```

boolean a = true;
real c;
c = sin(a);

```

would yield c equal to 0.8415. Try to avoid these constructions, since they lead to confusions.

## Integer

Signed four-byte integer. It can hold any value between -2147483648 and +2147483647. Integer is the recommended data type for the control of program loops (e.g. in for-next loops) and element numbering.

### Example

```

parameters
  integer i = 1, j = 2;
  real B[2,2] = [1,2;3,4]
  real b;
equations
  b = B[i,j];
  for i := 1 to 10 do ....end;

```

### Limitations

When used in standard functions, integers are treated as reals. An equation like:

```

parameters
  integer c;
equations
  c = 10*sin(time);

```

would yield c equal to 0.8415. Try to avoid these constructions, since they lead to confusions. Use the round function instead:

```

parameters
  integer c;
equations
  c = round(10*sin(time));

```

## Real

Signed 64 bit floating point number. The maximum representable number is 1.7976931348623158e+308. The minimum positive value unequal to zero is 2.2250738585072014e-308. If reals exceed this range during simulation, the numerical values window will display the values 1.#INF (positive infinite) or -1.#INF (negative infinite).

### Example

```

real a = 0.0;
real b = 1.04e-31, c = -3198.023e-64;
real B[2,2] = [1.2,22.4;3.0e3,-4.023e-6];

```

### Limitations

In practice, during simulation, real should not exceed 1e-100 .. 1e100 to prevent instability in the integration algorithms.

## String

A string is an array of characters. There is no limit to the amount of characters a String may contain. Simple string concatenation (e.g. concatenation that can be done during processing) is allowed. Strings must always be entered between single quotes ('). A single quote can be



escaped with a second quote, so if a single quote should be part of the string, it needs to be typed twice.

### Example

```
parameters
  string c = 'C:\data.txt';
  string b = 'This is a string with a " single quote';
variables
  real d;
  string name;
equations
  if time > 10 then stopsimulation (b); end;
  d = table(c,1);
  name = c + ' // file';
  toMatlab (d, name)
```

### Limitations

Strings may only be used as input for some special functions (e.g. table).

## 7.4 Functions

### Functions

In 20-sim you can use all kind of functions to describe your equations. They are classified according to the list below.

1. Arithmetic
2. Discrete
3. Event
4. Expansion
5. Extern
6. Matrix
7. Port
8. Source
9. Trigonometric

### Arithmetic

#### Syntax

$$Y = \text{abs}(X);$$

#### Description

Returns the absolute value of X or the elements of X.

#### Examples

<b>X</b>	<b>abs(X)</b>
1	1

2.1	2.1
-2.6	2.6
-1e-102	1e-102
[1.1,2.7;-3.6,-4]	[1.1,2.7;3.6,4]

### Limitations

- X and Y must have the same size.
- For scalars, the abs function can also be written as:  $Y = |X|$ ;

### Syntax

$y = algebraic(x);$

### Description

y becomes equal to x. This function forces the integration algorithm to find a solution by using the algebraic loop solver. Normally when algebraic loops occur in a model, 20-sim will itself will break the algebraic loop using the algebraic loop solver internally. You can use this function to break an algebraic loop at a user-defined position.

### Examples

```
u = sin(time);
a = algebraic(y);
y = K*(u - a);
```

### Note

Be very careful with this function. In most cases the symbolic engine of 20-sim will find and exact solution which will lead to much faster simulation!

### Syntax

$Y = ceil(X);$

### Description

Rounds X or the elements of X to the nearest integers greater than or equal to X.

### Examples

X	ceil(X)
1	1
2.1	3
-2.6	-2
3.4	4
[1.1,-2.7;3.5,-4.1]	[2,-2;4,-4]

### Limitations

X and Y must have the same size.

**Syntax**

```
y = constraint(x);
```

**Description**

This function iteratively assigns a value to *y* such that *x* approaches zero within a given error margin. It only works in combination with the MBDF simulation method! The function is very useful for entering constraints in physical systems and inverse dynamics.

**Examples**

This example makes a velocity *vm* equal to a reference velocity *vs*:

```
vs = sin(time);           // reference velocity
v = vm - vs;              // If v = 0 then the mass follows the reference velocity
F = constraint(v);        // Make F have a value that yields a zero velocity v
vm = (1/m)*int(F);        // mass
```

**Syntax**

```
y = ddt(x,init);
```

**Description**

Returns the derivative value of *x* with respect to the time. The initial value of *y* is equal to the value of *init*.

**Method**

20-sim will always try to rewrite equations in such a way that only integrals are used (integral form). This is done automatically and means all integration methods can be applied. Sometimes an integral form cannot be found. Then only the Backward-Differentiation Method can be used for simulation.

**Examples**

equation	integral form	integration
ddt(x,0) = u - k*x; x = ddt(sin(time),0);	x = int(u - k*x); not possible!	All methods Only BDF

**Limitations**

When no integral form can be found, the use of the derivative function can introduce noisy signals or may even cause signals to exceed the data range.

**Syntax**

```
y = dly(x,init);
```

**Description**

*y* is equal to the value of *x*, one simulation-time step delayed. The initial value of *y* is equal to *init*

**Example**

```
x = sin(time*0.3);
y = dly(x, 1.0);
```

**Limitations**

x,y and init must be scalars.

**Syntax**

```
Y = exp(X);
```

**Description**

Returns the exponential function of X or the elements of X.

$$y = e^x;$$
**Examples**

<b>x</b>	<b>exp(x)</b>
1	2.718282 (= $e^1$ )
2.1	8.166170 (= $e^{2.1}$ )
-2.6	0.074274 (= $e^{-2.6}$ )
[1,2.1;-2.6,1]	[2.718282,8.166170;0.074274,2.718282] ( = [ $e^1, e^{2.1}; e^{-2.6}, e^1$ ] )

**Limitations**

X and Y must have the same size.

**Syntax**

```
Y = exp10(X);
```

**Description**

Returns the exponential function (base 10) of X or the elements of X.

$$y = 10^x;$$
**Examples**

<b>x</b>	<b>exp10(x)</b>
1	10 (= $10^1$ )
2.1	125.89 (= $10^{2.1}$ )
-2.6	0.00251 (= $10^{-2.6}$ )

$[1, 2.1; -2.6, 1]$        $[10, 125.89; 0.00251, 10]$   
 $( = [10^1, 10^{2.1}; 10^{-2.6}, 10^1] )$

### Limitations

X and Y must have the same size.

### Syntax

$Y = \exp2(X);$

### Description

Returns the exponential function (base 2) of X or the elements of X.

$$y = 2^x;$$

### Examples

<b>X</b>	<b>exp2(x)</b>
1	2 ( $= 2^1$ )
2.1	4.8709 ( $= 2^{2.1}$ )
-2.6	0.16494 ( $= 2^{-2.6}$ )
$[1, 2.1; -2.6, 1]$	$[2, 4.8709; 0.16494, 2]$ ( $= [2^1, 2^{2.1}; 2^{-2.6}, 2^1]$ )

### Limitations

X and Y must have the same size.

### Syntax

$Y = \text{floor}(X);$

### Description

Rounds X or the elements of X to the nearest integers less than or equal to X.

### Examples

<b>X</b>	<b>floor(X)</b>
1	1
2.1	2
-2.6	-3
3.4	3
$[1.1, -2.7; 3.5, -4.1]$	$[1, -3; 3, -5]$

### Limitations

X and Y must have the same size.

**Syntax**

$$Y = \text{initialvalue}(X);$$
**Description**

Returns the initial value of X or the elements of X. Value should be assigned to X first.

**Examples**

<b>X</b>	<b>initialvalue(X)</b>
<i>1</i>	1
<i>sin(time)</i>	0
<i>[cos(time); sin(time)]</i>	[1;0]

**Limitations**

X and Y must have the same size.

**Syntax**

$$y = \text{int}(x, \text{init});$$
**Description**

Returns the integral of x with respect to the time. The initial value of y is equal to the value of init. This initial value is optional. If no value is entered, a default initial value of 0 is used.

**Examples**

$$\begin{aligned} y &= \text{int}(x, 0); \\ z &= \text{int}(\sin(\text{time} * w + p) - \cos(\text{time} * x + z), b); \end{aligned}$$
**Syntax**

$$y = \text{limint}(x, \text{min}, \text{max}, \text{init});$$
**Description**

Returns the integral of x with respect to the time. The initial value of y is equal to the value of init. The output of this integral is limited between a maximum and minimum bound given by the parameters min and max.

This function forces the integration algorithm to find the exact point where the gets saturated. If the integral is in saturated condition and the input changes sign, the output wanders away from the bounds immediately.

The limitedIntegrator block is used for the prevention of wind-up in PI and PID controllers in control applications. It is also used in kinematics, electrical circuits, process control, and fluid dynamics.

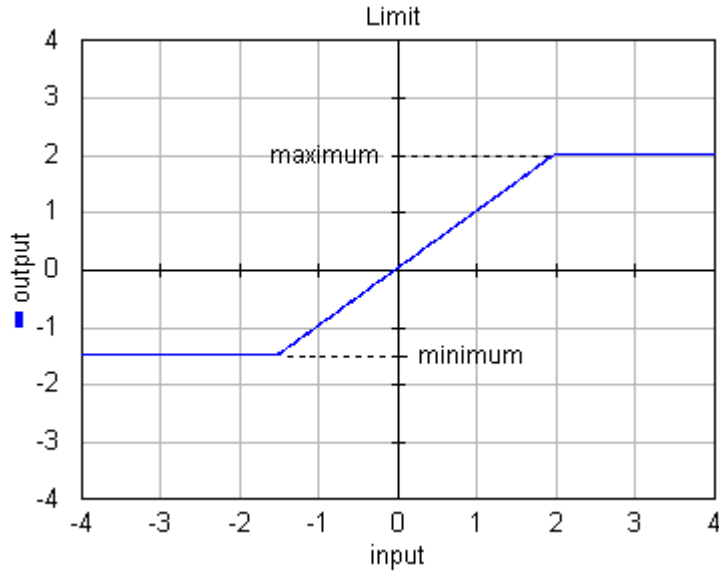
**Examples**

$$\begin{aligned} x &= 10 * \sin(\text{time} * 10); \\ y &= \text{limint}(x, -1, 1, 0); \end{aligned}$$

**Syntax**

$$y = \text{limit}(x, a, b);$$
**Description**

This function limits the signal  $x$  between a minimum of  $a$  and a maximum of  $b$ .

**Examples**

```
x = 10*sin(time);
y = limit(x,-5,5);
```

**Limitations**

$a, b, x$  and  $y$  must be scalars.  $a$  must be smaller than  $b$ .

**Syntax**

$$y = \log(x);$$
**Description**

Returns the natural logarithm of  $X$  or the elements of  $X$ .

**Examples**

<b>X</b>	<b>log(X)</b>
1	0
2.1	0.6931
4	1.3863

$[1,2.1;4,1]$ 

-2.6

 $[0,0.6931;1.3863,0]$ *not allowed!***Limitations**

X and Y must have the same size. X or the elements of X must be larger than zero.

**Syntax**

$$Y = \log_{10}(X);$$
**Description**

Returns the base 10 logarithm of X or the elements of X.

**Examples**

<b>X</b>	<b>log10(X)</b>
1	0
50	1.6990
100	2
$[1,50;100,1]$	$[0,1.6990;2,0]$
-2.6	<i>not allowed!</i>

**Limitations**

X and Y must have the same size. X or the elements of X must be larger than zero.

**Syntax**

$$Y = \log_2(X);$$
**Description**

Returns the base 2 logarithm of X or the elements of X.

**Examples**

<b>X</b>	<b>log2(X)</b>
1	0
2.1	1.0704
4	2
$[1,2.1;4,1]$	$[0,1.0704;2,0]$
-2.6	<i>not allowed!</i>

**Limitations**

X and Y must have the same size. X or the elements of X must be larger than zero.



**Syntax**

```
y = resint(x,newoutp,reset,init);
```

**Description**

Returns the integral of *x* with respect to the time. The initial value of *y* is equal to the value of *init*. The output of this integral is reset to the value of *newoutp* when the Boolean argument *reset* is *TRUE*.

**Examples**

```
x = 1;
reset = event(sin(time));
y = resint(x,0,reset,0);
```

or

```
x = 1;
reset = if y > 10 then true else false end;
y = resint(x,0,reset,0);
```

**Syntax**

```
Y = round(X);
```

**Description**

Rounds *X* or the elements of *X* to the nearest integer.

**Examples**

<b>X</b>	<b>round(X)</b>
1	1
2.1	2
-2.6	-3
3.7	4
[1.1,-2.7;3.5,-4.1]	[1,-3;4,-5]

**Limitations**

*X* and *Y* must have the same size.

**Syntax**

```
Y = sign(X);
```

**Description**

Returns the sign of *X* or the elements of *X*.

$$\begin{aligned}
 X &= < 0 : Y = -1 \\
 X &= 0 : Y = 0 \\
 X &> 0 : Y = 1
 \end{aligned}$$
**Examples**

<b>X</b>	<b>sign(X)</b>
1	1
2.1	1
-2.6	-1
0	0
[1,2.1;-2.6,0]	[1,1;-1,0]

**Limitations**

X and Y must have the same size.

**Syntax**

$$Y = \text{sqr}(X);$$
**Description**

Returns the square of X or the elements of X.

**Examples**

<b>X</b>	<b>sqr(X)</b>
1	1 ( $= 1^2$ )
2.1	4.41 ( $= 2.1^2$ )
-2.6	6.76 ( $= -2.6^2$ )
0	0 ( $= 0^2$ )
[1,2.1;-2.6,0]	[1,4.41;6.76,0] ( $= [1^2, 2.1^2; -2.6^2, 0^2]$ )

**Limitations**

x and y must be scalars.

**Syntax**

$$X = \text{sqrt}(Y);$$
**Description**

Returns the square root of X or the elements of X.

**Examples**

<b>X</b>	<b>sqrt(X)</b>
----------	----------------

1	1
2.1	1.44913
4	2
[1,2.1;4,1]	[1,1.44913;2,1]
-1	<i>not allowed!</i>

### Limitations

X and Y must have the same size. X or the elements of X must be larger than or equal to zero.

### Syntax

```
y = tdelay(x,delaytime);
```

### Description

Returns the (continuous) signal *x* delayed for an absolute time (given by *delaytime*). The initial value of *y* for *time* = 0 to *delaytime* is equal to zero. This block is intended to model a continuous delay in a continuous simulation. Use the Unit Delay block to model a digital delay.

### Examples

```
x = 10*sin(time*10);
y = tdelay(x,2);
```

### Limitations

*x*, *y* and *delaytime* must be scalars. *delaytime* must be a **positive** constant value.

### Syntax

```
Y = trunc(X);
```

### Description

Rounds X or the elements of X towards zero (i.e. the function *trunc* removes the fraction).

### Examples

X	trunc(X)
1	1
2.1	2
-2.6	-2
3.4	3
[1.1,-2.7;3.5,-4.1]	[1,-3;3,-5]

### Limitations

X and Y must have the same size.

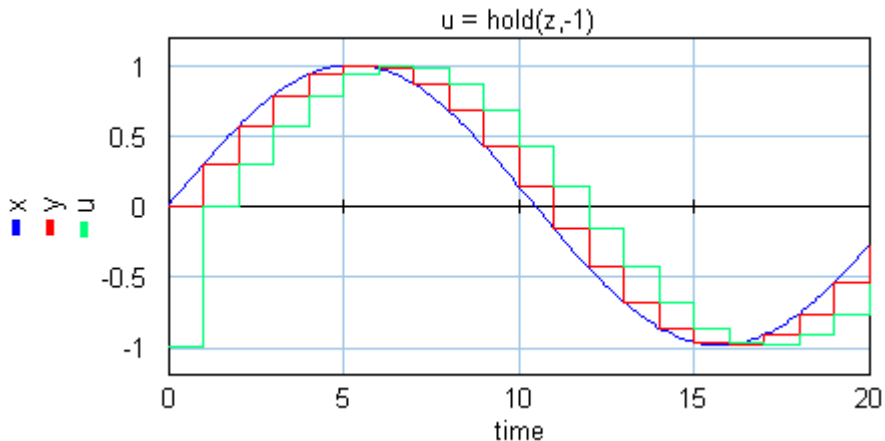
## Discrete

### Syntax

```
y = hold(x,init);
```

### Description

The hold function implements a zero order hold function operating at a specified sampling rate. It provides a mechanism for creating a continuous output signal y out of a discrete input signal x. The initial value of y is equal to the value of init.



### Examples

```
x = sin(time*0.3);
y = sample(x);
z = previous(y);
u = hold(z,-1);
```

### Limitations

x and y must be scalars. x be a discrete signal. y is a continuous signal. 20-sim will automatically detect the existence of discrete signals. Each chain of discrete signals will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose *Properties*, *Simulation* and *Discrete System*).

### Syntax

```
y = next(x,init);
```

### Description

The next function allows you to make constructs like:

$$x(k+1) = x(k) - 0.1 + u(k)$$

where k is the k<sup>th</sup> sample. Using the *next* function, this can be entered in 20-sim as:

```
next(x,0) = x - 0.1 + u;
```

### Limitations

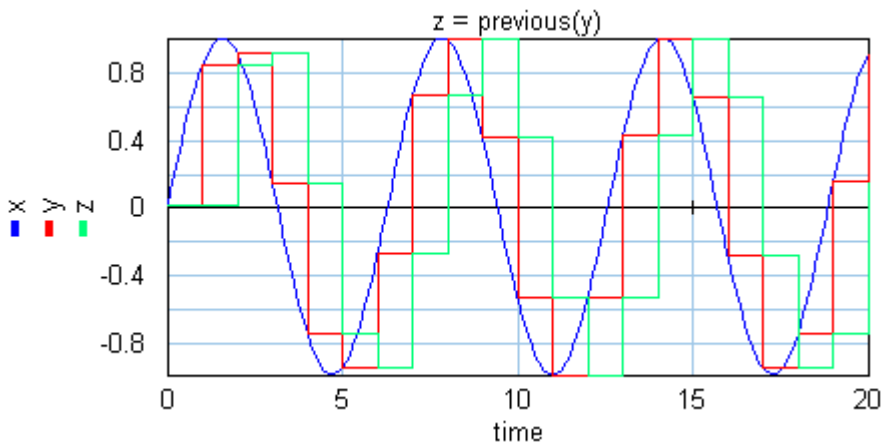
x and y will become discrete signals. 20-sim will automatically detect the existence of discrete signals. Each chain of discrete signals will be assigned a specific sample time. You can set this sample time to any desired value in the Simulator (choose *Properties*, *Simulation* and *Discrete System*).

### Syntax

```
y = previous(x,init);
```

### Description

The previous function delays the input signal x and holds it for one sample interval. It is equivalent to the z-1 discrete time operator.



### Examples

```
x = sin(time*0.3);
y = sample(x);
z = previous(y);
u = hold(z);
```

### Limitations

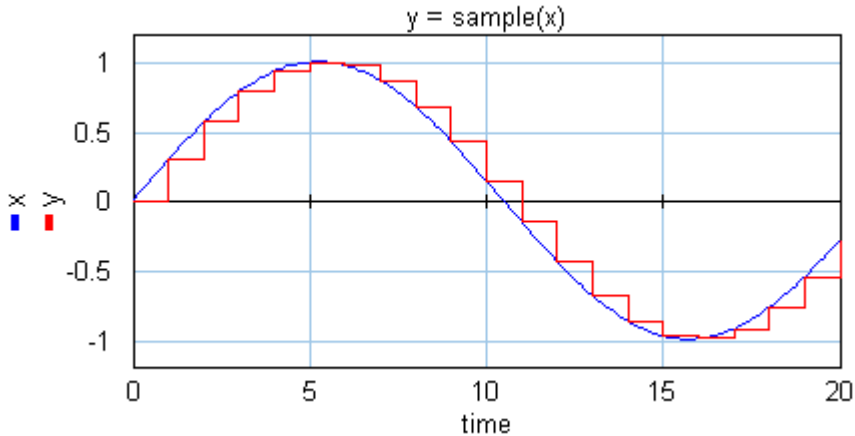
x and y will become discrete signals. 20-sim will automatically detect the existence of discrete signals. Each chain of discrete signals will be assigned a specific sample time. You can set this sample time to any desired value in the Simulator (choose *Properties*, *Simulation* and *Discrete System*).

### Syntax

```
y = sample(x,init);
```

### Description

The sample function implements a sample and hold function operating at a specified sampling rate. It provides a mechanism for discretizing a continuous input signal. The initial value of  $y$  is equal to the value of  $\text{init}$ . This initial value is optional. If no value is entered, a default initial value of 0 is used.



### Examples

```
x = sin(time*0.3);
y = sample(x);
z = previous(y);
u = hold(z);
```

### Limitations

- $x$  and  $y$  must be scalars.  $x$  represents a continuous signal and  $y$  represents a discrete signal.
- $y$  will become a discrete signals. 20-sim will automatically detect the existence of discrete signals. Each chain of discrete signals will be assigned a specific sample time. You can set this sample time to any desired value in the Simulator (choose *Properties*, *Simulation* and *Discrete System*).

### Event

### Syntax

```
y = event(x);
```

### Description

$y$  becomes true when  $x$  is zero. This function forces the integration algorithm to find the exact point where the input crosses zero. This is called a state event.

### Examples

```
x = sin(time*omega + phi);
y = event(x);
```

### Limitations

$y$  must be a boolean,  $x$  must be an expression yielding a scalar.

**Syntax**

```
y = eventdown(x);
```

**Description**

*y* becomes true when *x* is zero. This function forces the integration algorithm to find the exact point where the input crosses zero from a positive to a negative value. This is called a state event.

**Examples**

```
x = sin(time*omega + phi);
y = eventdown(x);
```

**Limitations**

*y* must be a boolean, *x* must be an expression yielding a scalar.

**Syntax**

```
y = event(x);
```

**Description**

*y* becomes true when *x* is zero. This function forces the integration algorithm to find the exact point where the input crosses zero from a negative to a positive value. This is called a state event.

**Examples**

```
x = sin(time*omega + phi);
y = eventup(x);
```

**Limitations**

*y* must be a boolean, *x* must be an expression yielding a scalar.

**Syntax**

```
y = frequencyevent(p,o);
```

**Description**

*y* becomes true every time when *p* [s] have passed. The function starts after an offset of *o* [s]. The offset parameter is optional. This function is a time event function.

**Examples**

```
parameters
    real period = 0.1 {s};
    real offset = 0.005 {s};
variables
    boolean y,z;
equations
    y = frequencyevent(1);           // y = true every second
    z = frequencyevent(period,offset); // z = true at 0.005 s, 0.105 s, 0.205 s
etc.
```

**Limitations**

$y$  must be a boolean,  $p$  and  $o$  must be a parameter or a constant.

**Syntax**

```
 $y = \text{timeevent}(x);$ 
```

**Description**

$y$  becomes true when time is equal to  $x$ . This functions forces the integration algorithm to do a calculation when time  $y$  becomes true. This is a time event function.

**Examples**

The example code below forces the integration algorithm, to do a calculation at the start of the step:

```
 $x = \text{step}(\text{start\_time});$   
 $y = \text{timeevent}(\text{start\_time});$ 
```

**Limitations**

$y$  must be a boolean,  $x$  must be an expression yielding a scalar.

**Expansion****Syntax**

```
 $\text{equal}([x1, x2, \dots, xn]);$ 
```

**Description**

This function is used to make all elements of a matrix equal. It returns the equations  $x2 = x1$ ,  $x3 = x1$ , .. ,  $xn = x1$ . During processing the equations will be automatically reshaped into a proper causal form. This function is created for use in library models that use a matrix with unknown size which results from the collect function.

**Examples**

Suppose we have  $m$  bonds connected to a submodel, collected in a port  $p$ . We could then use the function:

```
 $\text{collect}(p.e);$ 
```

During processing this equation will be expanded as:

```
 $[p.e1; p.e2; \dots; p.n];$ 
```

If we use the equal function:

```
 $\text{equal}(\text{collect}(p.e));$ 
```

this results in:



```
equal([p.e1;p.e2;...;p.n]);
```

which will be expanded in:

```
p.e2 = p.e1;
p.e3 = p.e1;
..
p.en = p.e1
```

### Limitations

This function is designed for a special class of models and should be used by experienced users only!

### Syntax

```
y = mul([x1,x2, ...,xn]);
```

### Description

This function is used for multiplication of variables of which one may be unknown. It returns the equation  $y = x1 * x2 * .. * xn$ . During processing this equation will be automatically reshaped into a causal form.

This function is created for use in library models that have unknown inputs such as *MultiplyDivide* model. Try to avoid the use of this function!

### Examples

#### equations

```
x1 = 1;
x2 = 2;
1 = mul([x1,x2,x3]);
```

```
y = sin(time);
x2 = 2;
y = mul([x1,x2]);
```

#### after reshaping (processing)

```
x1 = 1;
x2 = 2;
x3 = (1/x1)/x2;
```

```
y = sin(time);
x2 = 2;
x1 = y/x2;
```

### Limitations

This function is designed for a special class of models and should be used by experienced users only! y, x1, x2, ...,xn must be scalars. n may be 1 or higher!

### Syntax

```
y = sum([x1,x2, ...,xn]);
```

### Description

This function is used for summation of variables of which one may be unknown. It returns the equation  $y = x1 + x2 + .. xn$ . During processing this equation will be automatically reshaped into a causal form.

This function is created for use in library models that have unknown inputs such as *PlusMinus* model. Try to avoid the use of this function!

### Examples

#### equations

```
x1 = 1;
x2 = 2;
0 = sum(x1,x2,x3);
```

```
y = sin(time);
x2 = 2;
y = sum(x1,x2);
```

#### after reshaping (processing)

```
x1 = 1;
x2 = 2;
x3 = x1 + x2;
```

```
y = sin(time);
x2 = 2;
x1 = y - x2;
```

### Limitations

- This function is designed for a special class of models and should be used by experienced users only!  $y$ ,  $x_1$ ,  $x_2$ , ...,  $x_n$  must be scalars.  $n$  may be 1 or higher.
- Use the function `msum` if you want to use a standard summation of multiple variables.

### Extern

### Syntax

```
y = data(filename,column);
```

### Description

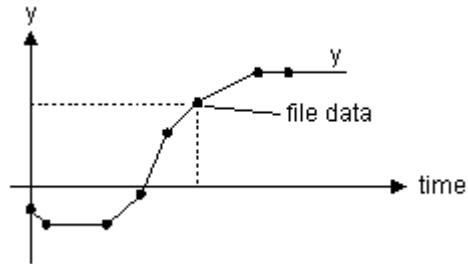
This function generates an output by linear interpolation of data read from file. The data on file is stored in columns. The first column contains the time values ( $t$ ) and the second column contains the corresponding output values ( $y$ ).

- The time data of the first column needs to be monotonically increasing.
- Discontinuities are allowed, by providing the same time point twice in the table.
- Values outside of the range, are computed by linear extrapolation of the last two points.

The first argument (*filename*) of this function must be a parameter of the type string and is used as a reference to a filename. This reference can be specified using the complete path or relative to the model directory. The second argument (*column*) of this function must be a parameter of the type integer denoting a whole number. It is used to denote the column number.

table (example):

0	-0.5
0.5	-1
2.5	-1
3.5	0
4.5	1
5.5	1.75
7	2.5
8	2.5



The input file must be an ASCII (text) file and should consist at least two columns of data. The first column (number 0) should always contain the time values. The other columns (number 1, 2, 3, etc.) should contain the corresponding data values. The parameter *column* is used to specify which column is used for as output data.

The various values must be separated by a space or a tab. Each new set of time and data values must start on a new line. No comment or other text may be part of the file. The filename of the input file can be specified using the complete path (e.g. c:\data\data.tbl). When no path is given, the file is assumed to be in the same directory as your model.

### Examples

```
parameters
    string filename = 'data.txt';
    integer col = 1;
variables
    real y;
equations
    y = data(filename,col);
```

### Limitations

*y* must be a scalar. *from\_file* must be string parameter. *x* must be an integer parameter.

### Syntax

```
Y = dll(filename,functionname,X);
```

### Description

Given a function (*functionname*) of a dll (*filename*), the dll function returns the output values (*X*) for a given input (*Y*).

Users can write their own source code using a native compiler such as Visual C++ or Borland C++. With these compilers it is possible to create DLL's with user defined functions that have an input- output relation which can be embedded in simulation code.

### Examples

```

parameters
    string filename = 'example.dll';
    string function = 'myFunction';
variables
    real x[2],y[2];
equations
    x = [ramp(1);ramp(2)];
    y = dll(filename,function,x);

```

### Limitations

*filename* and *functionname* must be string parameters. Note that the size of Y and X (scalars or matrices) must correspond with the size that is expected for the given dll-function.

### Search Order

20-sim uses the following search order for the dll-file:

1. The bin directory of 20-sim (usually C:\Program Files\20-sim 4.3\bin).
2. The current directory.
3. The Windows system directory.
4. The Windows directory.
5. The directories that are listed in the PATH environment variable.

The simplest place to put the dll-file is the bin directory, but it is always possible to give a complete path for the dll filename.

### Syntax

```
Y = dlldynamic(filename,functionname,X);
```

### Description

Given a function (*functionname*) of a dll (*filename*), the dll function returns the output values (X) for a given input (Y).

Users can write their own source code using a native compiler such as Visual C++ or Borland C++. With these compilers it is possible to create DLL's with user defined functions that have an input- output relation which can be embedded in simulation code.

### Examples

```

parameters
    string dllName = 'demoDynamicDll.dll';
    string functionName = 'SFunctionCalculate';
variables
    real x[2],y[2];
equations
    x = [ramp(1);ramp(2)];
    y = dlldynamic(dllName,functionName,x);

```

### Limitations

The *filename* and *functionname* must be string parameters. Note that the size of Y and X (scalars or matrices) must correspond with the size that is expected for the given dll-function.

## Search Order

20-sim uses the following search order for the dll-file:

1. The bin directory of 20-sim (usually C:\Program Files\20-sim 4.3\bin).
2. The current directory.
3. The Windows system directory.
4. The Windows directory.
5. The directories that are listed in the PATH environment variable.

The simplest place to put the dlldynamic-file is the bin directory, but it is always possible to give a complete path for the dll filename.

Almost every compiler that can build Windows applications, can also build dll-files containing dll-functions. For two compilers an example will be given how to build the **static dll's** (i.e. dll functions that do not contain internal model states) in combination with 20-sim. The two compilers are: Visual C++ and Borland C++ .

When the simulator has to call the user defined dll for the first time the dll is linked and the appropriate function is called. At the end of the simulation run the dll will be disconnected from the simulator. In general the dll-function called by the simulator has the following syntax in 20-sim:

*Y = dll(filename,functionname,X);*

For example (equation model):

```
parameters
    string filename = 'example.dll';
    string function = 'myFunction';
variables
    real x[2],y[2];
equations
    x = [ramp(1);ramp(2)];
    y = dll(filename,function,x);
```

The name of the function is the actual name which was given to the corresponding string parameter. The return value of the function determines whether the function was successful or not. A return value of 0 means success, every other value error. When a nonzero value is returned the simulation stops after finishing its current simulation step. The parameters given to the function correspond directly to the 20-sim parameters: double pointers for the inputs and outputs point to an array of doubles.

## Function arguments

The user-function in the dll must have certain arguments. The function prototype is like this:

*int myFunction(double \*inarr, int inputs, double \*outarr, int outputs, int major)*

where

- *inarr*: pointer to an input array of doubles. The size of this array is given by the second argument.

- *inputs*: size of the input array of doubles.
- *outarr*: pointer to an output array of doubles. The size of this array is given by the fourth argument.
- *outputs*: size of the output array of doubles.
- *major*: boolean which is 1 if the integration method is performing a major integration step, and 0 in the other cases. For example Runge-Kutta 4 method only has one in four model evaluations a major step.

### Initializing the DLL-file

When the dll is linked to the simulator it is often useful to perform some initializations. There are several ways to perform these initializations.

#### Method 1

When the simulator has attached the dll-file it automatically searches for a function with the name 'int Initialize()'. If this function is found it is called. The return value is checked for success, 1 means success, 0 means error. At the end of the simulation run just before the dll-file is detached the simulator searches for a function called 'int Terminate()'. In this function the necessary termination action can be performed like cleaning up allocated memory.

At the start of every run the simulator also searches a function with the name 'int InitializeRun()'. If it is found it is called the same way the Initialize function was called. At the end the same happens with the function 'int TerminateRun()'. This is very useful in multiple run simulations, in this case the dll-file is linked only once with the simulator, and only once the Initialize and Terminate functions are called. But for every subsequent run the InitializeRun and TerminateRun functions are called so every run can be initialized and terminated gracefully. In this case in the Terminate function collection of multiple run data could be collected and saved for example.

So suppose you have a multiple run with 2 runs, the following functions (if they exist) will be called in the dll-file in this order:

```
Initialize()
InitializeRun()
TerminateRun()
InitializeRun()
TerminateRun()
Terminate()
```

#### Method 2

Using the DLLEntryPoint function. This function is automatically called when the library is linked or detached. Both in Visual C++ and in Borland C++ this function has the same syntax. However when using visual C++ as the compiler, our simulator which is build with Visual C++ does not seem to be able to call this function. So the framework as given below only works with a Borland C++ dll.

```
// Every dll has an entry point LibMain || DllEntryPoint
// and an exit point WEP (windows exit point).
BOOL WINAPI DllEntryPoint( HINSTANCE hinstDll,DWORD fdwReason,LPCVOID
plvReserved)
{
```

```

    if( fdwReason == DLL_PROCESS_ATTACH )
    {
        return 1; // Indicate that the dll was linked successfully.
    }
    if( fdwReason == DLL_PROCESS_DETACH )
    {
        return 1; // Indicate that the dll was detached successfully.
    }
    return 0;
}

```

### Method 3

When using an object oriented language it is possible to have a global variable which is an instance of a class. When linking the dll-file to the simulator the constructor function of this global variable will be called automatically. In this constructor the initialization can be performed. When the dll-file is detached the destructor of the global variable is called. Some care should be taken with this method of terminating. E.g. if the user is asked for a filename using a FileDialog this sometimes causes the complete application to crash. The reason for this is that some of the dll-files contents was already destructed and that some functionality may not work anymore resulting in an application error. The solution for this problem is to use method 1 of initialization and destruction.

### Frame work for a Visual C++ dll-file implementation.

```

#include <windows.h>
#define DllExport __declspec( dllexport )
extern "C"
{
    DllExport int myFunction(double *inarr, int inputs, double *outarr, int outputs, int major)
    {
        ... // function body
        return 0; // return succesfull
    }
    DllExport int Initialize()
    {
        ... // do some initializations here.
        return 0; // Indicate that the dll was initialized successfully.
    }
    DllExport int Terminate()
    {
        ... // do some cleaning here
        return 0; // Indicate that the dll was terminated successfully.
    }
}

```

### Frame work for a Borland C++ dll-file implementation.

```

#include <windows.h>

```

```

extern "C"
{
    int _export myFunction(double *inarr, int inputs, double *outarr, int outputs, int
    major)
    {
        ... // function body
        return 0; // return succesfull
    }
    int _export Initialize()
    {
        ... // do some initializations here.
        return 0; // Indicate that the dll was initialized successfully.
    }
    int _export Terminate()
    {
        ... // do some cleaning here
        return 0; // Indicate that the dll was terminated successfully.
    }
}

// Every dll has an entry point LibMain || DllEntryPoint
// and an exit point WEP.
BOOL WINAPI DllEntryPoint( HINSTANCE hinstDll,DWORD fdwRreason,LPVOID
plvReserved)
{
    if( fdwRreason == DLL_PROCESS_ATTACH )
    {
        ... // do some initializations here.
        return 1; // Indicate that the dll was initialized successfully.
    }
    if( fdwRreason == DLL_PROCESS_DETACH )
    {
        ... // do some cleaning here
        return 1; // Indicate that the dll was initialized successfully.
    }
    return 0;
}

```

**Note**



Make sure that Borland C++ does not generate underscores in front of the exported function names! This can probably be found in the compiler settings.

### Working example

Here is a complete working example of how to use a dll-function from within the simulator. This code will compile with Visual C++. See the Borland C++ framework how to write this code in Borland C++.

```
#include <windows.h>
#include <math.h>
#include <fstream.h>
#define DllExport __declspec( dllexport )

ofstream outputStream;

extern "C"
{
    DllExport int myFunction(double *inarr, int inputs, double *outarr, int outputs, int
    major)
    {
        if( inputs != outputs )
            return 1;
        for( int i = 0; i < inputs; i++ )
        {
            outarr[i] = cos( inarr[i] );
            outputStream << inarr[i] << " " << outarr[i] << " ";
        }
        outputStream << endl;
        return 0;
    }

    DllExport int Initialize()
    {
        outputStream.open("c:\\data.log");
        return 0; // Indicate that the dll was initialized successfully.
    }

    DllExport int Terminate()
    {
        outputStream.close();
        return 0; // Indicate that the dll was terminated successfully.
    }
}
```

```
}
}
```

### Use within 20-sim

Suppose the dll has been created as "example.dll". With the following code this model can be tested:

```
parameters
    string dll_name = 'example.dll';
    string function_name = 'myFunction';
variables
    real in[2],out[2];
equations
    in = [ramp(1),ramp(2)];
    out = dll(dll_name, function_name,in);
```

Note that the general function "dll" is used. The arguments of this function, dll\_name and function\_name, are parameters which are used to denote the dll that should be used and the function of that dll that should be called. You can load this model from the Demonstration Models Library:

1. Open the *Editor*.
2. From the demo library open the model *DllFunction.emx* (choose *File* and *Open*)
3. Start the simulator (*Model* menu and *Start Simulator*).
4. Start a simulation run (select *Run* from the *Simulation* menu).

Almost every compiler that can build Windows applications, can also build dll-files containing dll-functions. For the Visual C++ compiler an example will be given how to build the dynamic dll's (i.e. dll functions that may contain internal model states) in combination with 20-sim.

The functions in the DLL are called in a specific sequence. For communication with the functions and the Simulator Kernel information is passed in a structure. This structure looks like this:

```

struct SimulatorSFunctionStruct
{
    double versionNumber;
    int nrInputs;
    int nrOutputs;
    int nrIndepStates;
    int nrDepStates;
    int nrAlgLoops;
    double simulationStartTime;
    double simulationFinishTime;
    double simulationCurrentTime;
    BOOL major;
    BOOL initialOutputCalculation;
};

```

### 1. Initialize

At the start of the simulation the function

*int Initialize()*

is called. When this function is not present it is not called. Any initializations of data structures can be performed here.

### 2. SFunctionInit

During initialization of the Simulator Kernel the function

*int SFunctionInit(SimulatorSFunctionStruct \*s)*

is called. Return value is 0 means error. every other value succes Argument is a pointer to the simstructure. On initialization the following fields should be filed in:

*nrIndepStates*

*nrDepStates*

*nrAlgLoop*

The following fields already have valid values:

<i>simulationStartTime</i>	giving the start time of the simulation
<i>simulationFinishTime</i>	giving the finish time of the simulation
<i>simulationCurrentTime</i>	giving the current time (actually the start time at the moment of initialization)

### 3. Initial values for the states:

```

int SFunctionGetInitialStates(double *initialIndepStates,
double *initialDepRates,
double *initialAlgloopIn,
SimulatorSFunctionStruct *simStruct);

```

Return value is 0 means error. every other value succes. The initial value for the independent states, dependent rates and algebraic loop variables can be specified by the DLL in this function. It is just called before the initial output calculation function in step 3. If all the initial values are zero, nothing has to be specified.

#### 4. Initial Output Calculation

It is possible that the DLL-function can give an initial output. A separate function is called so that the DLL can calculate it's initial output values. The boolean initialOutputCalculation in the simulatorSFunction structure is used. Just the sFunction is called. as in point 5.

#### 5. SFunction calling:

Here all the fields of the SimulatorSFunctionStruct are input for the function. The inputArray, stateArray, outputArray and rateArray are always given as arguments of the function. Dependent on the number of dependent states and algebraic loop variables more arguments can be given as shown in the functions below (sFunctionName is the name defined by the parameter name specified by the user):

Return value is 0 means error. every other value succes

*case: no dependent states, no algebraic loop variables*

```

int sFunctionName(double *inputArray,
double *stateArray,
double *outputArray,
double *rateArray,
SimulatorSFunctionStruct *simStruct);

```

*case: dependent states, no algebraic loop variables*

```

int sFunctionName(double *inputArray,
double *stateArray,
double *dependentRateArray,
double *outputArray,
double *rateArray,
double *dependentStateArray,
SimulatorSFunctionStruct *simStruct);

```

*case: no dependent states, algebraic loop variables*

```

int sFunctionName(double *inputArray,
double *stateArray,
double *algLoopInArray,
double *outputArray,
double *rateArray,
double *algLoopOutrray,

```

```
SimulatorSFunctionStruct *simStruct);
```

*case: dependent states, algebraic loop variables*

```
int sFunctionName(double *inputArray,  
double *stateArray,  
double *dependentRateArray,  
double *algLoopInArray,  
double *outputArray,  
double *rateArray,  
double *dependentStateArray,  
double *algLoopOutarray,  
SimulatorSFunctionStruct *simStruct);
```

the boolean `major` in the `SimulatorSFunctionStruct` determines whether the evaluation of the model is done at the time output is generated (`major == TRUE`) or that the model is evaluated because of determining model characteristics. For example Runge-Kutta4 integration method uses three minor steps before taking a major step where output is generated. Higher order methods can have different number of minor steps before a major step is taken.

## 6. Termination

At the end of the simulation the function:

```
int Terminate()
```

is called. When this function is not present it is not called. Any terminations of data structures can be performed here.

Frame work for a Visual C++ dll-file implementation.

```
#include <windows.h>  
#define DllExport __declspec( dllexport )  
extern "C"  
{  
DllExport int dllfunction(double *inarr, int inputs, double *outarr, int outputs, int major)  
{  
... // function body  
return 0; // return succesfull  
}  
DllExport int Initialize()  
{  
... // do some initializations here.  
return 0; // Indicate that the dll was initialized successfully.  
}  
DllExport int Terminate()  
{
```

```

... // do some cleaning here
return 0; // Indicate that the dll was terminated successfully.
}
}

```

Frame work for a Borland C++ dll-file implementation.

```

#include <windows.h>
extern "C"
{
int _export dllfunction(double *inarr, int inputs, double *outarr, int outputs, int major)
{
... // function body
return 0; // return succesfull
}
int _export Initialize()
{
... // do some initializations here.
return 0; // Indicate that the dll was initialized successfully.
}
int _export Terminate()
{
... // do some cleaning here
return 0; // Indicate that the dll was terminated successfully.
}

}
// Every dll has an entry point LibMain || DllEntryPoint
// and an exit point WEP.
BOOL WINAPI DllEntryPoint( HINSTANCE hinstDll,DWORD fdwRreason,LPVOID plvReserved)
{
if( fdwRreason == DLL_PROCESS_ATTACH )
{
... // do some initializations here.
return 1; // Indicate that the dll was initialized successfully.
}
if( fdwRreason == DLL_PROCESS_DETACH )
{
... // do some cleaning here
return 1; // Indicate that the dll was initialized successfully.
}
return 0;
}
}

```

## Working example

Here is a complete working example of how to use a dll-function from within the simulator. This code will compile with Visual C++. See the Borland C++ framework how to write this code in Borland C++.

```
#include <windows.h>
#include "SimulatorSFunctionStruct.h"

/
*****
*****
* in this source file we are gonna describe a linear system which is defined by
* the following transfer function description:

34
Y = ----- * U
s^2 + 6s + 34

or A, B, C, D system:

A = [ 0, -3.4;
      10, -6];
B = [ -3.4;
      0];
C = [0, -1];
D = 0
which has two poles on (-3 + 5i) and (-3 -5i)

steady state = 1

*****
*****/

#define DllExport __declspec( dllexport )

extern "C"
{

// called at begin of the simulation run
DllExport int Initialize()
{
// you can perform your own initialization here.

// success
return 0;
}
```

```

}

// called at end of the simulation run
DllExport int Terminate()
{
// do some cleaning here

// success
return 0;
}

DllExport int SFunctionInit (SimulatorSFunctionStruct *s)
{
// tell our caller what kind of dll we are
s->nrIndepStates = 2;
s->nrDepStates = 0;
s->nrAlgLoops = 0;

// dubious information, since 20-sim itself does not check and need this info
s->nrInputs = 1;
s->nrOutputs = 1;

// return 1, which means TRUE
return 1;
}

DllExport int SFunctionGetInitialStates (double *x0, double *xd0, double *xa0,
SimulatorSFunctionStruct *s)
{
// fill in the x0 array here. Since we specified no Dependent states, and No algebraic loop
variables
// the xd0 and xa0 may not be used.

// initial value is zero.
x0[0] = 0;
x0[1] = 0;

// return 1, which means TRUE
return 1;
}

DllExport int SFunctionCalculate(double *u, double *x, double *y, double *dx,
SimulatorSFunctionStruct *s)
{

```



```

// we could check the SimulatorSFunctionStruct here if we are in an initialization state and/or
// we are
// in a major integration step.
#if 0
if( s->initialialOutputCalculation )
; // do something

// possibly do some explicit action when we are in a major step.
if( s->major == TRUE )
; // do something
#endif
dx[0] = -3.4 * x[1] -3.4 * u[0];
dx[1] = 10 * x[0] -6 * x[1];

y[0] = -x[1];

// return 1, which means TRUE
return 1;
}

} // extern "C"
BOOL APIENTRY DllMain( HANDLE hModule,
    DWORD ul_reason_for_call,
    LPVOID lpReserved
)
{
    return TRUE;
}

```

### Use within 20-sim

Suppose the dll has been created as "demoDynamicDll.dll". With the following code this model can be tested:

```

parameters
    string dllName = 'demoDynamicDll.dll';
    string functionName = 'SFunctionCalculate';
equations
    output = dlldynamic (dllName, functionName, input);

```

Note that the general function "dlldynamic" is used. The arguments of this function, dllName and functionName, are parameters which are used to denote the dll that should be used and the function of that dll that should be called. You can load this model from the Demonstration Models Library:

1. Open the Editor.
2. From the demo library open the model *DllFunction.emx* (choose *File* and *Open*)
3. Start the simulator (*Model* menu and *Start Simulator*).
4. Start a simulation run (select *Run* from the *Simulation* menu).

## Syntax

$y = \text{table}(\text{file\_name}, x);$

## Description

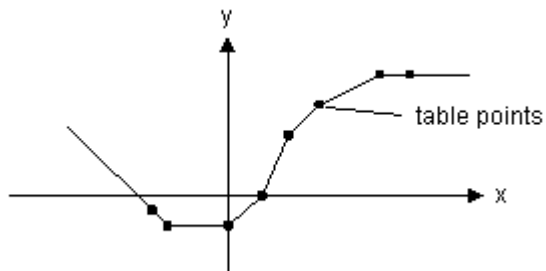
This model uses a one-dimensional table with data points to calculate the output  $y = f(x)$  as a function of the input  $x$ . The output  $y$  is calculated using linear interpolation between the table data points.

- The input data  $x$  of the first column needs to be monotonically increasing.
- Discontinuities are allowed, by providing the same input point twice in the table.
- Values outside of the table range, are computed by linear extrapolation of the last two points.

The first argument (*file\_name*) of this function must be a parameter of the type string and is used as a reference to a filename. This reference can be specified using the complete path or relative to the model directory. The second argument ( $x$ ) should be a real variable.

table (example):

-2.5	-0.5
-2	-1
0	-1
1	0
2	2
3	3.0
5	4
6	4.0



A table must be stored as an ASCII (text) file and should consist two columns of data. The first column consists of the  $x$ -values and the second column of the corresponding  $y$ -values. Each line of the file may only contain one  $x$ - and one corresponding  $y$ -value. The two values must be separated by a space or a tab. Each new set of  $x$ - and  $y$ -values must start on a new line. No comment or other text may be part of the table-file.

## Examples

```

parameters
    string filename = 'data.txt';
variables
    real y;
    real x;
equations
    x = ramp(1);
    y = table(filename,x);

```

## Limitations

x and y must be scalars. from\_file must be string parameter.

## Matrix

## Syntax

```

A = Adjoint(H);
A = Adjoint(R,P);

```

## Description

Returns the adjoint matrix [6,6] of a homogeneous matrix [4,4]:

$$H = \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_1 \\ r_{21} & r_{22} & r_{23} & p_2 \\ r_{31} & r_{32} & r_{33} & p_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} R & P \\ 0 & 1 \end{bmatrix} \rightarrow$$

$$\text{Adjoint}(H) = \begin{bmatrix} R & 0 \\ \text{skew}(P)*R & R \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & r_{13} & 0 & 0 & 0 \\ r_{21} & r_{22} & r_{23} & 0 & 0 & 0 \\ r_{31} & r_{32} & r_{33} & 0 & 0 & 0 \\ -p_3 \cdot r_{21} + p_2 \cdot r_{31} & -p_3 \cdot r_{22} + p_2 \cdot r_{32} & -p_3 \cdot r_{23} + p_2 \cdot r_{33} & r_{11} & r_{12} & r_{13} \\ p_3 \cdot r_{11} - p_1 \cdot r_{31} & p_3 \cdot r_{12} - p_1 \cdot r_{32} & p_3 \cdot r_{13} - p_1 \cdot r_{33} & r_{21} & r_{22} & r_{23} \\ -p_2 \cdot r_{11} + p_1 \cdot r_{31} & -p_2 \cdot r_{12} + p_1 \cdot r_{32} & -p_2 \cdot r_{13} + p_1 \cdot r_{33} & r_{31} & r_{32} & r_{33} \end{bmatrix}$$

or returns the adjoint matrix [6,6] of a rotation matrix R [3,3] and position vector P [3]:

$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}, \quad P = \begin{bmatrix} p_1 \\ p_2 \\ p_3 \end{bmatrix} \rightarrow$$

$$\text{Adjoint}(R, P) = \begin{bmatrix} R & 0 \\ \text{skew}(P)*R & R \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & r_{13} & 0 & 0 & 0 \\ r_{21} & r_{22} & r_{23} & 0 & 0 & 0 \\ r_{31} & r_{32} & r_{33} & 0 & 0 & 0 \\ -p_3 \cdot r_{21} + p_2 \cdot r_{31} & -p_3 \cdot r_{22} + p_2 \cdot r_{32} & -p_3 \cdot r_{23} + p_2 \cdot r_{33} & r_{11} & r_{12} & r_{13} \\ p_3 \cdot r_{11} - p_1 \cdot r_{31} & p_3 \cdot r_{12} - p_1 \cdot r_{32} & p_3 \cdot r_{13} - p_1 \cdot r_{33} & r_{21} & r_{22} & r_{23} \\ -p_2 \cdot r_{11} + p_1 \cdot r_{31} & -p_2 \cdot r_{12} + p_1 \cdot r_{32} & -p_2 \cdot r_{13} + p_1 \cdot r_{33} & r_{31} & r_{32} & r_{33} \end{bmatrix}$$

The Adjoint function is useful for dynamics described by twists and wrenches.

**Examples**

```

R = [cos(alpha),-sin(alpha),0 ; sin(alpha),cos(alpha),0 ; 0,0,0];
P = [p1 ; p2 ; p3];
A = Adjoint(R,P);

```

**Limitations**

H must be of size [4,4], R must always be of size[3,3] , P must have the size [3,1] and A must have size [6,6].

**Syntax**

```

Y = adjoint(T);
Y = adjoint(W,V);

```

**Description**

Returns the adjoint matrix [6,6] of a twist or wrench vector  $T$  [6,1]:

$$T = \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \\ v_1 \\ v_2 \\ v_3 \end{bmatrix} = \begin{bmatrix} W \\ V \end{bmatrix} \rightarrow$$

$$\text{adjoint}(T) = \begin{bmatrix} \text{skew}(W) & 0 \\ \text{skew}(V) & \text{skew}(W) \end{bmatrix} = \begin{bmatrix} 0 & -\omega_3 & \omega_2 & 0 & 0 & 0 \\ \omega_3 & 0 & -\omega_1 & 0 & 0 & 0 \\ -\omega_2 & \omega_1 & 0 & 0 & 0 & 0 \\ 0 & -v_3 & v_2 & 0 & -\omega_3 & \omega_2 \\ v_3 & 0 & v_1 & \omega_3 & 0 & -\omega_1 \\ -v_2 & v_1 & 0 & -\omega_2 & \omega_1 & 0 \end{bmatrix}$$

or returns the adjoint matrix [6,6] of an angular velocity vector  $W$  [3,1] and a velocity vector  $V$  [3,1]:

$$W = \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}, \quad V = \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} \rightarrow$$

$$adjoint(W, V) = \begin{bmatrix} skew(W) & 0 \\ skew(V) & skew(W) \end{bmatrix} = \begin{bmatrix} 0 & -\omega_3 & \omega_2 & 0 & 0 & 0 \\ \omega_3 & 0 & -\omega_1 & 0 & 0 & 0 \\ -\omega_2 & \omega_1 & 0 & 0 & 0 & 0 \\ 0 & -v_3 & v_2 & 0 & -\omega_3 & \omega_2 \\ v_3 & 0 & v_1 & \omega_3 & 0 & -\omega_1 \\ -v_2 & v_1 & 0 & -\omega_2 & \omega_1 & 0 \end{bmatrix}$$

The adjoint function is useful for dynamics described by twists and wrenches.

### Examples

```
W = [w1 ; w2 ; w3];
V = [v1 ; v2 ; v3];
Y = adjoint(W,V);
```

### Limitations

Y must be of size [6,6], W must always be of size [3,1], V must have the size [3,1] and T must have size [6,1].

### Syntax

```
y = antisym(A);
```

### Description

Returns an anti-symmetric matrix. This function is equal to:

```
y = (A - transpose(A))/2;
```

### Examples

```
A = [1,2;3,4];
Y = antisym(A);
```

### Limitations

A must be a square matrix. Y and A must be of the same size.

**Syntax**

```
y = columns(A);
```

**Description**

Returns the number of columns of A.

**Examples**

```
A = [1,2;3,4;5,6];
y = columns(A);
```

**Limitations**

y must be a scalar.

**Syntax**

```
Y = cross(A,B);
```

**Description**

This functions returns the vector cross product of the vectors A and B. That is  $Y = A \times B$  or:

```
Y[1] = A[2]*B[3] - A[3]*B[2]
Y[2] = A[3]*B[1] - A[1]*B[3]
Y[3] = A[1]*B[2] - A[2]*B[1]
```

**Examples**

```
parameters
    real A[3] = [1;2;3];
    real B[3] = [4;5;6];
variables
    real Y[3];
equations
    Y = Cross(A,B); // Y = [-3;6;-3]
```

**Limitations**

Y, A and B must be column vectors of size 3.

**Syntax**

```
y = det(A);
or
Y = |A|;
```

**Description**

Returns the determinant of the square matrix A.

**Examples**

```
A = [1,2;3,ramp(1)];
y = det(A);
```

**Limitations**

A must be a square matrix, y must be a scalar.

**Syntax**

```
Y = diag(x);
```

**Description**

Fills the diagonal elements of the matrix Y with the elements of the columnvector x.

**Example**

```
variables
  real x[3];
  real Y[3,3];
equations
  x = [1;2;3];
  Y = diag(x);
```

**Limitations**

Y must be a matrix of size [n,n]. x must be a column vector of size n.

**Syntax**

```
Y = eye(n);
```

**Description**

Returns the n-by-n identity matrix.

**Example**

```
Y = eye(3);
```

**Limitations**

Y must be a matrix of size [n,n]. n must be an integer value.

**Syntax**

```
H = homogeneous(R,P);
```

**Description**

Returns the homogenous matrix [4,4] of a rotation matrix R[3,3] and position vector P[3]:

$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}, \quad P = \begin{bmatrix} p_1 \\ p_2 \\ p_3 \end{bmatrix} \rightarrow H = \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_1 \\ r_{21} & r_{22} & r_{23} & p_2 \\ r_{31} & r_{32} & r_{33} & p_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

The homogeneous matrix gives a full coordinate transformation from one reference frame to another. It can be used for 3D dynamics.

**Examples**

```

R = [cos(alpha),-sin(alpha),0 ; sin(alpha),cos(alpha),0 ; ; 0,0,0];
P = [p1 ; p2 ; p3];
H = homogeneous(R,P);

```

**Limitations**

R must always be of size[3,3] , P must have the size [3,1] and H must have size [4,4].

**Syntax**

```
y = inner(A,B);
```

**Description**

Returns the scalar product of the column vectors A and B. A and B must be vectors of the same length. Inner(A,B) is the same as transpose(A)\*B.

**Example**

```

A[3] = [1;2;3];
B[3,1] = [4;5;6];
y = inner(A,B);

```

**Limitations**

A and B must be vectors of the same size [n,1] or [n]. y must be a scalar.

**Syntax**

```
Y = inverse(A);
```

**Description**

Returns the inverse of square non-singular matrix A.

**Examples**

```

A = [1,0;0,1+ramp(1)];
Y = inverse(A);

```

**Limitations**

A must be a non-singular square matrix. Y must have the same size as A.

**Syntax**

```

Y = inverseH(H);
Y = inverseH(R,P);

```

**Description**

Returns the inverse of a homogeneous matrix H [4,4]. The homogeneous matrix can be entered directly or by a rotation matrix R[3,3] and position vector P [3,1].

This function uses the special nature of a homogeneous matrix. I.e the inverse can be computed directly instead of the numerical approach of the standard inverse function.



## Examples

```
H = [cos(alpha),-sin(alpha),0,p1 ; sin(alpha),cos(alpha),0,p2 ; 0,0,0,p3 ; 0,0,0,1];
Y = inverseH(H);
or
R = [cos(alpha),-sin(alpha),0 ; sin(alpha),cos(alpha),0 ; 0,0,0];
P = [p1 ; p2 ; p3];
Y = inverseH(R,P);
```

## Limitations

H must be a homogeneous matrix of size [4,4], R must always be of size[3,3] , P must have the size [3,1] and A must have size [6,6].

## Syntax

```
x = linsolve(A,b [,method]);
```

## Description

This function solves the equation

$$A*x = b;$$

Where A is a square matrix of arbitrary size n and x and b are vectors of size n.

Returns the inverse of square non-singular matrix A.

The last argument is a string that specifies the desired method to use.

method	description
lu	LU decomposition (default method)
qr	QR factorization
cholesky	Cholesky factorization
gmres	Generalized Minimum Residual

The gmres method allows further steering of the method by specifying method parameters:

method parameter	description
tol	Set the desired tolerance to use
maxiter	Set the maximum number of iterations to use
ortho	Set the method of Gramm-Schmidt orthogonalization: <ol style="list-style-type: none"> <li>1 modified Gramm-Schmidt</li> <li>2 iterative Gramm-Schmidt</li> <li>3 classical Gramm-Schmidt</li> <li>4 iterative classical Gramm-Schmidt</li> </ol>

## Examples

```
A = [1,2;0,1+ramp(1)];
b = [1;5];
x = linsolve(A,b);
x2 = linsolve (A, b, 'qr');
x3 = linsolve (A, b, 'gmres tol=1e-8 ortho=4');
```

## Limitations

A must be a non-singular square matrix.

**Note**

The following equations

$$A*x = b;$$

$$x = \text{inverse}(A)*b;$$

$$x = (A^{-1})*b;$$

all lead in the calculation of the inverse of A and will give the same result as

$$x = \text{linsolve}(A,b);$$

For the inverse calculation, Cramers rule is used. This is a method which is fast for small matrix sizes. The linsolve function with the gmres method is superior to Cramers rule for larger matrix sizes.

**Syntax**

$$y = \text{max}(A);$$

**Description**

Returns the value of the largest matrix element of A.

**Examples**

$$A = [1,2;3,\text{ramp}(1)];$$

$$y = \text{max}(A);$$

**Limitations**

y must be a scalar.

**Syntax**

$$y = \text{min}(A);$$

**Description**

Returns the value of the smallest matrix element of A.

**Examples**

$$A = [1,2;3,\text{ramp}(1)];$$

$$y = \text{min}(A);$$

**Limitations**

y must be a scalar.

**Syntax**

$$y = \text{msum}(A);$$

**Description**

Returns the sum of the matrix elements of A.

**Examples**

$$A = [1,2;3,4;5,6];$$

$$y = \text{msum}(A);$$

**Limitations**

y must be a scalar.

**Syntax**

```

y = norm(A);
or
Y = ||A||;

```

**Description**

Returns the square root of the sum of the squared matrix elements of A:

$$y = \sqrt{\sum_{i=1}^n \sum_{j=1}^m A[i,j]^2}$$

**Examples**

```

A = [1,2;3,ramp(1)];
y = norm(A);

```

**Limitations**

y must be a scalar.

**Syntax**

```

y = norminf(A);

```

**Description**

Returns the largest row sum of the absolute values of the matrix A:

$$\max \left\{ \sum_{j=1}^n |a_{ij}|, 1 \leq i \leq m \right\}$$

**Examples**

```

A = [1,2;3,ramp(1)];
y = norminf(A);

```

**Limitations**

y must be a scalar.

**Syntax**

```

y = rows(A);

```

**Description**

Returns the number of rows of A.

**Examples**

```

A = [1,2;3,4;5,6];
y = rows(A);

```

**Limitations**

y must be a scalar.

**Syntax**

$$Y = \text{skew}(X);$$
**Description**

Returns the vector product:

$$X = \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} \rightarrow Y = \begin{bmatrix} 0 & -x_3 & x_2 \\ x_3 & 0 & -x_1 \\ -x_2 & x_1 & 0 \end{bmatrix}$$

**Examples**

$$X = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} \rightarrow Y = \begin{bmatrix} 0 & -3 & 2 \\ 3 & 0 & -1 \\ -2 & 1 & 0 \end{bmatrix}$$

**Limitations**

X must be a vector of size n. Y must be a matrix of size [n,n].

**Syntax**

$$y = \text{sym}(A);$$
**Description**

Returns a symmetric matrix. This function is equal to:

$$y = (A + \text{transpose}(A))/2;$$
**Examples**

$$A = [1,2;3,4];$$

$$Y = \text{sym}(A);$$
**Limitations**

A must be a square matrix. Y and A must be of the same size.

**Syntax**

$$H = \text{tilde}(T);$$

$$H = \text{tilde}(W,V);$$
**Description**

Returns the twist matrix [4,4] of a twist or wrench vector T [6,1]:

$$T = \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \\ v_1 \\ v_2 \\ v_3 \end{bmatrix}, \rightarrow \tilde{t}(T) = \begin{bmatrix} 0 & -\omega_3 & \omega_2 & v_1 \\ \omega_3 & 0 & -\omega_1 & v_2 \\ -\omega_2 & \omega_1 & 0 & v_3 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Or returns the twist matrix [4,4] of an angular velocity vector W [3,1] and a velocity vector V [3,1]:

$$W = \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}, V = \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix}, \rightarrow \tilde{t}(W,V) = \begin{bmatrix} 0 & -\omega_3 & \omega_2 & v_1 \\ \omega_3 & 0 & -\omega_1 & v_2 \\ -\omega_2 & \omega_1 & 0 & v_3 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

The tilde function is useful for dynamics described by twists and wrenches.

### Examples

```
W = [w1 ; w2 ; w3];
V = [v1 ; v2 ; v3];
H = tilde(W,V);
```

### Limitations

H must be of size [4,4], W must always be of size[3,1] , V must have the size [3,1] and T must have size [6,1].

### Syntax

```
y = trace(A);
```

### Description

Returns the sum of the diagonal elements of the matrix A.

### Examples

```
A = [1,2,3;4,ramp(1),6];
y = trace(A);
```

### Limitations

y must be a scalar.

### Syntax

```
Y = transpose(A);
```

### Description

Returns the transpose of the matrix A.

**Examples**

```
A = [1,2;3,ramp(1)];
Y = transpose(A);
```

**Limitations**

With the A matrix of size[n,m] , Y must have the size [m,n].

**Port****Syntax**

```
y = collect(p.e);
y = collect(p.f);
y = collect(m);
```

(with p.e and p.f powerportvariables and m a signal)

**Description**

Some models in 20-sim can have an unknown amount of signals or bonds connected. They are treated as an array with unknown length.

For example the PlusMinus model can have n signals that must be added and m signals that must be subtracted. 20-sim treats them as an array plus and an array minus with:

*plus = [plus1;plus2;...;plusn] and minus = [minus1;minus2;...;minusm]*

To assign an array of unknown length, the *collect* function is used. It creates an array with port variables or signals. This function is created for use in library models that have an unknown amount of bonds or signals connected. **Try to avoid the use of this function!**

**Examples**

Suppose we have m bonds connected to a submodel, collected in a port p. We could then use the equation:

```
Y = collect(p.e);
```

During processing, this equation will be rewritten as:

```
Y = [p.e1;p.e2;...;p.n];
```

Suppose we have a submodel with n input signals connected. We could then write the equation:

```
y = sum(collect(input));
```

During processing, this equation will be rewritten as:

```
y = sum([output1;output2;...;outputn]);
```

which is of course equal to:

$$y = output1 + output2 + .. + outputn;$$

### Limitations

This function is designed for a special class of models and should be used by experienced users only! The function is only valid when used in a submodel.

### Syntax

$$y = direct(p.e);$$

$$y = direct(p.f);$$

(with p.e and p.f powerportvariables)

### Description

This function is equal to the collect function, but utilizes the direction of the bonds connected to the submodel to sign the powerportvariables. This function is created specially for the bond graph submodels *OneJunction.emx* and *ZeroJunction.emx*. Try to avoid the use of this function!

### Examples

Suppose we have 4 bonds connected to a 0-junction, collected in a port p. p1 and p4 are pointing towards the junction and p2 and p3 are pointing from the 0-junction. We could then use the equation:

$$Y = direct(p.f);$$

During processing, this equation will be rewritten as:

$$Y = [p.f1;-p.f2;-p.f3,p.f4];$$

Which can of course be used in combination with the sum function:

$$sum(Y) = 0;$$

To get the 0-junction equation:

$$p.f1 - p.f2 - p.f3 + p.f4 = 0;$$

### Limitations

This function is designed for a special class of models and should be used by experienced users only! The function is only valid when used in a submodel.

### Syntax

$$y = first(p.e);$$

$$y = first(p.f);$$

$$y = first(m);$$

(with p.e and p.f powerportvariables and m a signal)

### Description

Some models in 20-sim can have an unknown amount of signals or bonds connected. They are treated as an array with unknown length. For example the PlusMinus model can have n signals that must be added and m signals that must be subtracted. 20-sim treats them as an array *plus* and an array *minus* with:

*plus* = [*plus1;plus2;...;plusn*] and *minus* = [*minus1;minus2;...;minusm*]

The function *first* returns the value of the first element of an array of unknown length. This function is created for use in library models that have an unknown amount of bonds or signals connected. **Try to avoid the use of this function!**

### Examples

Suppose we have *m* bonds connected to a submodel, collected in a port *p*. We could then use the equation:

$$y = \text{first}(p.e);$$

During processing, this equation will be rewritten as:

$$y = p.e1;$$

### Limitations

This function is designed for a special class of models and should be used by experienced users only! The function is only valid when used in a submodel.

### Source

### Syntax

$$y = \text{gauss}(x,s);$$

### Description

Returns gaussian noise with a variance *x* and seed *s*. The seed parameter is optional. When omitted, the default value (0) is used.

### Examples

```
x = 20;
y = gauss(x);
z = gauss(x,450);
```

### Limitations

*x* and *y* must be scalars. The seed *s* must be a number in the region <0,65535>.

### Syntax

$$y = \text{ramp}(x);$$

### Description

Returns a ramp signal with start time *x*:



```
time < x: y = 0
time >= x: y is time - x
```

### Examples

```
x = 20, amplitude = 10;
y = amplitude*ramp(x);
```

### Limitations

x and y must be scalars.

### Syntax

```
y = ran(x,s);
```

### Description

Returns uniformly distributed noise in the interval [-x,x] with seed s. The seed parameter is optional. When omitted, the default value (0) is used.

### Examples

```
x = 20;
y = ran(x);
z = ran(x,450);
```

### Limitations

x and y must be scalars. The seed s must be a number in the region <0,65000>.

20-sim generates a sequence of random numbers for each simulation differently depending upon the value of the seed parameter. The random noise function and gaussian noise function are affected by this. The default value of the seed is 0. The maximum value is 65535.

### default value (0)

When the seed value is 0 (default value), 20-sim generates a new sequence of random numbers for each simulation and for each new random function. E.g. when two random functions with default seed value (0) are used in one model, they will generate different sequences of random numbers during a simulation.

### other values (>0)

When the seed value is chosen larger than zero, 20-sim generates the same sequence of random numbers for each simulation. Moreover 20-sim will generate the same sequence of random numbers for each random function that uses the same seed parameter (>0). E.g. when two random functions with seed value 50, are used in one model, they will generate the same sequence of random numbers during a simulation.

### Syntax

```
y = step(x);
```

### Description

Returns a step signal with start time x:

```
time < x: y = 0
time >= x: y = 1
```

### Examples

```
x = 20, amplitude = 10;
y = amplitude*step(x);
```

### Limitations

x and y must be scalars.

## Trigonometric

### Syntax

```
Y = arcsin(X);
```

### Description

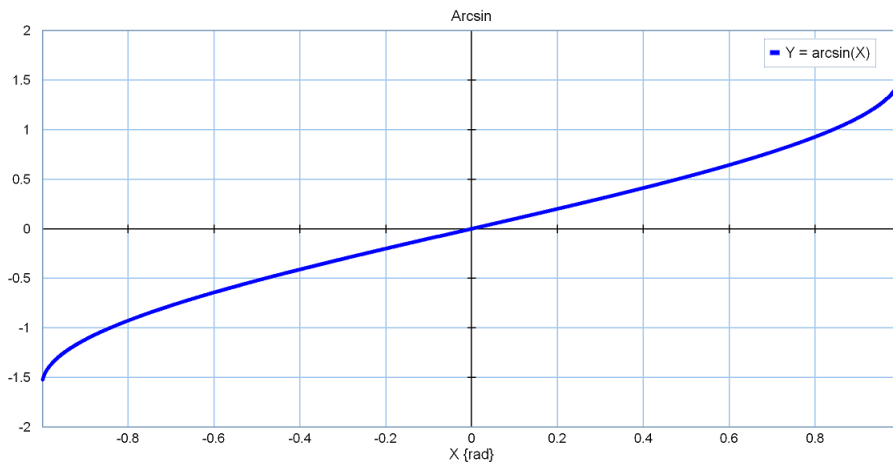
Returns the arcsine of the elements of X.

### Examples

```
b = cos(time);
a = arcsin(b);
X = [0.5*cos(time);0.75*cos(time)];
Y = arcsin(X);
```

### Limitations

Y and X must have the same size. The elements of X must be in the range [-1 ,1].



### Syntax

```
Y = arccos(X);
```

### Description

Returns the arccosine of the elements of X.

### Examples

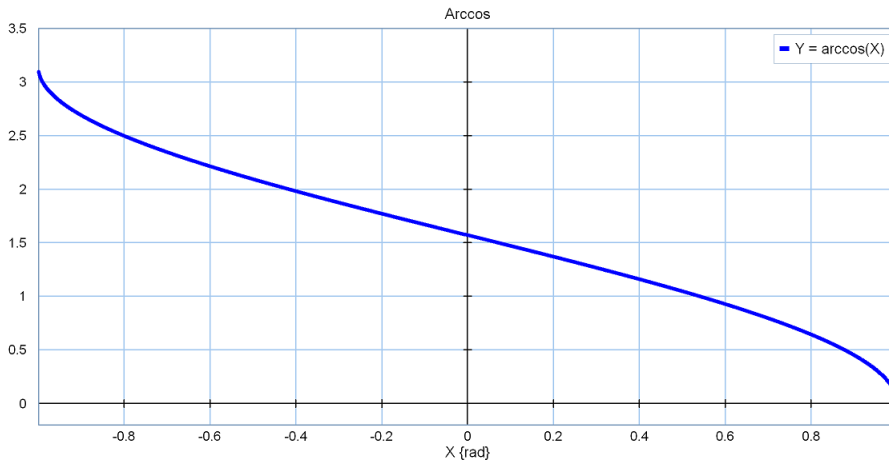
```

b = sin(time);
a = arccos(b);
X = [0.5*sin(time);0.75*sin(time)];
Y = arccos(X);

```

### Limitations

Y and X must have the same size. The elements of X must be in the range [-1 ,1].



### Syntax

```
Y = arccosh(X);
```

### Description

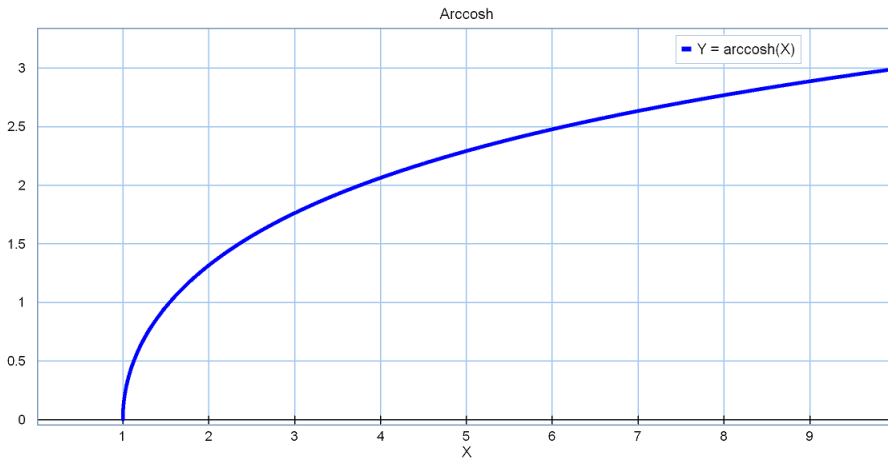
Returns the hyperbolic arccosine of the elements of X.

### Examples

```
y = arccosh(time + 1.0);
```

### Limitations

Y and X must have the same size. The elements of X must be 1 or bigger.



### Syntax

```
Y = arccsinh(X);
```

### Description

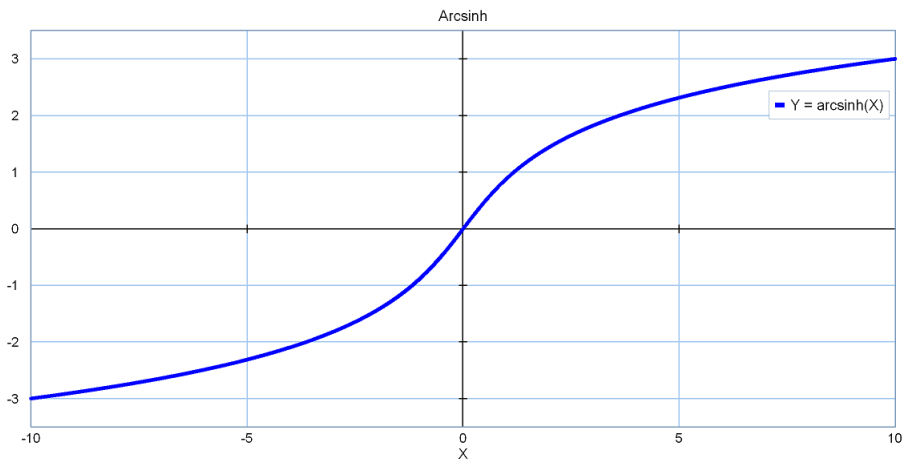
Returns the hyperbolic arcsine of the elements of X.

### Examples

```
a = arccsinh(time);
X = [0.5*cos(time);0.75*cos(time)];
Y = arccsinh(X);
```

### Limitations

Y and X must have the same size.



**Syntax**

```
Y = arctan(X);
```

**Description**

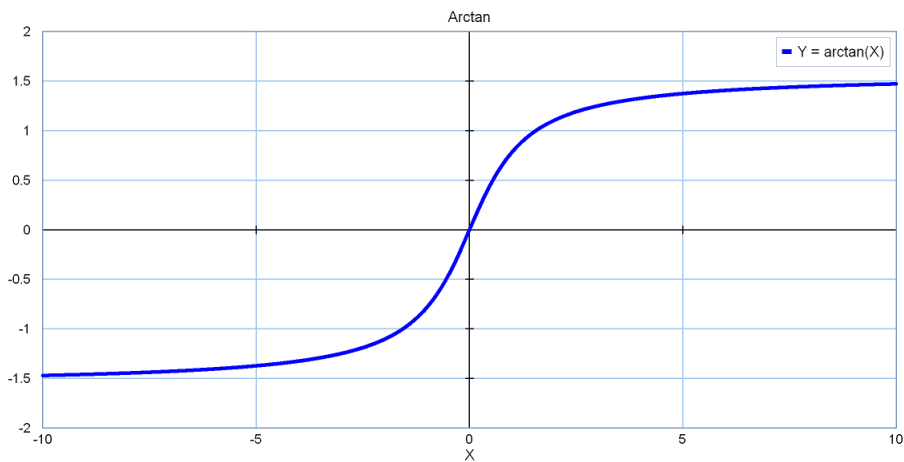
Returns the arctangent of the elements of X.

**Examples**

```
a = arctan(time);
X = [ramp(1);-0.5*ramp(9)];
Y = arctan(X);
```

**Limitations**

Y and X must have the same size.

**Syntax**

```
Y = arctanh(X);
```

**Description**

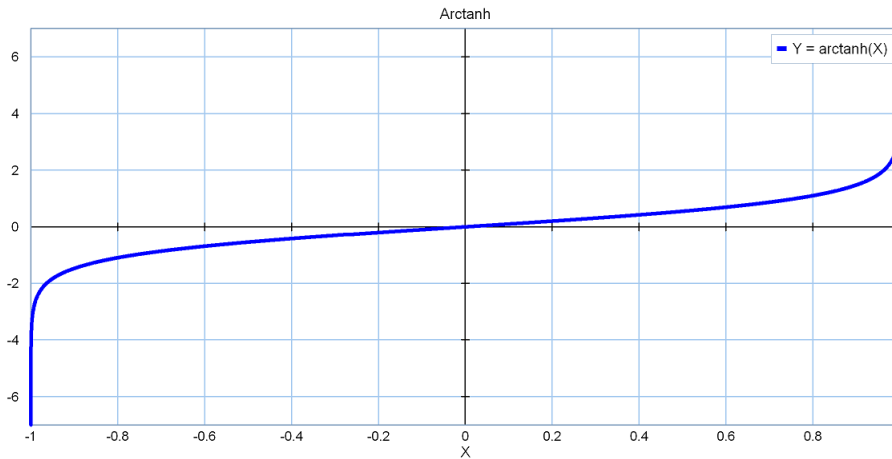
Returns the hyperbolic arctangent of the elements of X.

**Examples**

```
b = sin(time);
a = arctan(b);
X = [sin(time);-0.5*cos(time)];
Y = arctanh(X);
```

**Limitations**

Y and X must have the same size. The elements of X must be in the range  $[-1, 1]$ .



## Syntax

```
R = atan2(Y,X);
```

## Description

This is the four quadrant arctangent of the elements of Y and X. Unlike arctangent function, atan2 does distinguish between diametrically opposite directions.

## Examples

X, Y	<code>arctan(Y/X);</code>	<code>atan2(Y, X);</code>
1,1	<code>/4</code>	<code>/4</code>
-1,-1	<code>/4</code>	<code>-3 /4</code>
0,1	<code>-</code>	<code>/2</code>
0,0	<code>-</code>	set to 0 instead of undefined.

```
y = sin(time);
x = cos(time);
r = atan2(y,x);
```

```
X = [ramp(0);ramp(1)];
Y = [1;1];
R = atan2(Y,X);
```

## Limitations

r, x and y must have the same size. It produces results in the range  $(-\pi, \pi]$ . Atan2(0, 0) is defined as 0 instead of undefined.

**Syntax**

```
Y = cos(X);
```

**Description**

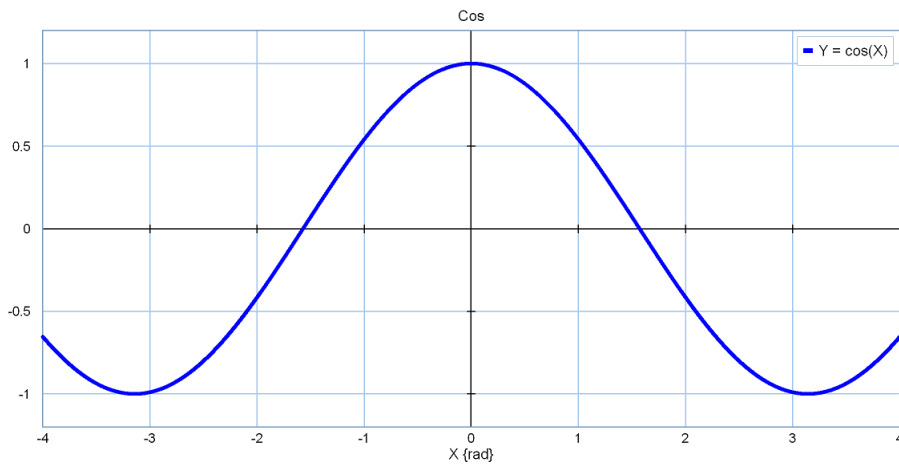
Returns the cosine of the elements of X.

**Examples**

```
b = ramp(2.5);
a = cos(b);
X = [ramp(0);ramp(1)];
Y = cos(X);
```

**Limitations**

Y and X must have the same size.

**Syntax**

```
Y = cosh(X);
```

**Description**

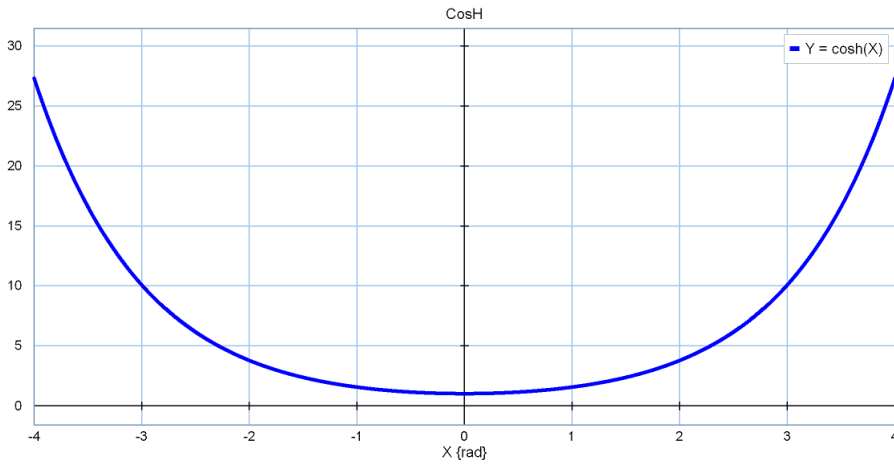
Returns the hyperbolic cosine of the elements of X.

**Examples**

```
b = ramp(2.5);
a = cosh(b);
X = [ramp(0);ramp(1)];
Y = cosh(X);
```

**Limitations**

Y and X must have the same size.



### Syntax

$Y = \sin(X);$

### Description

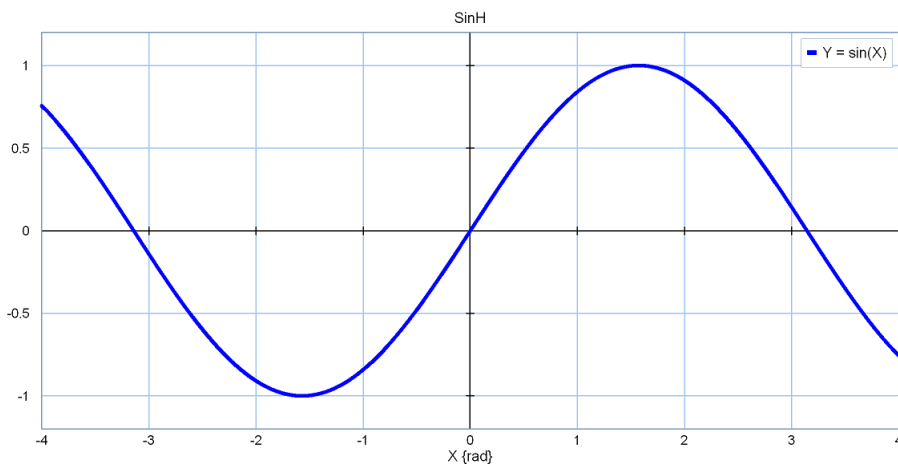
Returns the sine of the elements of  $X$ .

### Examples

```
b = ramp(2.5);
a = sin(b);
X = [ramp(0);ramp(1)];
Y = sin(X);
```

### Limitations

$Y$  and  $X$  must have the same size.





**Syntax**

$$Y = \sinh(X);$$
**Description**

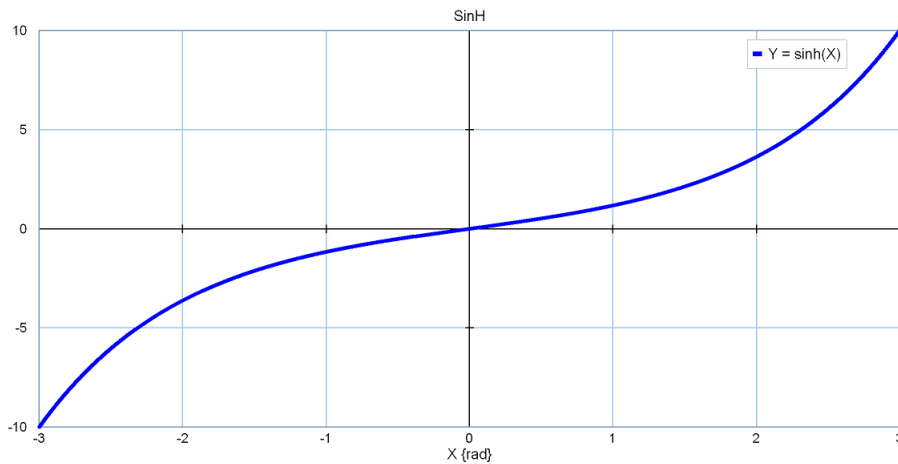
Returns the hyperbolic sine of the elements of X.

**Examples**

```
b = ramp(2.5);
a = sinh(b);
X = [ramp(0);ramp(1)];
Y = sinh(X);
```

**Limitations**

Y and X must have the same size.

**Syntax**

$$Y = \tanh(X);$$
**Description**

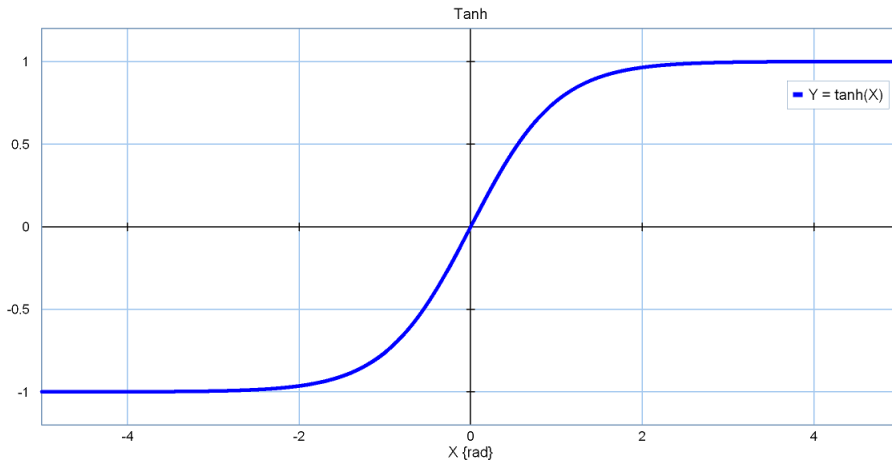
Returns the hyperbolic tangent of the elements of X.

**Examples**

```
b = ramp(2.5);
a = tanh(b);
X = [ramp(0);ramp(1)];
Y = tanh(X);
```

**Limitations**

Y and X must have the same size.



### Syntax

```
Y = tan(X);
```

### Description

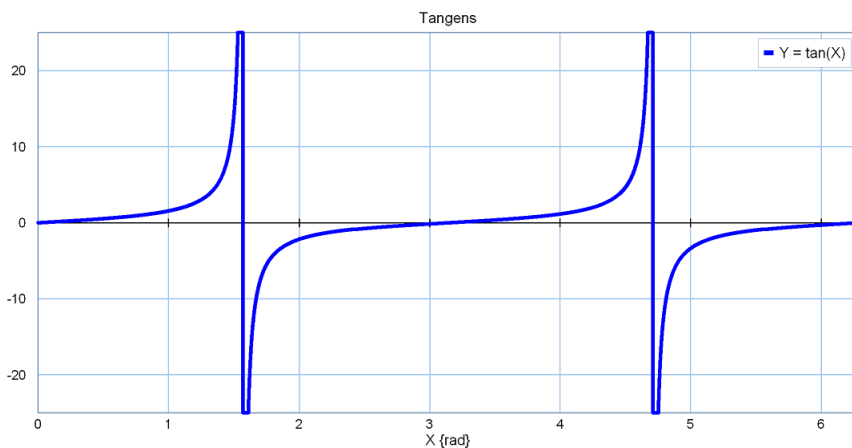
Returns the tangent of the elements of X.

### Examples

```
b = ramp(2.5);
a = tan(b);
X = [ramp(0);ramp(1)];
Y = tan(X);
```

### Limitations

Y and X must have the same size.



## 7.5 Operators

### Operators

In 20-sim you can use the following operators equations:

<b>Operator</b>	<b>Description</b>
*	Multiplication
+	Addition
-	Subtraction
.*	ArrayMultiplication
./	ArrayDivision
.^	ArrayPower
/	Division
div	Integer division
% or mod	Modulus operator
^	Power
and	Boolean and
or	Boolean or
xor	Boolean exclusive or
<	Less than
<=	Less than or equal
<>	Not equal
==	Equal
>=	Larger than or equal
>	Larger than
-	Prefix Minus Sign
+	Prefix Plus Sign
not	Prefix Boolean Not
..	Absolute / Determinant / Norm

### Arithmetic

Absolute / Determinant / Norm ( |..| )

### Syntax

|A| or ||A||

### Description

The upright stroke (|) is not a real operator. Depending on what's between the strokes, the following functions are applied:

```
| scalar | -> abs(scalar)
| matrix | -> det(matrix)
| vector | -> abs(vector)
|| matrix || -> norm(matrix)
```

## Syntax

$A * B$

## Description

$A * B$  multiplies A with B. For nonscalar A and B, the number of columns of A must equal the number of rows of B. If  $C = A*B$  then the elements of C can be calculated out of the matrix elements of A and B as:

$$C[i,j] = \sum_{k=1}^n A[i,k]B[k,j]$$

A scalar can be multiplied with a matrix of any size.

## Examples

<b>A</b>	<b>B</b>	<b>A * B</b>
5	3	15
-4.5	5.4	-24.3
2	[1,2;3,4]	[2,4;6,8]
[1,-2;-3,4]	4	[4,-8;-12,16]
[1,2,3;4,5,6]	[1,2;3,4;5,6]	[22,28;49,64]
[1,2;3,4;5,6]	[1,2,3;4,5,6]	not allowed!

## Limitations

For nonscalar A and B, the number of columns of A must equal the number of rows of B.

## Syntax

$A + B$

## Description

$A + B$  adds A and B. A and B must have the same size, unless one is a scalar. A scalar can be added to a matrix of any size.

## Examples

<b>A</b>	<b>B</b>	<b>A + B</b>
1	3	4
2.1	-3.2	-1.1
[1,2;3,4]	[1,1;5,5]	[2,3;8,9]

2	[1,2;3,4]	[3,4;5,6]
[1,2;3,4]	4	[5,6;7,8]
[1,2;3,4]	[5,6;7,8;9,10]	not allowed!

**Limitations**

If A and B are matrices, they must have the same size.

**Syntax**

$A - B$

**Description**

A - B subtracts B from A. A and B must have the same size, unless one is a scalar. A scalar can be subtracted from a matrix of any size.

**Examples**

<b>A</b>	<b>B</b>	<b>A - B</b>
5	3	2
-4.2	5.5	-9.7
[4,5;6,7]	[1,1;5,5]	[3,4;1,2]
[4,5;6,7]	4	[0,1;2,3]
4	[4,5;6,7]	not allowed!

**Syntax**

$A .* B$

**Description**

A .\* B multiplies the elements of A by the elements of B. A.\*B is the array or matrix with elements  $A(i,j) * B(i,j)$ .

**Examples**

<b>A</b>	<b>B</b>	<b>A .* B</b>
[1,-2,-4,2]	[1,2,1,4]	[1,-4,-4,8]
[2,0;0,2]	[1,2;3,4]	[2,0;0,8]
[2,0;0,2]	1	not allowed!

**Limitations**

A and B must have the same size.

**Syntax**

$$A ./ B$$
**Description**

$A ./ B$  divides the elements of  $A$  by the elements of  $B$ .  $A ./ B$  is the matrix with elements  $A(i,j)/B(i,j)$ .

**Examples**

<b>A</b>	<b>B</b>	<b>A ./ B</b>
$[1,-2,-4,2]$	$[1,2,1,4]$	$[1,-1,-4,0.5]$
$[2,0;0,2]$	$[1,2;3,4]$	$[2,0,0,0.5]$
$[2,0;0,2]$	$1$	<i>not allowed!</i>

**Limitations**

$A$  and  $B$  must have the same size.

**Syntax**

$$A.^B$$
**Description**

$A.^B$  raises the elements of  $A$  to the power of the elements of  $B$ .  $A.^B$  is the matrix with elements  $A(i,j)^{B(i,j)}$ .

**Examples**

<b>A</b>	<b>B</b>	<b>A.^B</b>
$[1,-2,-4,2]$	$[1,2,1,4]$	$[1,4,-4,16]$
$[2,2;3,2]$	$[1,0;3,4]$	$[2,1;27,16]$
$[2,0;0,2]$	$1$	<i>not allowed!</i>

**Limitations**

$A$  and  $B$  must have the same size.

**Syntax**

$$A / B$$
**Description**

$A / B$  divides  $A$  by  $B$ . For a nonscalar  $B$ ,  $A/B$  equals  $A \cdot \text{inverse}(B)$ . For a nonscalar  $A$ , each element of  $A$  is divided by the scalar  $B$ .

**Examples**

<b>A</b>	<b>B</b>	<b>A / B</b>
15	3	5
-40.5	5	-8.1
2	[1,2;3,4]	[-4,2;3,-1]
[1,-2;-3,4]	4	[0.25,-0.5;0.75,1]
[2,0;0,2]	[1,2;3,4]	[-4,2,3,-1]
1	0	not allowed!
1	[1,2,3;4,5,6]	not allowed!

**Limitations**

If A and B are matrices, they must have the same size. If B is a matrix and it becomes singular, simulation is stopped.

**Syntax**

*a div b*

**Description**

a div b divides the scalar a by the scalar b and rounds the output toward zero.

**Examples**

<b>a</b>	<b>b</b>	<b>a div b</b>
10	5	2
9.9	5	1
-8	2	-4
-7.9	2	-3
-7.9	-2	3

**Limitations**

a and b must be scalars.

**Syntax**

*a mod b*

**Description**

a mod b returns the signed remainder after division:

$a \bmod b = a - \text{trunc}(a / b) * b$

**Examples**

<b>a</b>	<b>b</b>	<b>a mod b</b>
10	5	0
9.9	5	4.9
-8	2	0
-7.9	2	-1.9
-7.9	-2	-1.9

**Limitations**

a and b must be scalars.

**Syntax**

$$A \wedge b$$
**Description**

$A \wedge B$  raises A to the power B. For a nonscalar A and integer B,  $A^B$  is computed by repeated multiplication of A. If B is negative A is inverted first. If B is zero,  $A^B$  is the identity matrix. For other values of B, it is rounded to its nearest integer value. Making B a nonscalar is not allowed.

**Examples**

<b>A</b>	<b>b</b>	<b>A ^ b</b>
5	3	125
4	-2.1	0.054409
5.5	0	1
3	2.1	10.04511
[2,0;0,2]	4	[16,0;0,16]
[1,2,3,4]	-2.1	[5.5,-2.5;-3.75,1.75]
[1,2,3,4]	0	[1,0;0,1]
[1,2,3,4]	[1,2;3,4]	not allowed!

**Limitations**

b must be a scalar. For a matrix A, b is rounded to the nearest integer value value.



## Boolean

### Syntax

*a and b*

### Description

*a and b* performs a logical AND between *a* and *b*. If *a* or *b* are not a boolean, 0 represents a logical false and any nonzero value represents a logical true. The truth table for this operator is shown below.

### Table

<b><i>a</i></b>	<b><i>b</i></b>	<b><i>a and b</i></b>
<i>false</i>	<i>false</i>	<i>false</i>
<i>false</i>	<i>true</i>	<i>false</i>
<i>true</i>	<i>false</i>	<i>false</i>
<i>true</i>	<i>true</i>	<i>true</i>

### Limitations

*a* and *b* must be scalars.

### Syntax

*a or b*

### Description

*a or b* performs a logical OR between *a* and *b*. If *a* or *b* are not booleans, 0 represents a logical false and any nonzero value represents a logical true. The truth table for this operator is shown below.

### Table

<b><i>a</i></b>	<b><i>b</i></b>	<b><i>a or b</i></b>
<i>false</i>	<i>false</i>	<i>false</i>
<i>false</i>	<i>true</i>	<i>true</i>
<i>true</i>	<i>false</i>	<i>true</i>
<i>true</i>	<i>true</i>	<i>true</i>

### Limitations

*a* and *b* must be scalars.

**Syntax***a xor b***Description**

a xor b performs a logical Exclusive OR between a and b. If a or b are not booleans, 0 represents a logical false and any nonzero value represents a logical true. The truth table for this operator is shown below.

**Table**

<b>a</b>	<b>b</b>	<b>a xor b</b>
<i>false</i>	<i>false</i>	<i>false</i>
<i>false</i>	<i>true</i>	<i>true</i>
<i>true</i>	<i>false</i>	<i>true</i>
<i>true</i>	<i>true</i>	<i>false</i>

**Limitations**

a and b must be scalars.

**Comparison****Syntax***a < b***Description**

The < operator compares two arguments and yields a boolean. If a is less than b, then a < b yields true. If a is equal or larger than b, then a < b yields false.

**Example**

<b>a</b>	<b>b</b>	<b>a &lt; b</b>
<i>1</i>	<i>2</i>	<i>true</i>
<i>1.01e2</i>	<i>101.0</i>	<i>false</i>
<i>31</i>	<i>1</i>	<i>false</i>
<i>-12</i>	<i>-11</i>	<i>true</i>

**Limitations**

a and b must be scalars.

**Syntax**

$$a \leq b$$
**Description**

The  $\leq$  operator compares two arguments and yields a boolean. If  $a$  is less than or equal to  $b$ , then  $a \leq b$  yields true. If  $a$  is larger than  $b$ , then  $a \leq b$  yields false.

**Example**

<b>a</b>	<b>b</b>	<b><math>a &lt; b</math></b>
<i>1</i>	<i>2</i>	<i>true</i>
<i>1.01e2</i>	<i>101.0</i>	<i>true</i>
<i>31</i>	<i>1</i>	<i>false</i>
<i>-12</i>	<i>-11</i>	<i>true</i>

**Limitations**

$a$  and  $b$  must be scalars.

**Syntax**

$$a \neq b$$
**Description**

The  $\neq$  operator compares two arguments and yields a boolean. If  $a$  is equal to  $b$ , then  $a \neq b$  yields false. If  $a$  is not equal to  $b$ , then  $a \neq b$  yields true.

**Example**

<b>a</b>	<b>b</b>	<b><math>a \neq b</math></b>
<i>1</i>	<i>1</i>	<i>false</i>
<i>1.01e2</i>	<i>101.0</i>	<i>false</i>
<i>31</i>	<i>1</i>	<i>true</i>
<i>true</i>	<i>false</i>	<i>true</i>

**Limitations**

$a$  and  $b$  must be scalars.

**Syntax**

$$a == b$$

**Description**

The `==` operator compares two arguments and yields a boolean. If `a` is equal to `b`, then `a==b` yields `true`. If `a` is not equal to `b`, then `a==b` yields `false`. It is typically used in an if-statement.

**Example**

<b>a</b>	<b>b</b>	<b>a == b</b>
<i>1</i>	<i>1</i>	<i>true</i>
<i>1.01e2</i>	<i>101.0</i>	<i>true</i>
<i>31</i>	<i>1</i>	<i>false</i>
<i>true</i>	<i>false</i>	<i>false</i>

**Note**

The normal equal sign (`=`) should only be used for equations. The equal sign (`=`) makes the left side of an equation equal to the right side. This is different to the equal statement (`==`) which compares two arguments and yields a boolean.

**Syntax**

$$a > b$$
**Description**

The `>` operator compares two arguments and yields a boolean. If `a` is less than or equal to `b`, then `a > b` yields `false`. If `a` larger than `b`, then `a > b` yields `true`.

**Example**

<b>a</b>	<b>b</b>	<b>a &gt; b</b>
<i>1</i>	<i>2</i>	<i>false</i>
<i>1.01e2</i>	<i>101.0</i>	<i>false</i>
<i>31</i>	<i>1</i>	<i>true</i>
<i>-12</i>	<i>-11</i>	<i>false</i>

**Limitations**

`a` and `b` must be scalars.

**Syntax**

$$a \geq b$$
**Description**

The `>=` operator compares two arguments and yields a boolean. If `a` is less than `b`, then `a >= b` yields `false`. If `a` larger than or equal to `b`, then `a >= b` yields `true`.

**Example**

<b>a</b>	<b>b</b>	<b>a &gt;= b</b>
<i>1</i>	<i>2</i>	<i>false</i>
<i>1.01e2</i>	<i>101.0</i>	<i>true</i>
<i>31</i>	<i>1</i>	<i>true</i>
<i>-12</i>	<i>-11</i>	<i>false</i>

**Limitations**

a and b must be scalars.

**Prefix****Syntax**

$$Y = +A$$
**Description**

The plus sign may be used as a prefix for scalars, vectors and matrices.

**Examples**

<b>A</b>	<b>+A</b>
<i>5</i>	<i>5</i>
<i>[4,5;-6,7.1]</i>	<i>[4;5;-6;7.1]</i>

**Syntax**

$$Y = -B$$
**Description**

The minus sign may be used as a prefix for scalars, vectors and matrices.

**Examples**

<b>A</b>	<b>-A</b>
<i>5</i>	<i>-5</i>
<i>[4,5;-6,7.1]</i>	<i>[-4;-5;6;-7.1]</i>

**Syntax**

$$y = \text{not } a$$
**Description**

The boolean prefix not performs an inversion of a.

**Table**

<b><i>a</i></b>	<b><i>not a</i></b>
<i>false</i>	<i>true</i>
<i>true</i>	<i>false</i>

**Limitations**

a must be a boolean.

**7.6 Statements****Statements**

Statements are important to guide the flow of information in equation models. 20-sim supports the following statements:

1. For to Do
2. If Then
3. If Then Else
4. If Then Else (expression)
5. Repeat Until
6. Switch Case
7. Stopsimulation
8. Warning
9. While Do
10. toMatlab
11. fromMatlab
12. doMatlab
13. Effortincausality
14. Flowincausality

## If Then

### Syntax

```

    if condition then
        equation;
    ....
end;

```

### Description

The simplest if statement evaluates a condition and performs the specified equation(s) if the condition is true. If the condition is not true, 20-sim ignores the equation(s).

### Examples

```

b = false;
y = ramp(1);
u = -ramp(1);
if time > 5 then
    y = -ramp(1); // equations to be executed if condition is true,
    u = ramp(1); // these are not executed if condition is false
end;
if time == 10 then // note the use of the equal operator ==
    b = true; // equations to be executed if condition is true,
end;

```

### Limitations

1. The output of the condition must be a boolean.
2. If needed, always use the equal operator (==) in the condition.

### Note

1. Take care when using event functions in if-then-else statements. In if-then-else statements only the equations of the true parts are evaluated, so event functions may not always be triggered!
2. Equations within an if statement have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially.

## If Then Else

### Syntax

```

    if condition then
        equation;
    ...
    else
        equation;
    ...
end;

```

### Description

The if-then-else statement evaluates a condition and performs the first set of equation(s) if the condition is true and the second set of equation(s) if the condition is false. If the condition is true, 20-sim ignores the second set of equation(s). If the condition is false, 20-sim ignores the first set of equation(s).

## Nesting

If-then-else statements may be nested as many times as desired. Do not forget to include the word "end;" to finish every nested statement!

### Examples

```

y = step(1);
u = -step(1);
if time > 5 then
    y = -ramp(1); // equations to be executed if condition is true,
    u = ramp(1); // these are not executed if condition is false
else
    y = ramp(1); // equations to be executed if condition is false,
    u = -ramp(1); // these are not executed if condition is true
end;

//Nesting
if time < 5 then
    a = 1;
    b = sin(time*1);
else
    if time == 5 then
        a = 2;
        b = sin(time*2);
    else
        a = 3;
        b = sin(time*3);
    end;
end;

```

### Limitations

1. The output of the condition must be a boolean.
2. If needed, always use the equal operator (==) in the condition.

### Note

1. Take care when using event functions in if-then-else statements. In if-then-else statements only the equations of the true parts are evaluated, so event functions may not always be triggered!
2. There is also an if-then-else expression.
3. Equations within an if statement have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially.



## If Then Else (expression)

### Syntax

```
y = if condition then
    expression
else
    expression
end;
```

### Description

The if-then-else expression evaluates a condition and makes y equal to the first expression if the condition is true and makes y equal to the second expression if the condition is false. If the condition is true, 20-sim ignores the second expression. If the condition is false, 20-sim ignores the first expression. Because the complete construct forms one expression, only one semicolon is used at the end.

### Nesting

If-then-else expression may be nested. Take care that **no semicolons** are used, because no matter how large the construct is, it is still one expression!

### Examples

```
y = if time > 5 then
    -ramp(1) // statement to be executed if condition is true,
else
    ramp(1) // statement to be executed if condition is false,
end;

// Nesting:
x = if time < 1 then
    1
else
    if time < 2 then
        2
    else
        if time == 2 then
            1
        else
            0
        end
    end
end;
```

### Limitations

1. The output of the condition must be a boolean.
2. If needed, always use the equal operator (==) in the condition.

### Note

1. Take care when using event functions in if-then-else expressions. In if-then-else expressions only the equations of the true parts are evaluated, so event functions may not always be triggered!
2. There is also an if-then-else statement.

- Equations within an if statement have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially.

## For To Do

### Syntax

```

    for variable = start to stop by step do
        equation;
        equation;
        ....
    end;

```

### Description

The for statement is designed to execute equation(s) a fixed number of times. It begins with the keyword **for** and an expression that specifies the number of times the equations within the for statement should be executed. The for statement ends with the keyword **end**. The default increment in a for statement is one (1), but you can use the keyword **by** to adjust the increment.

The equations within the for statement are always executed once. The for statement stops when the variable has exceeded the stop value.

### Examples

```

variables
    real i,y[10];
equations
    for i = 1 to 2 do
        // executed 2 times: y[1] and y[2]
        y[i] = ran (1);
    end;
    for i = 2 to 4.1 by 2 do
        // executed 3 times: y[2], y[4] and y[6]
        y[i] = ran (1);
    end;

```

### Limitations

- The start, stop and step values must be scalars. The step value is optional. There are no limitations to the number of equations that can be used within the for statement.
- Equations within an for statement have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially.

## While Do

### Syntax

```

    while condition do
        equation;
        equation;
        ....
    end;

```

### Description

The while statement is designed to execute equation(s) repeatedly, as long as the condition is true. The condition is evaluated before the equations are executed.

It is the user's responsibility to guarantee that the execution of the while statement finishes by making the condition become false at a certain time.

### Examples

```

variables
  real i,y[10];
equations
  i = 1;
  while i < 3 do
    // executed 2 times: y[1] and y[2]
    y[i] = ran (1);
    // i is incremented to guarantee a stop of the loop
    i = i+1;
  end;

```

### Limitations

1. The output of the condition must be a boolean. If the boolean does not become false, the loop never ends! There are no limitations to the number of equations that can be used within the while statement.
2. Equations within an while statement have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially.

### Repeat Until

#### Syntax

```

repeat
  equation;
  equation;
  ....
until condition;

```

#### Description

The repeat statement is designed to execute equation(s) repeatedly, as long as the condition is true. The condition is evaluated after the equations are executed.

It is the user's responsibility to guarantee that the execution of the repeat statement finishes by making the condition become false at a certain time.

### Examples

```

variables
  real i,y[10];
equations
  i = 1;
  repeat
    // executed 2 times: y[1] and y[2]
    y[i] = ran (1);
    // i is incremented to guarantee a stop of the loop
    i = i+1;
  until i > 2;

```

### Limitations

1. The output of the condition must be a boolean. If the boolean does not become false, the loop never ends! There are no limitations to the number of equations that can be used within the repeat statement.

2. If needed, always use the equal operator ( $=$ ) in the condition.
3. Equations within an repeat statement have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially.

## Switch Case

### Syntax

```

switch variable
  case condition1 do
    equations;
  case condition2 do
    equations;
  default do
    equations;
end;
```

### Description

The switch case statement is designed to execute equation(s) based on the condition of a variable. Only the equations of the valid branch are executed. If none of the branches is valid, the equations of the default branch are executed.

### Limitations

1. The switch variable should not be changed inside one of the branches.
2. Equations within a switch case statement have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially. Therefore it is advised only to use this statement in a code section.

## Stopsimulation

### Syntax

```
stopsimulation ('string');
```

### Description

The stopsimulation function stops the simulation as soon as it comes to action. It is useful when used in combination with an if statement. As soon as the simulation stops, the log window will appear showing the string that is used in the function.

### Examples

```

if x == 0 then
  stopsimulation('division by zero: y could not be calculated');
else
  y = 1/x;
end;
```

## Warning

### Syntax

```
warning ('string',boolean);
```

### Description

The warning function displays a message in the the log window. You can choose to display the string once (boolean = true) or every simulation step (boolean = false). It is advised to use the warning function in combination with an if-then statement or event-function.

## Examples

```
warning('this message will be displayed every simulationstep!',false);
if time > 1
    warning('this message will be displayed every simulationstep after time > 1!',
false);
end;
if x > 100 then
    warning('this message will be displayed only once after x > 100',true);
end;
if event(y) then
    warning('this message will be displayed when y is exactly 0',false);
end;
```

## toMatlab

### Syntax

```
toMatlab(<20-sim variable>)
toMatlab(<20-sim variable>, 'matlab variable name')
```

### Description

The **toMatlab** statement allows you to pass a variable from 20-sim to Matlab. The first argument is the name of the 20-sim variable to send to Matlab (source). The second (optional) argument '*matlab variable name*' is the name of the corresponding matlab variable (destination).

When the '*matlab variable name*' argument is omitted, 20-sim will use the full hierarchical name of the 20-sim variable.

A 20-sim variable named *Controller*\x becomes in Matlab: *Controller\_x*

The corresponding **fromMatlab** statement allows you to retrieve a variable from Matlab.

### Example

```
// this example shows how a variable can be transferred to matlab during simulation
variables
```

```
    real x;
    real y;
```

```
// at the start of the simulation
```

```
initialequations
```

```
    // create an empty array a
    doMatlab ('a = []; ');
    // create an variable
    doMatlab ('b=0; ');
```

```
// during simulation
```

```
equations
```

```
    // calculate x
    x = sin (time);
    // send it to Matlab
    toMatlab (x,'x');
    // and add it to array a
    doMatlab ('a = [ a x ]; ');
    // in Matlab add 2 to x
    doMatlab ('b = x + 2;');
```

```

// read matlab 'b' into 20-sim variable 'y'
fromMatlab(y,'b');

// at the end of the simulation
finalequations
    // plot the resulting array in Matlab
    doMatlab (' plot (a); ');

```

## domatlab

### Syntax

```
doMatlab('string')
```

### Description

The **doMatlab** statement allows you to pass a command line string to Matlab.

### Example

```

// this example shows how a variable can be transferred to matlab during
simulation
variables
    real x;
    real y;
// at the start of the simulation
initialequations
    // create an empty array a
    doMatlab ('a = []; ');
    // create a variable
    doMatlab ('b=0; ');
// during simulation
equations
    // calculate x
    x = sin (time);
    // send it to Matlab
    toMatlab (x,'x');
    // and add it to array a
    doMatlab ('a = [ a x ]; ');
    // in Matlab add 2 to x
    doMatlab ('b = x + 2; ');
    // read b
    fromMatlab(y,'b');
    // at the end of the simulation
finalequations
    // plot the resulting array in matlab
    doMatlab (' plot (a); ');

```

## frommatlab

### Syntax

```
fromMatlab(<20-sim variable>)
fromMatlab(<20-sim variable>, 'matlab variable name')
```

### Description

The **fromMatlab** statement allows you to retrieve a variable from Matlab and store it into a 20-sim variable.

The first argument is the name of the 20-sim variable to use as storage (destination).

The second (optional) argument '*matlab variable name*' is the name of the Matlab variable to retrieve (source).

When the '*matlab variable name*' argument is omitted, 20-sim will use the full hierarchical name of the 20-sim variable.

A 20-sim variable named *Controller*\x requests from Matlab: *Controller\_x*

The corresponding **toMatlab** statement allows you to pass a variable from 20-sim to Matlab.

### Example

// this example shows how a variable can be transferred to matlab during simulation variables

```
real x;
real y;
```

// at the start of the simulation

initialequations

```
// create an empty array a
doMatlab ('a = []; ');
// create an variable
doMatlab ('b=0; ');
```

// during simulation

equations

```
// calculate x
x = sin (time);
// send it to Matlab
toMatlab (x,'x');
// and add it to array a
doMatlab ('a = [ a x ]; ');
// in Matlab add 2 to x
doMatlab ('b = x + 2; ');
// read b
fromMatlab(y,'b');
// at the end of the simulation
```

finalequations

```
// plot the resulting array in matlab
doMatlab (' plot (a); ');
```

## Effortincausality

### Syntax

```

    effortincausality (portname) then
        equation;
        equation;
        ...
    else
        equation;
        equation;
        ...
    end;

```

### Description

The effortincausality statement evaluates if a port has causality effort in and performs the first set of equation(s) if the condition is true and the second set of equation(s) if the condition is false. If the condition is true, 20-sim ignores the second set of equation(s). If the condition is false, 20-sim ignores the first set of equation(s).

Depending on the domain you are working in, effort and flow correspond to particular variables. The table below shows the variables for the domains that are currently supported in 20-sim.

Domain	effort ( <b>e</b> )	flow ( <b>f</b> )
power	effort <b>e</b>	flow <b>f</b>
mechanical (translation)	force <b>F</b> [N]	velocity <b>v</b> [m/s]
mechanical (rotation)	torque <b>T</b> [Nm]	angular velocity <b>omega</b> [rad/s]
pneumatic	pressure <b>p</b> [Pa]	volume flow <b>phi</b> [m <sup>3</sup> /s]
thermal	temperature <b>T</b> [K]	entropy flow <b>dS</b> [J/Ks]
electric	voltage <b>u</b> [V]	current <b>i</b> [A]
hydraulic	pressure <b>p</b> [Pa]	volume flow <b>phi</b> [m <sup>3</sup> /s]
magnetic	current <b>i</b> [A]	voltage <b>u</b> [V]
pseudothermal	temperature <b>T</b> [K]	heat flow <b>dQ</b> [W]



## Examples

```

effortincausality p then
    R = if p.u > 0 then Ron else Roff end; // executed if causality of port p is effort (u)
in
else
    R = if p.i > 0 then Ron else Roff end; // executed if causality of port p is flow (i) in
end;
p.i = p.u/R;

```

## Note

1. Take care when using event functions in *effortincausality* statements. In this statement only the equations of the true parts are evaluated, so event functions may not always be triggered!
2. There is also a *flowincausality* statement.
3. Equations within an *effortincausality* have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially.

## Flowincausality

### Syntax

```

flowincausality (portname) then
    equation;
    equation;
    ...
else
    equation;
    equation;
    ...
end;

```

### Description

The *effortincausality* statement evaluates if a port has causality flow in and performs the first set of equation(s) if the condition is true and the second set of equation(s) if the condition is false. If the condition is true, 20-sim ignores the second set of equation(s). If the condition is false, 20-sim ignores the first set of equation(s).

Depending on the domain you are working in, effort and flow correspond to particular variables. The table below shows the variables for the domains that are currently supported in 20-sim.

Domain	effort ( <i>e</i> )	flow ( <i>f</i> )
power	effort <i>e</i>	flow <i>f</i>
mechanical (translation)	force <i>F</i> [N]	velocity <i>v</i> [m/s]
mechanical (rotation)	torque <i>T</i> [Nm]	angular velocity <i>omega</i> [rad/s]
pneumatic	pressure <i>p</i> [Pa]	volume flow <i>phi</i> [m <sup>3</sup> /s]
thermal	temperature <i>T</i> [K]	entropy flow <i>dS</i> [J/Ks]

electric	voltage $u$ [V]	current $i$ [A]
hydraulic	pressure $p$ [Pa]	volume flow $\phi$ [m <sup>3</sup> /s]
magnetic	current $i$ [A]	voltage $u$ [V]
pseudothermal	temperature $T$ [K]	heat flow $dQ$ [W]

### Examples

*flowincausality p then*

*R = if p.i > 0 then Ron else Roff end; // executed if causality of port p is flow (i) in else*

*R = if p.u > 0 then Ron else Roff end; // executed if causality of port p is effort (u) in end;*

*p.u = p.i\*R;*

### Note

1. Take care when using event functions in effortincausality statements. In this statement only the equations of the true parts are evaluated, so event functions may not always be triggered!
2. There is also an effortincausality statement.
3. Equations within an effortincausality have to be written in the correct order of execution, i.e. they are not rewritten into a causal form but executed sequentially.

## 7.7 Matrices and Vectors

### Declaration

Matrices and column vectors are declared in the *constants*, *parameters* and *variables* sections of a model. Declaration of matrices and column vectors is equal to to the declaration of scalars, the size however has to be specified explicitly. For example:

*parameters*

*real A[3,3], B[3,3];*

*integer C[2,2] = [1,3;5,7];*

*real K[4] = [1;2;3;4];*

*variables*

*real K[4],L[4],D[4,5];*

*integer M[2,2],N[2,2];*

Matrices and Vectors can only be of the datatype real or integer.

### Notation

Matrix sizes in 20-sim are always denoted by [n,m] where n is the numbers of rows and m is the numbers of columns. Elements can separately be denoted with commas (,) distinguishing between row elements and semicolons (;) distinguishing between rows.

matrix size	matrix form	20-sim notation
[4,1]	1	[1;3;5;7]
	3	
	5	

	7	
[1,4]	1 3 5 7	[1,3,5,7]
[2,3]	1 2 3 4 5 6	[1,2,3;4,5,6]
[3,2]	1 2 3 4 5 6	[1,2;3,4;5,6]

Column vectors are matrices with only one column. Consequently the column size may be omitted in the notation.

<b>column size</b>	<b>column form</b>	<b>20-sim notation</b>
[4]	1	[1;3;5;7]
	3	
	5	
	7	

## Use

Matrices and Vectors can be used in equations just like scalars. If possible, the element notation can be left out. **If equations get ambiguous, element notation must be used!**

### Whole matrix or vector

```
K = 1; // Make all elements of K equal to 1.
M = C; // Make matrix M equal to matrix C (sizes have to be equal).
N = D*inverse(L); // Make matrix N equal to the matrix product of D
// and the inverse of L (sizes of N, D and L have to be equal).
```

### Matrix and vector elements

```
N = [sin(time),cos(time);cos(time),-sin(time)]; // Make elements of N equal to
functions.
L[4] = time; // Make element 4 of columned L equal to time.
D[2,5] = A[2,2]*B[1,1]; // Declare one element
```

### Multiple elements (ranges)

To prevent multiple equations for assigning matrix elements, ranges can be assigned using a colon. E.g. 1:5 means element 1 to 5, 7:8 means element 7 and 8. Backward counting ranges (like 10:1) are not allowed!

```

D[2,1:5] = A[1,1:5]; // D[2,1] = A[1,1], ... , D[2,5] = A[1,5]
variables
  real v[3],p[6,6];
equations
  v = p[4:6,6]; // v[1] = p[4,6], ... , v[3] = p[6,6]

```

## Operators

Some scalar operators can also be used for matrices and vectors. Depending on the specific operator, the meaning may differ for scalars, vectors and matrices.

Operator	Description
*	Multiplication
+	Addition
-	Subtraction
.*	ArrayMultiplication
./	ArrayDivision
.^	ArrayPower
/	Division
^	Power
-	Prefix Minus Sign
+	Prefix Plus Sign
..	Absolute / Determinant / Norm

## Functions

A lot of special matrix and vector functions are supported in 20-sim:

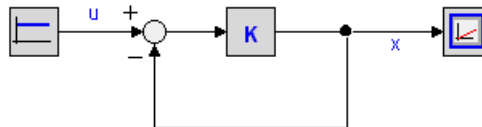
Function	Description
	Adjoint
	adjoint
	Antisym
	Columns
	Cross
	Determinant
	Diag
	Eye
	Homogeneous
	Inner
	Inverse
	InverseH

Linsolve  
 Max  
 Min  
 Msum  
 Norm  
 Norminf  
 Rows  
 Skew  
 Sym  
 Tilde  
 Trace  
 Transpose

## 7.8 Advanced Topics

### Algebraic Loops

An algebraic loop in a model is a loop consisting of elements without "memory like" functions. To calculate the variables in this loop, the variable values themselves are needed. Consider the following example of an algebraic loop in an amplifier with negative feedback:



Standard derivation of a simulation model would yield:

$$x = K \cdot (u - x)$$

The variable  $x$  depends on its own value and must be solved by **iteration**. In 20-sim every simulation algorithm is accompanied by an iteration routine. Fortunately 20-sim is able to solve many algebraic loops at equation level. For this model this leads to the analytic solution the system:

$$x = K \cdot u / (1 + K)$$

### Simulating algebraic loops

Although 20-sim contains a sophisticated algorithms to find analytic solutions, the occurrence of unbreakable loops can not always be prevented. The occurrence of algebraic loops may lead to an increase of simulation time, or even stop simulation when iteration fails.

The best solution for these problems is to have a critical look at the model and change the order of calculations in a model. Possible solutions are:

- Algebraic Loops occur when the order of calculations is arbitrary. When an algebraic loop occurs in an equation model or in a set of equation models, you may change the order of calculation by rewriting the equations. The calculation order in bond graph models can be changed by introducing hand-defined causality.
- Introduce 'parasitic' energy storage elements (e.g. a small mass, a small capacitor etc.) to break an algebraic loop. These elements introduce however, large poles in the state equations, which might increase the simulation time considerably.
- Delete elements in the algebraic loop which are not relevant for the model's simulation output (e.g. small dampers, very stiff springs etc.). Care should however be taken, since correct deletions are not always possible and require considerable modeling skill and intuition.
- Combine dual elements. Sometimes elements of the same type can be combined by adding the parameter values (e.g. combining a mass  $m_1$  and a mass  $m_2$  to a mass  $m_1 + m_2$ ). This will in most cases decrease the amount of algebraic loops.

## Causal Form

Equations within 20-sim may be entered in random form. During compilation, 20-sim will automatically try to rewrite equations into a causal form and set them in a correct order. I.e. a form where all output variables are written as function of input variables. Consider for example the following model:

```
variables
  real u,z;
equations
  u = sin(time);
  u = cos(z);
```

Here the (input) variable  $u$  is given by the equation  $u = \sin(\text{time})$ . Consequently the (output) variable  $z$  should be written as a function of  $u$ . This is exactly what 20-sim will try to do while compiling the model into simulation code. I.e. the function  $\cos$  will be inverted and the model will be rewritten to:

```
variables
  real u,z;
equations
  u = sin(time);
  z = arccos(u);
```

Some functions cannot be inverted. Consequently not all equations can be rewritten. 20-sim will report this to the user, during model checking.

## Indifferent Causality

For some models the causal form is not known beforehand. For example the iconic diagram model that describes a damper can be written as:

```
parameters
  real d;
equations
  p.F = d*p.v;
```

Here  $p.F$  denotes the force and  $p.v$  denotes the velocity of the powerport  $p$ . There is no preferred input (force or velocity). This can be explicitly stated, by giving the powerport  $p$  an indifferent causality. During compilation 20-sim will determine whether  $p.F$  or  $p.v$  is the input variable and consequently rewrite the equations.

### Preferred Causality

For some models there is a preferred causal form. For example the iconic diagram model that describes a spring can be written as:

```
parameters
  real k;
equations
  p.F = (1/k)*int(p.v);
```

Here  $p.F$  denotes the force and  $p.v$  denotes the velocity of the powerport  $p$ . The equation is written in integral form which is preferred. Consequently the preferred input is the velocity. Should the force be the input, the equation must be rewritten to a differential form, which is leads to less efficient simulation. This can be explicitly stated, by giving the powerport  $p$  an preferred causality. During compilation 20-sim will try to keep the model in this preferred form. If this is not possible the equations will be rewritten to the less preferred form.

### Fixed Causality

For some models there is only one causal form. For example a simple iconic diagram model that describes coulomb friction can be written as:

```
parameters
  real Rc;
equations
  p.F = Rc*abs(p.v);
```

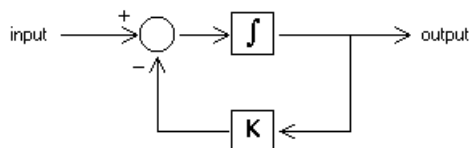
Here  $p.F$  denotes the force and  $p.v$  denotes the velocity of the powerport  $p$ . The equation is cannot be rewritten to a form where  $p.F$  is the input. This can be explicitly stated, by giving the powerport  $p$  an fixed causality. During compilation 20-sim will try to keep the model in this fixed form. If this is not possible an error message will be generated.

### Setting Causality

For some models, the equations are too complex to analyze causality. To help 20-sim, using the right causality, you can set causality for every port in the Interface Editor.

### Integral Form

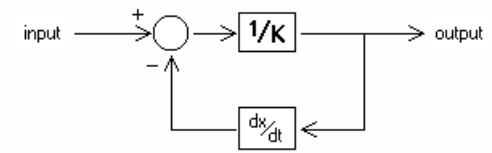
Consider the following first order linear model:



This model can be described by the dynamic equation:

$$\text{output} = \text{int}(\text{input} - K * \text{output})$$

Now look at the following model:



This model can be described by the dynamic equation:

$$output = (input - ddt(output)) / K$$

Note that we can rewrite this equation as:

$$ddt(output) = input - K * output$$

or

$$output = int(input - K * output)$$

This is the same equation as the previous model! Apparently, both models are the same! Both models can therefore be described by the dynamic equations:

$$\begin{aligned} ddt(output) &= input - K * output \\ output &= int(input - K * output) \end{aligned}$$

We call the first equation the *differential form* (no integrals). The second equation is called the *integral form* (no derivatives). In 20-sim, models can be entered in integral form as well as the differential form.

### Solving Differential Equations

During compilation, 20-sim will automatically try to rewrite equations into the integral form, since this leads to more efficient simulation. Sometimes an integral form cannot be found. Then algorithms will be applied to solve the differential directly. For example an equation like:

$$output = ddt(sin(a*time))$$

will be replaced by the following equation (applying the chain rule and using the known derivative for the sine function):

$$output = a * cos(a*time)$$

Sometimes a differential cannot be solved directly. Then only the Backward-Differentiation Methods can be used for simulation.

### Simulation Code

After compilation simulation code is generated. The equation in integral form:

$$output = int(input - K * output)$$

will be written as:

$$\begin{aligned} independent\ state &= output \\ independent\ rate &= input - K * output \end{aligned}$$

and can be handled by all integration methods. The equation in differential form:



$$\text{ddt}(\text{output}) = \text{input} - K * \text{output}$$

will be written as:

$$\begin{aligned} \text{dependent rate} &= \text{input} - K * \text{output} \\ \text{dependent state} &= \text{output} \end{aligned}$$

and can only be handled by the Backward-Differentiation Methods.

## Order of Execution

Equations within 20-sim may be entered in random form. During compilation, 20-sim will automatically try to rewrite equations into a correct order of execution. I.e. a form where all output variables are written as function of input variables and output variables of previous lines. Consider for example the following equations:

```
variables
  real u,z;
equations
  z = sin(u);
  u = cos(time);
```

Here the (input) variable  $z$  is given as a function of  $u$ . Consequently  $u$  should be calculated first. This is exactly what 20-sim will try to do while compiling the model into simulation code. I.e. the equations will be executed as:

```
u = cos(time);
z = sin(u);
```

## Code Blocks

Equations in a **code block** are not reordered. A code block is a set of equations inside a statement. Suppose we have the following equations:

```
if condition then
  code block 1
  ...
  ...
else
  code block 2
  ...
  ...
end;
```

To prevent incorrect executions of the if-statement, the equations of the code blocks will not be separated. Inside a code-block, equations can are not rewritten into an new order of execution. E.g. the following equations:

```
if time > 10 then
  z = sin(u);
  a = z^2;
  u = cos(time);
end;
```

Will be **not be reordered** and therefore not correctly executed! To get correct code, enter code blocks in a correct order, e.g.:

```

if time > 10 then
    u = cos(time);
    z = sin(u);
    a = z^2;
end;

```

## Prevent Order Changes

To make all equations a code block you can use the code section. E.g.

```

parameters
    real y = 8;
variables
    real x1, x2, x3;
code
    x1 = time;
    x2 = sin(time);
    x3 = y*x1;

```

## Integration Steps

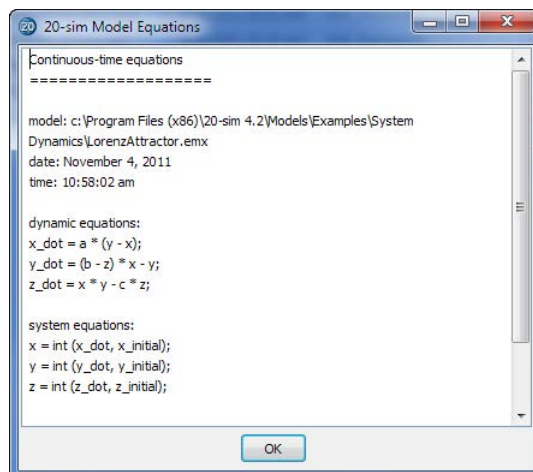
Some integration algorithms do more calculations before generating the next output value. These calculations are called minor steps, the output generation is called a major step. During a minor step, all model equations are executed. In most cases you will not notice this because only the results of the major step are shown in the simulator. There are however, exceptions. The next topic will discuss this in more detail.

## Show Equations

During processing a complete set of equations is generated of each model. To inspect these equations or copy them for use in other programs, you have to:

1. From the **Model menu** select the **Check Complete Model** command.
2. From the **Model menu** select the **Show Equations** command.

Now a window is popped up showing all the model equations.



*The model equations after compiling.*

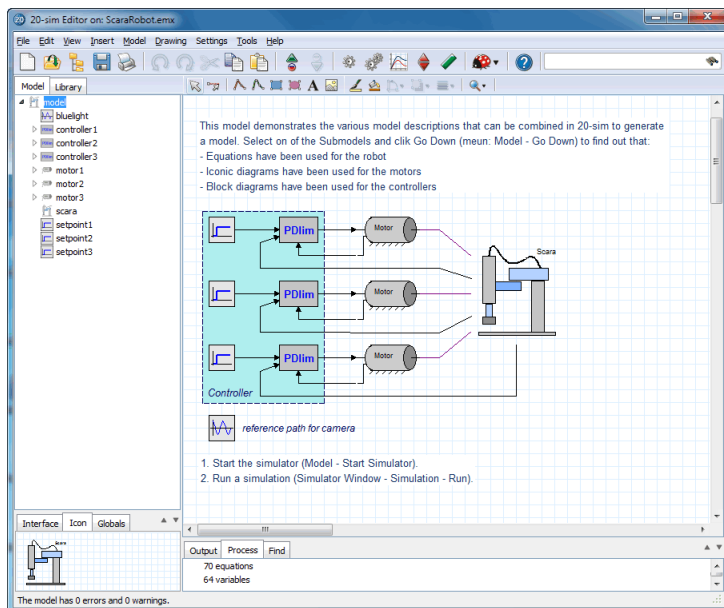


## 8 Toolboxes

### 8.1 3D Mechanics Toolbox

#### Introduction

With the 3D Mechanics Editor you can create 3D dynamic models of mechanical structures. The resulting 3D mechanical model can be connected with other 20-sim components. In the example shown below (*Getting Started\3D Mechanics Toolbox\ScaraRobotSimulation.emx*), you see a robot model that has been generated with the 3D Mechanics Editor. The model has two actuated rotation joints and one actuated translation joint. The rotation joints are directly coupled to gearboxes. The translation joint is coupled via a spindle.

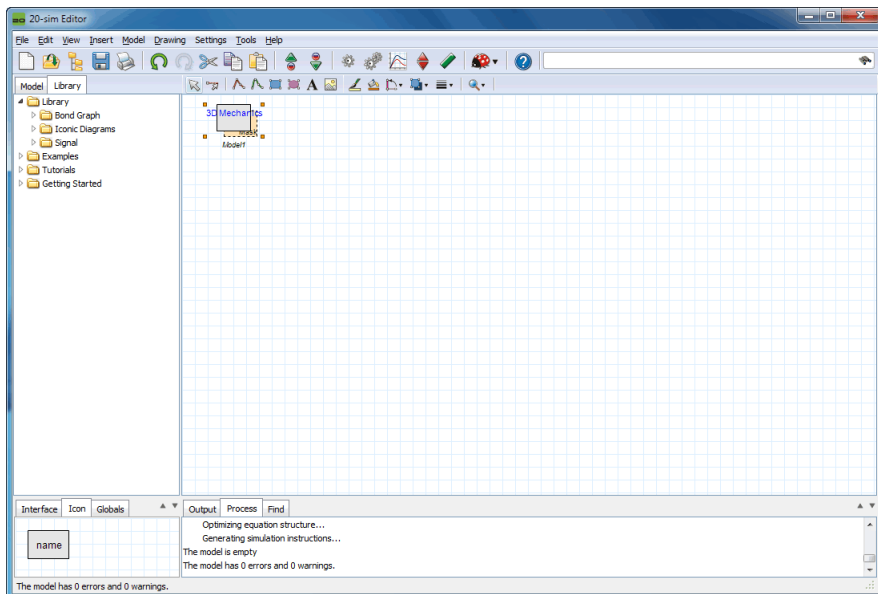


In 20-sim you can use plots to show the simulation results and use the 3D Animation Toolbox to show an animation of the 3D model.

You can open the *3D Mechanics Editor* by:

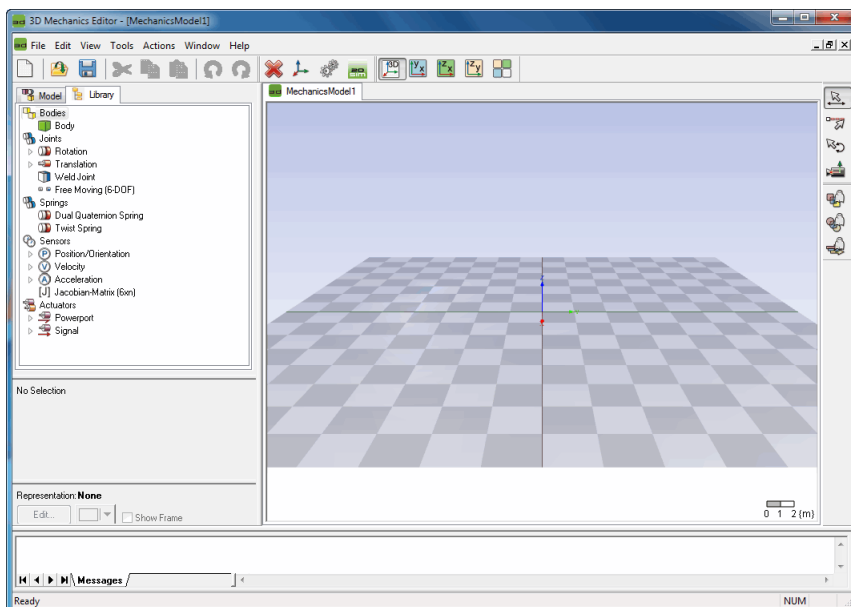
1. In the 20-sim Editor from the Tools menu select 3D Mechanics Toolbox and 3D Mechanics Editor.

Now a masked model is inserted in the *Editor* and the *3D Mechanics Editor* will be opened.



*If you select a 3D Mechanics model and select Go Down, the 3D Mechanics Editor will be automatically opened.*

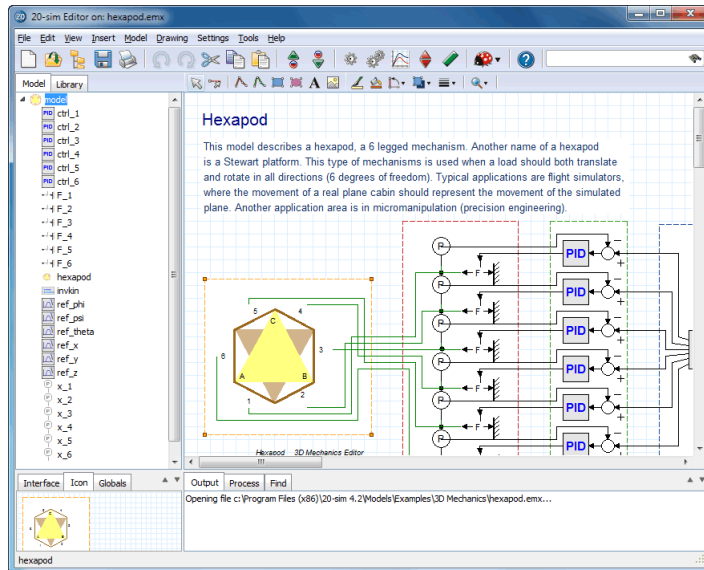
The first time you start 20-sim 3D Mechanics Editor the following screen will appear.



*The 3D Mechanics Editor*

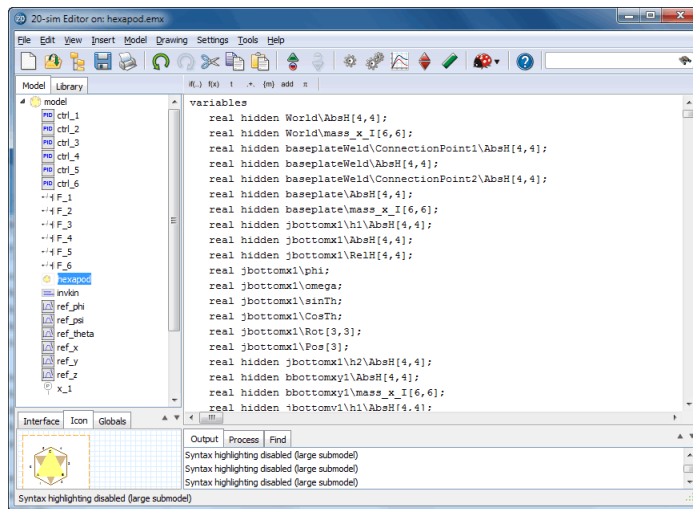
This topic is only important for users who are migrating from older version of 20-sim and want to use previously constructed 3D Mechanics models. In 20-sim 4.1, the *3D Mechanics Editor* operates on masked models. I.e. you can open the *3D Mechanics Editor* by selecting a *3D Mechanics model* and clicking the *Go Down* command. If you import a 20-sim 4.0 model, you will notice that this option does not work. We will explain the actions you have to perform to do make this trick work on older models.

1. Open the 20-sim model that contains a submodel that was generated by the 3D Mechanics Editor (make sure you have stored an emergency copy).



*The star shaped model was created using the 3D Mechanics Editor of 20-sim 4.0.*

2. Select the model that was generated by the 3D Mechanics Editor and select Go Down.



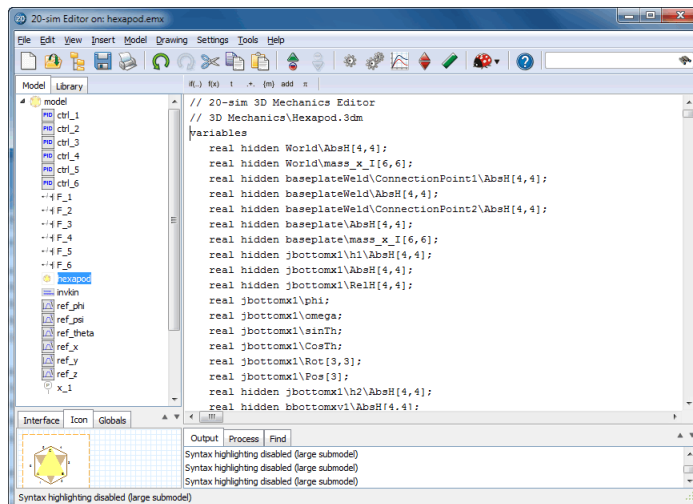
*The automatically generated equations of a 3D Mechanical Model.*

3. At the top of the model enter the following code:

// 20-sim 3D Mechanics Editor

// C:\Program Files\20-sim 4.1\Models\Examples\3D Mechanics\hexapod.3dm

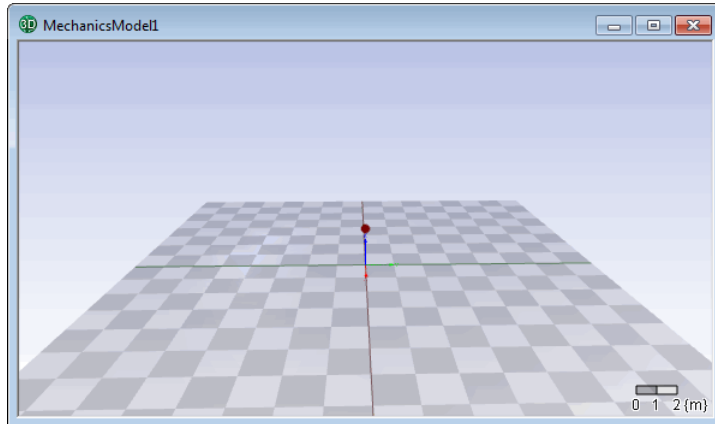
The first line tells 20-sim which editor should be opened. The second line shows the location of the corresponding 3D Mechanics configuration file. Enter the path and name of your own file here.



*The comment at the top tells 20-sim which editor should be opened and the corresponding configuration file.*

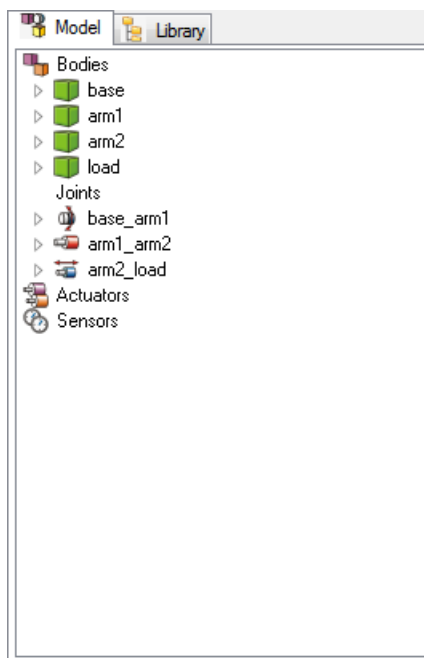
The next time you select the model and select Go Down the 3D Mechanics Editor will be opened with the proper 3D Mechanics model.

In the center of the 3D Mechanics Editor the **Edit window** is visible. At the start a reference frame and a base plane is shown. In the Edit window, you can insert components and assemble your model.



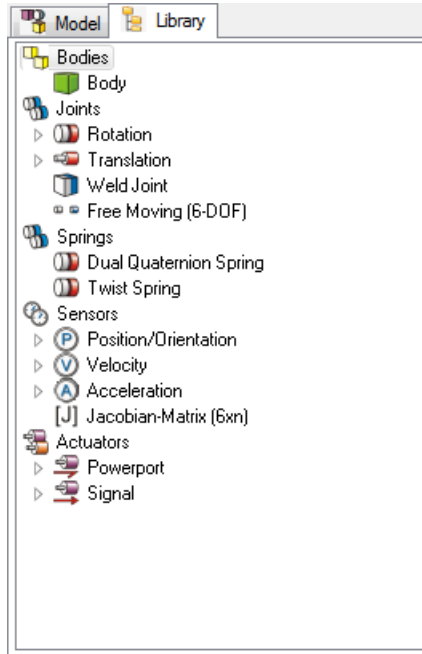
*In the Edit Window you can assemble your model.*

One of the two tabs at the left of the 3D Mechanics Editor is the **Model tab**. The Model tab contains a tree of all the components of in your current model. This tree can be used to select components and edit their properties.

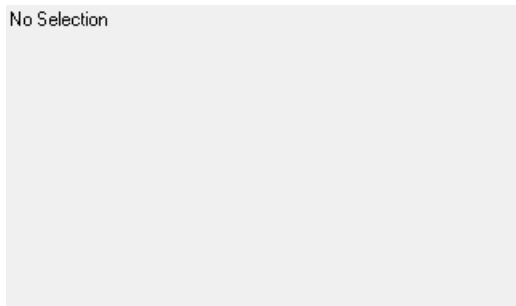




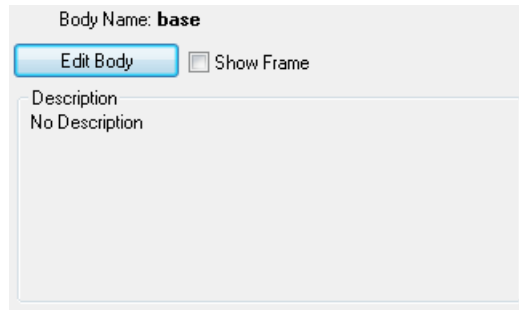
One of the two tabs at the left of the 3D Mechanics Editor is the **Library tab**. The Library tab contains predefined components, which you can use to construct your model with. The components in the library tree can be dragged into the Edit window.



Below the Bodies/Library tabs the *properties* of the selected component are shown. When no components are selected the selection properties are empty.



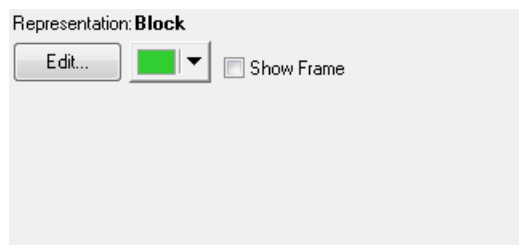
When a component is selected, the edit button will be enabled. You can click the button to change the component properties.



Below the Selection Properties, the 3D representation of the selected component is shown. When no components, the 3D Representation is empty.

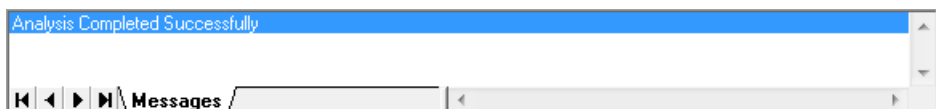


When a component is selected, the edit button will be enabled. You can click the button to change the 3D Representation of the component.







A component may be composed of several representations. Using the *Add Representation* and *Delete Representation* commands of the *Actions* menu you can add more representations or remove representations.




In the Output part of the 3D Mechanics Editor, messages will be shown during analysis of the model.








At the right of the 3D Mechanics Editor you will find the **Edit Mode** buttons. You can select them to enter several edit modes.

	Translation Mode	In this mode you can translate components.
	Connection Mode	In this mode you can make connections between components.
	Rotation Mode	In this mode you can rotate components.
	Camera Mode	In this mode you can change the camera position and orientation. I.e. the way you look at your model.

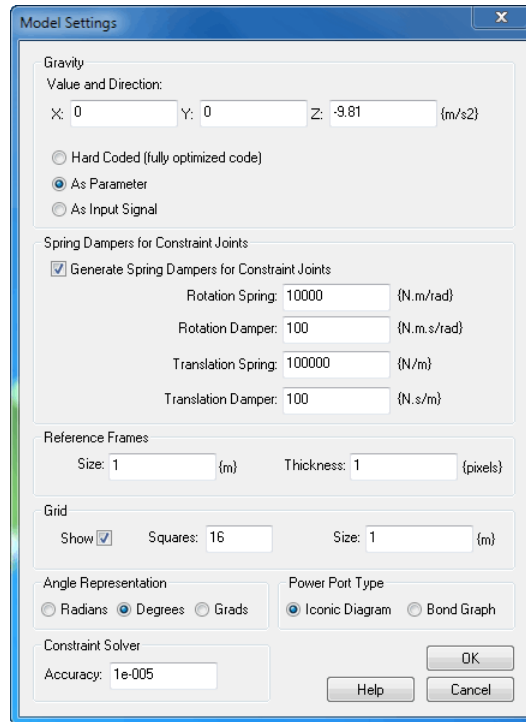
At the right of the 3D Mechanics Editor you will find the **Ghost Mode** buttons. You can use these buttons to make components transparent. This is useful when components are hidden inside other components.

	Ghost Mode for Bodies	Make every body transparent.
	Ghost Mode for Joints	Make every joint transparent.
	Ghost Mode for Sensors/Actuators	Make every sensor/actuator transparent.

In the button bar of the 3D Mechanics Editor you will find the **View Mode** buttons. You can select them to select different views.

	3D View	Default view.
	X-Y plane	View perpendicular to the x-y plane. You can only move objects along the x-y plane.
	X-Z plane	View perpendicular to the x-z plane. You can only move objects along the x-z plane.
	Y-Z plane	View perpendicular to the y-z plane. You can only move objects along the y-z plane.
	All	A combination of the all the views.

The *model Settings* command of the *Tools* menu will open the *Model Settings* dialog. In this dialog you can change some general settings such as the size of the reference frames or the amount of gravity.



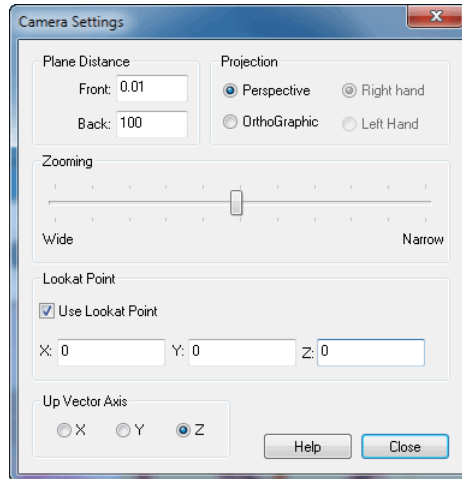
*The Model Setting Dialog.*

## Items

- Gravity: You can set the gravitational acceleration to any desired value.
  - Hard Coded: choose this option if you want to optimize for speed.
  - As Parameter: Use a gravity parameter, allowing you to change the value before the start of a simulation run.
  - As Input Signal: get the gravity value from an input signal, allowing you to change the value during simulation.
- Spring Dampers for Constraint Joints: Choose this option if you want to use spring dampers for closed kinematic chains.
  - Rotation Spring: Set the desired stiffness for the rotational spring.
  - Rotation Damper: Set the desired rotational damping.
  - Translation Spring: Set the desired stiffness for the translation spring.
  - Translation Damper: Set the desired translation damping.
- Reference Frames: Choose the size and thickness of the reference frames.

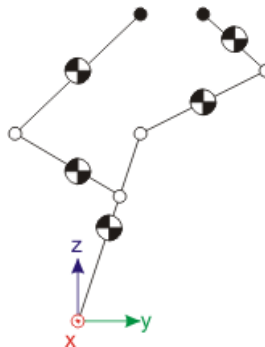
- Grid: Set the grid.
- Angle Representation: 20-sim uses SI-units for the model equations (e.g. radians). You can choose to show them in non-SI-units like degrees or grads.
- Power Port Type: Choose Iconic Diagram power ports or bond Graph power ports.
- Constraint Solver: set the accuracy of the constraint solver.

At the start of a model session, in the Edit window, a default camera is used. You can change camera settings by clicking **Camera Settings** from the **Tools** menu.



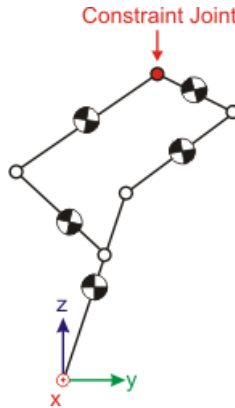
In the Camera Settings dialog you can change the range (front and back plane) and zooming of the camera, use a perspective view or orthographic and select the point to look at.

In the 3D Mechanics Editor you can connect bodies with joints. If no path from any body through a joint to another body and so on never returns to the starting body, we have an open chain mechanism. Open chain mechanisms are easy to simulate with all known integration methods.



*Open Chain Mechanism.*

If a path from any body through a joint to another body and so on returns to the starting body we have a closed chain mechanism. Closed chain mechanisms are generally more difficult to simulate.



*Closed Chain Mechanism.*

20-sim uses a special feature to simulate closed chain mechanisms. At an arbitrary place a joint is removed to create an open chain mechanism. Then the open chain is closed again using a *spring damper* joint or a *constraint* joint. You can choose which joint to use in the Model Settings Dialog.

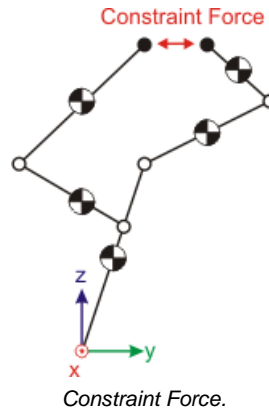
### Spring Damper Joint

A spring damper joint is a joint where all rigid connections are replaced by spring dampers. If weak spring dampers are used a certain amount of (unwanted) displacement will be possible. By increasing the stiffness and damping, the displacement can be decreased. You can set the spring stiffness and damping in the Model Settings Dialog.

### Constraint Joint

The constraint joint works exactly like the original joint but uses constraint forces to do the job. Constraint forces can only be simulated with special integration methods. In 20-sim the Modified Backward Differentiation Method is able to calculate constraint forces.

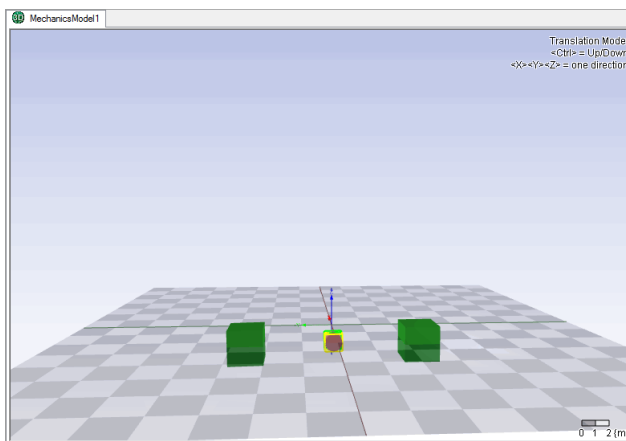
The concept of constraint forces is quite easy to understand if we look at the open chain mechanism below. At the tips of the mechanism a force is applied. If we apply a force that keeps the tips at the same position at each time step, it will effectively work as a rotation joint. That is exactly what constraint forces do. At every simulation step, an iterative procedure is run to find exactly that force that keeps the position offset at zero.



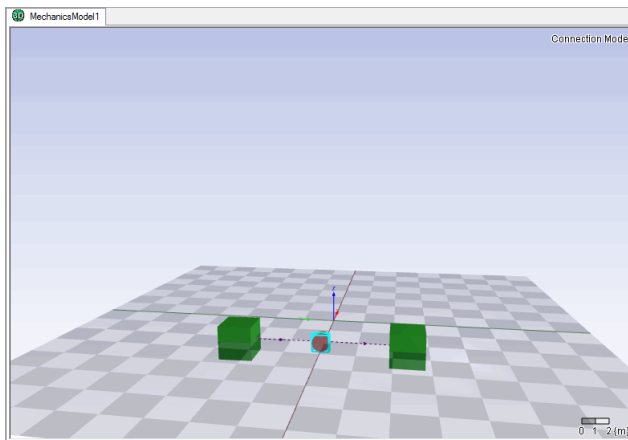
This iterative procedure is not standard for most integration methods. In 20-sim only the Modified Backward Differentiation Method supports it. In the 3D Mechanics Editor you do not have to worry about closed chain mechanisms. If necessary, standard joints are replaced automatically by constraint joints. You only have to realize that simulation of a mechanism with constraint joints in 20-sim should be performed using the Modified Backward Differentiation Method.

## Working Order

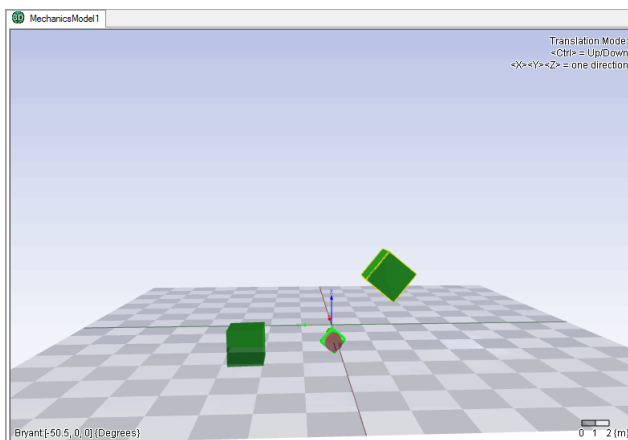
From the Library tab you can drag and drop components to the Edit window. If you put the editor in translation mode you can select the components and use the mouse to put them in the correct position.



A standard model will at least consist of some bodies and joints. The bodies have to be connected with the joints to define the degrees of freedom of the model. The connecting of joints and bodies can be done in the connection mode. By clicking on a body and then on a joint a connection is defined.



If all connections are defined, you can test the possible motions of your model. Return to the translation mode and click on a body. You will see arrows that indicate the possible motion of the connected joint. By dragging the mouse you can make the body move.



When the model is ready you can check it. When no errors are found you can update it to 20-sim.

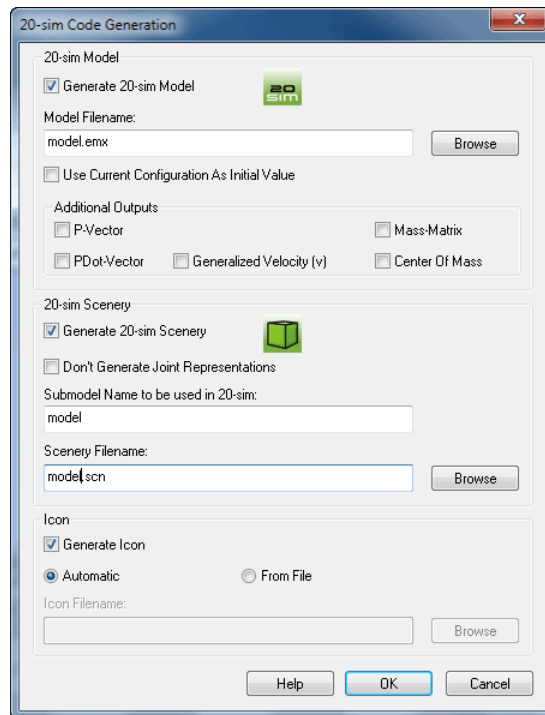
## Checking

When your 3D dynamic model has been created and assembled, you can check for errors by selecting the *Check Model* command from the *Actions* menu. If everything is OK the Output will show the message "Analysis Completed Successfully".

## Generating 20-sim Model

After the model has been checked, you can export it as a 20-sim submodel by selecting the *Generate 20-sim Model* command from the Actions menu.





## 20-sim Model

As you may know from the Joint Properties dialog, all joints have an initial value. During analysis of your model, some joints may have been twisted. You can use the current (twisted) configuration to generate a 20-sim model for, or reset it to its initial values first.

## Additional Outputs

For advanced users, some additional outputs may be useful. First time users are advised not to select these outputs.

## Output Filename

Use the *Browse* button to select a folder and a filename for the generated 20-sim model.

## 20-sim Scenery

In 20-sim you can use the 3D Animation Toolbox to show an animation of the mechanical structure. You can export the structure to a scenery file, which can be loaded in the 3D Animation Toolbox.

- **Don't Generate Joint Representations:** Each joint is represented in the 3D Animation as autonomous component with variables to denote the position and orientation. For large models you can save memory space by not exporting the joints.
- **Submodel Name to be used in 20-sim:** The 3D Animation will use 20-sim submodel names to identify the movements of object. You have to enter the submodel name, that you will use for the 3D dynamic model in 20-sim.
- **Scenery Filename:** Use the *Browse* button to select a folder and a filename for the generated scenery file.

## Library

The Library Tab shows all components that can be used to create your 3D Dynamic model.

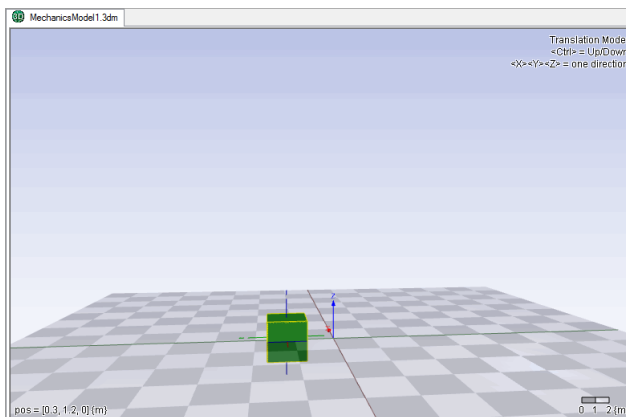
- Bodies
- Joints
- Sensors
- Actuators

## Position

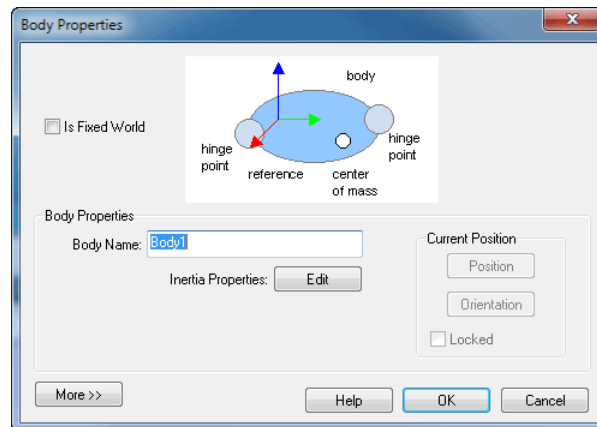
When you drag and drop a body into the Edit window, its position (i.e. the position of its reference frame) will be defined with respect to the base reference frame. You can change the position with the mouse pointer. From the **View** menu click *Mode and Translation* or click



the button to go to translation mode. If you put the mouse pointer on top of the body, you can change its position by pressing the left mouse button. If you pressing the *Ctrl-button* at the same time, the body will move up and down.



You can also set the position manually by double clicking the body. This will open the Body Properties dialog.




Using this dialog you can:

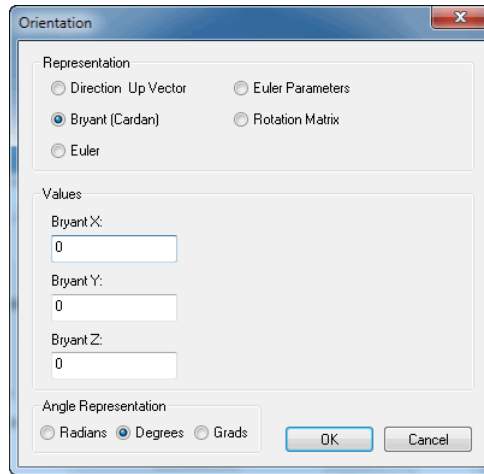
- change the name of the body
- set the inertia parameters
- change the position
- change the orientation
- make it a fixed body
- set more options

### Fixed Body

The purpose of building a 3D model in most cases is to construct some kind of mechanism using bodies and joints. The joints make the bodies move in a particular way, which can be inspected in the 3D Editor. Every body in 3D mechanics editor is floating by default, unless specifically set to be attached to the fixed world, or connected to another body by means of a joint. Any body can be set to be a fixed body by checking the **Is Fixed World** option in the **Body Properties dialog**. Changing the position of a fixed body in a mechanism will change the base position of the mechanism. Dragging the other bodies will only make the mechanism move, but not change the base position. If you want to model a floating mechanism (e.g. a satellite in space), all bodies should remain floating.

### Orientation

To set the orientation of a body, the same procedure can be followed as for the position of a body. If you set the Editor in Rotation mode ( , you can change the orientation of the body with the mouse pointer. You can also use the Body Properties dialog to set the orientation precisely by clicking the orientation button.



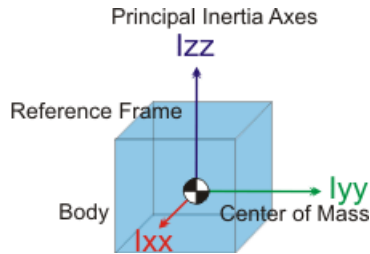
The orientation of a body is specified by the orientation of its reference frame. You can define this orientation using various representations.

- **Direction Up Vector:** Using the Direction Up vector method you have to specify the Y-axis (Direction) and Z-axis (Up) of the body reference frame.
- **Bryant angles:** Using Bryant angles we start with the initial body reference frame. First we rotate around the X-axis of the body reference frame, then we rotate around the Y-axis of the body reference frame and finally around the Z-axis of the body reference frame. Bryant angles are also known as X-Y-Z relative Euler angles or Cardan angles.
- **X-Y-X Euler:** Using X-Y-X Euler angles we start with the initial body reference frame. First we rotate around the X-axis of the body reference frame, then we rotate around the Y-axis of the body reference frame and finally around the X-axis of the body reference frame.
- **Euler Parameters:** Using Euler parameters we start with the initial body reference frame and rotate this frame around a vector  $K [X,Y,Z]$  about an angle  $\theta$ .
- **Rotation Matrix:** Using a  $3 \times 3$  rotation matrix, you can enter 9 elements that will transform the initial orientation of the body reference frame to the new orientation.

## Inertia Properties

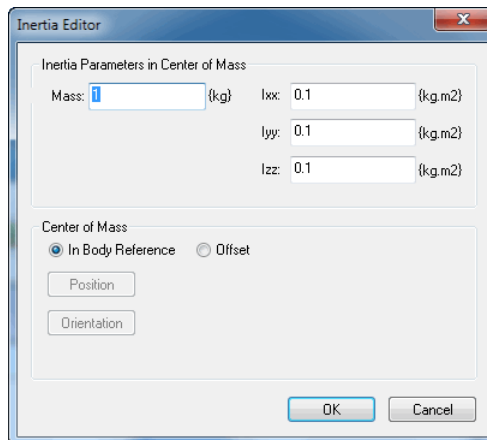
Each body has a mass and rotational inertia. The mass indicates the resistance of the body to a change in position. Given a fixed force, a body with a large mass will accelerate more slowly. This property is the same for all directions. Therefore the mass can be indicated by a single parameter.

The rotational inertia indicates the resistance of a body to a rotation. Given a fixed torque, a body with a large rotational inertia will start to rotate more slowly. The rotational inertia is not the same for all orientations. Generally, for any body three axes can be identified that indicate a stable rotation. The rotational inertia for these three principal axes of rotation is sufficient to describe the motion of a body. The connection of these three principal axes of rotation is generally known as the center of mass.

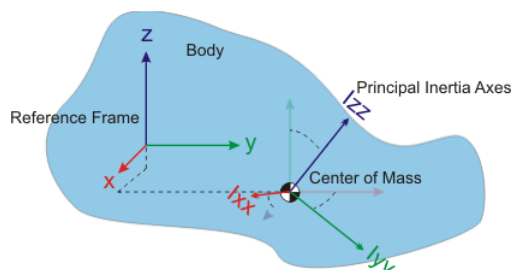


Any body, indifferent of its shape, which has the same mass, the same principal axes of rotation and the same rotational inertia, will show the same dynamic behavior. That is why you can change the representation of a body to any size, it will not change its dynamic properties.

If you open the **Body Properties Dialog** you can click the **Edit** button to change the inertia properties. You can set mass and the rotational inertias for each of the principle inertia axis.



The center of mass does not necessarily have to coincide with the body reference frame and the orientation of the principal inertia axes do not have to coincide with the orientation of the body reference frame.



You can enter the offset position of the center of mass and the orientation of the principal inertia axes, by clicking the offset button.

## More Options

If you click the More button in the *Body Properties dialog*, options are shown which form a shortcut for the normal way of building models. They are meant for experienced users.

First a list of connection points are shown and some buttons to edit these points. Connection points are used to indicate at which point a joint or other element is connected with the body. Connection Points are explained in more detail in the next section.

At the bottom two options are shown. If you choose the Generate Power Interaction Port option, a power port will be added to the body, which allows you to insert forces and torques onto the body, from other 20-sim submodels.

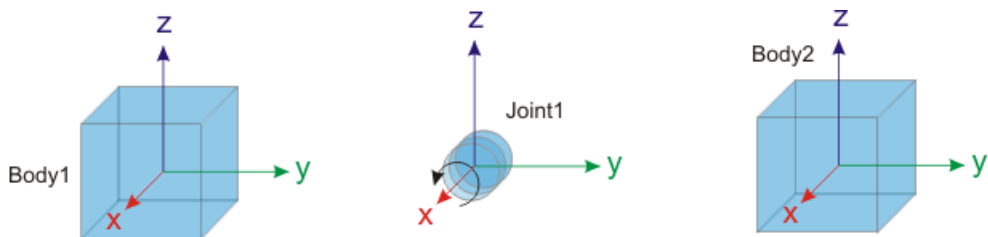
The Output Absolute H-matrix option, will create an 4x4 output signal that gives the position and orientation of the body, using an H-matrix. This signal can be connected to other 20-sim submodels.

## Properties

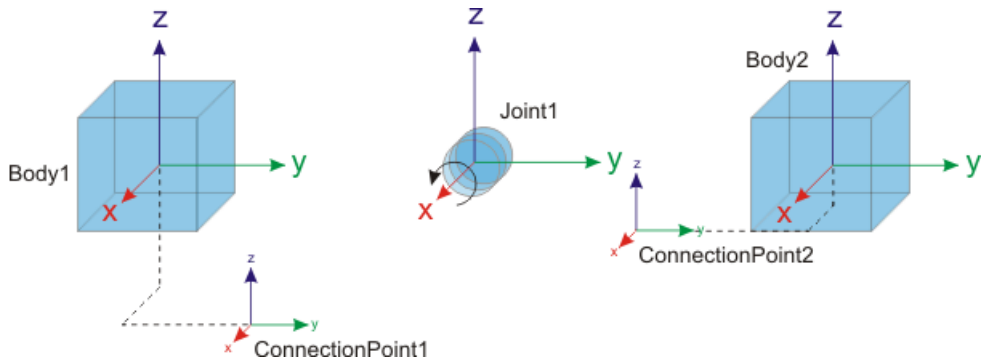
In order to make two bodies move with respect to each other, we have to connect them by joints. Joints do not have any mass or rotational inertia. They only constrain the motion of bodies. The position of a joint is indicated by its reference frame. Because the joint position and orientation is completely determined by the bodies that are connected, you do not have to specify any position or orientation parameters. These are automatically derived when you make connections.

## Connections

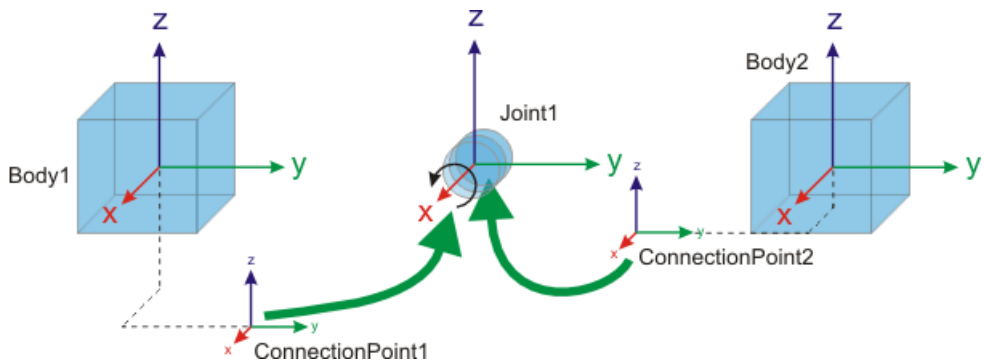
Making connections is not difficult when you understand how frames work. We will explain this with a simple example. Suppose we have two bodies and a rotational joint. The initial positions of the bodies and joints are indicated by their reference frames.



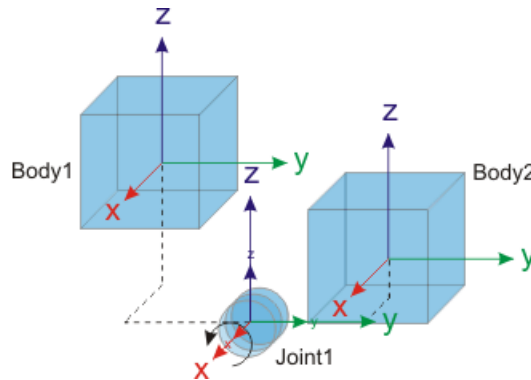
Now we have to define for each of the two bodies the offset to the joint. This can be done using connection points. A connection point is in fact a new frame with an offset from the body reference frame. As you can see, in the picture below, we have defined ConnectionPoint1 with an offset of  $[x = 1, y = 1, z = -1]$  with respect to the Body1 and we have defined ConnectionPoint2 with an offset of  $[x = 1, y = -1, z = -0.3]$  with respect to Body2.




Now the bodies and the joint can be assembled by changing the body positions in such a way that the frames of the connection points coincide with the reference frame of the joint exactly.

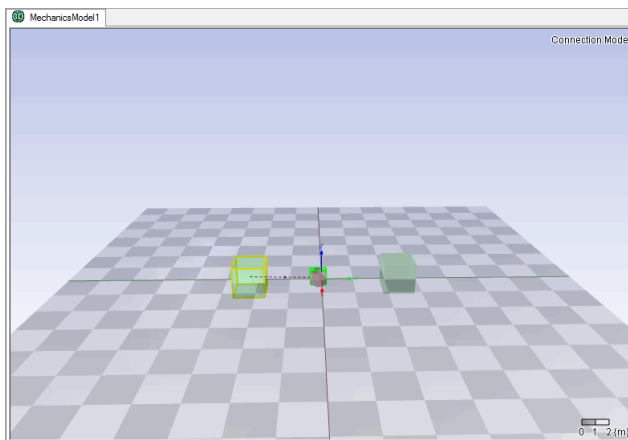


Suppose that Body1 is set as the reference body. Now the whole assembly will be moved until Body1 has its original position.



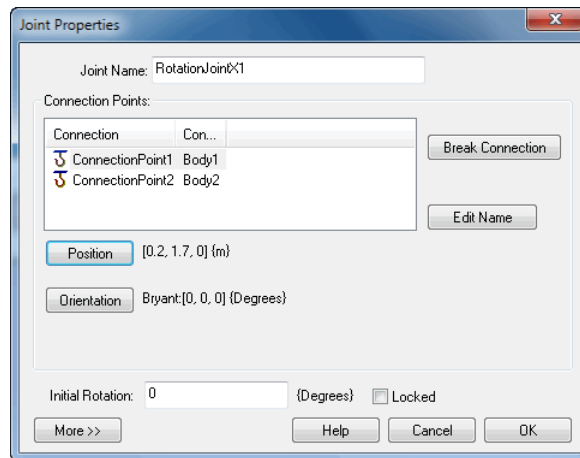
### Creating Connections

In the 3D Mechanics Editor most of the assembly of joints and bodies is automated. You simply have to make connections between joints and bodies. To make a connection you have to drag and drop bodies and a joint to the Edit window. Then change to Connection mode (  ). First click a body and then the joint it should be connected to.



The *Create Connection dialog* will pop to ask you for the location of the connection point. In the connection dialog you can set the offset (both the position as well as rotation) from the body reference frame to the connection point.





*The Joint Properties Dialog.*

After the dialog is closed the body will automatically assemble with the joint. When two bodies are assembled with a joint, you can view their constrained motions.

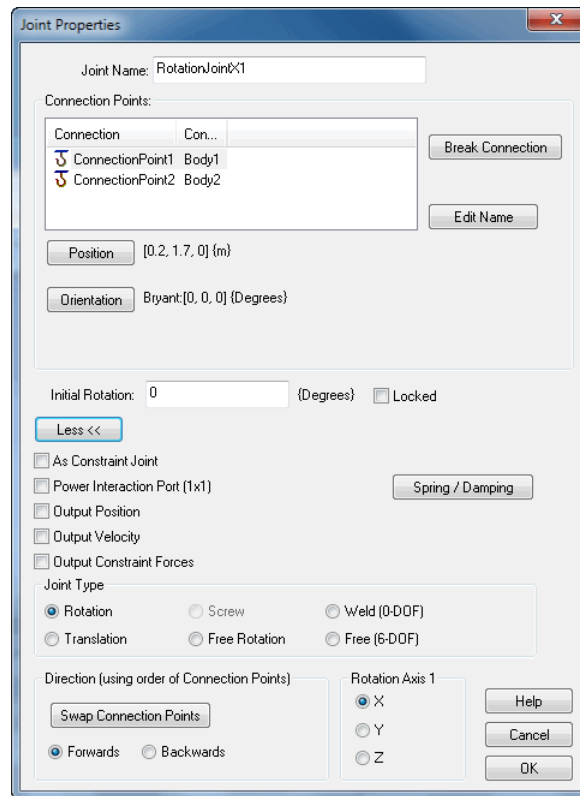
## Joint Properties

When you want to change the Connection Points after the connection has been made, you have to double clicking the joint. This will open the *Joint Properties Dialog*.

You can change the name, position, orientation, and the rotation axis of the connection points. You can also change the joint type and the initial rotation or translation of the joint. If you lock the joints, it will not move when you want to show the possible motions of the system.

## Advanced Properties

At the bottom of the Joint Properties you can click the More button to see the advanced properties.

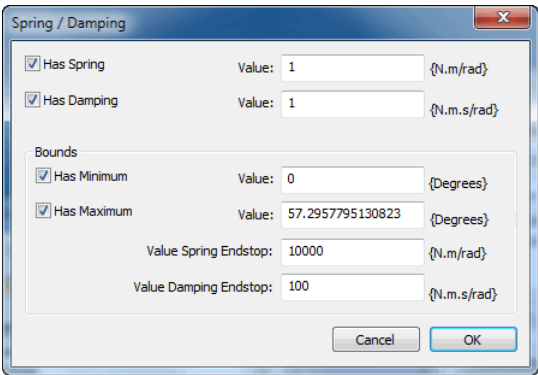


*The advanced properties of the Joint Properties Dialog.*

- As Constraint Joint: Calculate the joint using constraints.
- Power Interaction Port: add a power port to the joint to make it an actuated joint.
- Output Position: Create an output signal that gives the joint position.
- Output Velocity: Create an output signal that gives the joint velocity.
- Output Constraint Forces: Create an output signal that gives the forces and torques that act on the joint.

## Joint Restrictions

If you click the *More* button to see the *Advanced Joint Properties*, you can click the *Spring Damper* button. This will allow you to add damping to a joint or a spring and define end-stops.



- *Has Spring*: choose this option to define a spring parallel to the joint.
- *Has Damping*: select this option to define the damping (linear with the velocity).
- *Has Minimum*: set an endstop at the minimum joint rotation/extension.
- *Has Maximum*: set an endstop at the maximum joint rotation/extension.

**Joint Types**

Several types of joints are available in the library:

**Rotation Joints (Non-Actuated)**

joint	description
XYZ-Rotation	Joints which rotate around the principal axes.
Hinge XYZ-Rotation	Same as XYZ-Rotation but with a different representation.
Balljoint connection	XYZ- Balljoints with orientations of the principal axes.

**Rotation Joints (Actuated)**

joint	description
XYZ-Rotation	Joints which rotate around the principal axes.
Hinge XYZ-Rotation	Same as XYZ-Rotation but with a different representation.

**Translation Joints (Non-Actuated)**

joint	description
XYZ-Rotation	Joints which rotate around the principal axes.
Hinge XYZ-Rotation	Same as XYZ-Rotation but with a different representation.

Balljoint connection	XYZ- Balljoints with orientations of the principal axes.
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Translation Joints (Actuated)

joint	description
XYZ-Translation	Joints which rotate around the principal axes.

joint	description
XYZ-Translation	Joints which rotate around the principal axes.

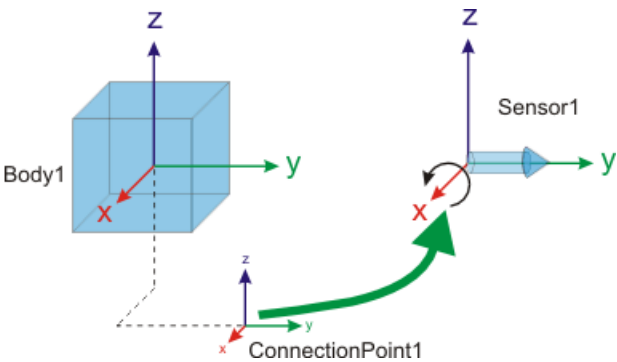
Other Joints

joint	description
Weld joint	A joint that welds two bodies together.
Free Moving Joint	Opposite of the weld joint. In practice this joint will only be used to give a body a fixed starting position with respect to another body.


Sensors are components that indicate the position or velocity of bodies as output signals.

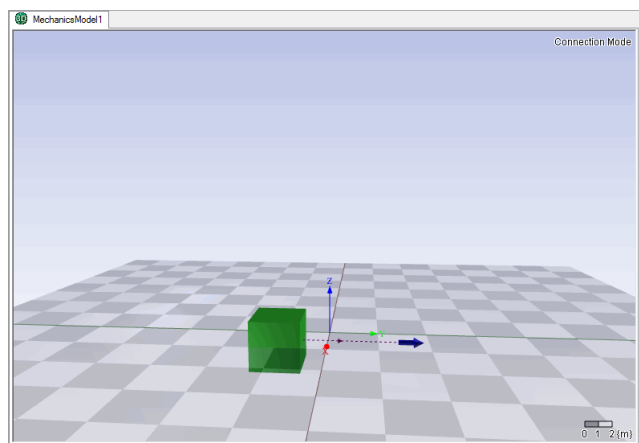
Connecting Sensors

Sensors have to be connected with bodies, just like joints.

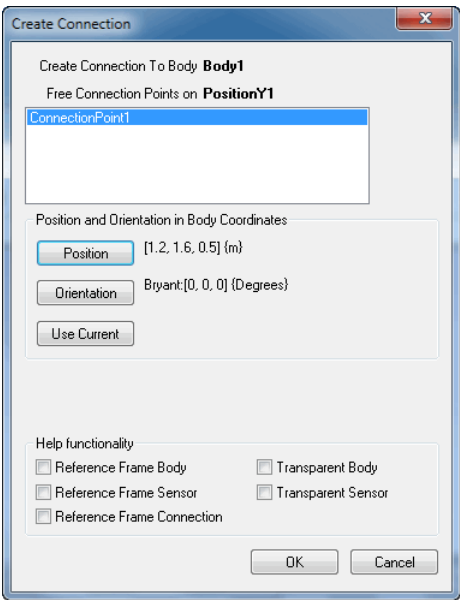


The position of the sensor is indicated by its connection point. The connection point is shown automatically when you make a connection between a body and a sensor. First change to

**Connection mode** ( , then click the body and then click the sensor.



The *Create Connection* dialog will pop up to ask you for the location of the connection point. In the connection dialog you can set the offset (both the position as well as rotation) from the body reference frame to the connection point.



**Sensor Types**

Various sensor types are available in the library.

**Position/Orientation**

**sensor**

- Position-X
- Position-Y

**output signal**

- A signal with the x-position of the body.
- A signal with the y-position of the body.

Position-Z	A signal with the z-position of the body.
Position (3x1)	A signal (size 3) with the x-, y- and z-position of the body.
H-matrix (4x4)	A 4x4 signal with the H-matrix.
Rotation (3x3)	A 3x3 signal with the rotation-matrix.

## Velocity

<b>sensor</b>	<b>output signal</b>
Velocity-X	A signal with the x-velocity of the body.
Velocity-Y	A signal with the y-velocity of the body.
Velocity-Z	A signal with the z-velocity of the body.
Velocity (3x1)	A signal (size 3) with the x-, y- and z-velocity of the body.
Omega-X	A signal with the rotational velocity in x-direction of the body.
Omega-Y	A signal with the rotational velocity in y-direction of the body.
Omega-Z	A signal with the rotational velocity in z-direction of the body.
Omega (3x1)	A signal (size 3) with all three rotational velocities.

## Acceleration

<b>sensor</b>	<b>output signal</b>
Acceleration-X	A signal with the x-acceleration of the body.
Acceleration-Y	A signal with the y-acceleration of the body.
Acceleration-Z	A signal with the z-acceleration of the body.
Acceleration (3x1)	A signal (size 3) with the x-, y- and z-acceleration of the body.
Rotational Acceleration-X	A signal with the rotational acceleration in x-direction of the body.
Rotational Acceleration-Y	A signal with the rotational acceleration in y-direction of the body.
Rotational Acceleration-Z	A signal with the rotational acceleration in z-direction of the body.
Rotational Acceleration (3x1)	A signal (size 3) with all three rotational accelerations.

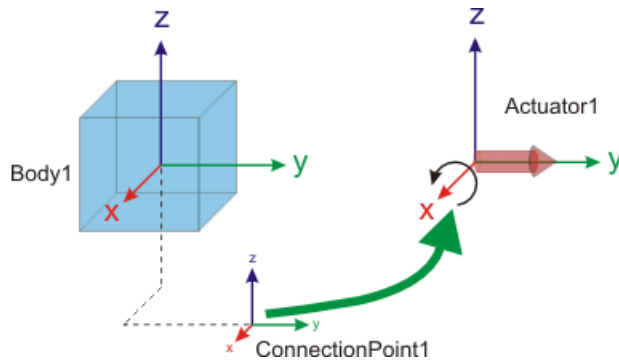
## Jacobian Matrix

This yields the Jacobian Matrix of the connected mass.


Actuators are components that impose a force or torque on bodies, where the force or torque is given by a power port or input signal.

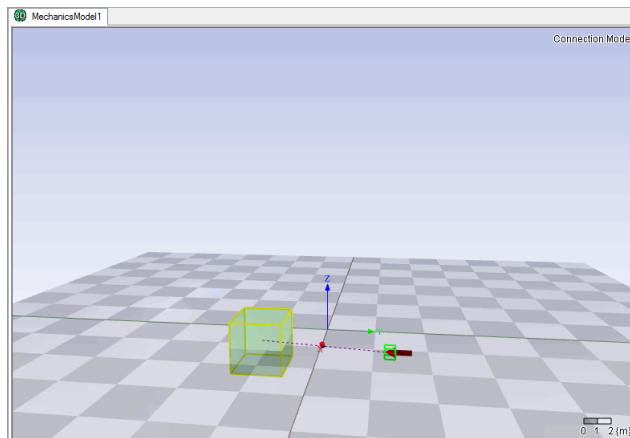
### Connecting Sensors

Actuators have to be connected with bodies, just like joints.

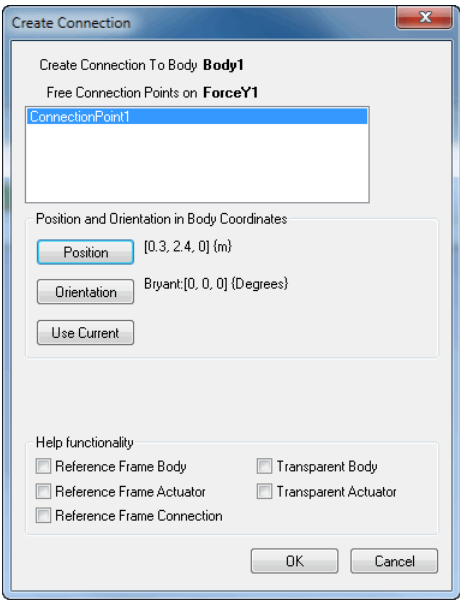


The position of the sensor is indicated by its connection point. The connection point is shown automatically when you make a connection between a body and a sensor. First change to

*Connection mode* (  ), then click the body and then click the sensor.

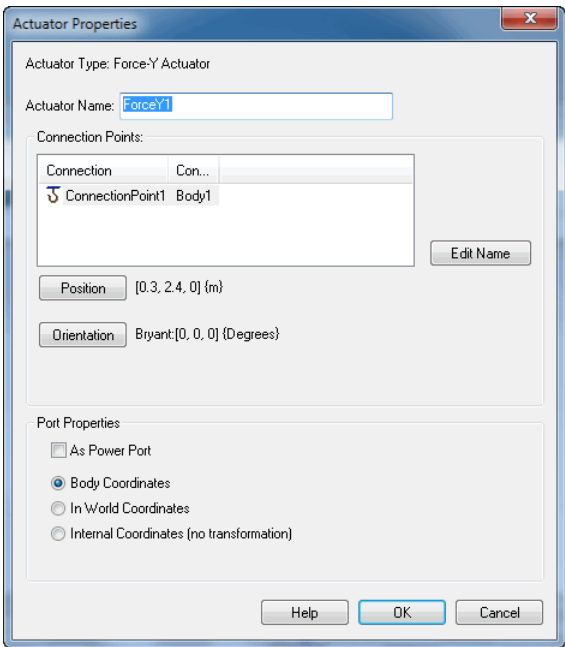


The *Create Connection dialog* will pop to ask you for the location of the connection point. In the connection dialog you can set the offset (both the position as well as rotation) from the body reference frame to the connection point.



**Local or Global Coordinates**

For each actuator, you can change its settings, by double clicking it. This will open the **Actuator Properties dialog**.

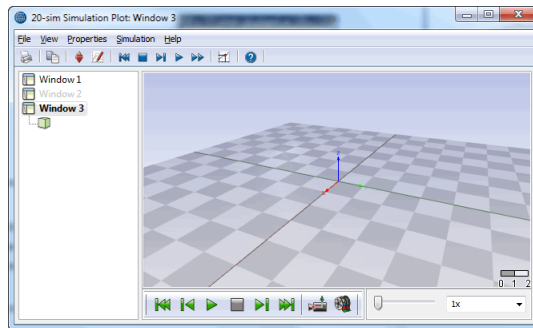




## 8.2 Animation Toolbox


### 3D Animation

In the *Simulator* choose *Tools and Animation* Toolbox and *3D Animation* to open a *3D Animation* window.






The 3D Animation window.

### Editing

- To start editing, from the *Properties* menu select *3D Properties* . This will open 3D Properties window where you build your animation.

### Running

- You can run an animation by clicking the green run button . You can also select the *Run* command from the *Replay* menu.
- At the top right of the window you see the Speed box  where you can set the replay speed. The default speed is to replay an animation at real time but you can set it to play an animation faster or slower.
- If you have multiple camera's in your animation, you can switch camera, by clicking the camera button .

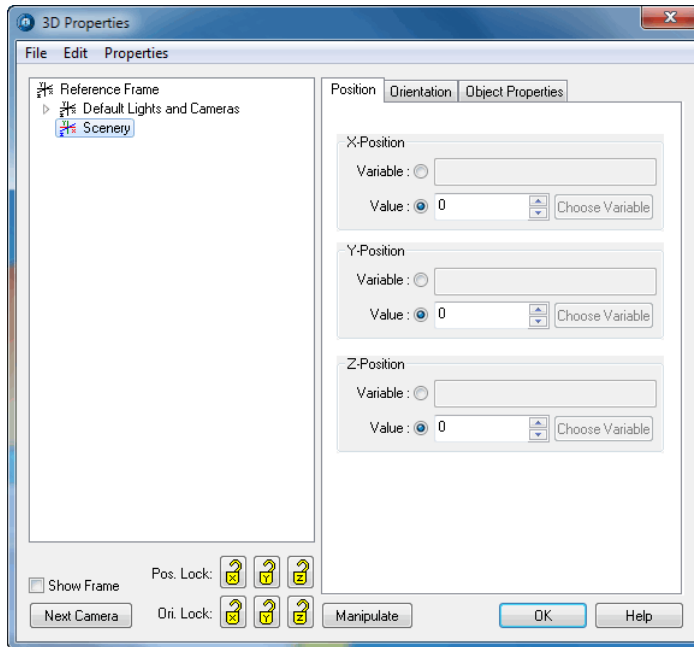
### Ray Trace

- Ray Tracing will add shadows and mirror images to a 3D Animation. From the *File* menu, select *RayTrace* to apply Ray Tracing to the current window.

### Creating Movies

- From the *File* menu select *Create Movie* to create movies from your animation.

The *3D Properties* window allows you to define the various objects that should be shown in a 3D Animation. The 3D Properties window can be opened, by *double clicking* the mouse pointer in the *Animation* window or using the *Properties* menu.



*The 3D Animation Properties window at start-up.*

## Menu

The menu of the 3D Animation Properties consists of three parts.

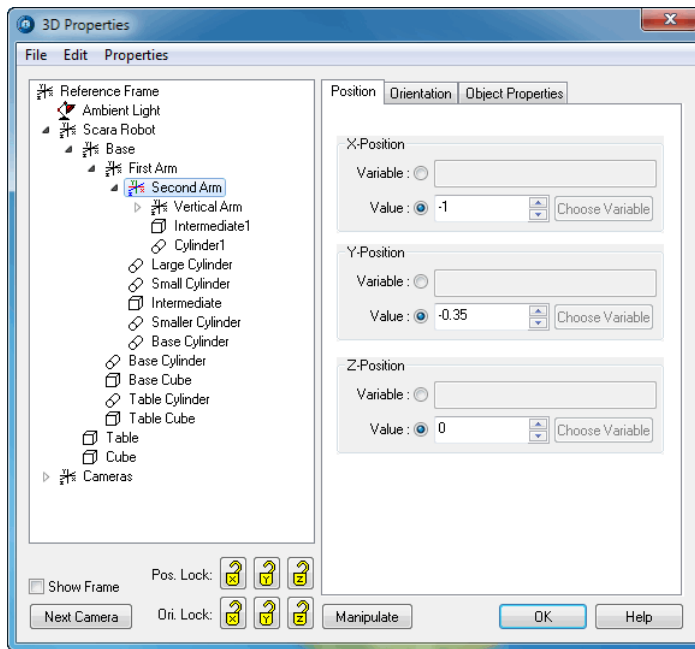
- The *File* menu allows you to store and load scenes (parts of the object tree) and create movies.
- The *Edit* menu allows you to create and edit objects.
- The *Properties* menu allows you to set the General Properties.

## Lights, Cameras and Objects

Two lights and five cameras are standard available when you start a new animation. You can delete or change these lights and cameras or add new additional lights and cameras. Inserting new objects can be done with the *Edit* menu by selecting the *Insert Object* command.

## Object Tree

The left side of the 3D Animation Properties window shows tree-like listing of the objects that are inserted. All objects are defined with respect to a reference frame. This can be done hierarchically by inserting new reference frames.



*The 3D Animation Properties window of the model ScaraRobot.emx.*

## Object Attributes

On the right side of the 3D Animation Properties window shows the attributes of a selected object (e.g. position, orientation, scaling etc.). Objects can be selected, by clicking the mouse pointer on top of the object in the objects tree.

## Show Frame

Each object has an object attached reference frame. This frame can be shown by selecting the object and clicking the **Show Frame** option. This is useful for manipulating objects.

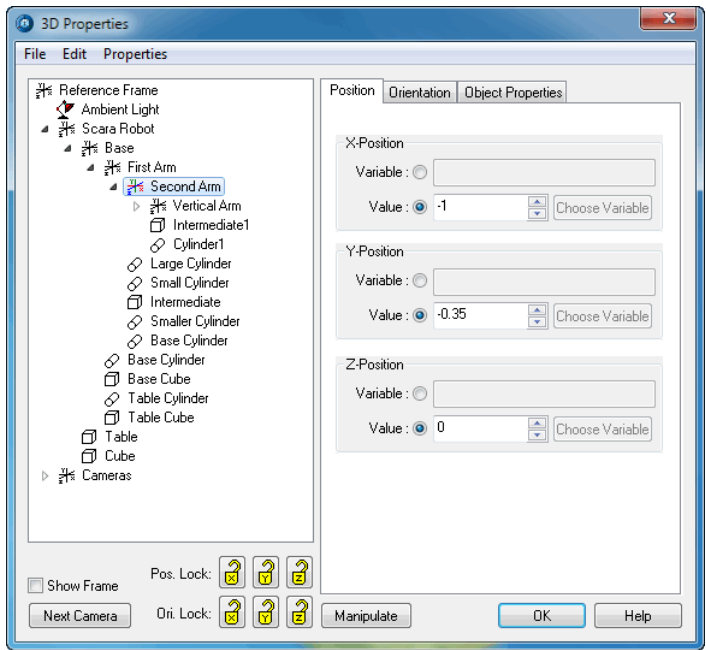
## Next Camera

Click the Next Camera button to seen the next camera view.

## Manipulate

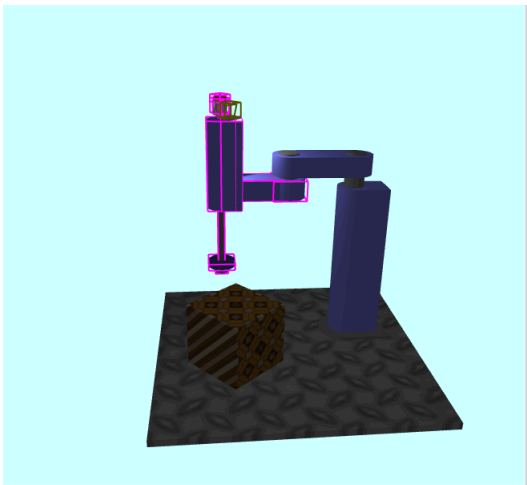
Click the Manipulate button to move an object with use of your mouse.

An object can be selected by pointing with the mouse in the object tree.



Select an object in the 3D Animation Properties window.

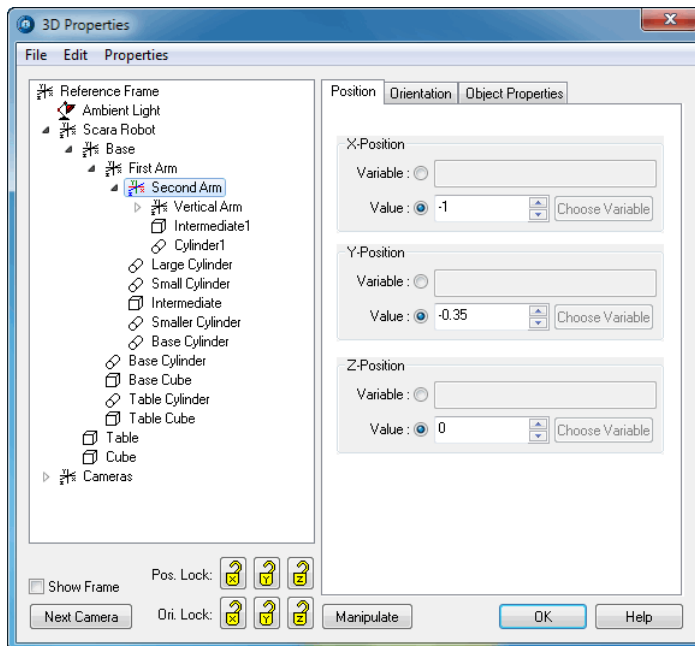
This selection is also shown in the 3D Animation window as a *pink box* around the object.



Indicating the selected object.

It is also possible to *select* an object with the mouse by *clicking* in the 3D Animation window. The selection will automatically jump to the object in the tree of the *3D Animation Properties* window.

To move an object, you have select it.



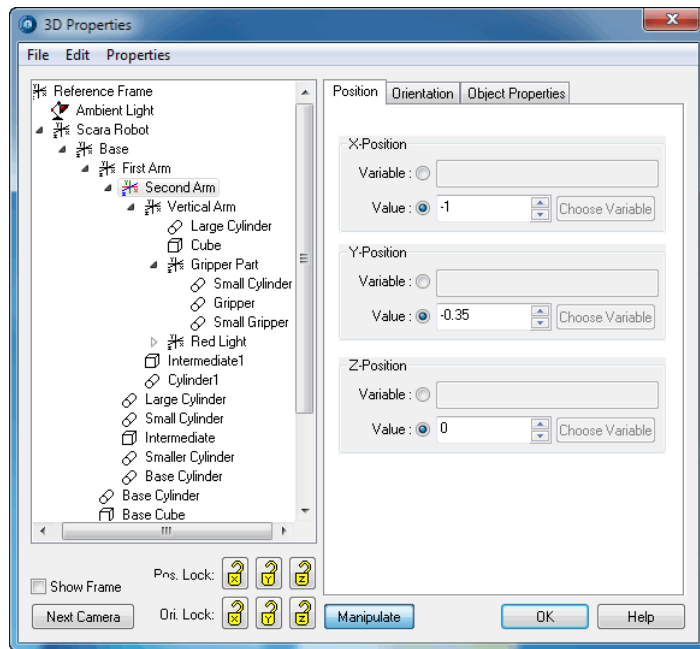
Select an object in the 3D Animation Properties window.

## Attributes

The right side of the 3D Animation Properties window shows the attributes of a selected object (e.g. position, orientation, scaling etc.). You can change the position or orientation to move an object.

## Manipulate

You can move an object directly by pushing the *Manipulate* button.



*Manipulate an object directly.*

A set of *locks* will be shown below the Manipulate button. You can use them to lock one or more directions and orientations. After this you must put the 3D Animation window on front (click on it with the mouse) and select one of the following keys:

Keys	Action
right arrow	move right (positive x-direction)
left arrow	move left (negative x-direction)
up arrow	move up (positive z-direction)
down arrow	move down (negative z-direction)
Ctrl + up arrow	move forward (positive y-direction)
Ctrl + down arrow	move backward (negative y-direction)
Alt+ right arrow	yaw right (positive z-axis rotation)
Alt+ left arrow	yaw left (negative z-axis rotation)
Alt+ up arrow	roll forward (negative x-axis rotation)
Alt + down arrow	roll back (positive x-axis rotation)
Ctrl+ Alt + right arrow	pitch right (positive y-axis rotation)
Ctrl+ Alt + left arrow	pitch left (negative y-axis rotation)
Keys above + Shift	Smaller steps (more accurate)

Ctrl + A

Next Camera

In the 3D Animation Properties you can load and store scenes. Scenes are simply part of an object tree or a complete object tree. This option can be used to obtain scenes from other experiments or to create pre-defined environments.

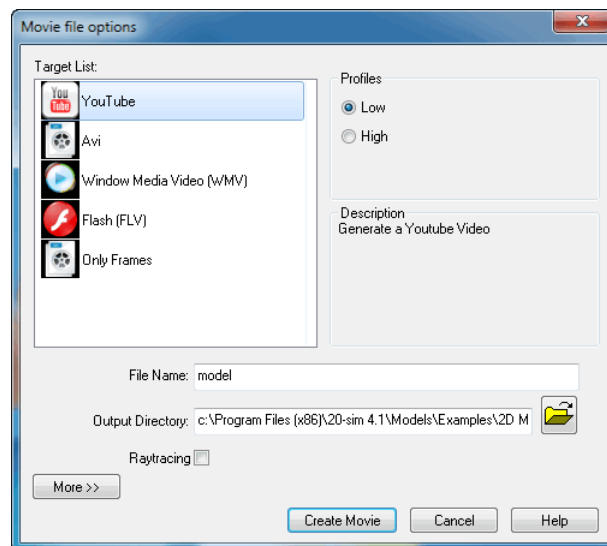
### Save Scene

The *Save Scene* command of the *File* menu, allows you to save a scene on file. Only the selected object and all object below will be saved.

### Load Scene

The *Load Scene* command of the *File* menu, allows you to open a scene from file and insert it under the selected object of the object tree.

With a few mouse clicks you can create movies from an animation. *Right click* on the 3D animation window and select *Create Movie*.



### Target List

You can create movies for various purposes:

- **YouTube:** Movies in mpg-format for placement on YouTube.
- **Avi:** Movies in avi format for use in movie editing software.
- **Windows Media Video:** Movies for the use in Microsoft programs (e.g. Powerpoint).
- **Flash:** Movies in flv format for the use on Internet sites.
- **Only Frames:** For the use in advanced movie editing programs that can handle collections of pictures

## Profiles

You can create movies with three profiles (low, medium, high). The corresponding sizes are shown in the table below.

	low	medium	high
YouTube	640 * 480	-	1280*720
Avi	640 * 480	1024*768	1920*1080
Windows Media Video	640 * 480	1024*768	1920*1080
Flash	640 * 360	1024*576	-
Only Frames	640 * 480	1024*768	1920*1080

Ray tracing will add shadows and mirror images to a 3D Animation. However ray tracing cost a lot of processing power. If you select the option Ray Tracing, the quality of your movie will be improved, but the time to create it will increase tremendously.

## More

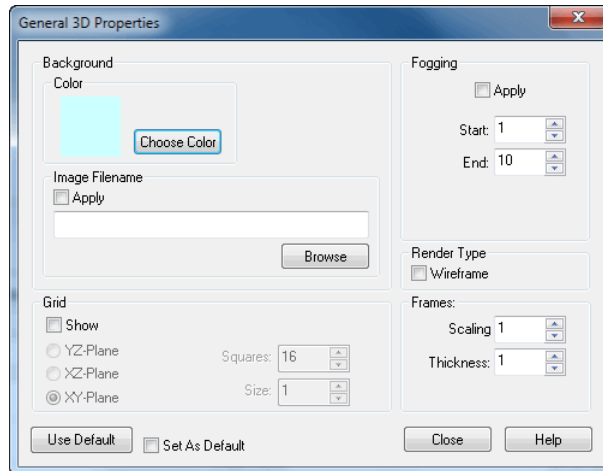
Choose the *More* button if the standard profiles are not up to your demands. You can set the size of a movie, the frame rate and speed up or slow down the speed.

## Create Movie

Click the *Create Movie* button to create a movie. The movie will be stored in the output directory that you have specified using the filename that you have given.

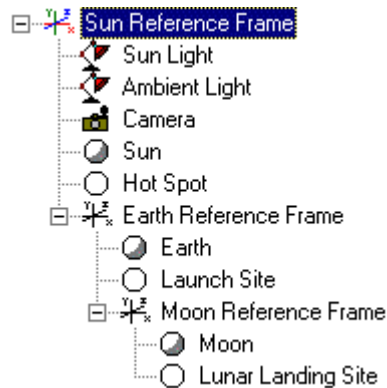


Using the *General Properties* command of the 3D Properties window helps you to select several options.



- **Background Color:** Change the background color to any desired color you like.
- **Background Image:** Use a bitmap image for the background.
- **Wireframe:** You can choose to show the animation as Wireframe.
- **Fogging:** Fog in any desired color can be added to the animation. The fog is minimal at a start plane and maximal at an end plane. You can set the distance of these planes.
- **Grid:** You can choose to show a grid.
- **Frames:** Set the frame scaling and thickness.

All objects in a 3D Animation are defined with respect to the **top reference frame**. The top reference frame is the reference frame on top of the objects tree. If you have multiple objects that move relative to the top reference frame but have a fixed position and orientation with respect to each other, it is useful to introduce an **additional reference frame**. Define all the objects with fixed position and orientation with respect to an additional reference frame and give this frame a movement with respect to the top reference frame.



*Relative reference frames.*

In the objects tree frame **hierarchy** is shown by **indentation**. In the example above, the Earth Reference Frame describes the earth motion with respect to the Sun Reference frame. The Moon Reference Frame describes the moon motion with respect to the Earth Reference Frame.

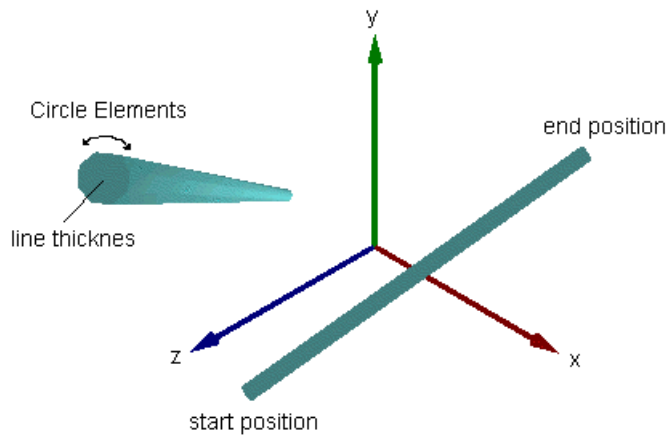
Each Reference Frame has a specific position, orientation and scaling. The scaling is defined with respect to the frame one level higher in the hierarchy. In the example above, the sphere and circle describing the Earth and the Launch Site can directly be copied to form the Moon and the Lunar Landing Site. Only the scaling of the Moon Reference Frame has to be set to correct values.

### Properties (Specific)

- *Override Group Color*: You can choose to give all objects that are defined in a frame the same color.

### Properties (General)

- position
- orientation
- scaling
- duplication

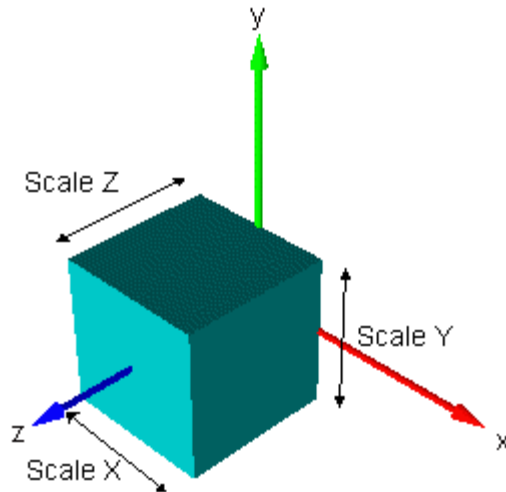


### Properties (Specific)

You can set the start position and end position of the line, enter the line thickness and set the number of circle elements.

### Properties (General)

- color
- mesh
- texture
- material
- duplication

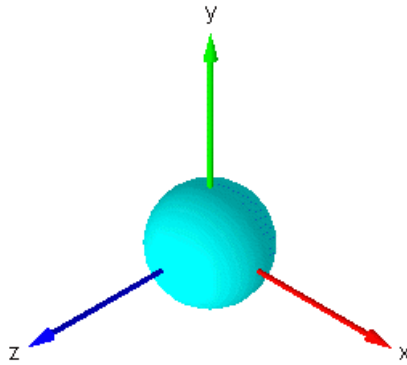


### Properties (Specific)

You can set the position of the origin and the rib length and choose to show the inside.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication

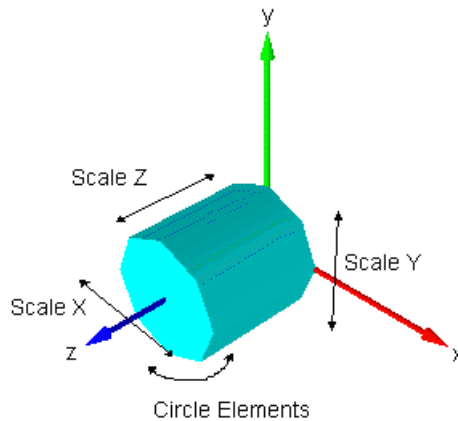


### Properties (Specific)

You can choose to **show the inside and outside**. The number of segments that are used to draw the circle is fixed.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication

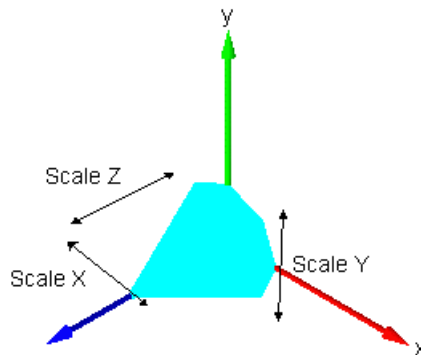


### Properties (Specific)

You can set the position of the **origin**, choose to **show the inside and outside**, set the number of circle elements. A cylinder can be shown with **open or closed sides**.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication

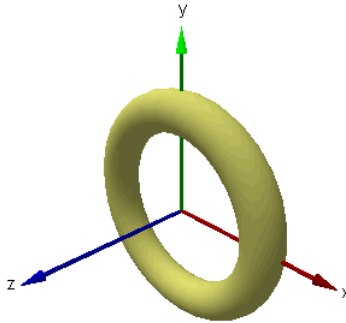


### Properties (Specific)

You can set the number of circle elements and choose to show the cone with **an open or closed side**.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication



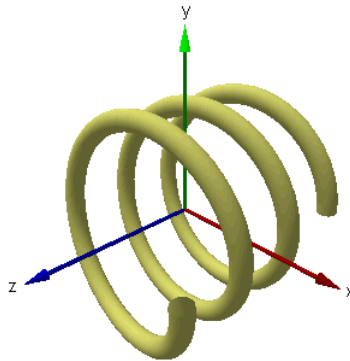
### Properties (Specific)

A Torus has some specific options:

- The *Torus Radius* denotes the length from the origin to the center of the tube.
- The *Tube Radius* denotes the tub thickness.
- With the *Number of Segments* you can set the total number of segments for one revolution.
- The *Points Per Segment* are the number of circle elements for each segment.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication



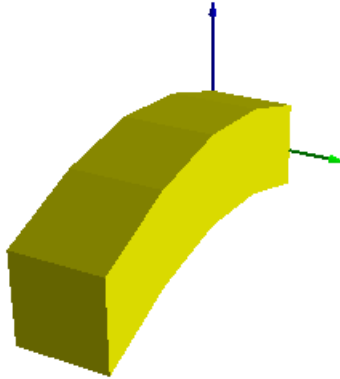
### Properties (Specific)

- The *Height* is the the length of the spiral.
- The *Spiral Radius* is the length from origin to the center of the tube.
- The *Tube Radius* denotes the tub thickness.
- The *Number of Turns* is the number of revolutions from bottom to top of the spiral. This may be a non-integer value.
- The *Number of Segments* is the total number of segments from bottom to the top of the spiral.
- The *Points Per Segment* are the number of circle elements for each segment.
- You can set the position of the origin.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication





### Properties (Specific)

- *Dimensions*: You can choose the *Segment Length*, the *Width* and *Height* of the beam.
- *Variable*: The beam offset (in the direction of the height) is given by a vector. The number of segments is equal to the number of vector elements. You can choose the vector as a variable from your model.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- material
- duplication

You can import object from files, using the 3D-files object. As soon as you insert a 3D-files object, 20-sim will open a file browser. Three formats are supported

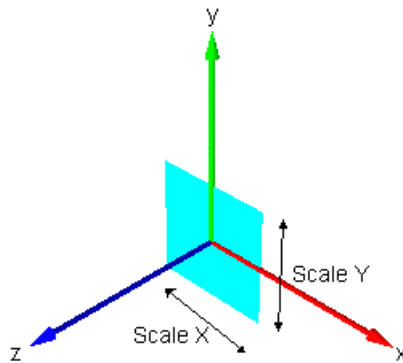
- **STL-files (\*.stl):** The STL file format or stereolithography format is another widely accepted interchange format between CAD packages.
- **DXF-files (\*.dxf):** This is AutoCAD's drawing interchange format. The DXF file format was originally designed by AutoDesk® to represent 3D models built with AutoCAD®. Now they are generally accepted as an interchange format between CAD packages.
- **Lightwave Object files (\*.lwo):** LightWave is a software package used for rendering 3D images, both animated and static.

### Properties (Specific)

- Use the Browse button to load another file.
- Set the **Override Color** check box to give the object any desired color.
- You can set the position of the **origin**.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication

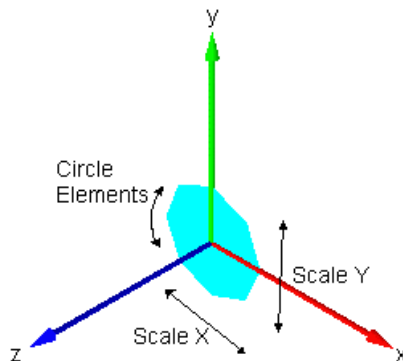


### Properties (Specific)

- You can set the position of the *origin*.

### Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication



### Properties (Specific)

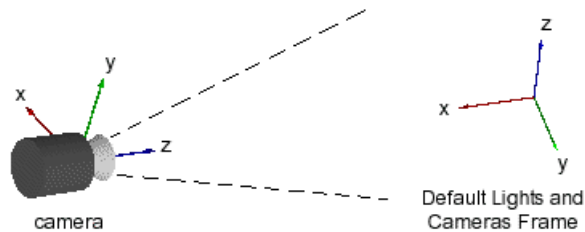
- You can set the number of circle elements.

## Properties (General)

- position
- orientation
- scaling
- color
- mesh
- texture
- material
- duplication

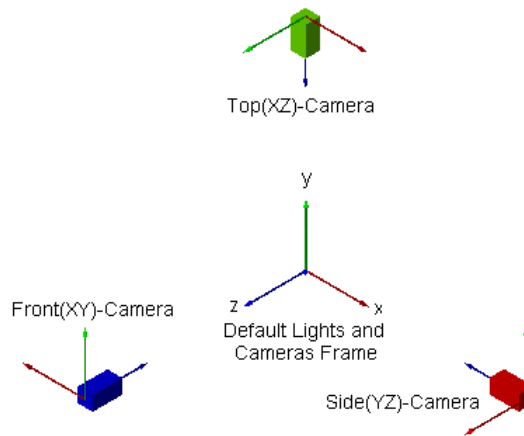
All objects in a 3D Animation are defined with respect to the *Default Lights and Cameras* frame. This frame coincides with the top *Reference Frame*. When you start up a 3D animation 5 default cameras are available showing several views of the origin of this frame.

Two cameras show the *Default Lights and Cameras* frame from a position of  $x = 5$ ,  $y = 5$  and  $z = 10$ . The cameras are pointed to the center of origin of the frame. The *Camera Looking At Origin* will keep looking at the origin, even if its position is changed. The *Perspective Camera* will not keep looking at the origin but keep its original orientation when its position is changed.



*The Camera Looking At Origin and Perspective Camera.*

Three *Front* cameras are positioned on top of each of the axes of the *Default Lights and Cameras* frame. The front cameras do not show perspective. I.e. they can be used for 2D-Animation.



## Properties (Specific)

### Camera Properties

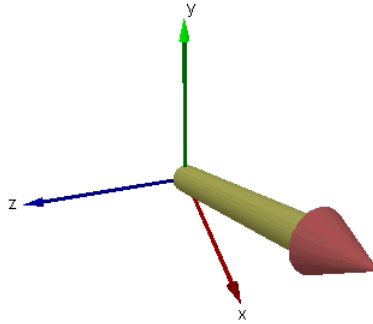
- *Plane Distance*: A camera only shows objects that lie between a front plane and a back plane. You can set the distance of these planes (seen from the camera).
- *Projection*: You can show all objects in perspective (objects further away look smaller) or Orthographic (objects further away are shown equally large). You can choose to show right hand frames or left-hand frames.
- Use the slider bar to set the *Zooming*.

### LookAtProperties

- When you enable the *Look at Position*, the camera will always look at a specific position, regardless the position of the camera itself
- You can make the look at position *static* or connect it to *variables* of your model.
- Use the *Always Look up Vector* to let the camera have a fixed angle of view.

### Properties (General)

- position
- orientation



### Properties (Specific)

The Vector object is a combination of a Cylinder object and a Cone object. The length of the Vector can be constant or determined by the value of the variable, the offset and the multiplication factor. You can set the vector diameter, the cone diameter and the cone height and set the number of circle elements. The color of the Cone and the Cylinder can be specified separately by the two color property pages. The first page is for the Cylinder and the second page is for the Cone.

### Properties (General)

- position
- orientation
- mesh
- texture
- material
- duplication

An Ambient Light source illuminates everything with a predefined color, regardless of the orientation, position, and surface characteristics of the objects available. It is constructed by making a spot light shine everywhere.

A Spotlight emits a cone of light of a certain color. The cone starts at a given position and the direction is given by the orientation. Only objects within the cone are illuminated.

### Color

- Ambient color: This is the main color of point light. For a spot light this option is turned off.
- Diffuse color: This is color of point light when it shines on matt surfaces.
- Specular color: This is color of point light when it is reflected in shiny surfaces.

### Direction

You can select the shape of the light bundle.

- **Parallel:** Select this option to make the light a parallel bundle (e.g. the sun light). For a spot light this option is turned off.
- **Spot Exponent [Wide-Narrow]:** Select this option to make the light intensity equal in all directions (Wide) or more intensive in the center beam of the spot light (Narrow)
- **Spot Angle [0..90]:** Select the angle of the cone from 0 degrees (very thin bundle) to 90 degrees (light in all directions).

### Attenuation

Light attenuation defines how the intensity of the light weakens as it travels away from the source. The attenuation is computed based on the following formula:

$$att = \frac{1}{k_0 + k_1d + k_2d^2}$$

where  $k_0$  is the constant attenuation,  $k_1$  is the linear attenuation,  $k_2$  is the quadratic attenuation and  $d$  is the distance from the light's position to an object.

A *Directional Light* illuminate all objects with light of equal intensity, as if it were at an infinite distance from the objects. The directional source is commonly used to simulate distant light sources, such as the sun. It is constructed by making a spot light shine in parallel bundles.

Most objects in a 2D-sim Animation can be positioned with respect to the frame one level up in the object tree. This position can be fixed (using fixed values) or change (using model variables) during simulation.

All objects in a 3D Animation have an orientation. This orientation can be made visible by showing the object attached reference frame. This orientation can be fixed (using fixed values) or changed (using model variables) during simulation.

The orientation of an object is defined as the transformation of the frame one level up the object tree {A} to the object attached reference frame {B}. Several methods can be used in 2D-sim to define this transformation.

### DirectX

Using the DirectX method you have to specify the Y-axis and Z-axis of the frame {B} in coordinates of frame {A}.

### Bryant angles

Start with the frame {B} coincident with a known frame {A}. First rotate {B} about the X-axis of {B} by an angle of X (rad), then rotate about the Y-axis of {B} by an angle of Y (rad) and then rotate {B} about the Z-axis of {B} by an angle of Z (rad). **Note:** Bryant angles are also known as X-Y-Z Euler angles or Cardan angles.

### Z-X-Z-Euler

Start with the frame {B} coincident with a known frame {A}. First rotate {B} about the Z-axis of {B} by an angle of X (rad), then rotate about the X-axis of {B} by an angle of Y (rad) and then rotate {B} about the Z-axis of {B} by an angle of Z (rad).

## Euler Parameters

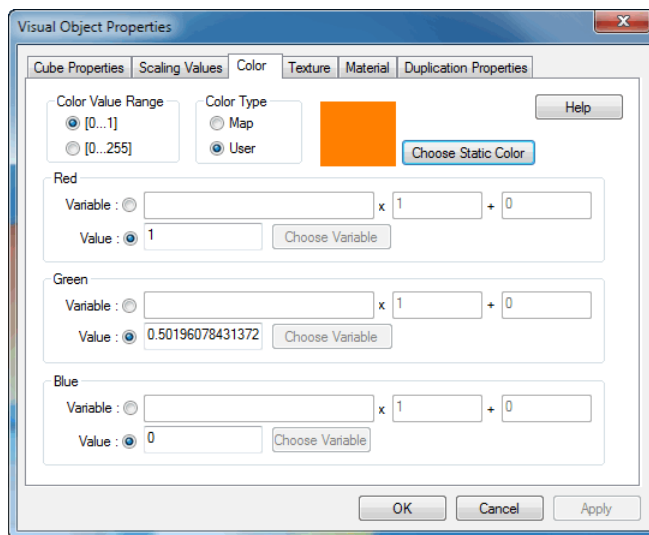
Start with a frame  $\{A\}$ . Rotate this frame around a vector  $K [X,Y,Z]^T$  about an angle  $\theta$  to get to the frame  $\{B\}$ .

Most objects in a 20-sim Animation can be scaled in size. This scaling can be fixed (using fixed values) or change (using model variables) during simulation.

Most objects in a 20-sim Animation can be shown with a preset color. The colors can be user defined or defined with respect to a color map.

## User Defined

The additive primary colors are red (R), green (G), and blue (B). By mixing these colors in different percentages, any other color can be created. When blue and green are mixed, the resulting color is cyan. When blue and red are mixed, the resulting color is magenta. If all three primary colors are mixed together, the resulting color is white.



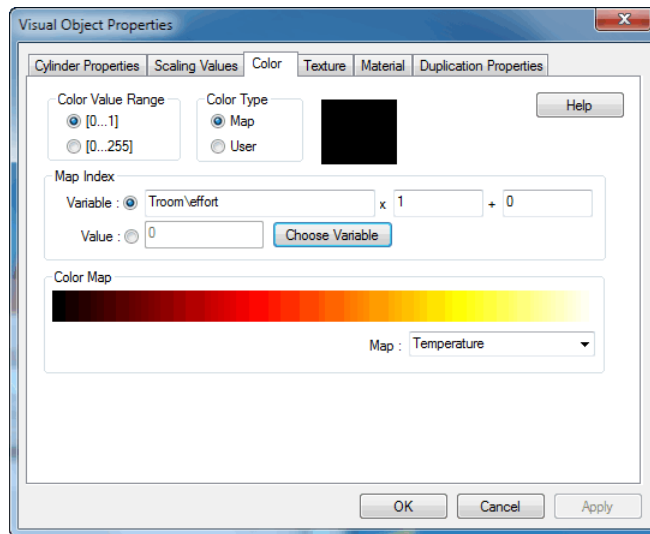
*The color tab.*

Color ranges can be set from 0 to 1 or 0 to 255. Constant values or model variables can be chosen for each primary color. Use the multiplication and addition terms for scaling and offset.

## Color Map

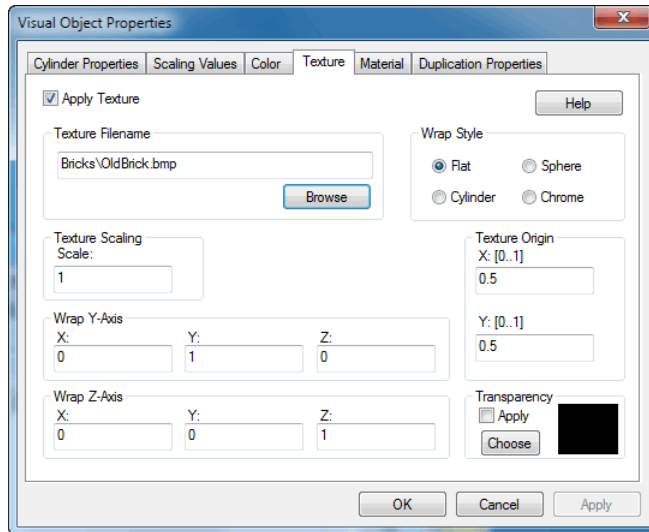
The color that is chosen is defined by a color map. Color ranges can be set from 0 to 1 or 0 to 255. A constant value or a model variable can be chosen. Use the multiplication and addition term for scaling and offset.





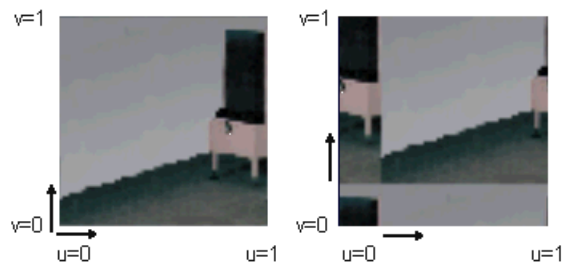
The rendering option defined in the General Properties can be overridden for each object. The options are: WireFrame, Unlit Flat, Flat and Gouraud.

Using the *Texture* attribute, you can wrap a bitmap file around an object. Using the browse button, you can easily select the desired bitmap file (bmp, jpg, gif, tif, etc.). Using the *transparency* option you can select a color in the bitmap that should be transparent.



## Texture Origin

A texture is defined in generalized coordinates (u,v). The bottom right of the texture has coordinates (0,0) and the top left (1,1). The offset parameters define how much offset is used to project the bitmap. This is shown in the figure below. At the left an offset of (0,0) is shown and at the right an offset (0.2,0.2) is shown.



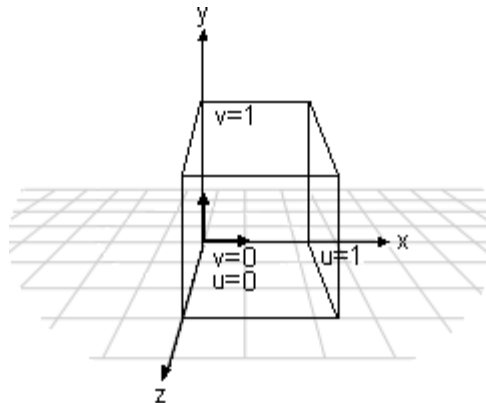
Depending on the type of texture wrapping (Flat, Cylinder, Sphere or Chrome) the three wrapping vectors () have a different meaning. This is explained in the next sections. To facilitate the explanation in the pictures below the origin vector equals (0,0,0), the Y-vector equals (0,1,0) and the Z-vector equals (0,0,1).

## Vectors

Using three vectors (Origin, Y-Axis and Z-Axis) and Offset parameters (X, Y) you can define how the texture should be wrapped around an object. The vectors are defined with reference to the object attached reference frame. The object attached reference frame can be made visible by selecting Show Frame. The vectors use generalized coordinates. I.e. the length, width and height of the object are defined as 1 and the vectors are scaled accordingly.

## Flat

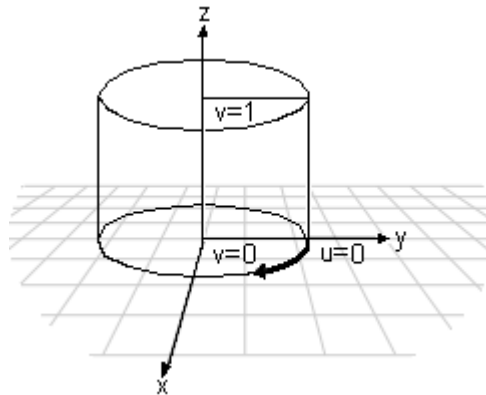
The flat wrap conforms to the faces of an object as if the texture were a piece of rubber that was stretched over the object. For a flat texture wrap, the effects of the various vectors are shown in the following illustration.



- The *Origin* vector defines the base from which the texture wrapping is performed.
- The *Y-vector* equals the v axis of the texture wrap.
- The *Z-vector* is always perpendicular to the texture wrap.

## Cylindrical

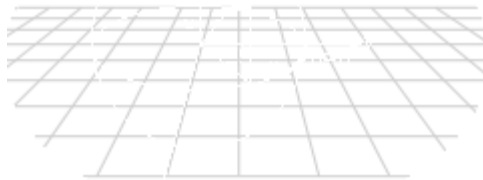
The cylindrical wrap treats the texture as if it were a piece of paper that is wrapped around a cylinder so that the left edge is joined to the right edge. The object is then placed in the middle of the cylinder and the texture is deformed inward onto the surface of the object. For a cylindrical texture wrap, the effects of the various vectors are shown in the following illustration.



- The *Origin* vector defines the base from which the texture wrapping is performed.
- The *Y-vector* specifies the point on the outside of the cylinder where  $u$  equals 0.
- The *Z-vector* specifies the axis of the cylinder.

### Spherical

For a spherical wrap, the  $u$ -coordinate is derived from the angle that the vector  $[x \ y \ 0]$  makes with the  $x$ -axis (as in the cylindrical map) and the  $v$ -coordinate from the angle that the vector  $[x \ y \ z]$  makes with the  $z$ -axis. Note that this mapping causes distortion of the texture at the  $z$ -axis.



- The *Origin* vector defines the base from which the texture wrapping is performed.
- The *Y-vector* specifies the point on the outside of the sphere where  $u$  equals 0.
- The *Z-vector* specifies the point on the outside of the sphere where  $v$  equals 0.

### Chrome

A chrome wrap allocates texture coordinates so that the texture appears to be reflected onto the objects. The chrome wrap takes the reference frame position and uses the vertex normals in the mesh to calculate reflected vectors. The texture  $u$ - and  $v$ -coordinates are then calculated from the intersection of these reflected vectors with an imaginary sphere that surrounds the mesh. This gives the effect of the mesh reflecting whatever is wrapped on the sphere.

A material defines how a surface reflects light. A material has two components: an emissive property (background color) and a specular property (reflected light), whose brightness is determined by a power setting.

### Specular Highlights

The value of the power determines the sharpness of the reflected highlights, with a value of 5 giving a metallic appearance and higher values giving a more plastic appearance.

### Emissive Color

The emissive color is the background color of the object. If you choose the color white the object looks like a light bulb. If you choose the color black the object does not radiate any background color.

Some objects in a 20-sim Animation can be shown as a closed shape (sides closed) or open shape (sides open).

All objects in a 20-sim Animation are built out of a set of planar surface elements. Curved objects have to be built up out of a lot of surface elements to give the impression of a smooth surface. For some objects you can set the amount of surface elements used to create circular surfaces.

The Animation Engine in 20-sim is based on the Microsoft® Direct3D. Direct3D uses the following formula to normalize the distance from a light source to the object surface into a value from 0.0 to 1.0, inclusive:

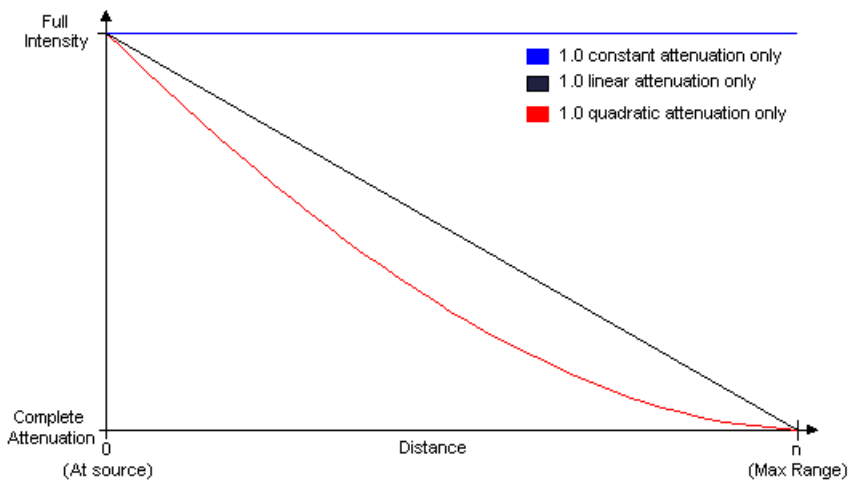
$$D_n = \frac{R - D}{R}$$

In the preceding formula,  $D_n$  is the normalized distance,  $R$  is the light's range, and  $D$  is the distance, in world space, from the light source to the object surface. A normalized distance is 1.0 at the light's source, and 0.0 at the light's range.

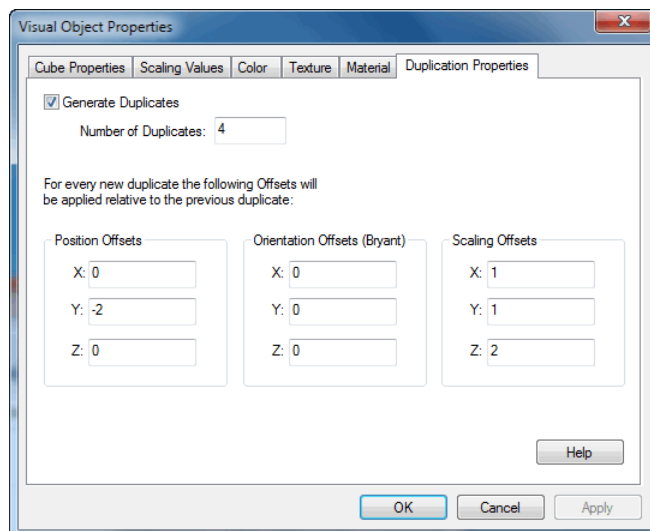
With the normalized distance in hand, Direct3D then applies the following formula to calculate light attenuation over distance for point lights and spotlights:

$$A = \text{Attenuation}_{\text{constant}} + D_n \cdot \text{Attenuation}_{\text{linear}} + D_n^2 \cdot \text{Attenuation}_{\text{quadratic}}$$

In this attenuation formula,  $A$  is the calculated total attenuation and  $D_n$  is the normalized distance from the light source to the object. The constant, linear and quadratic attenuation factors act as coefficients in the formula. You can produce a wide variety of attenuation curves by making simple adjustments to them. Most applications will set the linear attenuation factor to 1.0 and set the remaining factors to 0.0 to produce a light that steadily falls off over distance. Similarly, you could apply a constant attenuation factor of 1.0 by itself to make a light that doesn't attenuate (but will still be limited by range). The following illustration shows the three most common attenuation curves.



All objects in a 20-sim Animation can be duplicated. This property is useful when drawing a lot of the same objects.

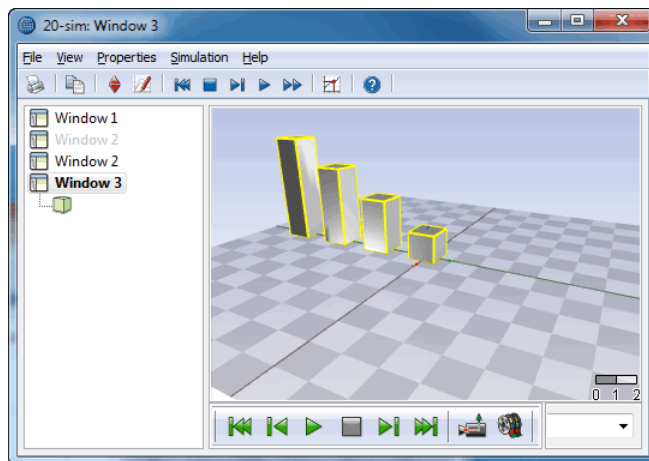


You can choose several options:

- **Number of Duplicates:** Select the number of duplicates of the object.

- **Position Offsets:** Select the position offset of the first duplicate from the original object. This offset is repeated for every next duplicate.
- **Orientation Offset:** Select the orientation offset of the first duplicate from the original object. This offset is repeated for every next duplicate.
- **Scaling Offset:** Select the scaling of the first duplicate compared to the original object. This scaling is repeated for every next duplicate.

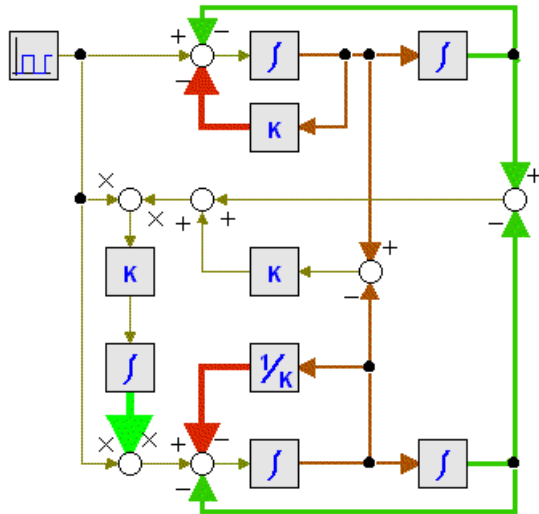
The example below shows a cube that is duplicated according to the specifications given in the figure above. As shown, the first duplicate is a little larger than the original object. The second duplicate is a little larger than the first duplicate etc.



## Graph Animation

To Animate the results of a simulation in the graphical model select the *Graph Animation* command from the *Tools* menu (Simulator). During simulation, the thickness and color of bonds and signals will correspond with the values they carry.

The color of a bond or signal always corresponds with the sign, red for negative values and green for positive values. The thickness of signals corresponds with the value. For signals that is obvious but for bonds or connections carry two variables: effort and flow (also know as across and through). For bonds and connections you can choose to let the thickness correspond with the effort, flow or power ( $\text{effort} \times \text{flow}$ ), depending on the Animation command that was chosen.



You can start Animation in the Simulator:

1. Run a simulation until you are satisfied with the results.
2. From the **Tools** menu, select **Animation Toolbox** then **Graph Animation**.
3. A menu pops up. Choose the options you like and click **OK** to start Animation.



## Graph Animation Menu



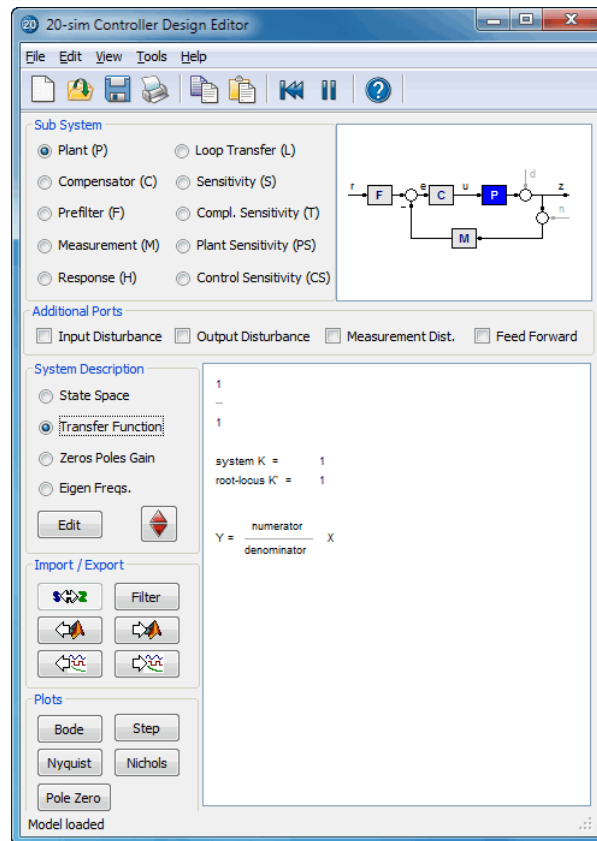
### Items

- *Animation Kind*: For signals, the thickness always corresponds with their value. For bonds and connections you can choose. Select here to what the thickness of bonds and connections should represent: effort, flow or power (effort\*flow).
- *Animation Ranges*: The thickness of bonds and signals can vary from 1 to 5 pixels. Select here the range that should correspond with a thickness of 5 pixels.

## 8.3 Control Toolbox

### Controller Design Editor

The 20-sim *Controller Design Editor* allows you to enter or edit linear time-invariant models of a plant with control loop. The control loop is separated in a compensator, prefilter and measurement. You can open the *Controller Design Editor* from the *Tools* menu of the 20-sim Editor or by clicking Go Down on a ControlledLinearSystem model that was inserted in the Editor.



## Sub System

- You can choose to show a single element in the loop:
  - Plant (P), Compensator (C), Prefilter (F) or Measurement (M)**
- or view the response of the system:
  - Response (H), Loop Transfer (L), Sensitivity (S), Compl. Sensitivity (T), Plant Sensitivity (PS) or Control Sensitivity (CS).**


The corresponding transfer function is shown in the editor.

## Additional Ports






Select one of the radio buttons **Input Disturbance**, **Output Disturbance**, **Measurement Dist.** or **Feedforward**. The first three options allow you to use external disturbance in your model. The last option allows you to use an external feedforward controller (e.g. a B-Spline network). The selected inputs are shown in the picture.

## System Description

- Pressing the **Edit** button will open a dialog for editing the linear system. Each description (State Space, Transfer Function, Zeros Poles Gain or Eigen Frequency) has a special dialog and can be used to specify continuous-time and discrete-time systems.

- In the 20-sim Simulator, out of an existing (non-linear) model a symbolic linear-system can be derived by means of linearization. This means that the relevant model parameters are preserved in the Linear System and the parameters button  can be used to change parameters.

## Import/Export

- Pressing the **s<->z** button  will transform a continuous-time linear system into a discrete-time linear system and back.
- Pressing the **Filter** button opens the Filter Editor, where a filter can be designed. This filter can then be combined with the current linear system or replace the current linear system. If the linear system is a discrete-time system, the designed analog filter is automatically transferred into its digital equivalent.
- Pressing the **From Matlab** button  and the **To Matlab** button  allows for an instant exchange of the linear system with the Matlab workspace. Information is transferred numerically (no parameter relations are preserved)
- The  button is only active when a Linear System has been imported through linearization. Clicking the button will import parameters from the simulation.
- The  button is only active when a Linear System has been imported through linearization. Clicking the button will export the current parameters to the simulation.

## Plots

You can inspect the time- and frequency responses of the selected transfer function using:

- Step Response
- Bode Plot
- Nyquist Plot
- Nichols Chart
- Poles and Zeros (including root locus)

## Output

- Clicking the **20-sim** button will export the linear system as a new 20-sim submodel.
- Clicking the **Matlab** button will export the 20-sim Linear System to a Matlab m-file. If the Linear System is symbolic, all parameter relations are preserved.

State space models use linear differential equations (continuous) or difference equations (discrete) to describe system dynamics. They are of the form:

$$\begin{aligned} \frac{dx}{dt} &= A \cdot x + B \cdot u & x_{n+1} &= A \cdot x_n + B \cdot u_n \\ y &= C \cdot x + D \cdot u & y_n &= C \cdot x_n + D \cdot u_n \end{aligned}$$

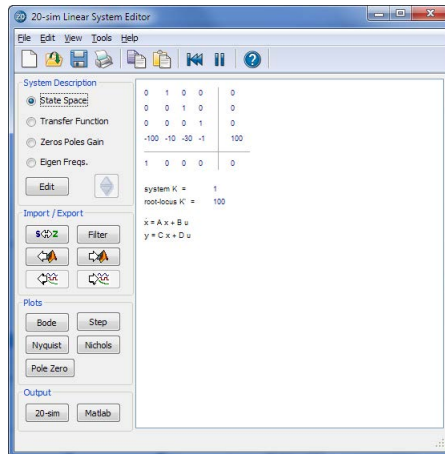
(continuous)                      (discrete)

with for example:

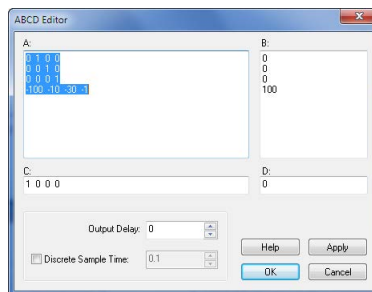
$$A = \begin{bmatrix} 0 & 0.5 \\ -1 & -1 \end{bmatrix} \quad B = \begin{bmatrix} -0.1 \\ 0.1 \end{bmatrix}$$

$$C = \begin{bmatrix} 0 & 1 \end{bmatrix} \quad D = \begin{bmatrix} 0 \end{bmatrix}$$

where  $x$  is the state vector and  $u$  and  $y$  are the input and output vectors. These models may arise from the equation of physics, from state space identification or as the result of linearization.



You can enter state space models by selecting the *State Space* button and clicking the *Edit* button.



This opens an editor in which you can enter the A, B, C and D matrices. Depending on the selection of the Discrete Linear System check box (and Sample Time) the system is a continuous-time or discrete-time system. You can enter the matrix elements in the white space areas. Separate column elements with Spaces or Commas. Enter new rows by clicking the Enter key (new line) or using a semicolon. Brackets ( e.g. [ ... ] ) may be used to denote the a matrix or vector.

The A-matrix, shown in the figure above can for example be entered as:

```
0 1
-0.5 -1
```

or

0,1;-0.5,-1

or

[0,1;  
-0.5,-1]

### Output Delay

To inspect the effects of time delay in your model, you can add output delay. The result will be visible in the various plots that you can show of a linear system. The unit of the output delay is seconds.

### Discrete Sample Time

If you want to transfer a linear system from continuous time to discrete time directly (i.e. replace the  $s$  by a  $z$ ), select Discrete Sample time and fill in the sample time value. You can also transfer back directly by deselecting Discrete Sample time.

### Commands

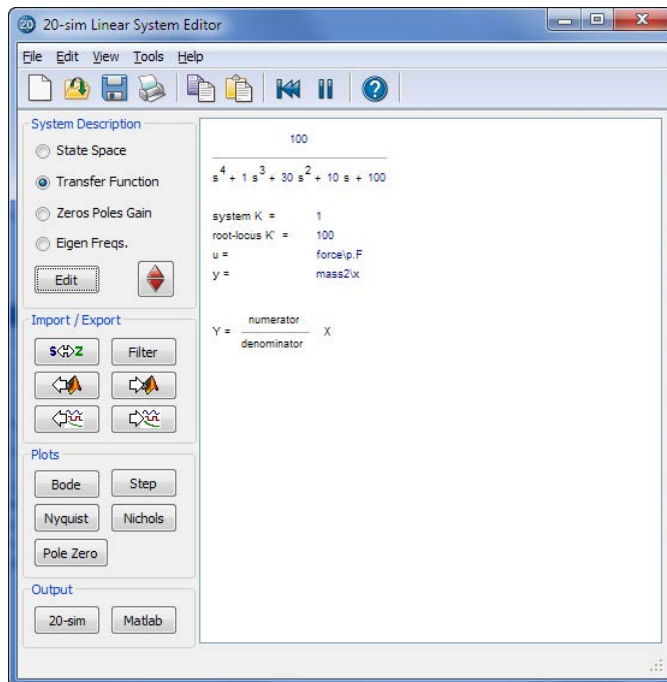
- *Help*: Open the help file.
- *Apply*: Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero).
- *OK*: Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero) and close the editor.
- *Cancel*: Do not apply any changes to the system and close the editor.

A continuous time or discrete time SISO transfer function:

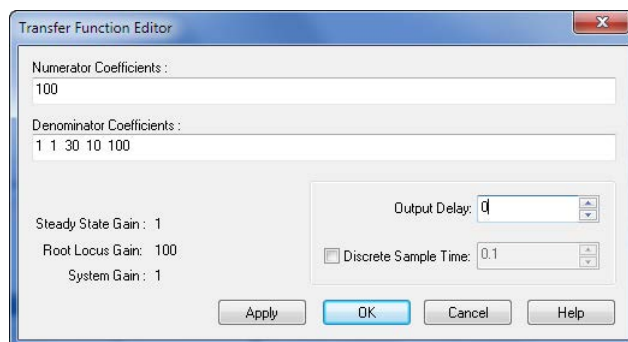
$$h(s) = \frac{n(s)}{d(s)} \quad h(z) = \frac{n(z)}{d(z)}$$

(continuous)                      (discrete)

is characterized by its numerator  $n$  and denominator  $d$ , both polynomials of the variable  $s$  or  $z$ .



You can enter transfer functions by selecting the *Transfer* Function button and clicking the *Edit* button.



This opens an editor in which you can enter the coefficients of the numerator and denominator polynomials. You can enter the elements in the white space areas. Separate the elements with Spaces. Polynomials should be entered in descending powers of  $s$  or  $z$ . The Steady State Gain, Root Locus Gain and System Gain are parameters, that are automatically derived from the transfer function.

In the editor shown above the transfer function

$$\frac{0.1 \cdot s + 0.1}{s^2 + s + 0.5}$$

was given. You can enter the coefficients as:

0.1 0.1

and

1 1 0.5

or

0.1,0.1

and

1,1,0.5

### Output Delay

To inspect the effects of time delay in your model, you can add output delay. The result will be visible in the various plots that you can show of a linear system. The unit of the output delay is seconds.

### Discrete Sample Time

If you want to transfer a linear system from continuous time to discrete time directly (i.e. replace the  $s$  by a  $z$ ), select Discrete Sample time and fill in the sample time value. You can also transfer back directly by deselecting Discrete Sample time.

### Commands

- *Help*: Open the help file.
- *Apply*: Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero).
- *OK*: Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero) and close the editor.
- *Cancel*: Do not apply any changes to the system and close the editor.

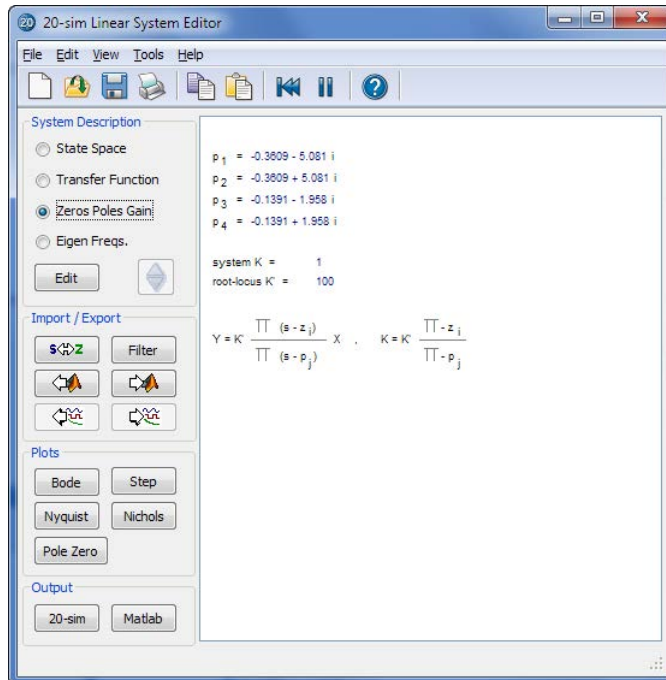
A continuous-time SISO transfer function can be described by the transfer function:

$$h(s) = \frac{n(s)}{d(s)} = \frac{n_i \cdot s^i + n_{i-1} \cdot s^{i-1} + \dots + n_0 \cdot s^0}{d_j \cdot s^j + d_{j-1} \cdot s^{j-1} + \dots + d_0 \cdot s^0}$$

This transfer function can be rewritten in pole zero notation with

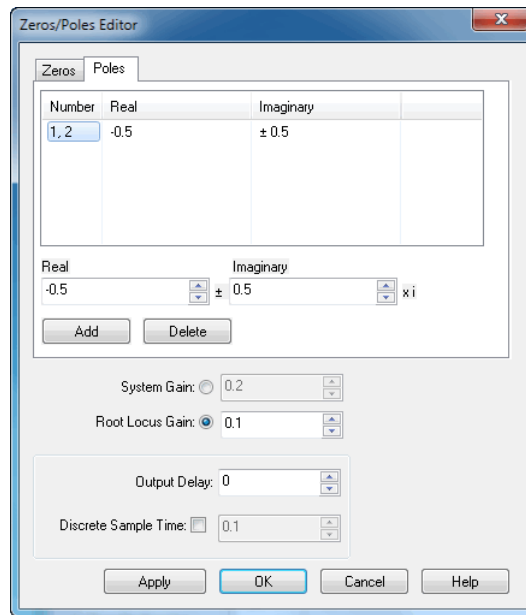
$$h(s) = K_{RL} \frac{(s - z_1)(s - z_{i-1}) \dots (s - z_0)}{(s - p_1)(s - p_{j-1}) \dots (s - p_0)}$$

where  $p_1 \dots p_1$  are the poles and  $z_1 \dots z_1$  are the zeros and  $K_{RL}$  is the Root Locus Gain of the system. The same can be done for a discrete-time SISO transfer function.



You can enter zeros and poles by selecting the *Zeros & Poles* button and clicking the *Edit* button.





This opens an editor in which you can enter the real and imaginary parts of the zeros and poles as well as the Root Locus Gain. If preferred, you can also enter the System Gain. Note that zeros and poles always have conjugate when the imaginary part is non-zero. I.e. when you enter a pole with imaginary part 0.5 an extra pole is added with imaginary part -0.5.

### Output Delay

To inspect the effects of time delay in your model, you can add output delay. The result will be visible in the various plots that you can show of a linear system. The unit of the output delay is seconds.

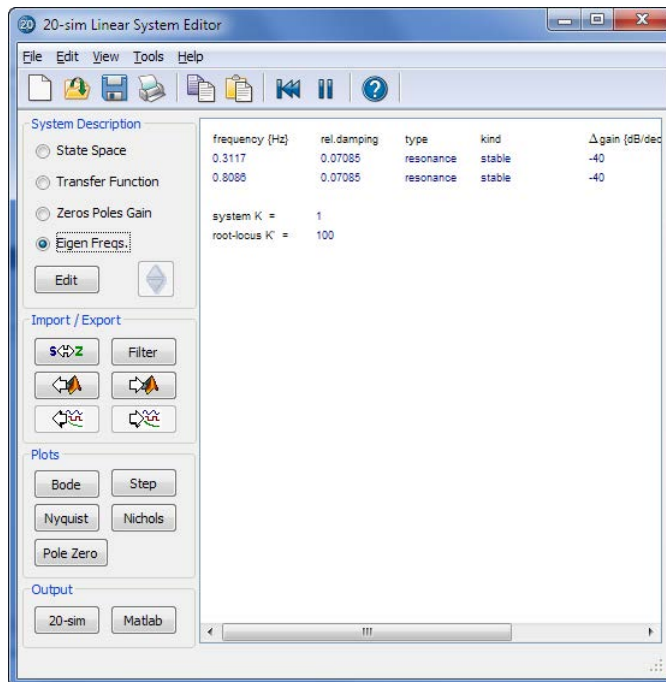
### Discrete Sample Time

If you want to transfer a linear system from continuous time to discrete time directly (i.e. replace the  $s$  by a  $z$ ), select Discrete Sample time and fill in the sample time value. You can also transfer back directly by deselecting Discrete Sample time.

### Commands

- **Add/Delete:** Add or delete selected poles or zeros.
- **Help:** Open the help file.
- **Apply:** Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero).
- **OK:** Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero) and close the editor.
- **Cancel:** Do not apply any changes to the system and close the editor.

The Eigen Frequencies view is closely related to the pole zero notation and bode plot. It shows the resonance frequencies and anti-resonance frequencies that result from the given poles and zeros as well as some characteristic parameters from the bode plot.

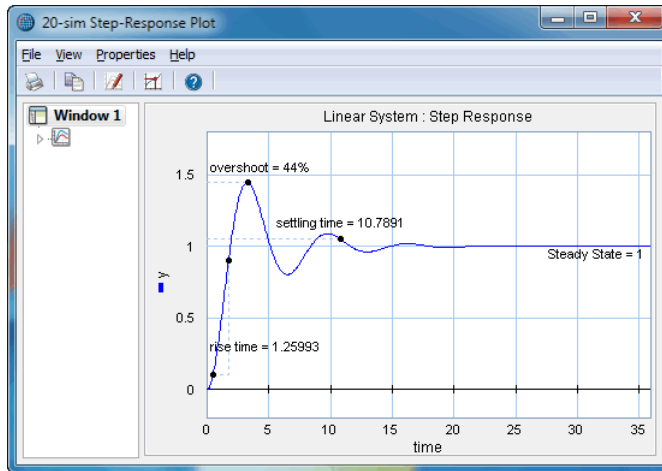


You can enter transfer functions by selecting the *Eigen Freqs.* button and clicking the *Edit* button.

The *Step Response* command calculates the systems response  $y$  on a unit step input:

$$u = 0 \text{ (time } < 0 \text{ )}$$

$$u = 1 \text{ (time } \geq 0 \text{ )}$$



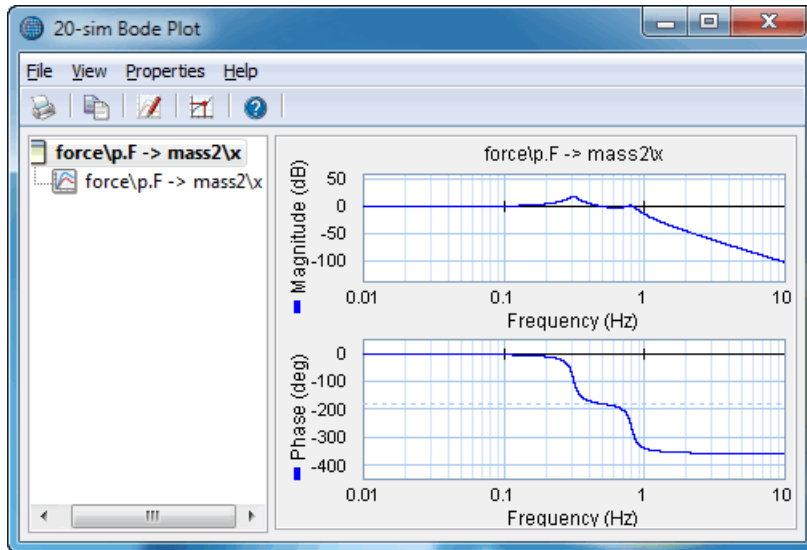
20-sim automatically generates an appropriate range for the time response, based on the system dynamics. With the Plot Properties command (right mouse menu), you can change this horizon and recalculate the step response (click the Step command again).

### Plot Options

Using the right mouse menu, you can use several options:

- **Plot Properties:** Set the general plot properties for the step response and specify the curve properties.
- **Numerical Values:** Inspect numerical values.
- **Step Characteristics:** Display rise time, overshoot, settling time and the steady state value of the step response.
- **Copy to Clipboard:** Copy the plot to the windows clipboard.
- **Print:** Print the plot.
- **Zoom in:** Show a detail of the plot.
- **Zoom out:** Show a larger portion of the plot.
- **Zoom Normal:** Show the complete plot.

Bode Plots show the amplitude and phase of a linear system as function of the frequency. Bode plots can be shown for every 20-sim model through Linearization. During Linearization you are asked to enter the input variable and output variable for which linearization should be performed. After that the linear system is calculated and shown in the Linear System Editor. From the Linear System Editor you can generate a bode plot. These actions can also be predefined using the Frequency Response command of the *Properties* menu.



20-sim automatically generates a range of logarithmically displayed frequencies, based on the system dynamics. With the **Plot Properties** command (**right mouse menu**), you can change this horizon and recalculate the bode response (click the Bode command again).

The magnitude part of the plot can be displayed in dB or in absolute values. The phase part can be displayed in radians or degrees. The frequency can be displayed in radians per second or in Hz.

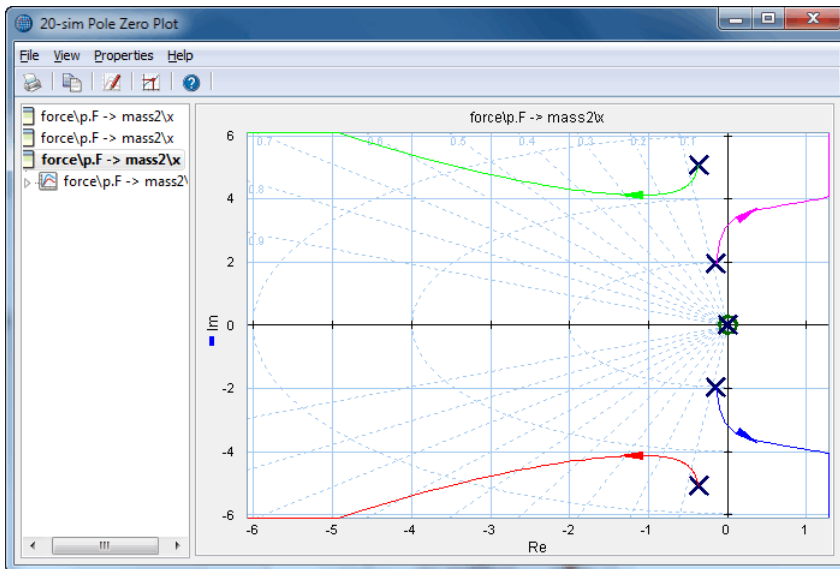
### Plot Options

Using the toolbar or the right mouse menu, you can use various options:

- *Plot Properties*: Set the plot properties.
- *Numerical Values*: Inspect numerical values.
- *Magnitude (dB)*: Display magnitude in decibels
- *Magnitude (-)*: Display magnitude in absolute values.
- *Phase (rad)*: Display phase in radians.
- *Phase (deg)*: Display phase in degrees.
- *Frequency (rad/sec)*: Display frequency in radians per second.
- *Frequency (Hz)*: Display frequency in Hz.
- *Phase/Gain Margins*: Display the gain and phase margins.
- *Modulus Margin*: Display the Modulus Margin.

- *Peak Response*: Display the peak response.
- *Copy to Clipboard*: Copy the plot to the windows clipboard.
- *Print*: Print the plot.
- *Zoom in*: Show a detail of the plot.
- *Zoom out*: Show a larger portion of the plot.
- *Zoom Normal*: Show the complete plot.

The **Pole Zero** command plot the poles and zeros of a system and computes the root locus plot.



20-sim automatically generates a range of real and imaginary parts, based on the system dynamics. With the **Plot Properties** command (right mouse menu), you can change this horizon and recalculate the pole zero diagram (click the **Pole Zero** command again).

### Root Locus

You can show the rootlocus plot by selecting **Root Locus** from the right mouse menu. Inspect the root locus gain by selecting **Numerical Values** from the right mouse menu.

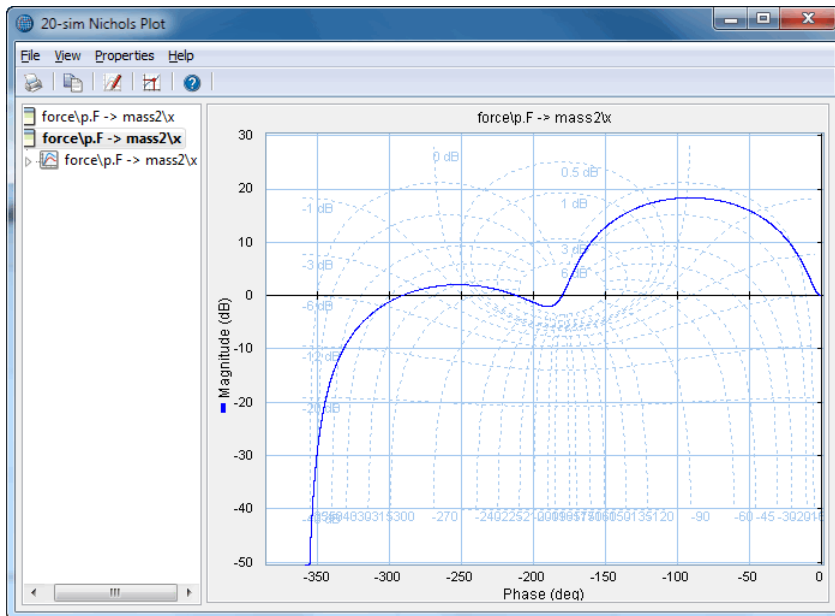
### Plot Options

Using the right mouse menu, you can use several options:

- *Plot Properties*: Set the plot properties.
- *Numerical Values*: Inspect numerical values.
- *Root Locus*: Show or hide the root locus plot.
- *Copy to Clipboard*: Copy the plot to the windows clipboard.
- *Print*: Print the plot.
- *Zoom in*: Show a detail of the plot.

- *Zoom out*: Show a larger portion of the plot.
- *Zoom Normal*: Show the complete plot.

The *Nichols* command computes the Nichols chart of a system.



20-sim automatically generates a range of logarithmically displayed frequencies, based on the system dynamics. With the **Plot Properties** command (right mouse menu), you can change this horizon and recalculate the Nichols chart (click the **Nichols** command again). The magnitude part of the plot can be displayed in decibels (dB) or in absolute values. The phase part can be displayed in radians or degrees.

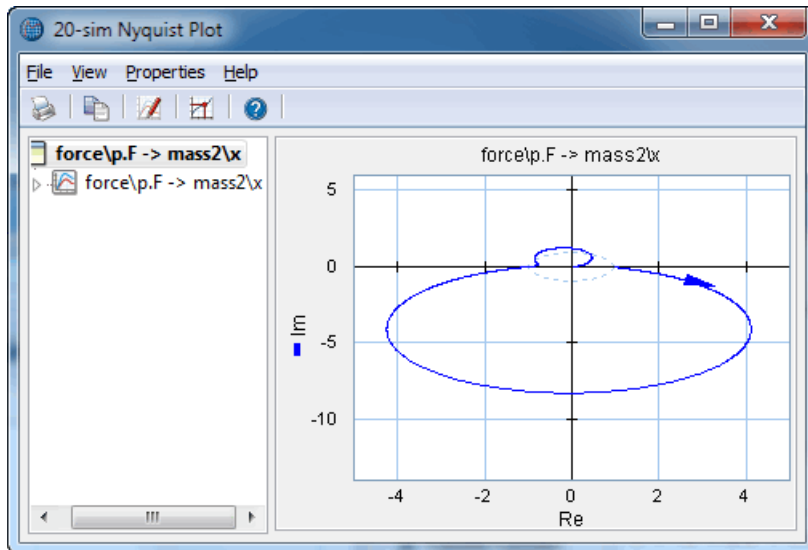
### Plot Options

Using the right mouse menu, you can use several options:

- *Plot Properties*: Set the plot properties.
- *Numerical Values*: Inspect numerical values.
- *Magnitude (dB)*: Display magnitude in decibels
- *Magnitude (-)*: Display magnitude in absolute values.
- *Phase (rad)*: Display phase in radians.
- *Phase (deg)*: Display phase in degrees.
- *Frequency (rad/sec)*: Display frequency in radians per second.
- *Frequency (Hz)*: Display frequency in Hz.
- *Phase/Gain Margins*: Display the gain and phase margins.
- *Modulus Margin*: Display the Modulus Margin.
- *Copy to Clipboard*: Copy the plot to the windows clipboard.

- *Print*: Print the plot.
- *Zoom in*: Show a detail of the plot.
- *Zoom out*: Show a larger portion of the plot.
- *Zoom Normal*: Show the complete plot.

The **Nyquist** command computes the Nyquist plot of a system.



20-sim automatically generates a range of real and imaginary parts, based on the system dynamics. With the **Plot Properties** command (right mouse menu), you can change this horizon and recalculate the Nyquist diagram (click the **Nyquist** command again).

### Plot Options

Using the right mouse menu, you can use several options:

- *Plot Properties*: Set the plot properties.
- *Numerical Values*: Inspect numerical values.
- *Phase/Gain Margins*: Display the gain and phase margins.
- *Modulus Margin*: Display the Modulus Margin.
- *Copy to Clipboard*: Copy the plot to the windows clipboard.
- *Print*: Print the plot.
- *Zoom in*: Show a detail of the plot.
- *Zoom out*: Show a larger portion of the plot.
- *Zoom Normal*: Show the complete plot.

## MLP Network Editor

Human brains consist of billions of neurons that continually process information. Each neuron is like a tiny computer of limited capability that processes input information from other neurons into output information to other neurons. Connected together, these neurons form the most intelligent system known.

For some years now, researchers have been developing models that mimic the activity of neurons to produce a form of artificial intelligence. These "Neural Networks" are formed from tens or hundreds of simulated neurons connected together in much the same way as the brain's neurons. Just like the neurons of the brain, artificial neurons can change their response to a given set of inputs, or "learn".

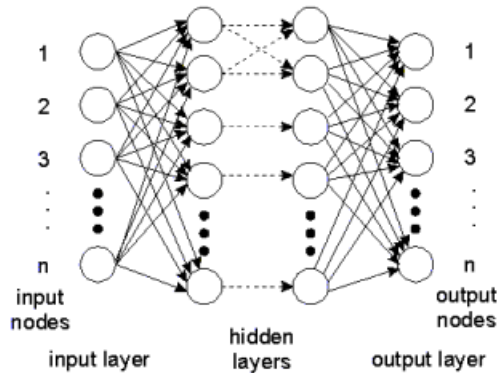
In the past many learning algorithms have been developed, mostly with limited success. The introduction of the backpropagation paradigm, however, appeared a turning point. It is an extremely effective learning tool that can be applied to a wide variety of problems.

The backpropagation paradigm requires supervised training. This means neural networks must be trained by repeatedly presenting examples to the network. Each example includes both inputs (information you would use to make a decision) and desired outputs (the resulting decision, prediction, or response). Based on a calculation on the inputs, the desired outputs and the network's own response to the inputs, the backpropagation paradigm tries to adapt the response of each neuron to achieve an improved neural network behavior. This trial-and-error process continues until the network reaches a specified level of accuracy.

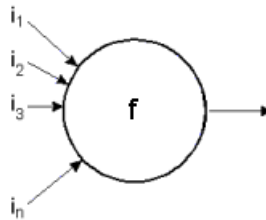
Once a network is trained and tested its neurons can be "frozen". This means the neurons' ability to learn or adapt is stopped. The network can then be used to perform the task it was trained for.

In backpropagation type neural networks, the neurons or "nodes" are grouped in layers. We can distinguish three groups of layers in a backpropagation type neural network: one input layer, one or more hidden layers and one output layer. The nodes between two adjacent layers are interconnected. Fully connected networks occur when each node of a layer is connected with each node of the adjacent layer.





As the figure shows, information (i.e. input signals) enters the network through the input layer. The sole purpose of the input layer is to distribute the information to the hidden layers. The nodes of the hidden layers do the actual processing. The processed information is captured by the nodes of the output layer, and transported as output signals to the world outside.



$$y = f ( w_1*i_1 + w_2*i_2 + w_3*i_3 + \dots + w_n*i_n )$$

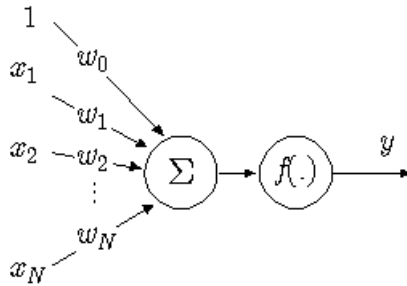
The nodes of the hidden layers process information by applying factors (weights) to each input. This is shown in the figure above. The sum of the weighted input information ( $S$ ) is applied to an output function. The result is distributed to the nodes of the next layer.

When the network is in being trained, the weights of each node are adapted according to the backpropagation paradigm. When the network is in operation, the weights are constant.

Depending on the kind neural network, various topologies can be discerned. The 20-sim Neural Network Editor supports two well-known networks:

1. Adaptive B-spline networks
2. Multi-layer Perceptron networks

The basic element of the Multi Layer Perceptron (MLP) neural network, is the artificial neuron. An artificial neuron, is a unit that performs a simple mathematical operation on its inputs. In the figure below, the neuron is graphically presented.

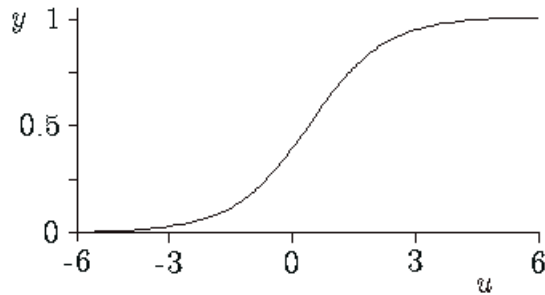


The input,  $\mathbf{x}$ , of the neuron consists of the variables  $x_1 \dots x_n$  and a bias term, known as the **momentum constant**, which is equal to 1. Each of the input values is multiplied by a weight,  $w_i$ , after which the results are added. On the result, a simple mathematical function,  $f(x)$ , is performed. This function is also known as the **activation function**. The calculations the neuron performs are thus given by:

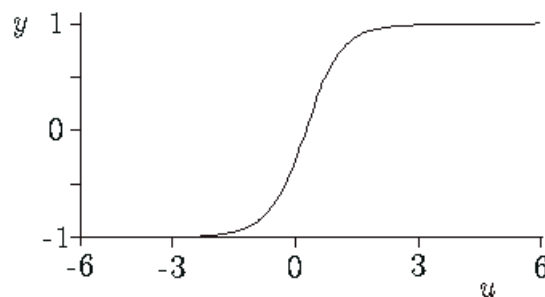
$$y = f(w_0 + x_1 w_1 + \dots + x_n w_n)$$

Numerous choices for the functions exist. Frequently used implementations are the Sigmoid functions:

$$f(u) = 1 / (1 + e^{-u})$$



$$f(u) = c_1 * \tanh(c_2 * u)$$



(in the picture  $c_1 = c_2 = 1$ )

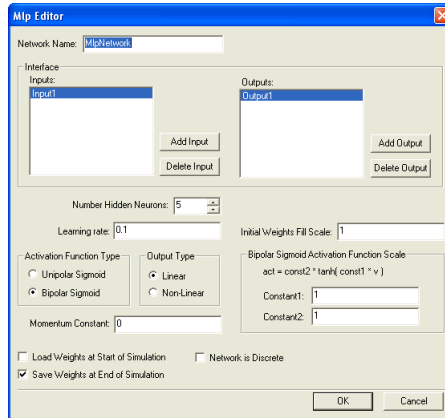
## MLP Network

An MLP network, as any type of back-propagation network can consist of many neurons, which are ordered in layers. The neurons in the hidden layers do the actual processing, while the neurons in the input and output layer merely distribute and collect the signals. Although many hidden layers can be used, it has been shown that an MLP with one hidden layer can approximate any continuous function. Therefore in 20-sim, the MLP networks only have one hidden layer.

### Training the MLP network

The MLP network is trained by adapting the weights. During training the network output is compared with a desired output. The error between these two signals is used to adapt the weights. This rate of adaptation is controlled by the **learning rate**. A high learning rate will make the network adapt its weights quickly, but will make it potentially unstable. Setting the learning rate to zero, will make the network keep its weights constant.

The MLP Editor can be used to define a 20-sim Multi Layer Perceptron (MLP) network. The editor is opened when you try to edit this submodel (using the Go Down command).



## General Settings

- **Network Name:** this is the local name of the submodel representing the MLP network (this option is not yet supported).
- **Number Hidden Neurons:** The MLP network specified by this editor has one layer of hidden neurons. You can specify here the number of neurons that should be used.
- **Learning Rate:** Specify the learning rate that should be used during training. If you do not want the network to learn, enter a zero value here.
- **Initial Weights Fill Scale:** To start proper learning of the network, all initial weights will be given a random value (unequal to zero!) between -scale and +scale. You can enter the scale factor here.
- **Activation Function Type:** Select one of the following activation functions
  - Unipolar Sigmoid:  $act = 1/(1 + \exp(-v))$
  - Bipolar Sigmoid:  $act = const2 * \tanh(const1 * v)$
- **Bipolar Sigmoid Activation Function Scale:** If a Bipolar Sigmoid was chosen as the activation function, you can enter here the values of const1 and const2.
- **Momentum Constant:** Select the momentum constant here.
- **Load Weights at Start of Simulation:** Select this option, if you want to use predefined weights stored on file (saved in a previous run). Before each simulation run, you will be asked to enter the filename of this weights file.
- **Save Weights at Start of Simulation:** Select this option, if you want to store the weights on file. After each simulation run, you will be asked to enter the filename of this weights file.
- **Network is Discrete:** Select this option if the B-spline network is connected with discrete-time models. Deselect this option if the network is connected with continuous models.

## Inputs

- **Add Input:** Add a new input to the network. You will be prompted to give a specific input name. This name will be shown in the Inputs list.

- Delete Input: Delete the input selected in the Inputs list.

### **Outputs**

- Add Output: Add a new output to the network. You will be prompted to give a specific output name. This name will be shown in the Outputs list.
- Delete Output: Delete the output selected in the Outputs list.

## **B-Spline Network Editor**

Human brains consist of billions of neurons that continually process information. Each neuron is like a tiny computer of limited capability that processes input information from other neurons into output information to other neurons. Connected together, these neurons form the most intelligent system known.

For some years now, researchers have been developing models that mimic the activity of neurons to produce a form of artificial intelligence. These "Neural Networks" are formed from tens or hundreds of simulated neurons connected together in much the same way as the brain's neurons. Just like the neurons of the brain, artificial neurons can change their response to a given set of inputs, or "learn".

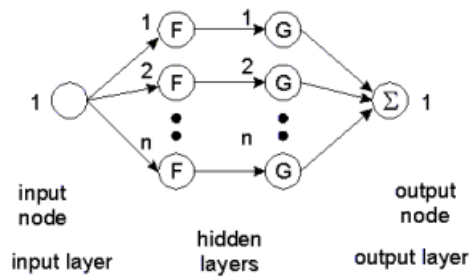
In the past many learning algorithms have been developed, mostly with limited success. The introduction of the backpropagation paradigm, however, appeared a turning point. It is an extremely effective learning tool that can be applied to a wide variety of problems.

The backpropagation paradigm requires supervised training. This means neural networks must be trained by repeatedly presenting examples to the network. Each example includes both inputs (information you would use to make a decision) and desired outputs (the resulting decision, prediction, or response). Based on a calculation on the inputs, the desired outputs and the network's own response to the inputs, the backpropagation paradigm tries to adapt the response of each neuron to achieve an improved neural network behavior. This trial-and-error process continues until the network reaches a specified level of accuracy.

Once a network is trained and tested its neurons can be "frozen". This means the neurons' ability to learn or adapt is stopped. The network can then be used to perform the task it was trained for.

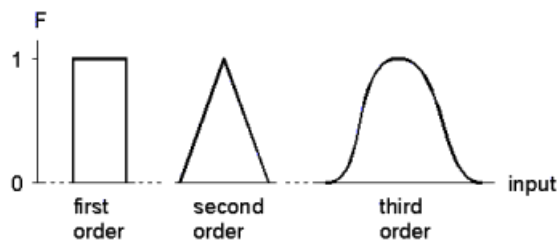
### **One-dimensional B-spline network**

An adaptive B-spline network can be used to relate  $k$  inputs and a single output  $y$  on a restricted domain of the input space. The following network shows a realization with one input:



The network is shown with two hidden layers. Some authors prefer to show a B-spline network with only one hidden layer. For a proper understanding of multi-dimensional B-spline networks we prefer to show the network with two hidden layers.

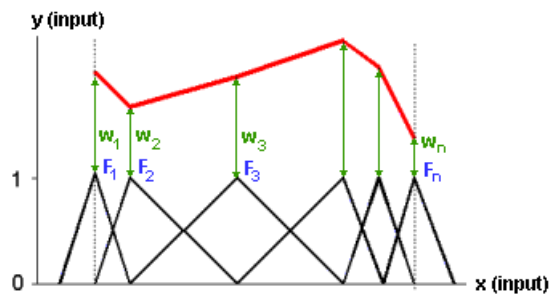
The first hidden layer distributes the inputs over several nodes. In the figure above input 1 is distributed over  $n$  nodes. Each node of this layer has only one input. To this input a "basis function"  $F$  is applied. As basis functions, B-splines are used of any desired order. An  $N$ -th order B-spline function consists of pieces of  $(N-1)$ th order polynomials, such that the resulting function is  $(N-1)$  times differentiable. The figure below shows examples of B-spline functions of different order. A spline function differs from zero on a finite interval.



The second hidden layer also consists of  $n$  nodes. Each node of this layer has only one input. To this input a function  $G$  is applied which is merely a multiplication by a weight:

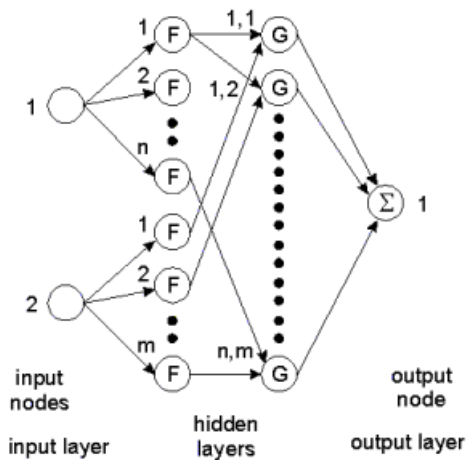
$$G = w * i$$

The output node sums the results of all second hidden layer nodes. When the spline functions of the various nodes are properly spaced, every one dimensional function can be approximated. This is shown in the figure below where the various splines ( $F_1$  to  $F_n$ ) combined with the various weights ( $w_1$  to  $w_n$ ), together form an output function.



**Two-dimensional B-spline network**

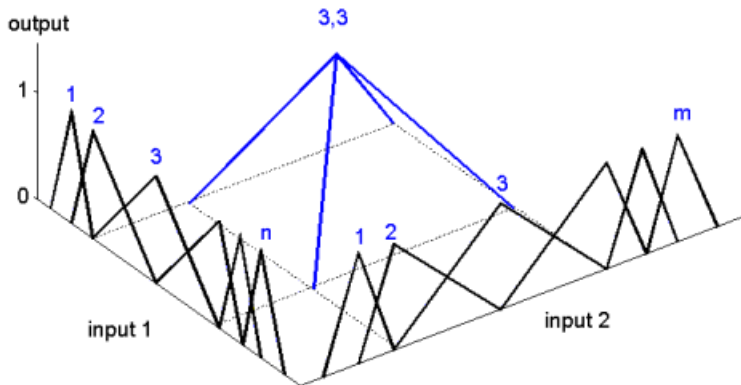
Two-dimensional B-spline networks have two input nodes. The first hidden layer, as with the one-dimensional network, consists of nodes, to which a basis function *F* is applied. This is shown in the figure below. To the first input a group of *n* nodes are applied, and to the second input a group of *m* nodes are applied.



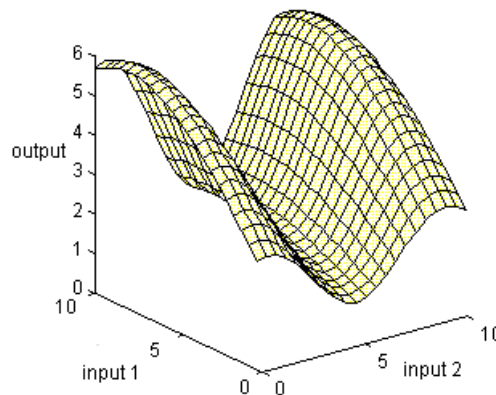
The second hidden layer now consists of nodes which each have two inputs. For every combination of a node from one group and a node from the second group, a node exists. To each node of the second hidden layer, a function *G* is applied which is merely a multiplication of the two inputs multiplied by a weight:

$$G = w * i_1 * i_2$$

Again the output node sums the results of all second hidden layer nodes. When the spline functions of the various nodes are properly spaced, every two dimensional function can be approximated. The figure below shows the spacing of various spline functions of the two inputs and one output of a node of the second hidden layer.



The output node sums the results of all second hidden layer nodes. When the spline functions of the various nodes are properly spaced, every two dimensional function can be approximated. This is shown in the figure below.



### More-dimensional B-spline networks

In a same way more dimensional B-spline networks can be created, using more inputs. The 20-sim B-spline Editor supports networks with up to 256 inputs and one output.

### Training the B-spline network

The B-spline network is trained by adapting the weights. During training the network output is compared with a desired output. The error between these two signals is used to adapt the weights. This rate of adaptation is controlled by the **learning rate**. A high learning rate will make the network adapt its weights quickly, but will make it potentially unstable. Setting the learning rate to zero, will make the network keep its weights constant. Learning of B-spline networks can either be done after each sample (**learn at each sample**), or after series of samples (**learn after leaving spline**).

### Learn at each Sample

When learning at each sample, after every sample the weights are adapted according to:



$$\Delta w_j = \gamma \cdot (y_d - y) \cdot F_j(x)$$

with

$\Delta w_j$  : adaptation of the weight  $w_j$

$\gamma$  : learning rate

$F_j(x)$  : B-spline function number  $j$

$x$  : input

$y_d$  : desired output

$y$  : network output

Given a certain input ( $x$ ), only a limited number of splines  $F_i(x)$  are nonzero. Therefore only a few weights are adapted each sample.

### Learn after Leaving Spline

When learning after leaving a spline, the network will keep track of the input ( $x$ ) and the corresponding nonzero splines  $F_i(x)$ . For each nonzero spline, a sample will be stored consisting of the input ( $x$ ), the output ( $y$ ) and desired output ( $y_d$ ). Only after the input has left the region where a spline is nonzero, its weight is updated according to:

$$\Delta w_j = \gamma \cdot \frac{\sum_{i=1}^n (y_{d,i} - y_i) \cdot F_j(x_i)}{\sum_{i=1}^n F_j(x_i)}$$

Here  $n$  is the number of samples that have been taken.

The B-Spline Editor can be used to define a 20-sim B-Spline network. The editor is opened when you try to edit this submodel (using the Go Down command).

20-sim B-Spline Editor

Network Name:  Network Order:

Learning

☒ Learn at each sample  
☐ Learn after leaving spline

Learning Rate:

Regularization

☐ Apply Regularization  
Regularization Width:

input1

Input Name:

Regions

Number	lower	upper	Nr. of Splines
1	0	10	10

Lower:  Number of Splines:   
Upper:

☐ Load Weights at Start of Simulation ☐ Network is Discrete  
☒ Save Weights at End of Simulation

## General Settings

- **Network Name:** this is the local name of the submodel representing the B-Spline network (this option is not yet supported).
- **Order:** Enter the order of the B-Splines that must be used.
- **Learn at Each Sample:** Select this option if you want the network to adapt the weights after every simulation step
- **Learn after leaving Spline:** Select this option if you want the network to adapt the weights only leaving the spline region.
- **Learning Rate:** Specify the learning rate that should be used during training. If you do not want the network to learn, enter a zero value here.
- **Apply Regularization:** This option is not yet supported.
- **Load Weights at Start of Simulation:** Select this option, if you want to use predefined weights stored on file (saved in a previous run). Before each simulation run, you will be asked to enter the filename of this weights file.
- **Save Weights at End of Simulation:** Select this option, if you want to store the weights on file. After each simulation run, you will be asked to enter the filename of this weights file.
- **Network is Discrete:** Select this option if the B-spline network is connected with discrete-time models. Deselect this option if the network is connected with continuous models.

## Input Settings

The tabs shown in the editor is used to specify the inputs of the network. Each tab shows the specific settings of that input.

- **Add Input:** Add a new input to the network. A new tab will be added with default settings.
- **Delete Input:** Delete the input defined in the selected tab (the tab that is in front).

Each input is associated with a certain number of splines. To give the user more flexibility, each input can be divided in certain regions that each have their own density of splines.

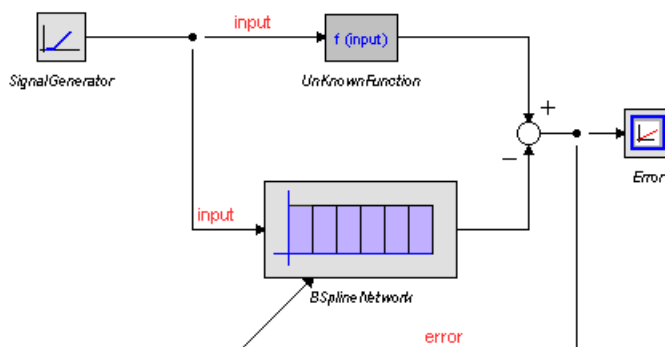
- **Add:** Add a new region of splines.
- **Delete:** Delete the selected region of splines.
- **Split:** Split the selected region into two regions.

Each region can be edited. Just select it from the Regions list and use the following options:

- **Upper / Lower:** The upper and lower bound of a region.
- **Number of Splines:** The number of splines. The more splines you choose, the more accurate will the network output be, for this region of inputs.

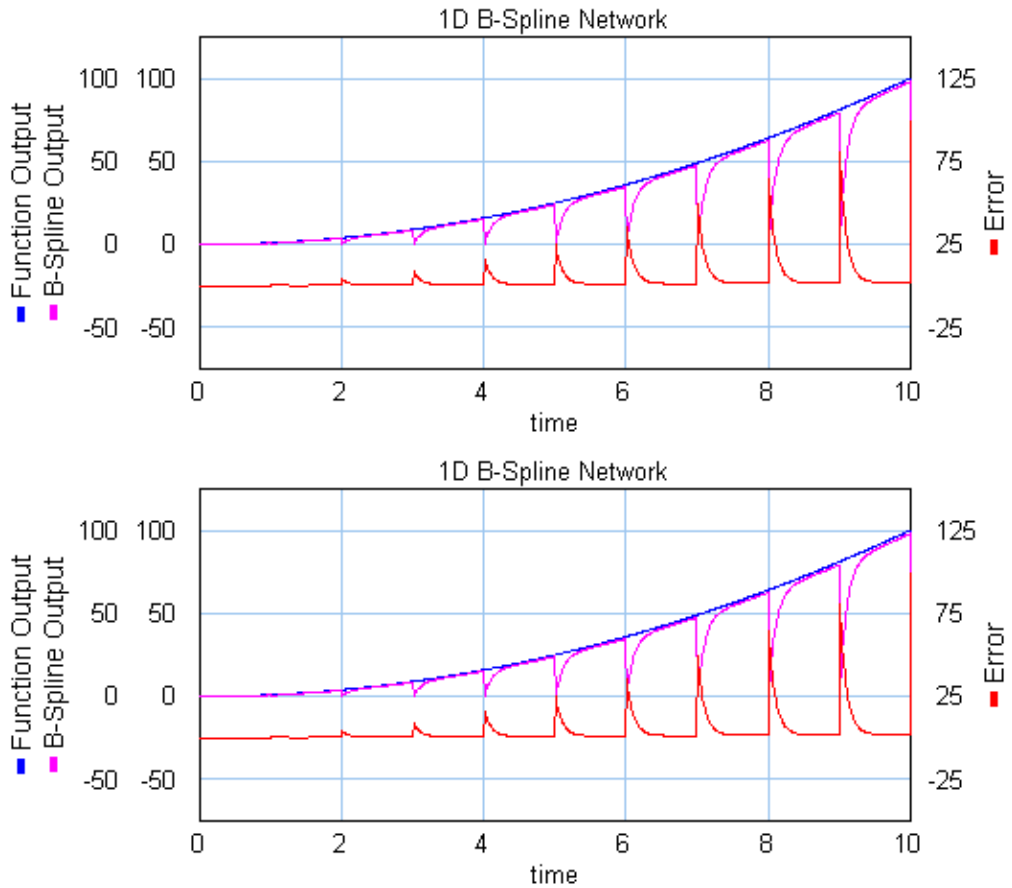
Now we have trained the B-spline network and saved the weights. We can run the network with every desired input. We only have to keep in mind that the network was defined for input signals between 0 and 10.

1. In the Editor from the **File** menu select **Open**.
2. In the model library choose Examples\Control\Neural Networks
3. Select the model 1DBSplineNetwork-Run.emx. Now the predefined model will be opened.



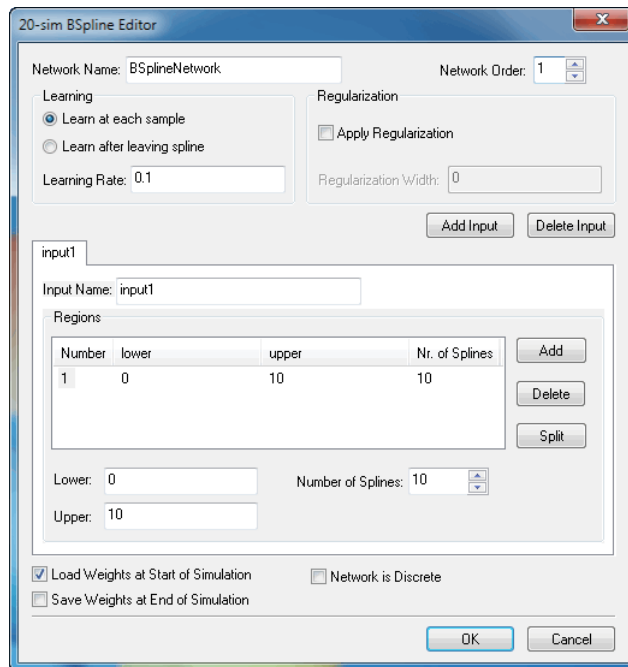
As you can see, this is exactly the same model as used for training, but now a ramp input is used.

4. From the menu select **Model** and **Start Simulator**. Now a Simulator will be opened with the predefined experiment loaded.
5. From Simulator menu click **Simulation** and **Run**. Do **not save** the weights file at the end of the run! The results will look like:

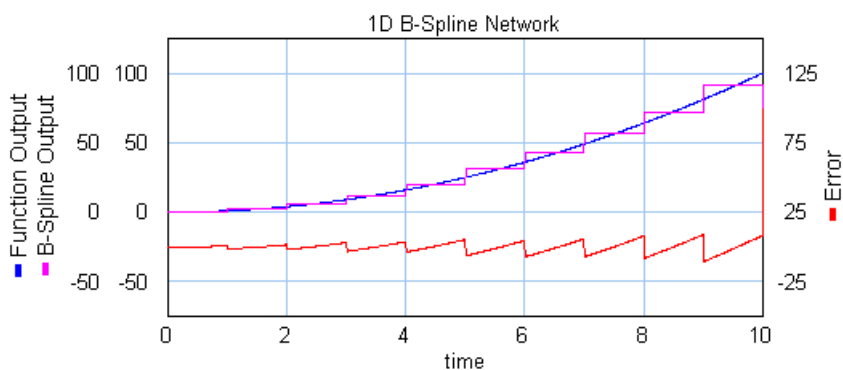


As you can see, the B-Spline Network still has its training settings and still prompts for a weight file at the end of the simulation. Now we are going to change the settings of the B-Spline Network.

- Open the B-Spline Editor (select the model, Go Down). To create a normal run with the network, we have to set the learning rate to zero, and load the weights file before simulation. Change the settings of the network, until it looks like:



7. Click **OK** to close the B-Spline Editor. From the Editor menu click **Model** and **Check Complete Model**. This will implement the changed settings.
8. Return to the Simulator and click **Simulation** and **Run**. Before the run, an Open dialog will asking you to enter the name of the Weights File. This is a file that contains all the weights of the trained B-Spline network. Use the file that you saved during training, or the predefined weights file *1DBSplineNetwork.wgt*. The simulation results will look like:



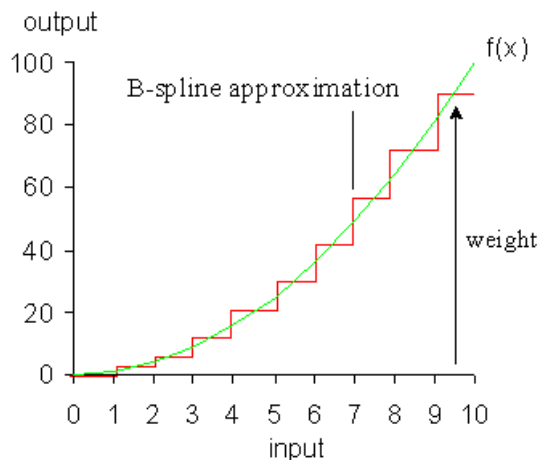
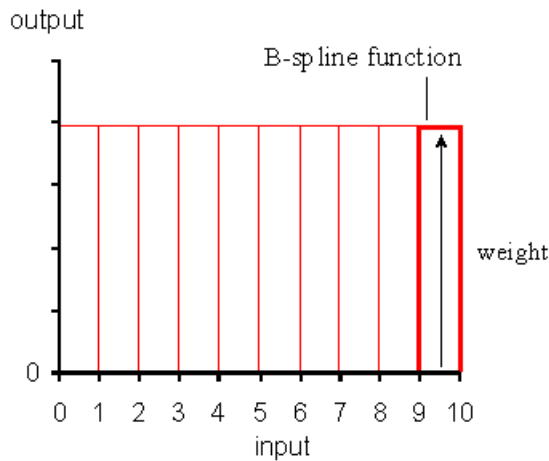
As you can see the function is approximated by the B-Spline network by 10 first order splines.

## Non Linear Function

In this lesson we will use a B-spline network with one input to approximate the simple non-linear function:

$$F = \text{input}^2$$

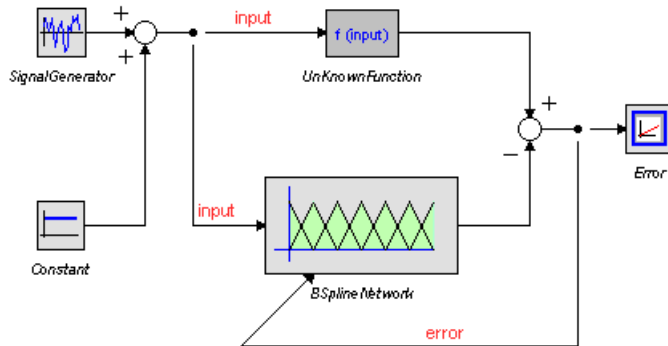
The input,  $x$ , of this function ranges from 0 to 10. It will be approximated by a B-Spline network with one input. As is shown in the figure below (left), 10 first order B-splines are used. The tenth B-spline is indicate with fat lines. The output of the B-spline network is a combination of all ten B-Splines. In other words, the non-linear function will be approximated by 10 intervals of constant value.



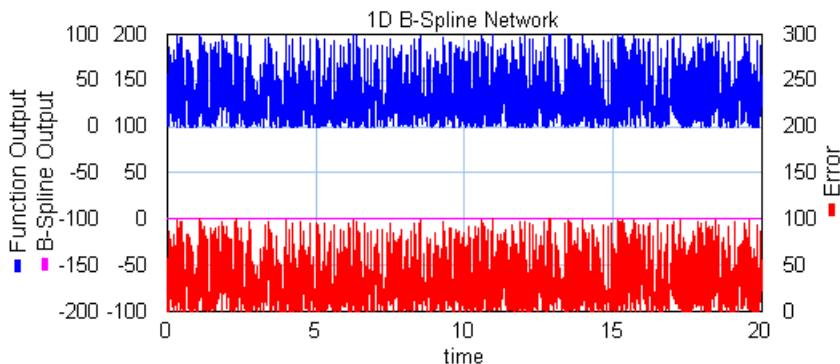
At the start the B-spline has undefined weights. They can either be chosen at random values or all set to zero. A normal session should therefore start with training the network to adjust the weights to give a best approximation of the non-linear function. With these weights we can run the network with any desired input signal.

## Defining the B-Spline Network

We will use the model below to train the B-spline network. It has already been prepared for you.



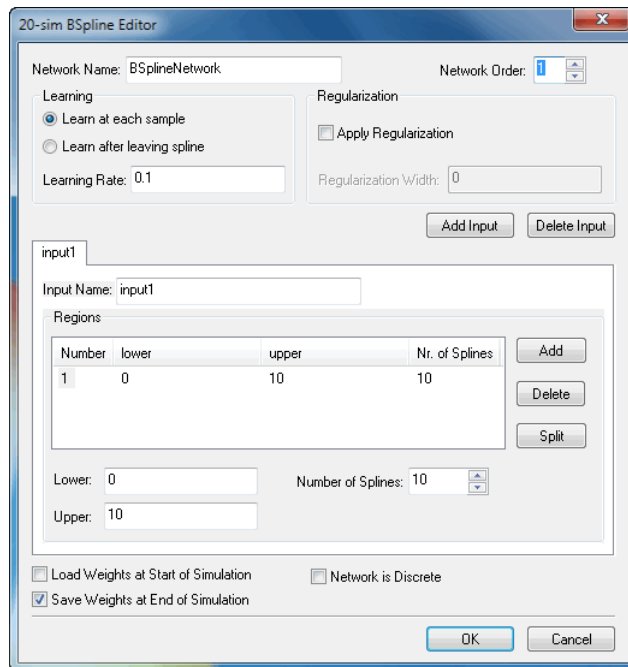
1. In the Editor from the **File** menu select **Open**.
2. In the model library choose Examples\Control\Neural Networks
3. Select the model *1DBSplineNetwork-Train.emx*. Now the predefined model will be opened.
4. From the menu select **Model** and **Start Simulator**. Now a Simulator will be opened with the predefined experiment loaded.
5. From Simulator menu click **Simulation** and **Run**. The results will look like:



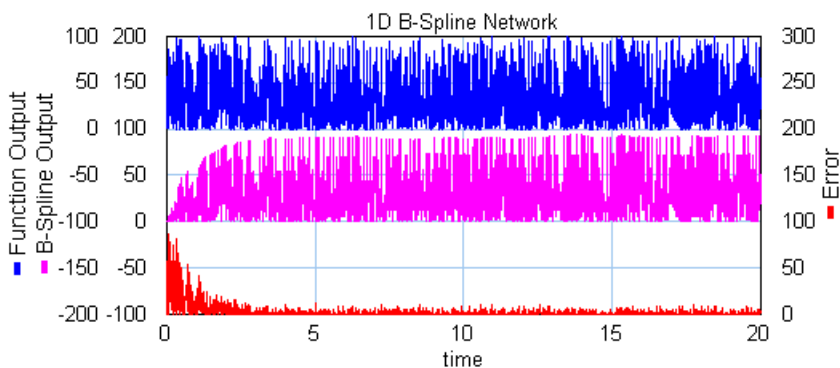
As you can see, the B-Spline output is zero and there is no learning. Now we are going to change the settings of the B-Spline Network.

## Training the Network

6. Return to the Editor. Select the BSplineNetwork model and click **GoDown** from the **Model** menu. Now the B-Spline Editor will pop-up. Change the settings (Network Order, Learning Rate, Input Upper Limit, Save Weights) until it looks like:



7. Click **OK** to close the B-Spline Editor. Note that the icon of the BSplineNetwork model has changed to correspond with the first order splines that are used. From the Editor menu click **Model** and **Check Complete Model**. This will implement the changes in settings.
8. Return to the Simulator and click **Simulation** and **Run**. The results will look like:



As you can see the error rapidly descends, due to the network learning. After the Simulation Run, Save dialog opens, asking you to enter a name for the Weights File. This is a file that contains all the weights of the trained B-Spline network. We can use these weights for normal runs with the network.

9. Enter file name (do not use the predefined weights file!), e.g. *test.wgt* and click **Save**.



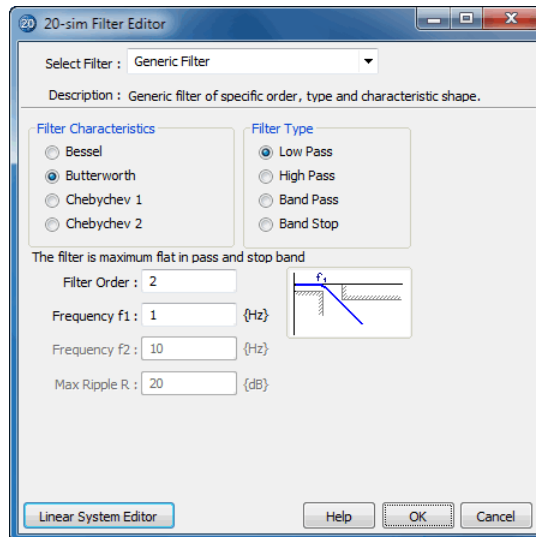
10. Close the **Simulator**.

Now all is prepared to perform a normal run with the Network.

## Filter Editor

The Filter Editor of 20-sim allows you to create continuous-time filters and controllers. The result is a linear system presented in the Linear System Editor of 20-sim. The filter can also be applied to an existing linear system.

You can open the Controller Design Editor from the Tools menu of the 20-sim Editor or by clicking Go Down on a Filter model.



## Procedure

1. Select a filter or controller of your choice from the list of available filters and controllers.

## Filters

- Generic Filter
- Lead Filter
- Lag Filter
- Low Pass First Order Filter
- Low Pass Second Order Filter
- High Pass First Order Filter
- High Pass Second Order Filter
- Notch Filter
- Universal Notch Filter

## Controllers

- P Controller
- I Controller
- D Controller
- PI Controller
- PD Controller
- PID Controller
- PID-1 Controller
- PID-2 Controller
- PID Compensator

A short description of the selected filter will be given in the description field. Depending on the filter that was chosen three or more parameters will be shown.

2. The second step is to fill in the desired parameters.
3. Choose the desired output:
4. Select the **Linear System Editor** button to export the filter to the Linear System Editor.
5. Select the **OK** button to store the filter model on file or update the filter model in the Editor.

The P Controller can be used to create an additional gain for a linear system.

- Gain  $K_p$ : The controller gain  $K_p$  determines the amount of gain the controller adds for each frequency.

### Transfer function of the controller:

$$H_P(s) = K_p$$

The I Controller can be used to create an almost ideal integrator (when the frequency goes to zero).

- Gain  $K_i$ : The filter gain  $K_i$  determines the frequency gain of the controller at frequency  $\omega = 1$  [rad/s].
- Frequency  $f_i$ : The integration behavior of the controller stops at frequency  $f_i$  in Hz. A decrease of this frequency corresponds to a more pure integration behavior.

### Transfer function of the controller

$$H_I(s) = \frac{K_i}{2\pi f_i + s}$$

The D Controller can be used to create an almost ideal derivative (when the frequency goes to infinity).

- Gain  $K_d$ : The controller gain  $K_d$  determines the frequency gain of the controller at frequency  $\omega = 1$  [rad/s].
- Frequency  $f_d$ : The differentiation behavior of the controller stops at frequency  $f_d$  in Hz. An increase of this frequency corresponds to a more pure differentiation behavior, reducing the tameness of the controller.

### Transfer function of the controller

$$H_D(s) = K_d \frac{2\pi f_d s}{s + 2\pi f_d}$$

The PD Controller consists of a differentiator with proportional gain.

- Gain  $K_p$ : The controller gain  $K_p$  determines the low frequency gain of the controller.
- Gain  $K_d$ : The controller gain  $K_d$  determines the gain of the controller at frequency  $\omega = 1$  [rad/s].
- Frequency  $f_d$ : The differentiation behavior of the controller stops at frequency  $f_d$  in Hz. An increase of this frequency corresponds to a more pure differentiation behavior, reducing the tameness of the controller.

### Transfer function of the controller:

$$H_{PD} = H_P + H_D$$

that equals

$$H_{PD} = \frac{(K_p + K_d 2\pi f_d)s + K_p 2\pi f_d}{s + 2\pi f_d}$$

The PI Controller consists of an integrator with a proportional gain.

- Gain  $K_p$ : The controller gain  $K_p$  determines the high frequency gain of the controller.
- Gain  $K_i$ : The controller gain  $K_i$  determines the frequency gain of the controller at frequency  $\omega = 1$  [rad/s].
- Frequency  $f_i$ : The integration behavior of the controller stops after frequency  $f_i$  in Hz. A decrease of this frequency corresponds to a more pure integration behavior.

### Transfer function of the controller:

$$H_{PI} = H_P + H_I$$

that equals

$$H_{PI} = \frac{K_p s + K_p 2\pi f_i + K_i}{s + 2\pi f_i}$$

The PID-1 Controller consists of an integrator and differentiator with proportional gain. It resembles a PID Controller, but has different input parameters.

- Gain  $K_p$ : The controller gain  $K_p$  determines the frequency gain of the controller in the pass band (where integration and differentiation are of no interest).
- Length  $L_i$ : The length  $L_i$  determines the frequency at which integration starts, that is  $f_i / L_i$  in Hz. A decrease of this frequency corresponds to a more pure integration behavior.
- Length  $L_d$ : The length  $L_d$  determines the frequency at which differentiation stops, that is  $f_d * L_d$  in Hz. An increase of this frequency corresponds to a more pure differentiation behavior, reducing the tameness of the controller.
- Frequency  $f_i$ : The integration behavior of the controller stops at frequency  $f_i$  in Hz.
- Frequency  $f_d$ : The differentiation behavior of the controller starts at frequency  $f_d$  in Hz.

**Transfer function of the controller:**

$$H_{PID} = K_p \left( 1 + \frac{L_i - 1}{1 + \frac{L_i s}{2\pi f_i}} + \frac{(L_d - 1)s}{L_d 2\pi f_d + s} \right)$$

that equals

$$H_{PID} = \frac{K_p L_d L_i s^2 + K_p (-2\pi f_i + L_i L_d 2\pi f_d + (L_i + L_d) 2\pi f_i) s + K_p L_i L_d 4\pi^2 f_i f_d}{L_i s^2 + (2\pi f_i + L_i L_d 2\pi f_d) s + L_i L_d 4\pi^2 f_i f_d}$$

The PID-2 Controller consists of an integrator and differentiator with proportional gain. It resembles a serial PID Controller, but has different input parameters.

- Gain  $K_p$ : The controller gain  $K_p$  determines the frequency gain of the controller in the pass band (where integration and differentiation are of no interest).
- Length  $L_i$ : The length  $L_i$  determines the frequency at which integration starts, that is  $f_i / L_i$  in Hz. A decrease of this frequency corresponds to a more pure integration behavior.
- Length  $L_d$ : The length  $L_d$  determines the frequency at which differentiation stops, that is  $f_d * L_d$  in Hz. An increase of this frequency corresponds to a more pure differentiation behavior, reducing the tameness of the controller.
- Frequency  $f_i$ : The integration behavior of the controller stops at frequency  $f_i$  in Hz.
- Frequency  $f_d$ : The differentiation behavior of the controller starts at frequency  $f_d$  in Hz.

#### Transfer function of the controller:

$$H_{PID} = K_p L_i \left( \frac{\frac{s}{2\pi f_i} + 1}{\frac{s}{2\pi f_i / L_i} + 1} \right) \left( \frac{\frac{s}{2\pi f_d} + 1}{\frac{s}{2\pi f_d * L_d} + 1} \right)$$

that equals

$$H_{PID} = \frac{K_p L_d L_i s^2 + K_p L_i L_d 2\pi(f_i + f_d)s + K_p L_i L_d 4\pi^2 f_i f_d}{L_i s^2 + (2\pi f_i + L_i L_d 2\pi f_d)s + L_i L_d 4\pi^2 f_i f_d}$$

The PID Compensator consists of an integrator and differentiator with proportional gain (PID Controller) together with a high-frequency roll-off filter.

- Gain  $K$ : The controller gain  $K$  determines the frequency gain of the controller in the pass band (where integration and differentiation are of no interest).
- Integration  $\tau_{i\_i}$ : The integration time constant  $\tau_{i\_i}$  determines the frequency  $f_i = 1 / \tau_{i\_i}$  [rad/s] after which the integrating behavior stops.
- Differentiation  $\tau_{i\_d}$ : The differentiation time constant  $\tau_{i\_d}$  determines the frequency  $f_d = 1 / \tau_{i\_d}$  [rad/s] after which the differentiation behavior starts.
- HF roll-off  $\tau_{i\_h}$ : The filter time constant  $\tau_{i\_h}$  determines the frequency  $f_h = 1 / \tau_{i\_h}$  [rad/s] of the high-frequency roll-off filter. Frequencies higher than  $f_h$  are filtered out.
- Tameness  $\beta$ : The tameness factor  $\beta$  influences the differentiating behavior. After frequency  $f_{db} = f_d / \beta$  the differentiation behavior stops. Decreasing  $\beta$  increases this frequency  $f_{db}$ , resulting in a more pure differentiating behavior and therefore in a reduce of differentiation tameness.

#### Transfer function of the controller:

$$H_{PIDH} = H_{PI} \cdot H_D \cdot H_H$$

that equals

$$H_{PID} = K \left( \frac{\tau_i s + 1}{\tau_i s} \right) \cdot \left( \frac{\tau_d s + 1}{\tau_d \beta s + 1} \right) \cdot \left( \frac{1}{\tau_h s + 1} \right)$$

The PID Controller consists of an integrator and differentiator with proportional gain.

- Gain  $K_p$ : The controller gain  $K_p$  determines the frequency gain of the controller in the pass band (where integration and differentiation are of no interest).
- Gain  $K_i$ : The controller gain  $K_i$  determines the shape of the frequency response at low frequencies.
- Gain  $K_d$ : The controller gain  $K_p$  determines the shape of the frequency response at high frequencies.
- Frequency  $f_i$ : The integration behavior of the controller starts at frequency  $f_i$  in Hz. A decrease of this frequency corresponds to a more pure integration behavior.
- Frequency  $f_d$ : The differentiation behavior of the controller stops at frequency  $f_d$  in Hz. An increase of this frequency corresponds to a more pure differentiation behavior, reducing the tameness of the controller.

#### Transfer function of the controller:

$$H_{PID} = H_P + H_I + H_D$$

that equals

$$H_{PID} = \frac{(K_p + K_d 2\pi f_d)s^2 + (K_p 2\pi f_i + K_d 4\pi^2 f_i f_d + K_p 2\pi f_d + K_i)s + K_p 4\pi^2 f_i f_d + K_i 2\pi f_d}{s^2 + (2\pi f_i + 2\pi f_d)s + 4\pi^2 f_i f_d}$$

The Generic Filter can be used to design a filter of a specific order, type and characteristic shape.

#### Filter Characteristics

The filter can have a Bessel, Butterworth or Chebychev characteristic shape. Each characteristic has its own advantages and disadvantages; it depends on the purpose of the filter what to choose here:

A *Bessel* filter is maximal flat in both the pass band and the stop band. It is used when the phase response should be nearly linear throughout the pass band, i.e. the group delay is almost constant throughout the pass band. This preserves the wave shape of filtered signals in the pass band. A disadvantage is the low roll-off steepness. Often a high filter order is required to obtain the desired roll-off.

A *Butterworth* filter is maximally flat in the pass band and monotonic overall. As a consequence of this smoothness, the roll-off steepness is rather low. As with Bessel filters, a rather high filter order is required to obtain the desired roll-off.

A *Chebyshev 1* filter has a ripple in the pass band and is monotonic in the stop band. This filter rolls off faster than Bessel, Butterworth and Chebyshev 2 filters at the same filter order. A disadvantage is the greater deviation and discontinuous phase response in the pass band.

A *Chebyshev 2* filter is monotonic in the pass band and has a ripple in the stop band. This filter rolls off faster than Bessel and Butterworth filters at the same filter order. Not as fast as a Chebyshev 1 filter, but it is free of a pass band ripple. A disadvantage is the ripple and discontinuous phase response in the stop band.

### Filter Type

- A *low pass* filter will filter out high frequencies and let low frequencies pass the filter.
- A *high pass* filter does the opposite; it will filter out low frequencies and let high frequencies pass the filter.
- A *band pass* filter will filter out low and high frequencies and let middle frequencies pass the filter.
- A *band stop* filter does the opposite; it will filter out the middle frequencies and let low and high frequencies pass the filter.

### Filter Order

The filter order specifies how steep the filter will roll off at a specified filter frequency. The higher the order, the steeper the roll off will be. Note that the filter order also has a large influence on the phase response of the filter.

### Frequency $f_1$

For a low pass filter  $f_1$  is the frequency in Hz where the roll off starts. For a high pass filter it is the frequency where the roll off ends. For a band pass or band stop filter  $f_1$  is the start frequency of the band.

### Frequency $f_2$

For a band pass or band stop filter  $f_2$  is the stop frequency in Hz of the band. It is disabled for low pass and high pass filters.

### Max. Ripple $R$

Only available when a Chebyshev 1 filter is selected.  $R$  specifies the maximum allowed ripple in dB for the filter in the pass band.

### Stop Band $R$

Only available when a Chebyshev 2 filter is selected.  $R$  specifies the distance of the stop band to the unity gain axis in dB. This is the amount of attenuation in dB of the filter in the stop band (the absolute value is used).

The high pass filter can be used to filter out undesired low frequencies.

- Gain  $K$ : The filter gain  $K$  determines the high frequency gain of the filter.
- Frequency  $f$ : The filter roll off stops at frequency  $f$  in Hz. Higher frequencies will pass the filter, lower frequencies will be filtered out.

### Transfer function of the filter:

$$H(s) = K \frac{s}{s + 2\pi f}$$

The high pass filter can be used to filter out undesired low frequencies.

- Gain  $K$ : The filter gain  $K$  determines the high frequency gain of the filter.
- Frequency  $f$ : The filter roll off stops at frequency  $f$  in Hz. Higher frequencies will pass the filter, lower frequencies will be filtered out.
- Quality  $Q$ : The filter quality indicates how steep the phase response will increase up to the frequency  $f$ . A quality  $Q > 0.707$  results in a peak in the magnitude response at frequency  $f$ .

#### Transfer function of the filter:

$$H(s) = K \frac{s^2}{s^2 + 2\pi f \frac{s}{Q} + (2\pi f)^2}$$

The Lag Filter can be used to add a lag in the phase response of a system.

- Gain  $K$ : The filter gain  $K$  determines the low frequency gain of the filter.
- Frequency  $f1$ : The lag in the phase response of the filter starts at frequency  $f1$  in Hz. This corresponds to an integrating behavior in the magnitude response from frequency  $f1$ .
- Frequency  $f2$ : The lag in the phase response of the filter stops at frequency  $f2$  in Hz. This corresponds to a constant attenuation in the magnitude response of the filter after frequency  $f2$ .

#### Transfer function of the filter

$$H_{lag}(s) = K \left( \frac{\frac{s}{2\pi f_2} + 1}{\frac{s}{2\pi f_1} + 1} \right)$$

The Lead Filter can be used to add a lead in the phase response of a linear system.

- Gain  $K$ : The filter gain  $K$  determines the low frequency gain of the filter.
- Frequency  $f1$ : The lead in the phase response of the filter starts at frequency  $f1$  in Hz. This corresponds to a differentiating behavior in the magnitude response from frequency  $f1$ .
- Frequency  $f2$ : The lead in the phase response of the filter stops at frequency  $f2$  in Hz. This corresponds to a constant gain in the magnitude response of the filter after frequency  $f2$ .

#### Transfer function of the controller

$$H_{lead}(s) = K \left( \frac{\frac{s}{2\pi f_1} + 1}{\frac{s}{2\pi f_2} + 1} \right)$$



The low pass filter can be used to filter out undesired high frequencies.

- Gain  $K$ : The filter gain  $K$  determines the low frequency gain of the filter.
- Frequency  $f$ : The filter roll off starts at frequency  $f$  in Hz. Lower frequencies will pass the filter, higher frequencies will be filtered out.

#### Transfer function of the filter

$$H(s) = \frac{K}{\frac{s}{2\pi f} + 1}$$

The low pass filter can be used to filter out undesired high frequencies.

- Gain  $K$ : The filter gain  $K$  determines the low frequency gain of the filter.
- Frequency  $f$ : The filter roll off starts at frequency  $f$  in Hz. Lower frequencies will pass the filter, higher frequencies will be filtered out.
- Quality  $Q$ : The filter quality indicates how steep the phase response will decrease at the frequency  $f$ . A quality  $Q > 0.707$  results in a peak in the magnitude response at frequency  $f$ .

#### Transfer function of the filter

$$H(s) = \frac{K(2\pi f)^2}{s^2 + 2\pi f \frac{s}{Q} + (2\pi f)^2}$$

The notch filter can be used to filter out an undesired frequency.

- Gain  $K$ : The filter gain  $K$  determines the frequency gain of the filter.
- Frequency  $f$ : The filter attenuates at frequency  $f$  in Hz. Lower and higher frequencies will pass the filter.
- Quality  $Q$ : The filter quality indicates how steep the magnitude response will be at the frequency  $f$ .

#### Transfer function of the filter:

$$H(s) = K \frac{s^2 + (2\pi f)^2}{s^2 + 2\pi f \frac{s}{Q} + (2\pi f)^2}$$

The universal notch filter can be used to filter out an undesired frequencies.

- Gain  $K$ : The filter gain  $K$  determines the low frequency gain of the filter.
- Frequency  $f_z$ : The filter attenuates at the zero frequency  $f_z$  in Hz. Lower and higher frequencies will pass the filter. A lead in the phase response will start at this zero frequency  $f_z$ .
- Frequency  $f_p$ : The filter amplifies at the pole frequency  $f_p$  in Hz. The phase lead will stop at this pole frequency  $f_p$ .
- Damping  $d_z$ : The filter damping of the zero  $d_z$  indicates how steep the magnitude response will be at the frequency  $f_z$ . More damping will result in a less steep behavior.
- Damping  $d_p$ : The filter damping of the pole  $d_p$  indicates how steep the magnitude response will be at the frequency  $f_p$ . Again, more damping will result in a less steep behavior.

**Transfer function of the filter:**

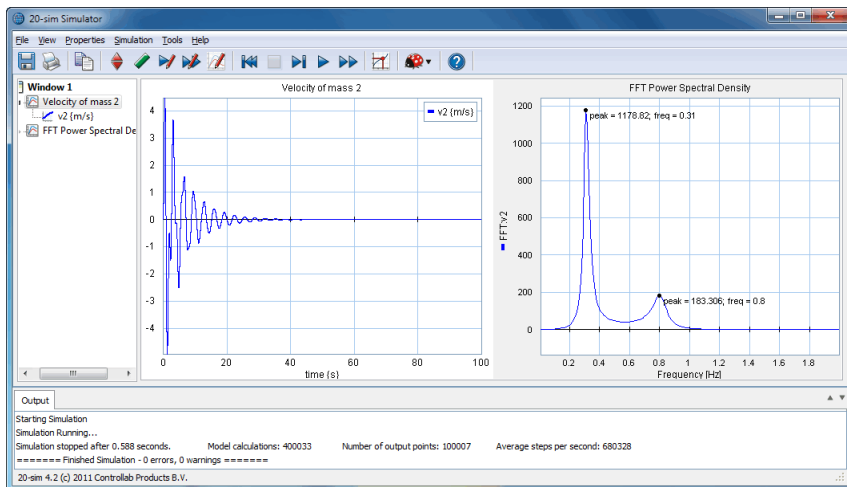
$$H(s) = K \frac{\frac{1}{(2\pi f_z)^2} s^2 + \frac{2d_z}{2\pi f_z} s + 1}{\frac{1}{(2\pi f_p)^2} s^2 + \frac{2d_p}{2\pi f_p} s + 1}$$

## 8.4 Frequency Domain Toolbox

### FFT Analysis

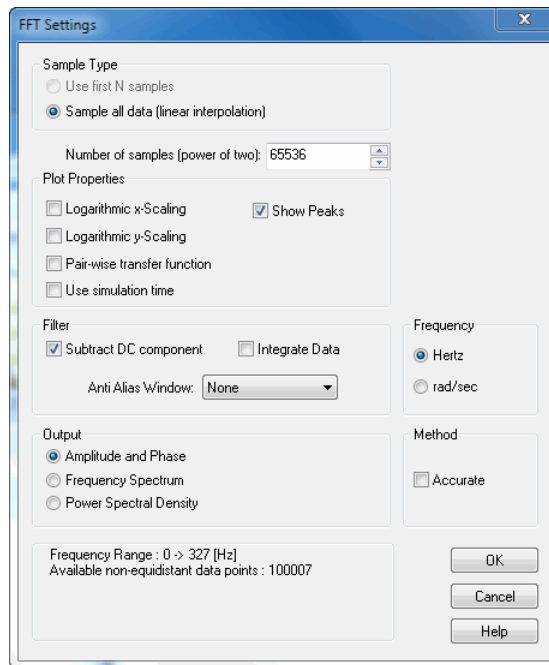
In FFT-Analysis, the Fast Fourier Transform is used to calculate the frequency contents of simulation signal. Three representations are supported:

- **Amplitude and Phase:** This representation shows the amplitude and phase of the signal as function of the frequency. This results is a graph very similar to a bode plot.
- **Frequency Plot:** This representation shows the frequency contents of the signal. Summation of the peak values yields the average power of the original time signal.
- **Power Spectral Density:** This representation shows the frequency contents of the signal. Integration over the frequency range yields the average power of the original time signal.



*FFT plot showing the power spectral density.*

FFT analysis can be performed in the Simulator by choosing the **FFT Analysis** command from the **Tools** menu. After selecting this command, a window will pop-up showing the FFT settings:



## Items

- **Sample Type**
  - **Use First N samples:** The first N simulation points will be used for the FFT calculations. This option is preferred if you have run a simulation with equidistant points (fixed step size).
  - **Sample all Data:** The complete simulation run will be sampled at equidistant points in time. Data points will be calculated through linear interpolation. This is the only option when you have run a simulation with variable step size.
- **Number of samples:** Choose the number of samples you would like to use for the FFT calculations. The number must be a power of two.
- **Plot Properties:** You can select logarithmic scaling and shared Y-axis and indicate the peaks in the plot.
- **Filter**
  - **Subtract DC-component:** If your signal contains a DC-component, the resulting Spectral Density plot will show a high peak at 0 Hz, which may obscure all other frequencies. Choose Subtract DC-component, to remove this peak from the Spectral Density plot.
  - **Integrate Data:** You can integrate the FFT data to inspect the energy contents of each frequency. This option is useful for analyzing resonance frequencies. Integrated FFT-data will usually show a sudden increase exactly at these frequencies.
- **Anti-Alias Window:** You can choose a Hamming, Hahn or Quadratic window to prevent aliasing.
- **Frequency:** Show the results in Herz or radians per second.
- **Output:** select the desired representation of the frequency data:

- *Amplitude and Phase*
- *Frequency Plot*
- *Power Spectral Density*
- *Status Window*: The bottom part of the window shows the number of simulation points and the chosen frequency range.

The results of an FFT plot strongly depend on the actual frequency contents of the time domain plot: if a frequency is not present in the original time signal, the FFT plot will not show it, even if the model is very much capable of showing activity for such a frequency. E.g. if you use a 50 Hz input signal for a current amplifier model, the FFT will certainly not show much. Instead use a frequency sweep input signal containing all frequencies of interest in order to get an output plot with enough frequency content. In other words: to get a good FFT plot, take care that you use input signals for your model that excite all frequencies of interest!

FFT plots show very good use when you want to compare a model with an existing system through measured data. In many cases, the measured data will show noise, making it hard to determine the resonant frequencies. If you make an FFT plot of both measurement data and model output, you can easily compare the resonant peaks.

The Fast Fourier Transform is an approximation of the standard Fourier Transform, using a time limited set of data. The begin and end parts of this limited data set may lead to aliasing effects (i.e. yielding not existing frequency peaks). Especially when using small data sets aliasing may lead to unwanted results.

To reduce aliasing, the data set can be preprocessed using special windows. These windows reduce the values at the begin and end of the data set and thus reduce the aliasing effects. Given an input array  $A[i]$  and an output array  $B[i]$ , with  $i = 1, 2, \dots, N$ , 20-sim supports the following windows:

- *None*: no preprocessing  $A == B$
- *Hamming Window*:  $B(i) = (0.54 + 0.46 \cdot \cos(\pi \cdot (i-1)/(N-1))) \cdot A(i)$ ,  $i = 1, 2, \dots, N$ .
- *Hann Window*:  $B(i) = 0.5 \cdot (1 + \cos(\pi \cdot (i-1)/(N-1))) \cdot A(i)$ ,  $i = 1, 2, \dots, N$ .
- *Quadratic Window*:  $B(i) = (1 - 2 \cdot ((i-1)/(N-1))^2) \cdot (1 - (i-1)/(N-1)) \cdot A(i)$ ,  $i = 1, 2, \dots, (N-1)/2+1$ ;  $B(i) = 2 \cdot (1 - ((i-1)/(N-1))^3) \cdot A(i)$ ,  $i = (N-1)/2+2, \dots, N$ .

## Model Linearization

In the *Simulator*, select the **Tools** menu and then click the **Linearize Model** to start linearization. Linearization will generate a linear, state-space description (linear system) out of any 20-sim model:

$$\begin{aligned} dx/dt &= Ax + Bu \\ y &= Cx + Du \\ x(0) \end{aligned}$$

Where:

$x$  = state vector  
 $x(0)$  = state vector initial value  
 $dx/dt$  = state vector derivative  
 $y$  = output  
 $u$  = input

And:

$A$  = system matrix  
 $B$  = input gain matrix  
 $C$  = output gain matrix  
 $D$  = direct link gain matrix

This linear system shows an input-output behavior that is closely related to the input-output behavior of the original model.

The result is shown in the Linear System Editor. In the Linear System Editor you can choose out of several plot options to show the response of the linear system, such as step responses and Bode plots.

### Working Point

Non-linear models can show variable behaviour. Think for example of an arm. When you stretch it and push against a wall, it is very stiff. When your arm is bent and you push it against a wall, it will be more compliant. Depending on which state it is in, linearization of a non-linear system will therefore result in different linear systems.

To get the correct linear system, we have to bring the non-linear system into the correct state. This can be done by giving it the proper inputs and simulate the system for a while until the desired state is reached. This is called the working point. When the working point is reached, the simulation must be stopped to perform linearization.

When linearization is performed without simulation, the working point is the initial state of the non-linear system.

### Symbolic and Numeric

In the 20-sim Simulator, out of an existing (non-linear) model, a symbolic linear-system can be derived. This means that states, rates and matrix elements are related to the parameters of the original model:



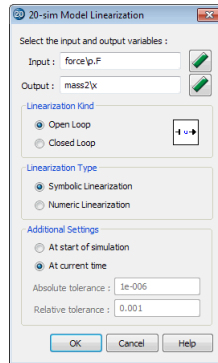
As a result you will get a linear system with the original model parameters that can be changed at will, without having to linearize again.

Symbolic linearization is not possible if the original model contains functions that cannot be differentiated. For such models linearization has to be performed numerically. The resulting linear system has to be recalculated through linearization for different model parameters.

### Procedure

1. Run a simulation until the working point is reached.

- Stop the simulation at operating point and select the **Linearize** command from the **Tools** menu.
- Enter your options in the Linearization Dialog.

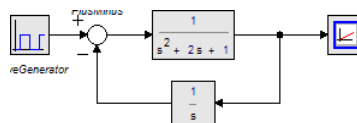


*The Linearization Toolbox.*

## Items

- Input:** Use the button to select the input (u).
- Output:** Use the button to select the output (y).
- Linearization Kind:** Choose between open loop and closed loop linearization.
- Linearize Type:** Choose between Symbolic and Numeric linearization.
- Additional Settings:** When you are performing numeric linearization, select **At current time** when you want to linearize at the operating point where the simulation was stopped. Select **At start of simulation** when you want to linearize at the start of the simulation.
- Tolerances:** 20-sim calculates a numerical linear state space model by small deviations of the complete model from the chosen setpoint. The deviations are based on the given absolute and relative tolerances. For most models the default values are sufficient. For stiff models you can change these values by hand.
- OK:** click the OK button to start Linearization.

During linearization you are asked to enter an input signal and an output signal of your (non-linear) model. During linearization, 20-sim will derive a corresponding linear system. It is important to understand that 20-sim will **cut** the model at the input. This will be explained with the example model below. It shows a linear system with feedback.

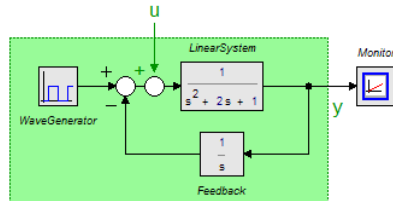


## Closed Loop

Suppose we would choose the following settings:

*input u: WaveGenerator\output*  
*output y: Monitor\input*  
*kind: Closed Loop*

This means that 20-sim will **add an input u** and linearize the model between this variable and the variable *Monitor\output* (equal to y in the figure below). 20-sim will thus linearize the system between u en y and (in this example) and yield the **closed loop system**.

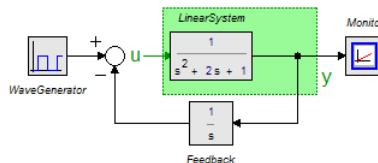


## Open Loop

Suppose we would choose the following settings:

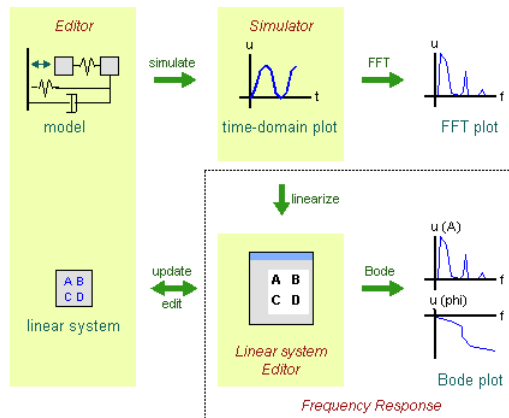
*input u: PlusMinus\output*  
*output y: Monitor\input*  
*kind: Open Loop*

This means that 20-sim will **cut** the model at the variable *PlusMinus\output* (equal to u in the figure below) and linearize the model between this variable and the variable *Monitor\input* (equal to y in the figure below). 20-sim will thus linearize the system between u en y and (in this example) and yield the **open loop system**.





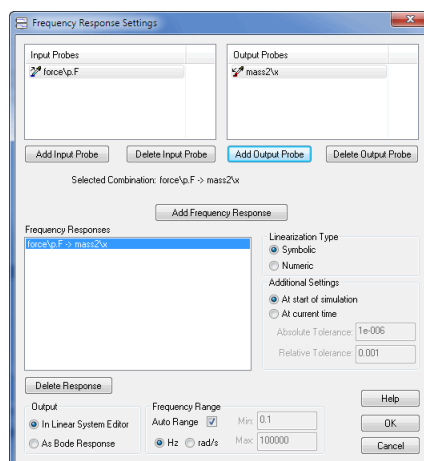
Next to time domain analysis through the standard time domain plots, 20-sim can also show results in the frequency domain through FFT analysis and Bode Plots. The picture below shows the various actions and resulting plots.



Bode plots originate from linear systems theory. A bode plot shows the amplitude and phase response (as a function of the frequency) of a linear system. In 20-sim linear systems can be derived in the Simulator out of any linear or non-linear model (model linearization). The resulting linear system is shown in the Linear System Editor. In this editor you can generate Bode plots. The generation of Bode plots can be automated in the Frequency Response dialog. In this dialog you can define the linearization settings and desired linearization output (Linear System Editor or Bode plot).

Procedure

1. Select the **Frequency Response** from the command from the **Properties** menu.
2. Enter your options in the Frequency Response Dialog.

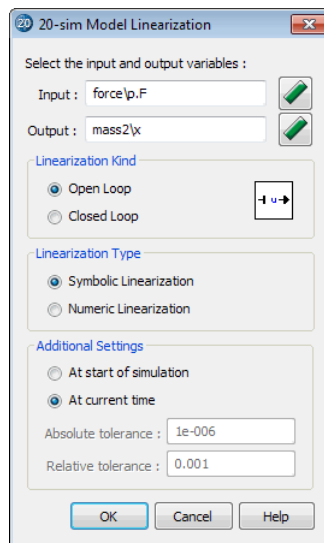


*The Frequency Response dialog.*

## Items

- **Input Probes:** Enter possible input signals for linearization here.
- **Output Probes:** Enter possible output signals for linearization here.
- **Frequency Response:** With the Add Frequency Response you can add new input/output pairs. For every input/output pair linearization will be performed with a corresponding linear system as result.
- **Symbolic/Numeric:** Select the desired linearization method.
- **At start of simulation/At current time:** Select the time of the linearization.
- **Tolerances:** For numeric linearization you can enter the absolute and relative tolerances.
- **Output:** Select the desired output of the linearization.
- **Frequency Range:** Select the desired frequency range.
- **OK:** click the OK button to close the dialog.

When using numerical linearization, absolute and relative tolerances can be set. In this section is explained how 20-sim uses these tolerances to derive a linear system for the model equations.



## Algorithm

Suppose you have chosen the following tolerance values.

$\alpha$  = absolute tolerance (e.g.  $1e-6$ )

$\beta$  = relative tolerance (e.g.  $1e-3$ )

Suppose we have the following model:

$$\begin{aligned} \text{ddt}(x) &= 4 * x + 2 * u; \text{ // with } u = 1 \\ y &= 1 * x + 3 * u; \text{ // with } x = 2 \end{aligned}$$

During the linearization procedure (suppose linearization from  $u$  to  $y$ ) 20-sim will vary the input variable and state variables. First we will show the variation for the input  $u$ :

$$\begin{aligned}u' &= (1 + \text{beta}) * u + \text{alpha} \\u'' &= (1 - \text{beta}) * u - \text{alpha} \\\text{delta}_u &= \text{beta} * u + \text{alpha}\end{aligned}$$

this will yield

$$\begin{aligned}x_{\text{dot}}' &= 10.002002 \text{ and } y' = 5.003003 \\x_{\text{dot}}'' &= 9.997998 \text{ en } y'' = 4.996997\end{aligned}$$

Out of this 20-sim will calculate the B and D vectors of the state-space ABCD representation:

$$\begin{aligned}B &= (x_{\text{dot}}' - x_{\text{dot}}'') / (2 * \text{delta}_u) = 2 \\D &= (y' - y'') / (2 * \text{delta}_u) = 3\end{aligned}$$

The variation of state variables is done accordingly:

$$\begin{aligned}x' &= (1 + \text{beta}) * x + \text{alpha} \\x'' &= (1 - \text{beta}) * x - \text{alpha} \\\text{delta}_x &= \text{beta} * x + \text{alpha}\end{aligned}$$

this will yield

$$\begin{aligned}x_{\text{dot}}' &= 10.008004 \text{ en } y' = 5.002001 \\x_{\text{dot}}'' &= 9.991996 \text{ en } y'' = 4.997999\end{aligned}$$

Out of this 20-sim will calculate the A matrix and C vector of the state-space ABCD representation:

$$\begin{aligned}A &= (x_{\text{dot}}' - x_{\text{dot}}'') / 2 * \text{delta}_x = 4 \\C &= (y' - y'') / 2 * \text{delta}_x = 1\end{aligned}$$

The example system is linear, so the corresponding ABCD representation will give an equal system. The shown algorithm works equivalent for non-linear models. Suppose we have the following non-linear model:

$$\begin{aligned}\text{ddt}(x) &= 4 * \sin(x) + 2 * u; \text{ // with } u = 1 \\y &= 1 * x + 3 * u; \text{ // with } x = 2\end{aligned}$$

This will yield:

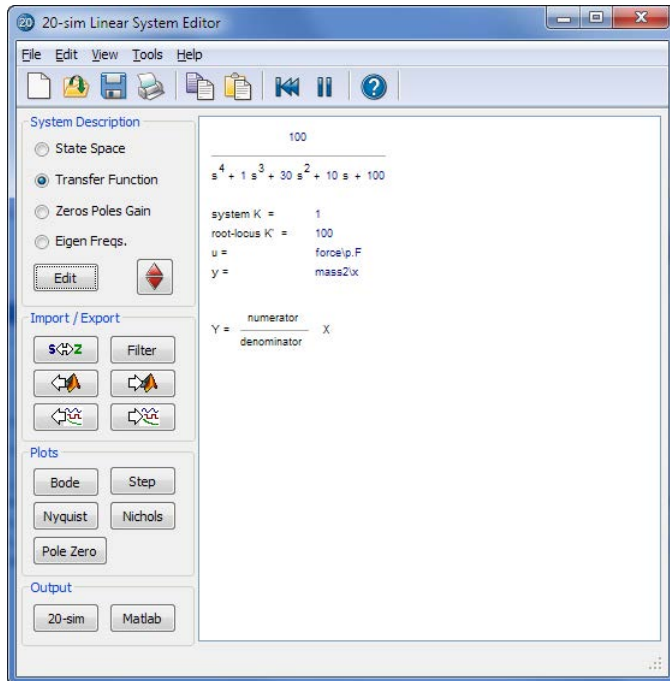
$$B = 2, D = 3, A = -1.668445, C = 1;$$

## Tolerance Values

The absolute tolerance is necessary only if the input or state is zero. In that case the contribution of the relative tolerance is zero and will not give a contribution to the algorithm. There is however a problem with the absolute tolerance. Suppose the input =  $1e-12$  and the state =  $1e+6$  (ill-scaled model). For the input an absolute tolerance of  $1e-6$  will yield a far too large deviation, while the same absolute tolerance is negligible compared to the state. Only if both the state and input are nonzero the absolute tolerance can be made non-zero to yield good results.

## Linear System Editor

The Linear System Editor of 20-sim allows you to enter or edit linear time- invariant models. It supports continuous and discrete-time single input / single output (SISO) systems. You can open the Linear System Editor from the Tools menu of the 20-sim Editor or by clicking Go Down on the Linear System model. A linear system can also be the result of a linearization operation in the 20-sim Simulator.




### Menu

Some menu items are of particular importance.






- **File:** You can use the file menu to open, import and export linear systems.
- **Edit - Tolerance:** You can specify the tolerance for transforming between state-space and transfer functions.
- **Edit - Reduce System:** You can reduce the system order by pole-zero cancelation. The distance between poles and zeros to match for cancelation is given by the **Reduction Tolerance**.
- **View:** the view menu can be used for holding, clearing and refreshing plots.

### System Description

- Pressing the **Edit** button will open a dialog for editing the linear system. Each description (State Space, Transfer Function, Zeros Poles Gain or Eigen Frequency) has a special dialog and can be used to specify continuous-time and discrete-time systems.

- In the 20-sim Simulator, out of an existing (non-linear) model a symbolic linear-system can be derived by means of linearization. This means that the relevant model parameters are preserved in the Linear System and the parameters button  can be used to change parameters.

## Import/Export

- Pressing the **s<->z** button  will transform a continuous-time linear system into a discrete-time linear system and back.
- Pressing the **Filter** button opens the Filter Editor, where a filter can be designed. This filter can then be combined with the current linear system or replace the current linear system. If the linear system is a discrete-time system, the designed analog filter is automatically transferred into its digital equivalent.
- Pressing the **From Matlab** button  and the **To Matlab** button  allows for an instant exchange of the linear system with the Matlab workspace. Information is transferred numerically (no parameter relations are preserved)
- The  button is only active when a Linear System has been imported through linearization. Clicking the button will import parameters from the simulation.
- The  button is only active when a Linear System has been imported through linearization. Clicking the button will export the current parameters to the simulation.

## Plots

You can inspect the time- and frequency responses of the linear system using:

- Step Response
- Bode Plot
- Nyquist Plot
- Nichols Chart
- Poles and Zeros (including root locus)

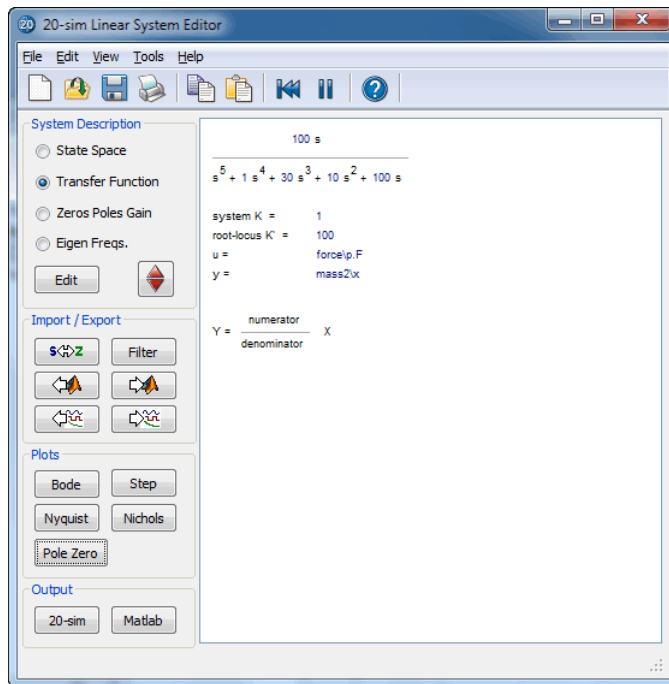
## Output

- Clicking the **20-sim** button will export the linear system as a new 20-sim submodel.
- Clicking the **Matlab** button will export the 20-sim Linear System to a Matlab m-file. If the Linear System is symbolic, all parameter relations are preserved.

In the 20-sim Simulator, out of an existing (non-linear) model a symbolic linear-system can be derived by means of linearization. This means that the relevant model parameters are preserved in the Linear System.




The relation between the original model parameters and the linear system elements is always shown in the white square of Linear System editor, just below the system description. An example is shown in the first figure below:




As you can see, the some elements of the A, B, C and D matrix are related to the spring constant and masses of the original model.

### Editing

A symbolic linear system can be edited by changing the original model parameters. Click the Edit Parameters button  and a Parameters Editor pops-up. Change the desired parameters, close the Parameters Editor and the linear system will be updated.


### Updating Parameters

When the parameters have been changed in the Linear System Editor you can update the parameters in the Simulator by clicking the **Update to Simulator** button .

Click the **Update from Simulator** button  to do it the other way.

### Exporting

You can export a symbolic Linear System to Matlab, with preservation of the parameter relations, by clicking the **Matlab** button or selecting *Export to Matlab* command from the *File* menu. This will generate an m-file that you can use in Matlab.

The Linear System Editor works on continuous time as well as discrete time system. Pressing the **s<->z** button  will transform a continuous-time linear system into a discrete-time linear system and back. You can choose between a Bilinear transformation (Tustin), a Forward Euler transformation and a Backward Difference transformation. When a continuous-time system is transferred, the user is asked to specify the sample time of the discrete-time system.

If you want to transfer a linear system directly (i.e. replace the z by s or vice versa), click the **Edit** button and select or deselect the Discrete Sample time.

Models with time delays can not be linearized in 20-sim, because there is no direct relation between the inputs and outputs of the model. For systems with control loops it is however useful to see how the unavoidable time delay of these loops can affect the model behaviour.

Therefore in the linear system editor you can add output delay. The effects of this output delay is shown in the various plots that you can show of a linear system. The unit of the output delay is seconds.

### Note

Output delay is not saved when you store a linear system model and will therefore not affect the behaviour of the model!

State space models use linear differential equations (continuous) or difference equations (discrete) to describe system dynamics. They are of the form:

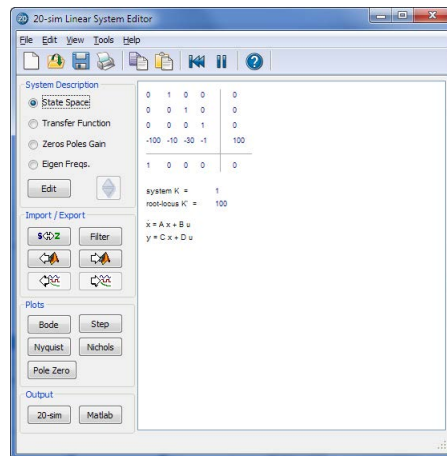
$$\begin{aligned} \frac{dx}{dt} &= A \cdot x + B \cdot u & x_{n+1} &= A \cdot x_n + B \cdot u_n \\ y &= C \cdot x + D \cdot u & y_n &= C \cdot x_n + D \cdot u_n \end{aligned}$$

(continuous)                      (discrete)

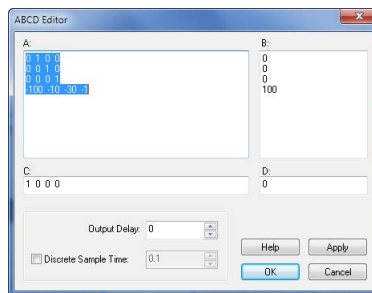
with for example:

$$\begin{aligned} A &= \begin{bmatrix} 0 & 0.5 \\ -1 & -1 \end{bmatrix} & B &= \begin{bmatrix} -0.1 \\ 0.1 \end{bmatrix} \\ C &= \begin{bmatrix} 0 & 1 \end{bmatrix} & D &= \begin{bmatrix} 0 \end{bmatrix} \end{aligned}$$

where x is the state vector and u and y are the input and output vectors. These models may arise from the equation of physics, from state space identification or as the result of linearization.



You can enter state space models by selecting the *State Space* button and clicking the *Edit* button.



This opens an editor in which you can enter the A, B, C and D matrices. Depending on the selection of the Discrete Linear System check box (and Sample Time) the system is a continuous-time or discrete-time system. You can enter the matrix elements in the white space areas. Separate column elements with Spaces or Commas. Enter new rows by clicking the Enter key (new line) or using a semicolon. Brackets ( e.g. [ ... ] ) may be used to denote the a matrix or vector.

The A-matrix, shown in the figure above can for example be entered as:

```
0 1
-0.5 -1
```

or

```
0,1;-0.5,-1
```

or

```
[0,1;
-0.5,-1]
```



## Output Delay

To inspect the effects of time delay in your model, you can add output delay. The result will be visible in the various plots that you can show of a linear system. The unit of the output delay is seconds.

## Discrete Sample Time

If you want to transfer a linear system from continuous time to discrete time directly (i.e. replace the  $s$  by a  $z$ ), select Discrete Sample time and fill in the sample time value. You can also transfer back directly by deselecting Discrete Sample time.

## Commands

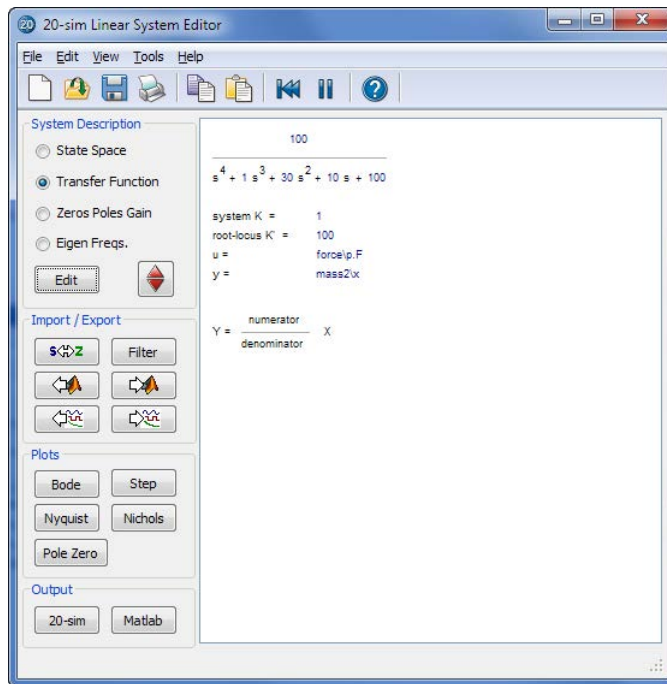
- *Help*: Open the help file.
- *Apply*: Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero).
- *OK*: Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero) and close the editor.
- *Cancel*: Do not apply any changes to the system and close the editor.

A continuous time or discrete time SISO transfer function:

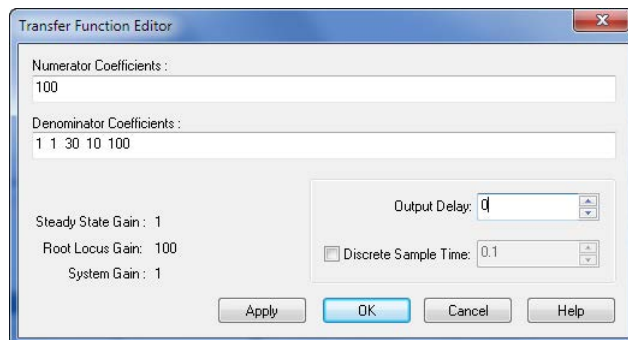
$$h(s) = \frac{n(s)}{d(s)} \quad h(z) = \frac{n(z)}{d(z)}$$

(continuous)                      (discrete)

is characterized by its numerator  $n$  and denominator  $d$ , both polynomials of the variable  $s$  or  $z$ .



You can enter transfer functions by selecting the *Transfer* Function button and clicking the *Edit* button.



This opens an editor in which you can enter the coefficients of the numerator and denominator polynomials. You can enter the elements in the white space areas. Separate the elements with Spaces. Polynomials should be entered in descending powers of  $s$  or  $z$ . The Steady State Gain, Root Locus Gain and System Gain are parameters, that are automatically derived from the transfer function.

In the editor shown above the transfer function

$$\frac{0.1 \cdot s + 0.1}{s^2 + s + 0.5}$$

was given. You can enter the coefficients as:

0.1 0.1

and

1 1 0.5

or

0.1,0.1

and

1,1,0.5

### Output Delay

To inspect the effects of time delay in your model, you can add output delay. The result will be visible in the various plots that you can show of a linear system. The unit of the output delay is seconds.

### Discrete Sample Time

If you want to transfer a linear system from continuous time to discrete time directly (i.e. replace the  $s$  by a  $z$ ), select Discrete Sample time and fill in the sample time value. You can also transfer back directly by deselecting Discrete Sample time.

### Commands

- *Help*: Open the help file.
- *Apply*: Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero).
- *OK*: Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero) and close the editor.
- *Cancel*: Do not apply any changes to the system and close the editor.

### Steady State Gain

Given the transfer function:

$$h(s) = \frac{n(s)}{d(s)} = \frac{n_i \cdot s^i + n_{i-1} \cdot s^{i-1} + \dots + n_0 \cdot s^0}{d_j \cdot s^j + d_{j-1} \cdot s^{j-1} + \dots + d_0 \cdot s^0}$$

the **Steady State Gain** is defined as:

$$K_{ss} = \lim_{s \rightarrow 0} h(s)$$

Note that the steady state gain can be zero or infinite depending on the element values of the numerator and denominator!

## Root Locus Gain

Given an system described by the transfer function:

$$h(s) = \frac{n(s)}{d(s)} = \frac{n_i \cdot s^i + n_{i-1} \cdot s^{i-1} + \dots + n_0 \cdot s^0}{d_j \cdot s^j + d_{j-1} \cdot s^{j-1} + \dots + d_0 \cdot s^0}$$

This transfer function can be rewritten in pole zero notation with

$$h(s) = K_{RL} \frac{(s - z_i)(s - z_{i-1}) \dots (s - z_0)}{(s - p_j)(s - p_{j-1}) \dots (s - p_0)}$$

where  $p_i \dots p_1$  are the poles and  $z_i \dots z_1$  are the zeros of the system. The gain  $K_{RL}$  is known as the *Root Locus Gain*. Note that it can easily be derived from the transfer function as:

$$K_{RL} = \frac{\text{first element of } n(s)}{\text{first element of } d(s)} = \frac{n_i}{d_j}$$

## System Gain

Given the transfer function:

$$h(s) = \frac{n(s)}{d(s)} = \frac{n_i \cdot s^i + n_{i-1} \cdot s^{i-1} + \dots + n_0 \cdot s^0}{d_j \cdot s^j + d_{j-1} \cdot s^{j-1} + \dots + d_0 \cdot s^0}$$

If  $n_0$  and  $d_0$  are unequal to zero, this transfer function can be rewritten in pole zero notation with:

$$h(s) = K_s \frac{(z'_i s + 1)(z'_{i-1} s + 1) \dots (z'_0 s + 1)}{(p'_j s + 1)(p'_{j-1} s + 1) \dots (p'_0 s + 1)}$$

The gain  $K_s$  is known as the *System Gain*. If  $n_0$  is zero and  $n_1$  is nonzero an equivalent notation can be found with an extra  $s$  multiplied:

$$h(s) = K_s \frac{(z'_i s + 1)(z'_{i-1} s + 1) \dots (z'_1 s + 1) \cdot s}{(p'_j s + 1)(p'_{j-1} s + 1) \dots (p'_0 s + 1)}$$

If more numerator element are zero, extra multiplications with  $s$  are added. The same goes for denominator elements equal to zero. In general the System Gain can be derived from the transfer function as:

$$K_s = \frac{\text{last nonzero element of } n(s)}{\text{last nonzero element of } d(s)}$$

## Relating the Gains

The elements of the System Gain are related to the poles and zeros of the Root Locus Gain as:

$$z'_i = \frac{-1}{z_i} \quad , \quad p'_j = \frac{-1}{p_j} \quad etc.$$

If  $z_0$  and  $p_0$  are unequal to zero, the following equation holds:

$$K_{RL} = K_s \frac{z_i \cdot z_{i-1} \cdot \dots \cdot z_0}{p_j \cdot p_{j-1} \cdot \dots \cdot p_0}$$

The Root Locus Gain and the Steady State Gain are related as:

$$K_{SS} = K_{RL} \frac{-z_i \cdot -z_{i-1} \cdot \dots \cdot -z_0}{-p_j \cdot -p_{j-1} \cdot \dots \cdot -p_0}$$

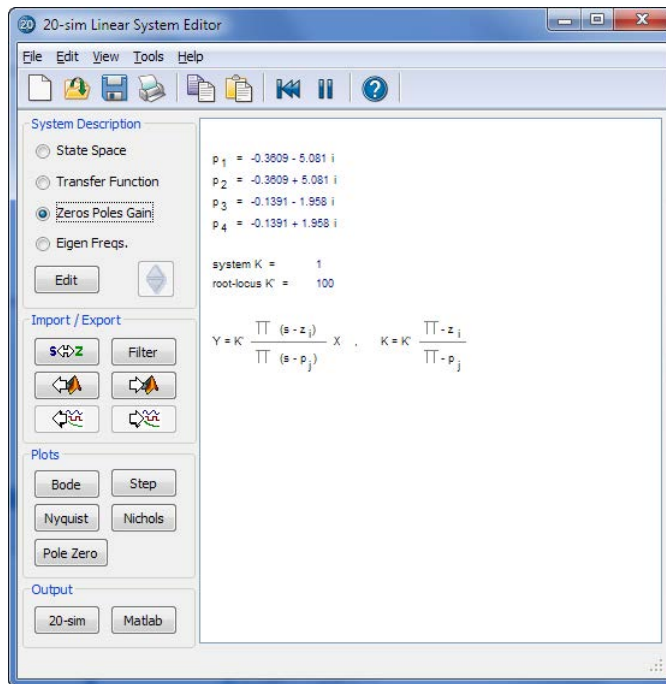
A continuous-time SISO transfer function can be described by the transfer function:

$$h(s) = \frac{n(s)}{d(s)} = \frac{n_i \cdot s^i + n_{i-1} \cdot s^{i-1} + \dots + n_0 \cdot s^0}{d_j \cdot s^j + d_{j-1} \cdot s^{j-1} + \dots + d_0 \cdot s^0}$$

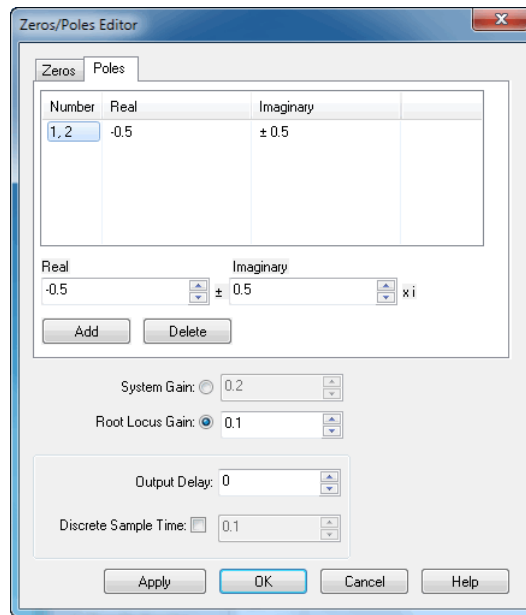
This transfer function can be rewritten in pole zero notation with

$$h(s) = K_{RL} \frac{(s - z_i)(s - z_{i-1}) \dots (s - z_0)}{(s - p_j)(s - p_{j-1}) \dots (s - p_0)}$$

where  $p_i \dots p_1$  are the poles and  $z_i \dots z_1$  are the zeros and  $K_{RL}$  is the Root Locus Gain of the system. The same can be done for a discrete-time SISO transfer function.



You can enter zeros and poles by selecting the *Zeros & Poles* button and clicking the *Edit* button.



This opens an editor in which you can enter the real and imaginary parts of the zeros and poles as well as the Root Locus Gain. If preferred, you can also enter the System Gain. Note that zeros and poles always have conjugate when the imaginary part is non-zero. I.e. when you enter a pole with imaginary part 0.5 an extra pole is added with imaginary part -0.5.

### Output Delay

To inspect the effects of time delay in your model, you can add output delay. The result will be visible in the various plots that you can show of a linear system. The unit of the output delay is seconds.

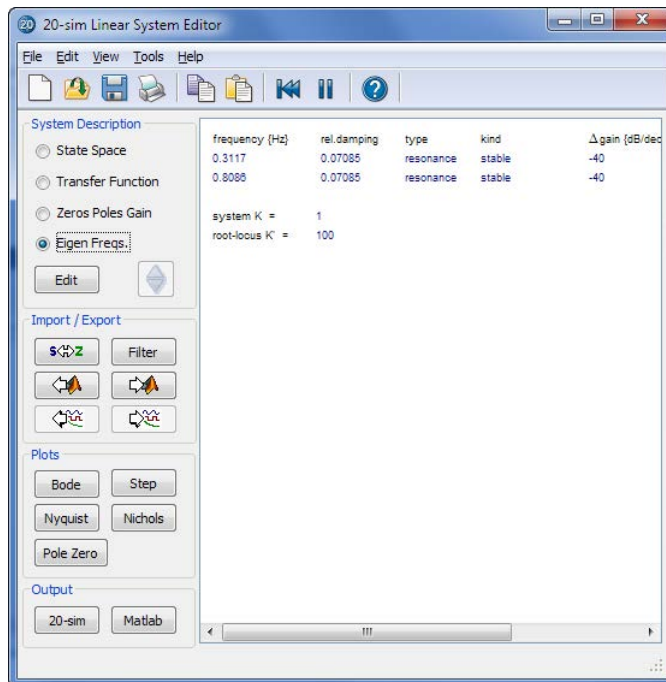
### Discrete Sample Time

If you want to transfer a linear system from continuous time to discrete time directly (i.e. replace the  $s$  by a  $z$ ), select Discrete Sample time and fill in the sample time value. You can also transfer back directly by deselecting Discrete Sample time.

### Commands

- **Add/Delete:** Add or delete selected poles or zeros.
- **Help:** Open the help file.
- **Apply:** Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero).
- **OK:** Apply the current changes of the system, recalculate each plot that is active (step, Bode, Nyquist, Nichols, pole zero) and close the editor.
- **Cancel:** Do not apply any changes to the system and close the editor.

The Eigen Frequencies view is closely related to the pole zero notation and bode plot. It shows the resonance frequencies and anti-resonance frequencies that result from the given poles and zeros as well as some characteristic parameters from the bode plot.



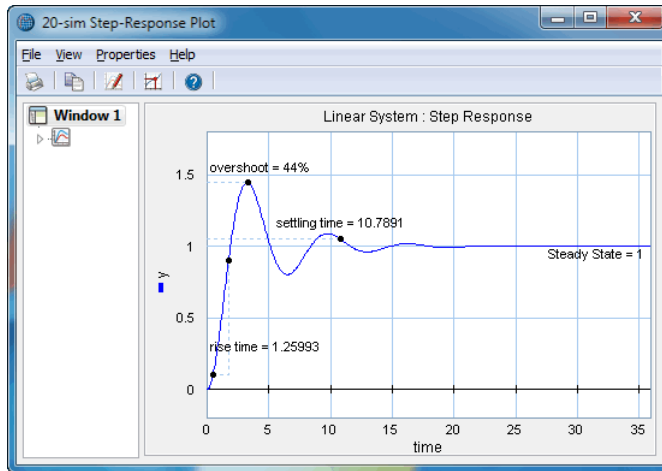
You can enter transfer functions by selecting the *Eigen Freqs.* button and clicking the *Edit* button.

The *Step Response* command calculates the systems response  $y$  on a unit step input:



$$u = 0 \text{ (time } < 0 \text{ )}$$

$$u = 1 \text{ (time } \geq 0 \text{ )}$$



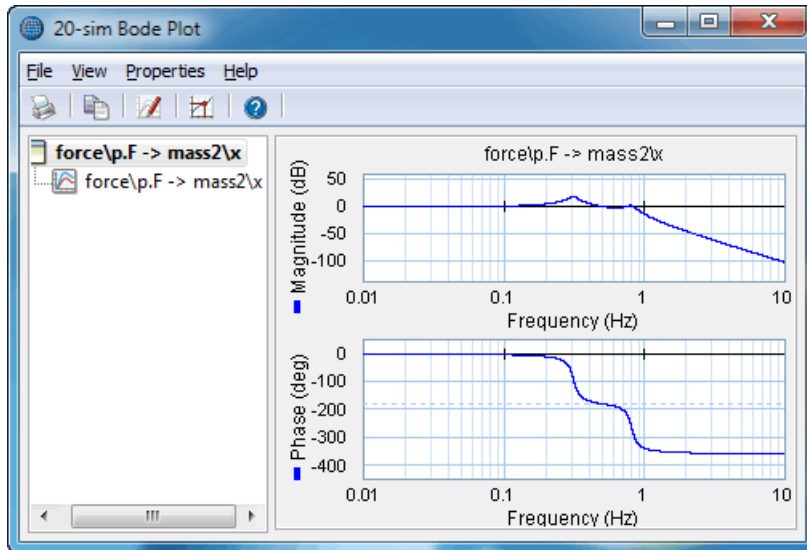
20-sim automatically generates an appropriate range for the time response, based on the system dynamics. With the Plot Properties command (right mouse menu), you can change this horizon and recalculate the step response (click the Step command again).

### Plot Options

Using the right mouse menu, you can use several options:

- **Plot Properties:** Set the general plot properties for the step response and specify the curve properties.
- **Numerical Values:** Inspect numerical values.
- **Step Characteristics:** Display rise time, overshoot, settling time and the steady state value of the step response.
- **Copy to Clipboard:** Copy the plot to the windows clipboard.
- **Print:** Print the plot.
- **Zoom in:** Show a detail of the plot.
- **Zoom out:** Show a larger portion of the plot.
- **Zoom Normal:** Show the complete plot.

Bode Plots show the amplitude and phase of a linear system as function of the frequency. Bode plots can be shown for every 20-sim model through Linearization. During Linearization you are asked to enter the input variable and output variable for which linearization should be performed. After that the linear system is calculated and shown in the Linear System Editor. From the Linear System Editor you can generate a bode plot. These actions can also be predefined using the Frequency Response command of the *Properties* menu.



20-sim automatically generates a range of logarithmically displayed frequencies, based on the system dynamics. With the **Plot Properties** command (**right mouse menu**), you can change this horizon and recalculate the bode response (click the Bode command again).

The magnitude part of the plot can be displayed in dB or in absolute values. The phase part can be displayed in radians or degrees. The frequency can be displayed in radians per second or in Hz.

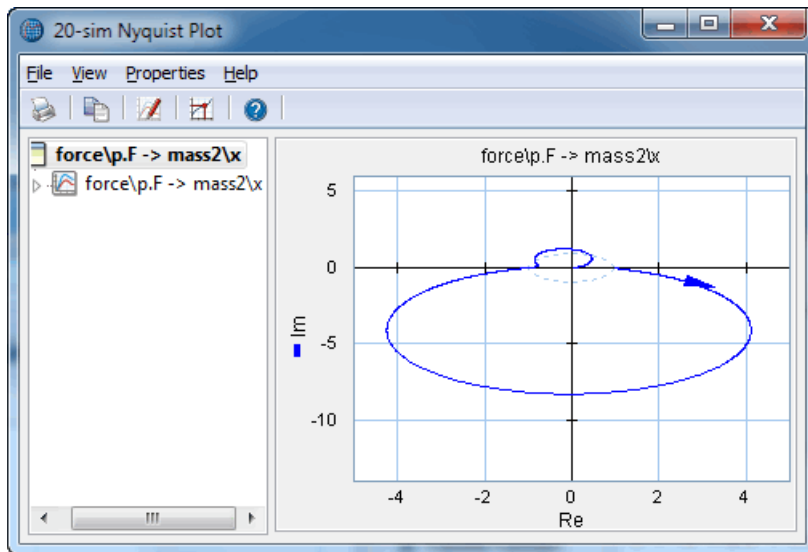
### Plot Options

Using the toolbar or the right mouse menu, you can use various options:

- *Plot Properties*: Set the plot properties.
- *Numerical Values*: Inspect numerical values.
- *Magnitude (dB)*: Display magnitude in decibels
- *Magnitude (-)*: Display magnitude in absolute values.
- *Phase (rad)*: Display phase in radians.
- *Phase (deg)*: Display phase in degrees.
- *Frequency (rad/sec)*: Display frequency in radians per second.
- *Frequency (Hz)*: Display frequency in Hz.
- *Phase/Gain Margins*: Display the gain and phase margins.
- *Modulus Margin*: Display the Modulus Margin.

- *Peak Response*: Display the peak response.
- *Copy to Clipboard*: Copy the plot to the windows clipboard.
- *Print*: Print the plot.
- *Zoom in*: Show a detail of the plot.
- *Zoom out*: Show a larger portion of the plot.
- *Zoom Normal*: Show the complete plot.

The **Nyquist** command computes the Nyquist plot of a system.



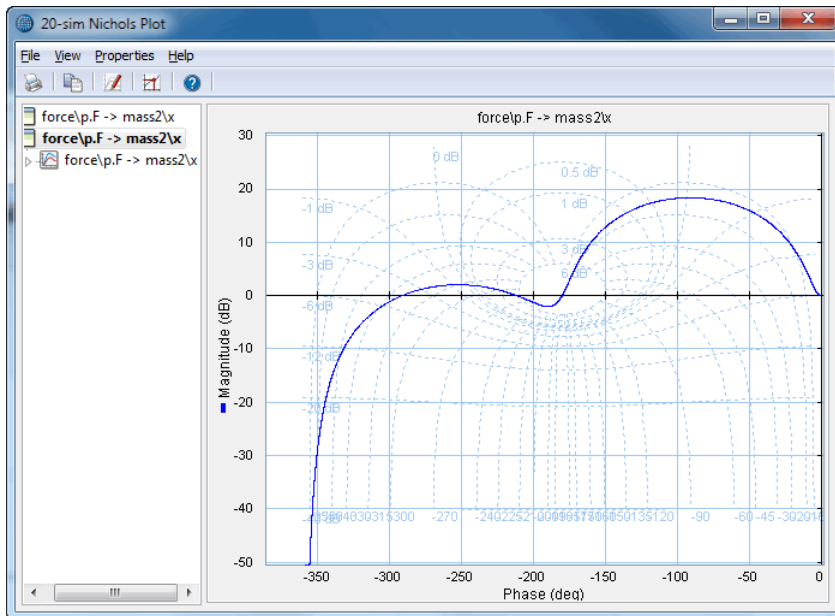
20-sim automatically generates a range of real and imaginary parts, based on the system dynamics. With the **Plot Properties** command (right mouse menu), you can change this horizon and recalculate the Nyquist diagram (click the **Nyquist** command again).

### Plot Options

Using the right mouse menu, you can use several options:

- *Plot Properties*: Set the plot properties.
- *Numerical Values*: Inspect numerical values.
- *Phase/Gain Margins*: Display the gain and phase margins.
- *Modulus Margin*: Display the Modulus Margin.
- *Copy to Clipboard*: Copy the plot to the windows clipboard.
- *Print*: Print the plot.
- *Zoom in*: Show a detail of the plot.
- *Zoom out*: Show a larger portion of the plot.
- *Zoom Normal*: Show the complete plot.

The *Nichols* command computes the Nichols chart of a system.



20-sim automatically generates a range of logarithmically displayed frequencies, based on the system dynamics. With the **Plot Properties** command (right mouse menu), you can change this horizon and recalculate the Nichols chart (click the **Nichols** command again). The magnitude part of the plot can be displayed in decibels (dB) or in absolute values. The phase part can be displayed in radians or degrees.

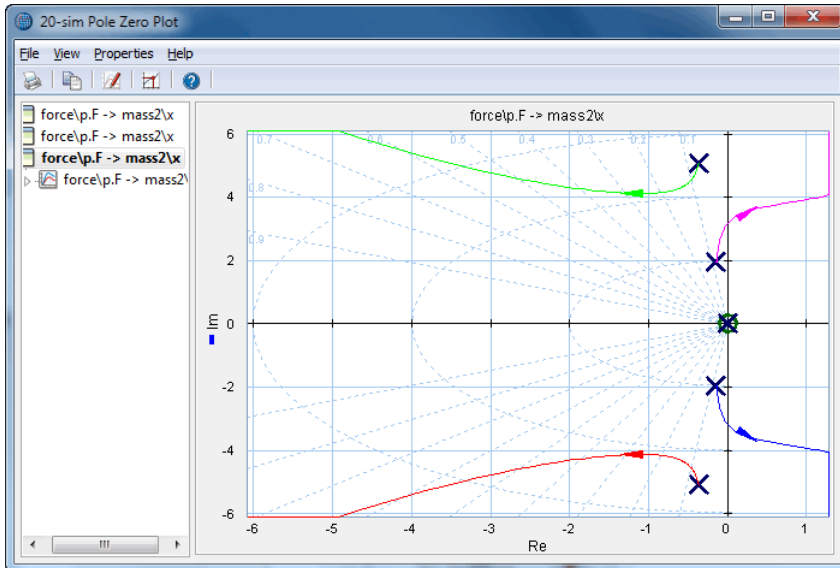
### Plot Options

Using the right mouse menu, you can use several options:

- *Plot Properties*: Set the plot properties.
- *Numerical Values*: Inspect numerical values.
- *Magnitude (dB)*: Display magnitude in decibels
- *Magnitude (-)*: Display magnitude in absolute values.
- *Phase (rad)*: Display phase in radians.
- *Phase (deg)*: Display phase in degrees.
- *Frequency (rad/sec)*: Display frequency in radians per second.
- *Frequency (Hz)*: Display frequency in Hz.
- *Phase/Gain Margins*: Display the gain and phase margins.
- *Modulus Margin*: Display the Modulus Margin.
- *Copy to Clipboard*: Copy the plot to the windows clipboard.
- *Print*: Print the plot.
- *Zoom in*: Show a detail of the plot.

- *Zoom out*: Show a larger portion of the plot.
- *Zoom Normal*: Show the complete plot.

The **Pole Zero** command plots the poles and zeros of a system and computes the root locus plot.



20-sim automatically generates a range of real and imaginary parts, based on the system dynamics. With the **Plot Properties** command (right mouse menu), you can change this horizon and recalculate the pole zero diagram (click the **Pole Zero** command again).

### Root Locus

You can show the rootlocus plot by selecting **Root Locus** from the right mouse menu. Inspect the root locus gain by selecting **Numerical Values** from the right mouse menu.

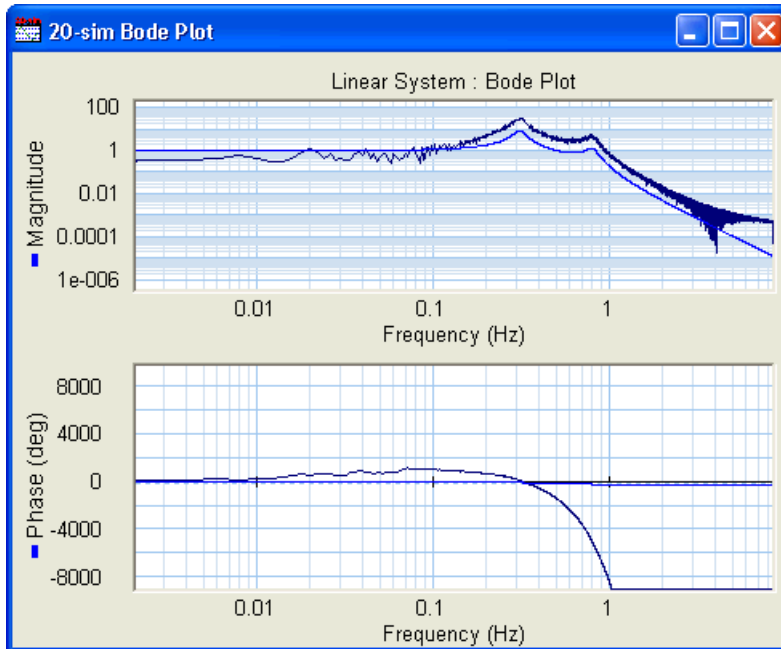
### Plot Options

Using the right mouse menu, you can use several options:

- *Plot Properties*: Set the plot properties.
- *Numerical Values*: Inspect numerical values.
- *Root Locus*: Show or hide the root locus plot.
- *Copy to Clipboard*: Copy the plot to the windows clipboard.
- *Print*: Print the plot.
- *Zoom in*: Show a detail of the plot.
- *Zoom out*: Show a larger portion of the plot.
- *Zoom Normal*: Show the complete plot.

You can import data from measurements or other software tools to compare it with the response of your model. 20-sim accepts data in two formats:

- **Gain-Phase:** The data should be stored in a text-file with three columns. The first column should contain the frequency and the second and third column, the corresponding gain and phase data.
- **Real-Imag:** The data should be stored in a text-file with three columns. The first column should contain the frequency and the second and third column, the corresponding real and imaginary data.



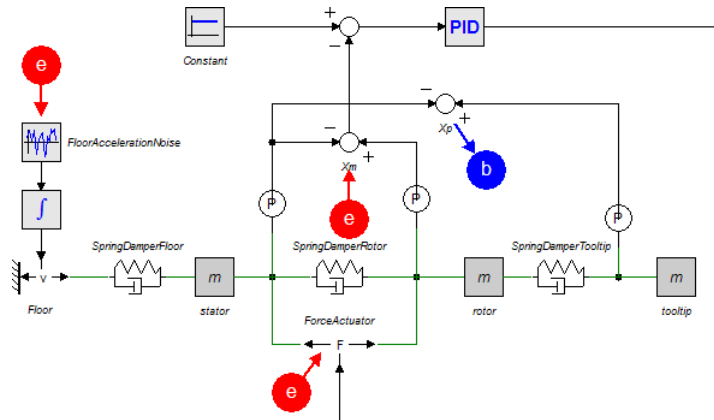
## Import Data

1. Open the Linear System Editor with your linear system.
2. Open the plot (e.g. Bode, Nyquist) in which you want to show the data.
3. Set the Magnitude (- or dB), Phase (rad or deg) and Frequency (rad/s or Hz) according to the data you want to import.
4. In the Linear System Editor from the **File** menu select **Import**.
5. Select Import **Gain-Phase** or **Import Real-Imag**.

Now a file dialog opens helping you to select the file to import. When you have selected a file and closed the dialog, the data should be visible in your plot. An example is shown in the figure above.

## Dynamic Error Budgeting

The performance of precision machines is mostly limited by the disturbances that are injected in these machines. These disturbances are often stochastic in nature. Dynamic Error Budgeting is a method whereby the effect of these disturbances on the final performance can be calculated. The advantage of this method is that it enables the designer to enter the contributions of the individual disturbances and view and optimize the overall machine performance.



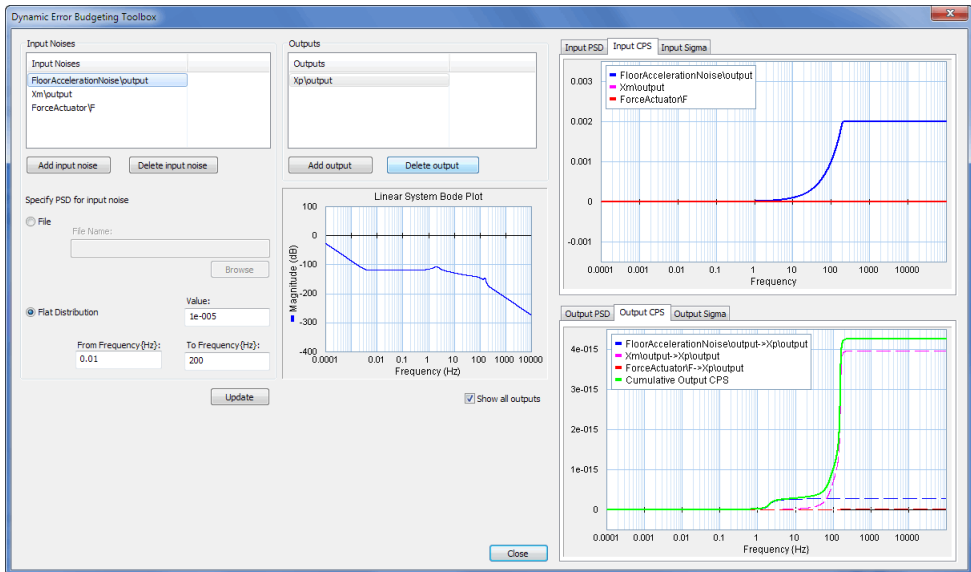
The Dynamic Error Budgeting toolbox shows the total error as a result of injected disturbances.

## Running the Toolbox

1. Open the example model *Dynamic Error Budgeting* from the *Getting Started/Frequency Domain Toolbox*.

You can open the Dynamic Error Budgeting tool in the *Simulator*:

2. From the **Tools** menu select **Frequency Domain Toolbox** and **Dynamic Error Budgeting**.



*The Dynamic Error Budgeting tool.*

The tool allows you to enter disturbances (as power spectral density) in the *Input Noises* section.

- For each disturbance you have to select a corresponding variable by clicking the **Add input noise** button.

Each disturbance is effectively a summation to the chosen variable, just like closed loop linearization. You can inspect each disturbance in the graph on the top right.

Next you have to select an output variable, where the result of the disturbances is calculated.

- Select the output by clicking the **Add Output** button.

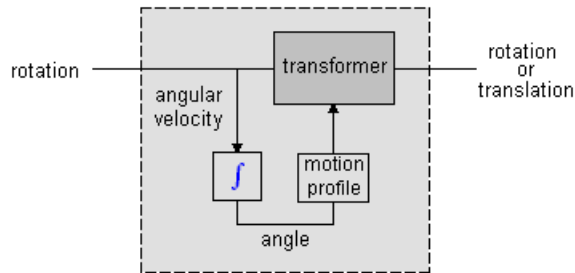
In the graph on the bottom right you can see the resulting error at the selected output as a result of the disturbances. The error is given in the form of a power spectral density (PSD) and cumulative power spectral density (CPS). The square root of the final value of the CPS is equal to the standard deviation of the output error. The standard deviations are shown in the *Output Sigma* tab.

## 8.5 Mechatronics Toolbox

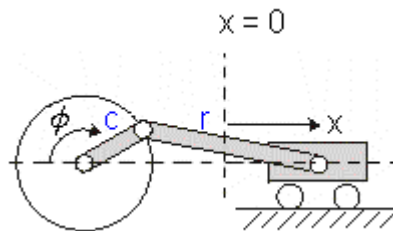
### Cam Wizard

Cams and mechanisms are all based on the same principle. The motion of an input axis is transformed to an output axis or translation. The transformation is a function of the input angle. This function is called the **cam motion profile**.





The 20-sim cam wizard helps you to generate cam and mechanism models. You can use various types of motion profiles which are continuous in velocity, acceleration or even in jerk! An example of a mechanism that can be generated by the Cam wizard is the crank-rod mechanism, where a rotary input motion is transformed to a translating output motion.

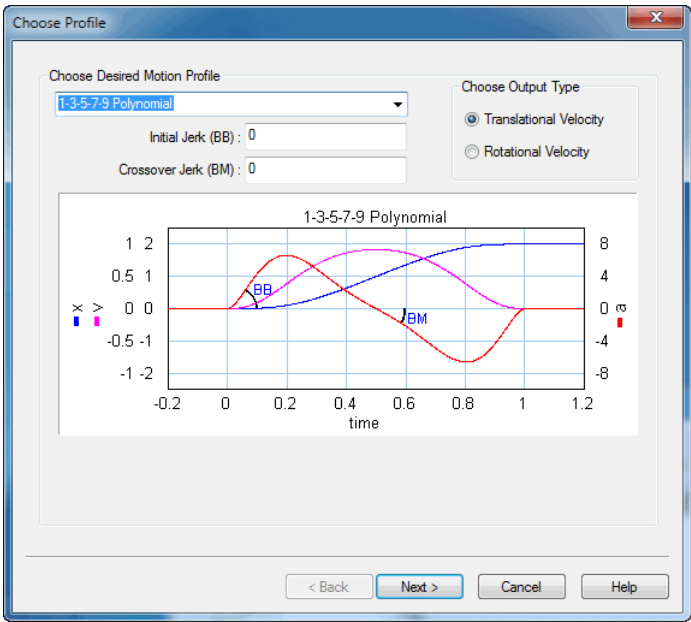


The models that are generated by the 20-sim Cam wizard are fully dynamic! This means:

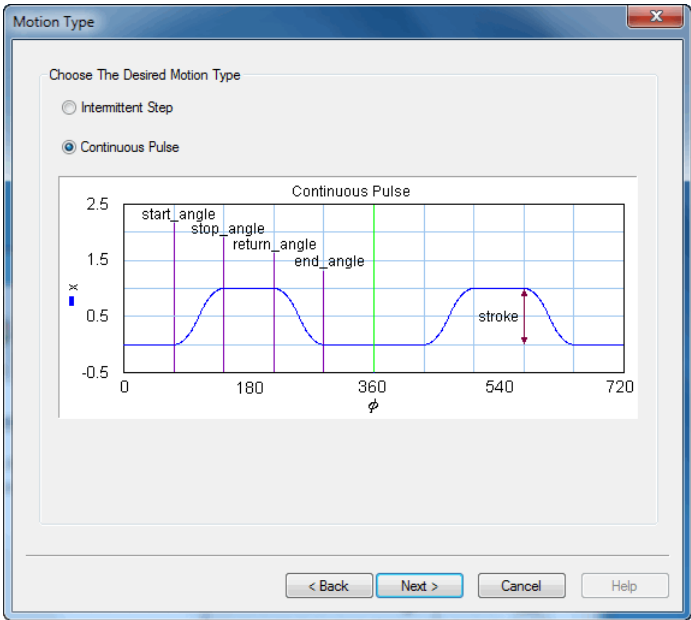
- The models describe the output velocity as function of the input velocity but also the input torque as function of the output load.
- The speed of the input axis does not have to be constant nor does the output load.
- No inertia, stiffness or other dynamic behavior is included, but this can be easily incorporated by coupling elements from the 20-sim library (inertias, springs etc.) to the input or output of the model.

To generate a cam or mechanism model in 20-sim, follow the next steps.

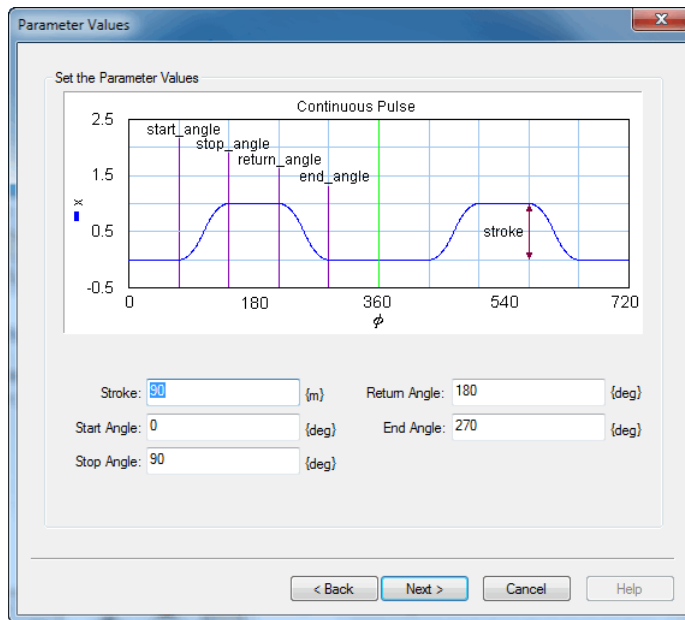
1. Open the model library and drag the model *CamManipulator.emx* to the editor.
2. Make an input connection (rotation) and an output connection (rotation/translation) to the model.
3. Select the camwizard model and click Go Down. Now the wizard will be opened.
4. Choose the desired motion profile, the profile parameters and type of output (translation/rotation):



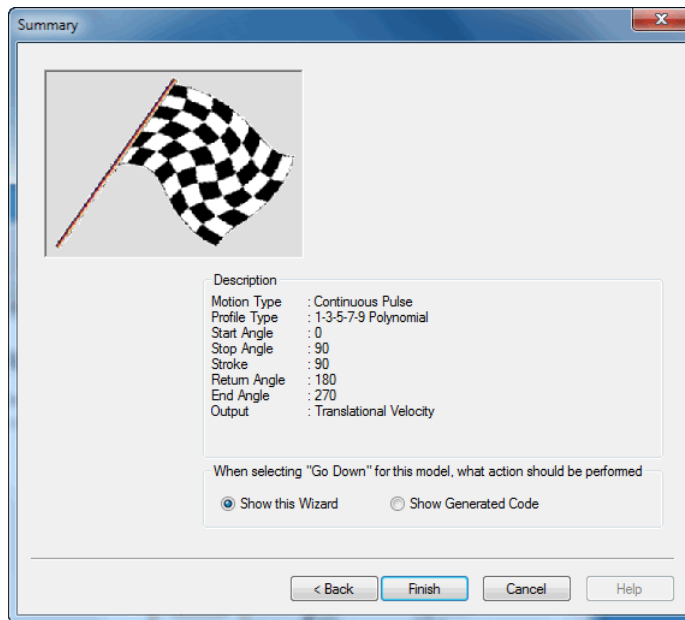
5. Select the type of cam motion profile:



6. Enter the parameters values (Stroke, Start Angle Stop Angle). If you have chosen a continuous pulse as output, you must also enter the values for the Return Angle and End Angle:



7. In the last page, the resulting values are shown:

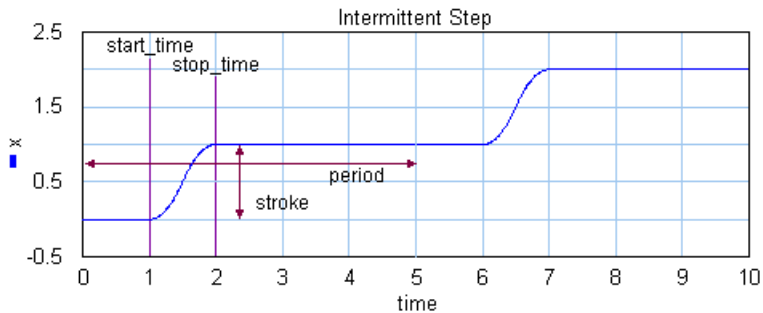


## Note

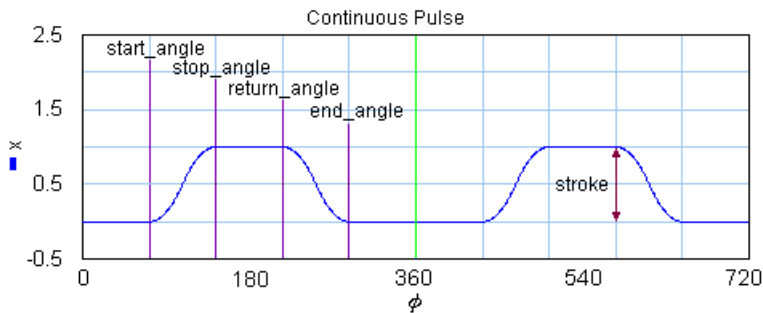
1. If you have changed the settings of this wizard, you have to process the model first (from the *Model* menu, choose *Check Complete Model*) before the changes become effective.
2. You can change parameter values during simulation (from the **Properties** menu select Parameters).
3. This is a masked model that uses the dll-file MotionProfile.dll to open the wizard. This dll-function must be stored in the bin directory of 20-sim. To see the SIDOPS code of a masked model press the *shift-key*, while clicking the *Go Down* command.

## Motion Types

Two types of motion profiles can be generated by the Cam wizard: **intermittent steps** and **continuous pulses**. The intermittent step motion does not return to its starting position, but gradually moves further away. It is characterized by the parameters stroke, start\_angle and stop\_angle.



The **continuous pulse** motion output returns at the end of each cycle returns to the starting position. It is characterized by the parameters stroke, *start\_angle*, *stop\_angle*, *return\_angle* and *end\_angle*.



## Motion Profiles

In mechanical engineering an important part of design is the reduction of vibrations. Every time a construction is in motion, vibrations are induced. When cams or mechanisms are used, the amount of vibrations, depend on the kind of motion that is induced. E.g. a sudden step change will induce violent vibrations in comparison with with a fluent motion. An important parameter to characterize motions, is the order:

1. **Zero Order:** Motions that are discontinuous in the position (e.g. a step).
2. **First Order:** Motions that are continuous in the position but discontinuous in the velocity (e.g. a ramp).
3. **Second Order:** Motions that are continuous in the position and velocity but discontinuous in the acceleration.
4. **Third Order:** Motions that are continuous in the position, velocity and acceleration.
5. **Fourth Order:** Motions that are continuous in the position, velocity, acceleration and jerk.

The specific shape of a motion profile can have a significant influence on the dynamic behavior. Some profiles minimize the maximum velocity, some profile minimize acceleration, while other profiles tend to make a tradeoff between the maximum velocity and acceleration. If we take a standard motion with stroke 1 and motion time 1 sec., the following table can be generated:

profile	order	$v_{\max}$	$a_{\max}$	$y(0)$	$y(1/2)$
Ramp	1	1	infinite	infinite	0
Crank-Rod <sup>2</sup>	2	$> 1.57$	$> 4.93$	infinite	$< -15.5$
Trapezoidal	2	2	4	infinite	-infinite
Partial Trapezoidal <sup>1</sup>	2	1.67	4.17	infinite	0
Geneva Mechanism	2	2.41	8.49	infinite	-118.5
Sine	2	1.57	4.93	infinite	-15.5
Cubic	3	2	4	32	-32
Partial Cubic <sup>3</sup>	3	1.67	5.55	55.6	0
Cycloidal	3	2	6.28	39.5	-39.5
Modified Sine	3	1.76	5.53	69.4	-23.2
Modified Trapezoidal	3	2	4.88	61.4	-61.4
MSC50	3	1.26	9.20	173.6	0
MSC% <sup>4</sup>	3	1.37	7.20	113.1	0
3-4-5 Polynomial	3	1.88	5.77	60	-30
1-3-5-7-9 Polynomial <sup>5</sup>	3/4	2.05	10.25	BB	BM

1: Parameter CV = 20%

2: For  $l_w \gg l_c$  the Crank Rod profile equals the sine profile, for  $l_w > l_c$  performance deteriorates.

3: Parameter CV = 20%, CA = 20%

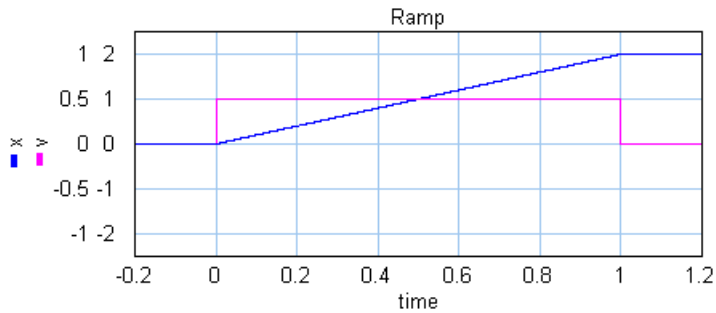
4: Parameter n = 30%, alpha = 10%

5: Parameter BB = 30%, BM = 10%

Here  $y(0)$  is the initial jerk (derivative of acceleration) and  $y(1/2)$  the crossover (halftime) jerk.

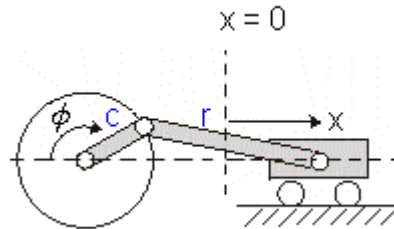
### Ramp

The ramp profile is a first order profile. It has a constant velocity and acceleration peaks at the start and end of the motion.

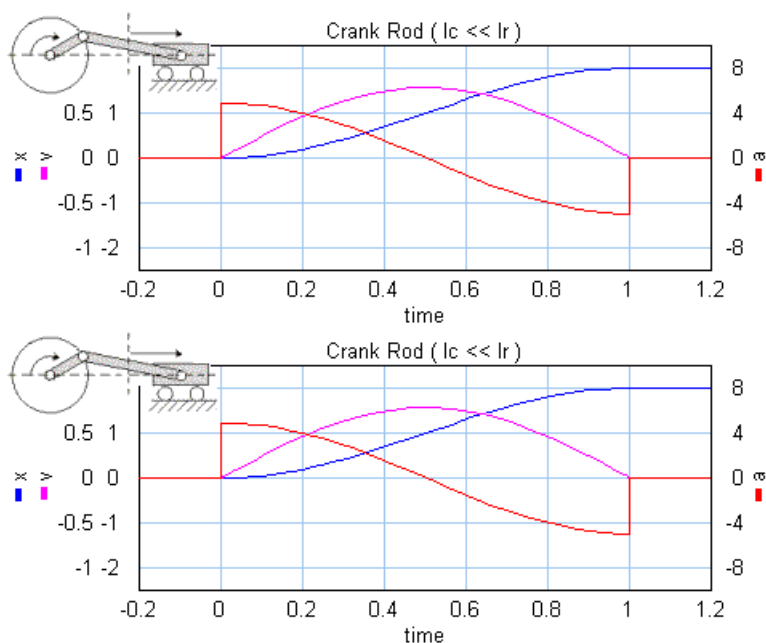


### Crank Rod Mechanism

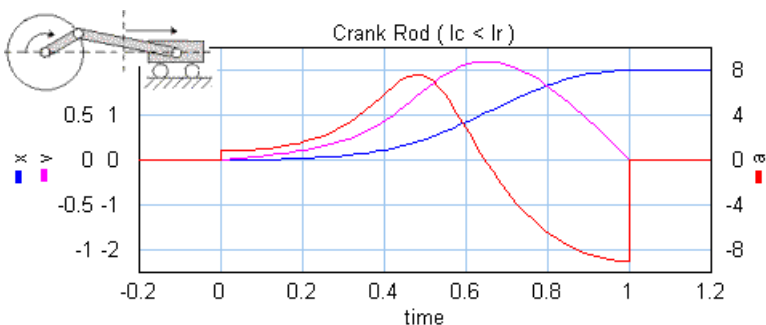
A Crank Rod mechanism converts a rotary motion into a repeating translation and



If the rod is much longer than the crank, the resulting motion profile will approach the sine profile. Below the motion profile is shown for half a rotation of the crank (angle from 0 to 180 degrees in 1 sec.).



If the rod gets smaller, the maximum velocity and acceleration increase.

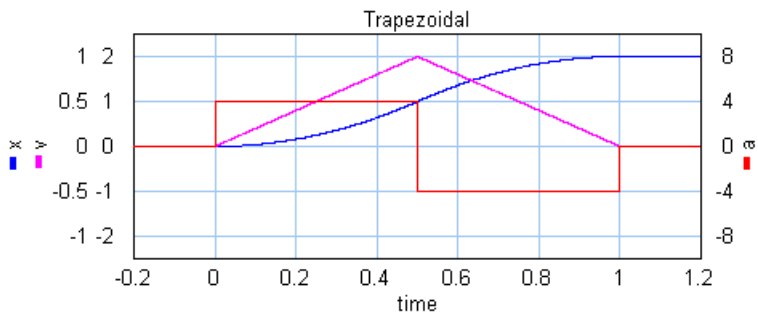


**Note:** A real crank-rod mechanism will not suddenly stop at half a rotation and therefore not show a discontinuous acceleration.

### Trapezoidal

The trapezoidal profile is a second order profile. It has a constant acceleration at the start of the motion and a constant deceleration at the end of the motion.

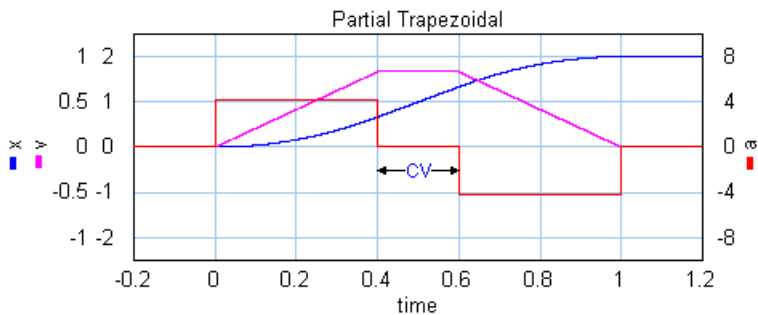




This profile is most widely used in early servo systems. Because of the discontinuity in the acceleration this motion profile can still induce a lot of vibrations. Therefore in modern servo systems third order profiles are preferred.

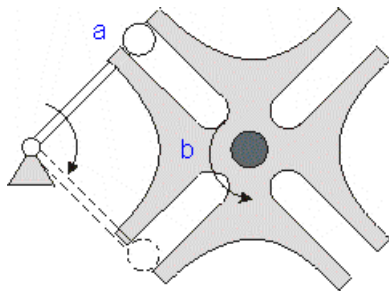
**Partial Trapezoidal**

The partial trapezoidal profile is a second order profile. It has is equal to the trapezoidal motion, but has a constant velocity part, during a fraction **CV** (%) of the motion.

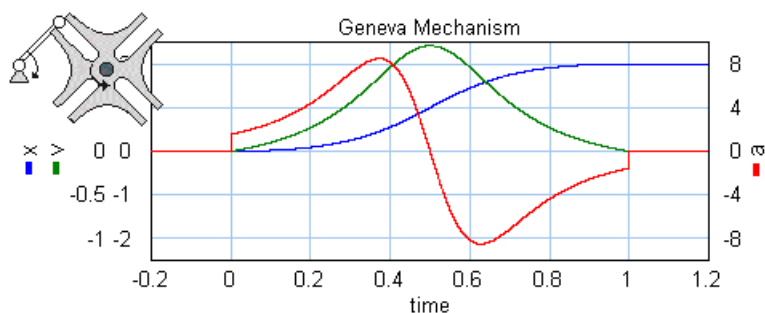


**Geneva Mechanism**

A Geneva mechanism is an old motion profile generation mechanism. A continuously rotating crankshaft (a) generates an intermittent motion of a second shaft (b). The result is a second order profile.



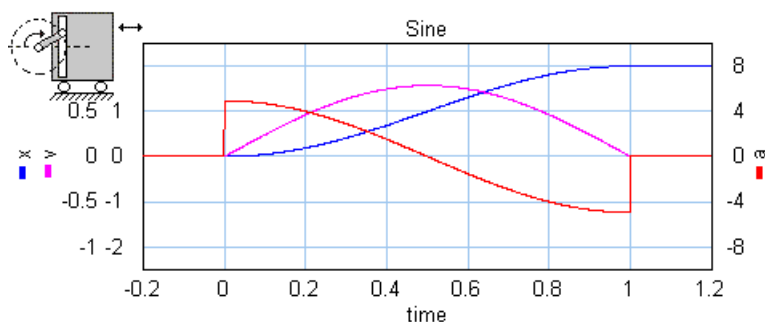
The motion profile generator yields the motion of the second shaft (b). It is shown below:



## Sine

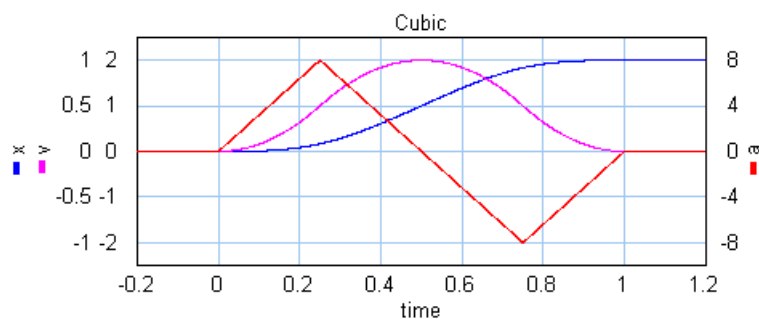
The sine profile is a second order profile of which the displacement can be described as:

$$x = 0.5 - \cos(p * t) / 2.$$



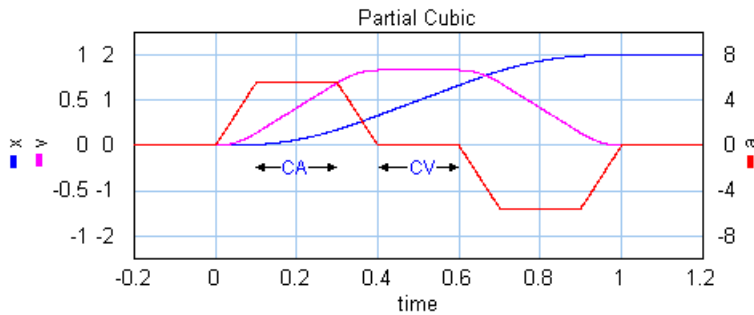
## Cubic

The cubic profile is a third order profile of which the acceleration is constantly increasing and decreasing.



## Partial Cubic

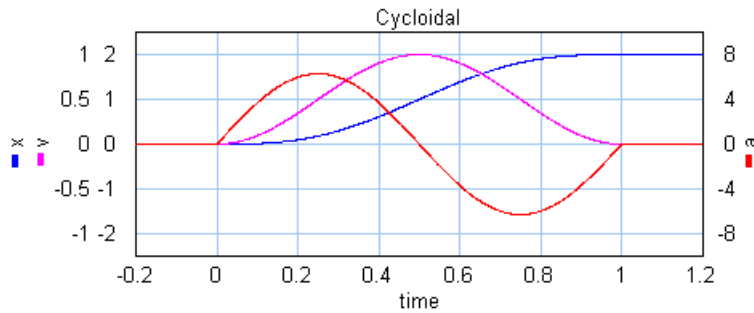
The partial cubic profile (3rd order) is a modified cubic profile with a constant velocity during a fraction **CV** (%) of the motion and a constant acceleration during a fraction **CA** (%) of the motion.



### Cycloidal

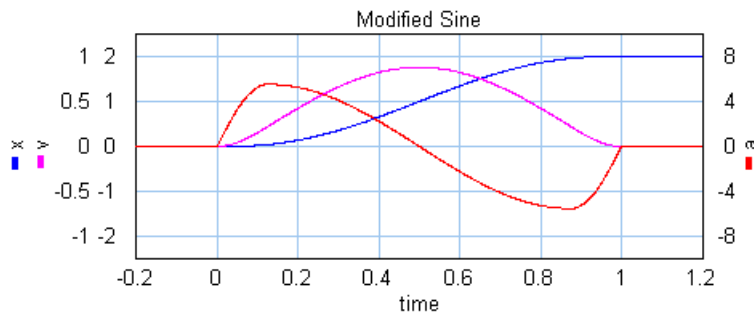
The cycloidal profile is a third order profile, of which the velocity can be described as:

$$v = stroke * (1 - \cos(t * a))$$



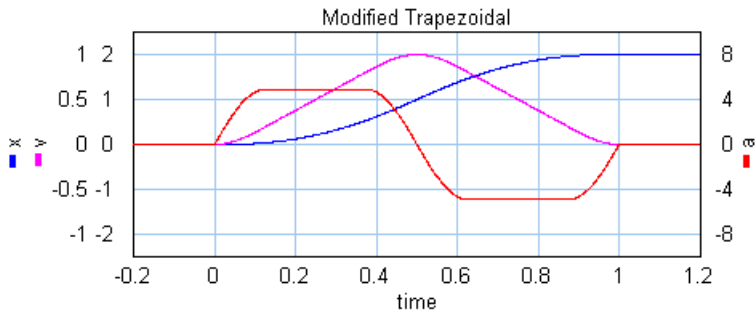
### Modified Sine

The modified sine profile is also a third order profile. It is a modification of the cycloidal profile to get a lower maximum velocity and a lower maximum acceleration.



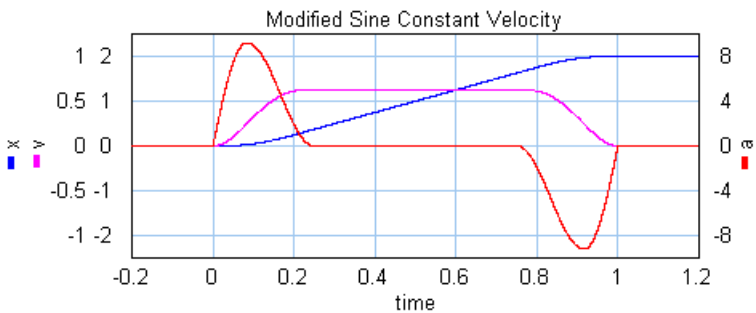
### Modified Trapezoidal

The modified trapezoidal profile is a modification of the trapezoidal profile (to make it a third order profile). This profile yields a very low maximum acceleration.



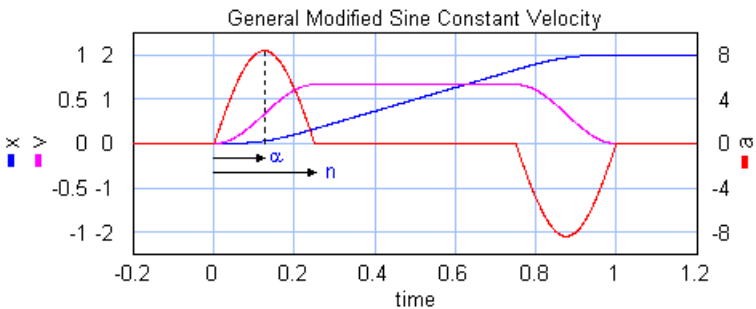
### Modified Sine with Constant Velocity (MSC50)

The modified sine with constant velocity profile (3rd order) is a modification of the modified sine profile. It has a constant velocity during 50% of the motion.



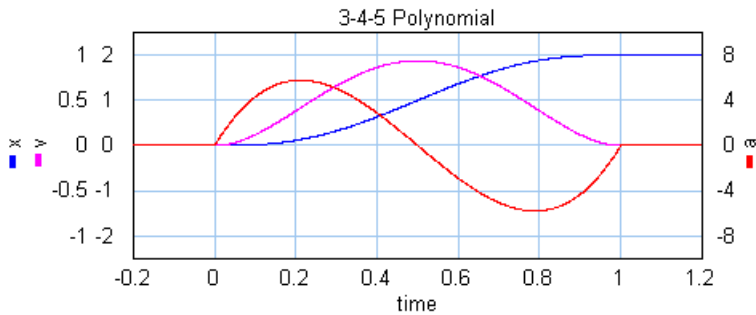
### General Modified Sine with Constant Velocity (MSC%)

The modified sine with constant velocity profile (3rd order) is a modification of the modified sine profile. It has a constant velocity during a user definable part of the of the motion. The non-zero acceleration part is defined by two parameters which are both defined as a fraction of the motion. The first parameters **alpha** (%) defines the start of the acceleration and the second parameters **n** (%) defines the end of the acceleration.



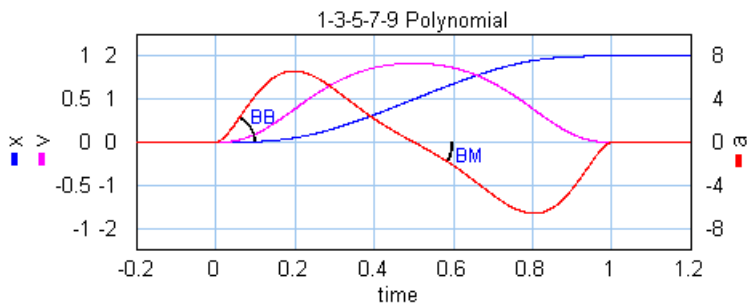
### 3-4-5 Polynomial

The is a third profile described by a 5th order polynomial.



### 1-3-5-7-9 Polynomial

This is a third/fourth order profile described by a 9th order polynomial. The profile is characterized by two parameters that denote the initial jerk, **BB**, and the crossover jerk, **BM**. If **BB** is chosen zero, this is a fourth order profile. If **BB** is chosen non-zero, this is a third order profile.



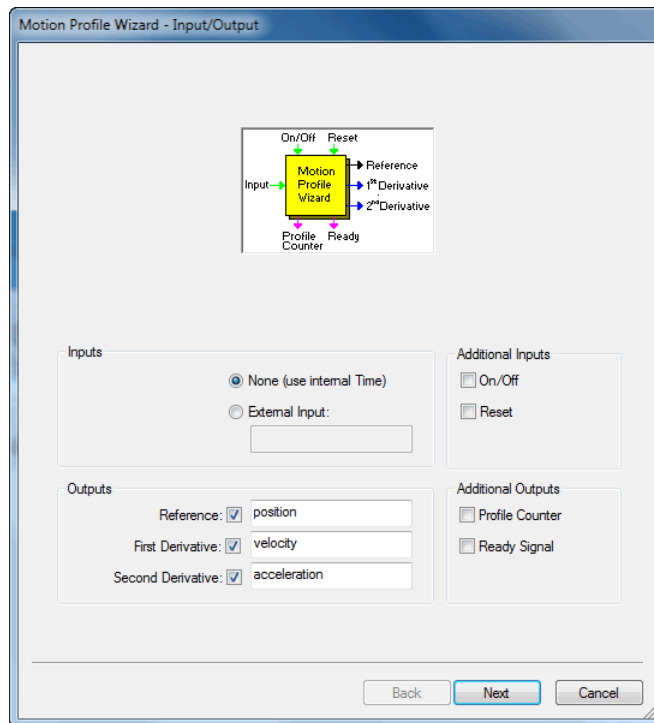
### Motion Profile Wizard

The 20-sim Motion Profile Wizard helps you to define motion profiles. To generate such a profile, follow the next steps.

1. Open the 20-sim model library and go to the section Signal\Sources.
2. Drag and drop the model MotionProfileWizard.emx to the editor.
3. Select the model and click **Go Down**.

This is a masked model. Clicking Go Down will open the *Motion Profile Wizard*.

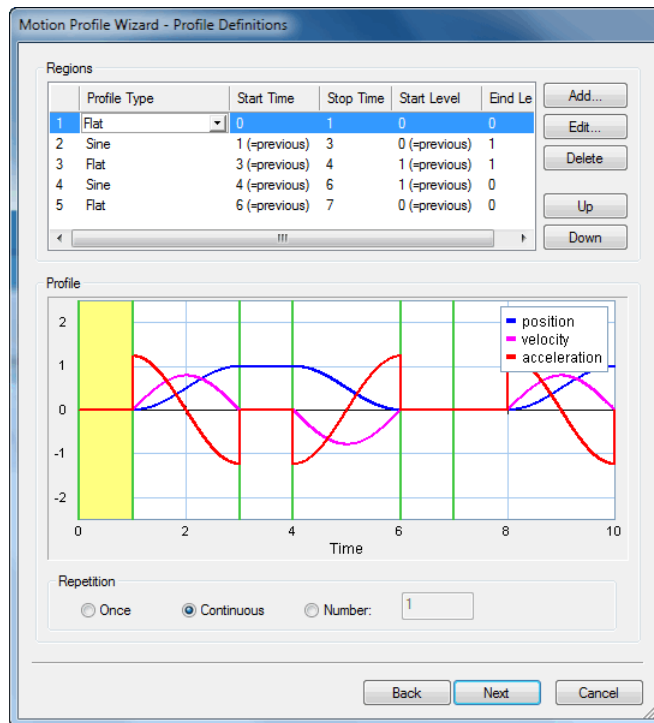
4. Select the inputs and outputs:



A number of inputs and outputs are available:

- **External Input:** Normally the time will be used for the x-axis of the profile. You can however use an external input as x-axis variable.
- **On/Off:** Use this input signal to start (onoff = TRUE) and stop (onoff = FALSE) the profile.
- **Reset:** When the reset signal gets high (reset = TRUE) the profile will be started.
- **Reference:** The motion profile reference signal, e.g. position.
- **First Derivative:** The first derivative of the motion profile reference signal, e.g. velocity.
- **Second Derivative:** The second derivative of the motion profile reference signal, e.g. velocity.
- **Profile Counter:** Gives the number of profiles that have been generated.
- **Ready Signal:** Gets high (ready = TRUE) when the profile is completely generated.

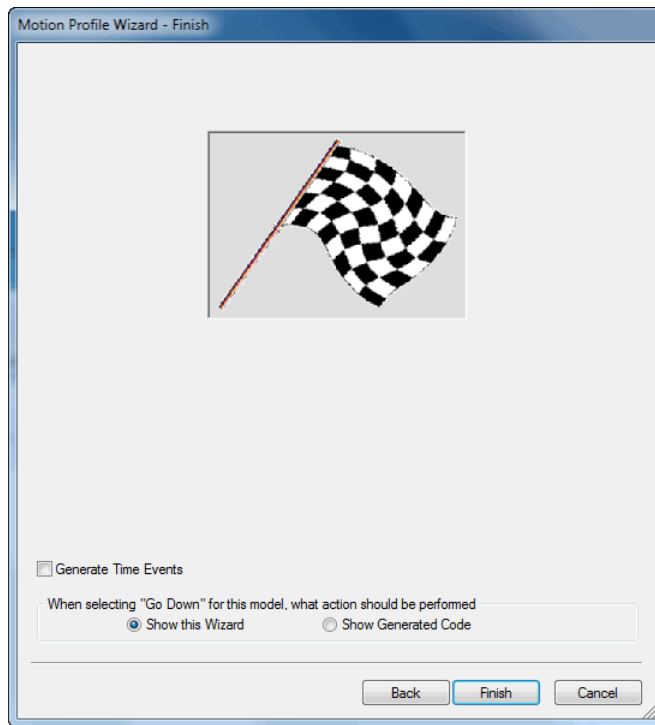
5. Click **Next** to enter the desired profile.
6. You can enter as many profiles as needed to design the complete motion. You can choose out of a number of predefined profiles.



7. Choose the number of times the motion should be repeated.

8. Click **Next** to go to the last page.

In the last page, you can choose to generate Time Events and what to show the next time (the wizard or the generated code). Use the default settings if you are not sure what to use.



9. Click **Next** to go to close the Wizard.
10. In the Editor from the **Model** menu Check Complete Model to make the changes effective.

If you select the model *MotionProfile.emx* and click **Go Down**, the old style Motion Profile Wizard will open. This wizard is kept in 20-sim to allow you to run old models. The wizard has been replaced by a new wizard which is far more powerful.

### Description

The 20-sim Motion Profile Wizard helps you to define motion profiles. To generate such a profile, follow the next steps.

1. Open the 20-sim model library and go to the section Signal\Sources.
2. Drag and drop the model MotionProfile.emx to the editor.
3. Select the model and click Go Down. Now the wizard will be opened.
4. Select the type of motion.
5. Choose the desired profile and output signals.
6. Enter the profile parameters.
7. Close the wizard.



During simulation the parameter values are used that you have selected in the wizard. These parameters are available in the *Parameters* Editor where you can change them as you would do with any other model. If you have changed the settings of this wizard, you have to process the model first (from the *Model* menu, choose *Check Complete Model*) before the changes become effective.

You can choose out of a number of predefined motion profiles in the Motion Profile Wizard.

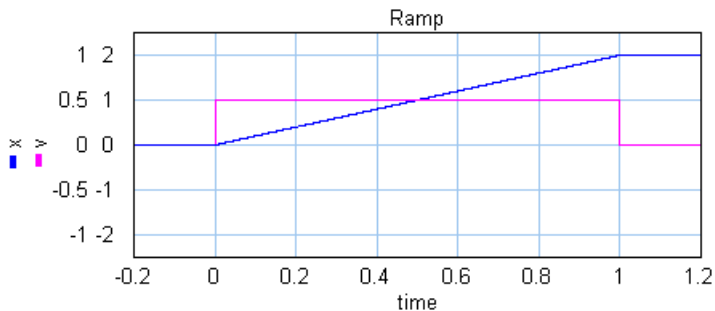
- Flat
- Ramp
- Trapezoidal
- Partial Trapezoidal
- Geneva Mechanism
- Sine
- Cubic
- Partial Cubic
- Cycloidal
- Standard Modified Sine
- Modified Trapezoidal
- Modified Sine with Constant Velocity (MSC50)
- General Modified Sine with Constant Velocity (MSC%)
- 3-4-5 Polynomial
- 1-3-5-7-9 Polynomial

### Flat

The flat profile is a zero order profile. It has a constant position, zero velocity and acceleration.

### Ramp

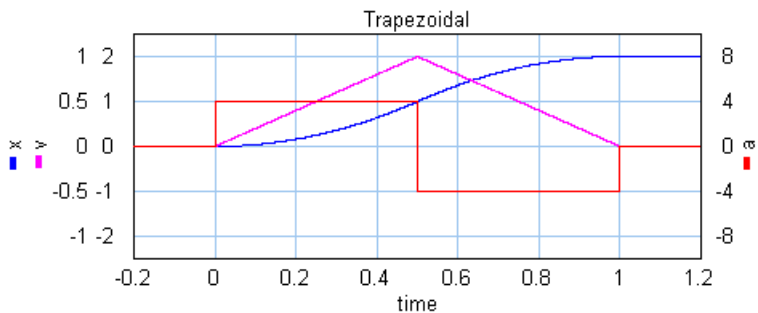
The ramp profile is a first order profile. It has a constant velocity and acceleration peaks at the start and end of the motion.



*The ramp profile.*

### Trapezoidal

The trapezoidal profile is a second order profile. It has a constant acceleration at the start of the motion and a constant deceleration at the end of the motion.

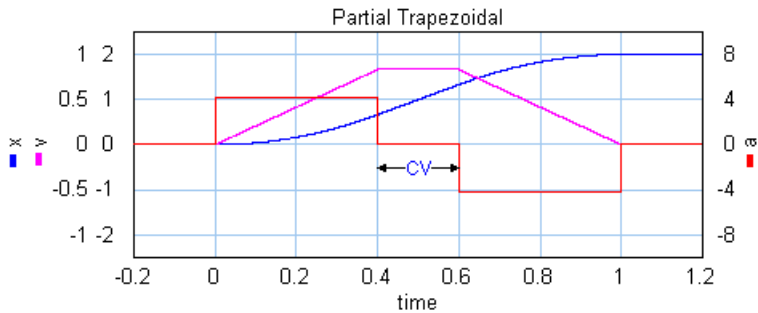


*The trapezoidal profile.*

This profile is most widely used in early servo systems. Because of the discontinuity in the acceleration this motion profile can still induce a lot of vibrations. Therefore in modern servo systems third order profiles are preferred.

**Partial Trapezoidal**

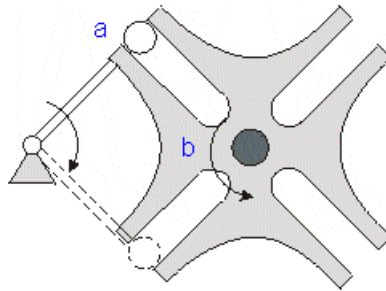
The partial trapezoidal profile is a second order profile. It has is equal to the trapezoidal motion, but has a constant velocity part, during a fraction **CV** (%) of the motion.



*The partial trapezoidal profile.*

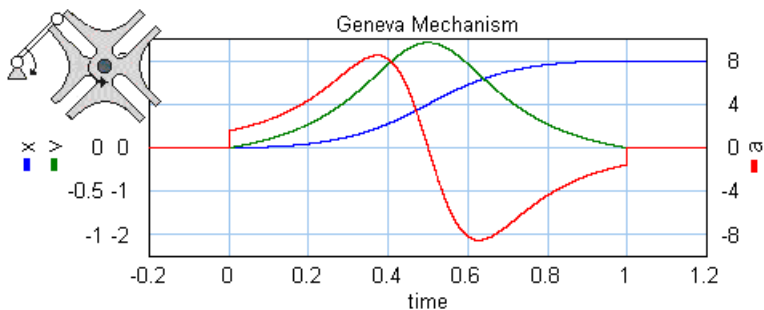
**Geneva Mechanism**

A Geneva mechanism is an old motion profile generation mechanism. A continuously rotating crankshaft (a) generates an intermittent motion of a second shaft (b). The result is a second order profile.



*A Geneva mechanism.*

The motion profile generator yields the motion of the second shaft (b). It is shown below:

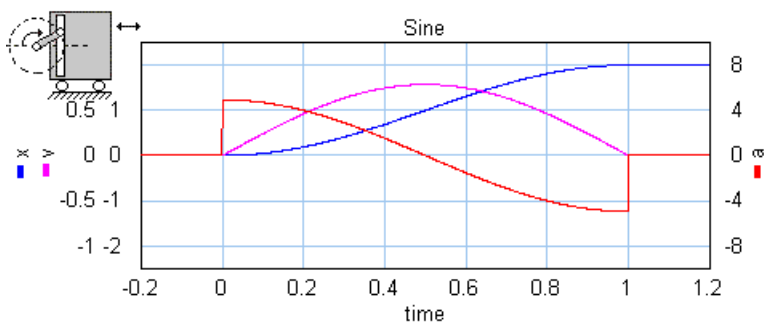


*The Geneva mechanism profile.*

## Sine

The sine profile is a second order profile of which the displacement can be described as:

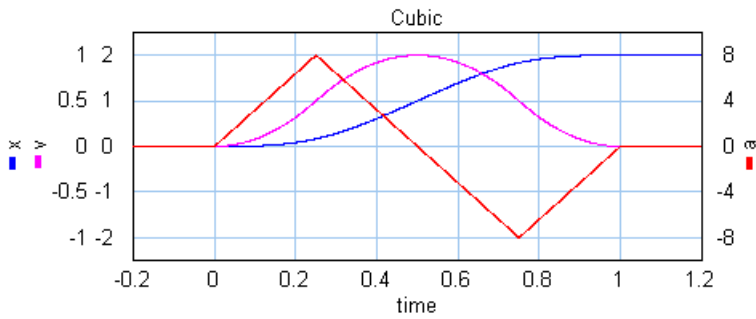
$$x = 0.5 - \cos(p * t) / 2.$$



*The sine profile.*

## Cubic

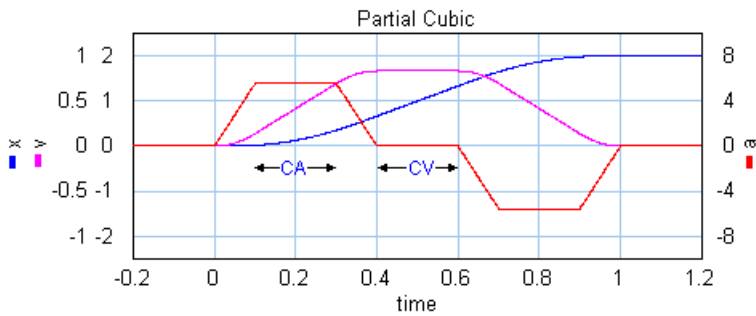
The cubic profile is a third order profile of which the acceleration is constantly increasing and decreasing.



*The cubic profile.*

### Partial Cubic

The partial cubic profile (3rd order) is a modified cubic profile with a constant velocity during a fraction **CV** (%) of the motion and a constant acceleration during a fraction **CA** (%) of the motion.

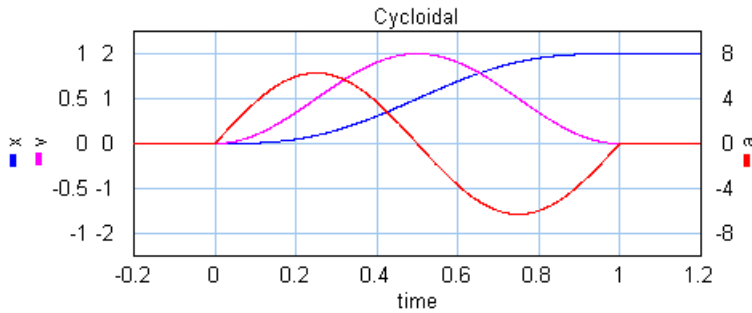


*The partial cubic profile.*

### Cycloidal

The cycloidal profile is a third order profile, of which the velocity can be described as:

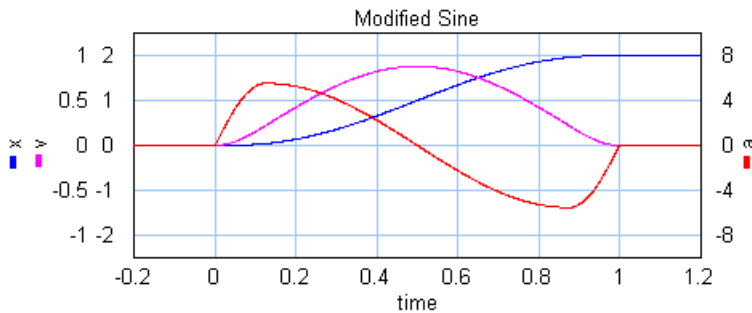
$$v = \text{stroke} * (1 - \cos(t * a))$$



*The cycloidal profile.*

### Modified Sine

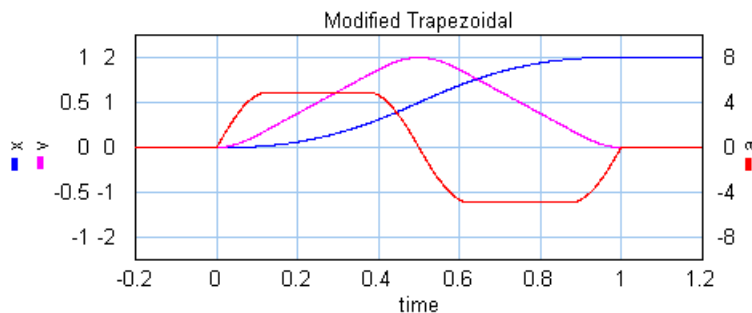
The modified sine profile is also a third order profile. It is a modification of the cycloidal profile to get a lower maximum velocity and a lower maximum acceleration.



*The modified sine profile.*

### Modified Trapezoidal

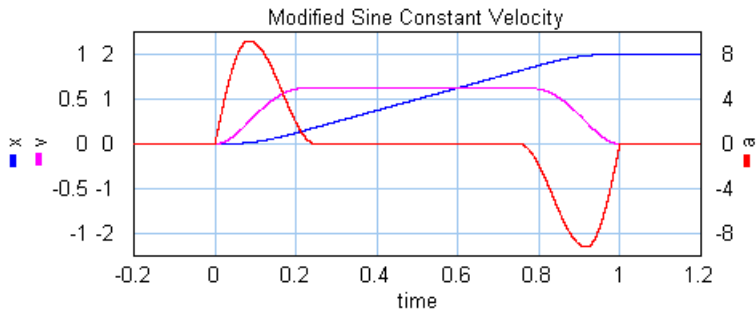
The modified trapezoidal profile is a modification of the trapezoidal profile (to make it a third order profile). This profile yields a very low maximum acceleration.



*The modified trapezoidal profile.*

Modified Sine with Constant Velocity (MSC50)

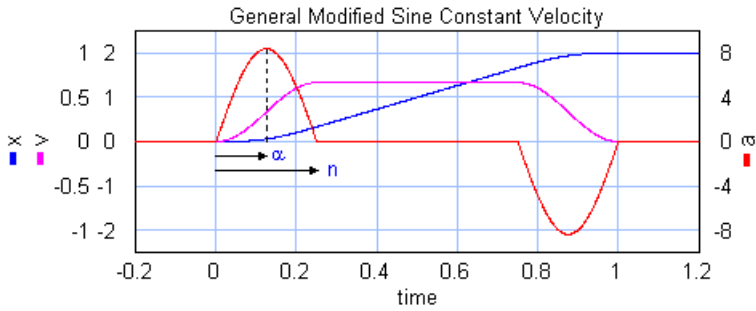
The modified sine with constant velocity profile (3rd order) is a modification of the modified sine profile. It has a constant velocity during 50% of the motion.



The modified sine with constant velocity profile.

General Modified Sine with Constant Velocity (MSC%)

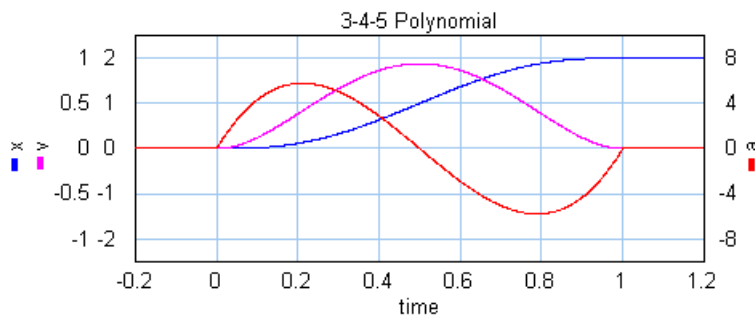
The modified sine with constant velocity profile (3rd order) is a modification of the modified sine profile. It has a constant velocity during a user definable part of the motion. The non-zero acceleration part is defined by two parameters which are both defined as a fraction of the motion. The first parameters **alpha** (%) defines the start of the acceleration and the second parameters **n** (%) defines the end of the acceleration.



The general modified sine with constant velocity profile.

3-4-5 Polynomial

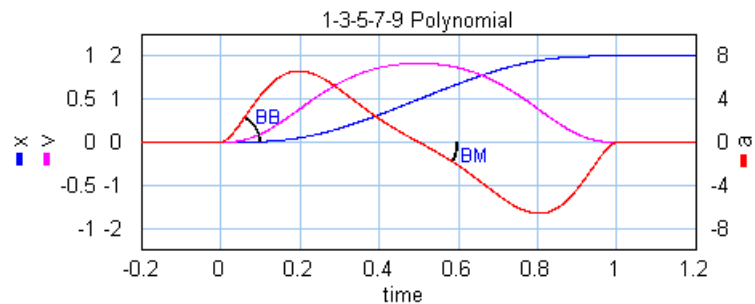
The is a third profile described by a 5th order polynomial.



The 1-3-5 polynomial profile.

1-3-5-7-9 Polynomial

The is a third/fourth order profile described by a 9th order polynomial. The profile is characterized by two parameters that denote the initial jerk, **BB**, and the crossover jerk, **BM**. If BB is chosen zero, this a a fourth order profile. If BB is chosen non-zero, this is a third order profile.



The 1-3-5-7-9 polynomial profile.

To keep the polynomial consistent, i.e. the polynomial does not change when the amplitude is changed, the initial jerk (**BB**) and the crossover jerk (**BM**) are defined for a standard motion with:

- *stroke* = 1
- *start\_time* = 0
- *stop\_time* = 1

Comparison of Profiles

The specific shape of a motion profile can have a significant influence on the dynamic behavior. Some profiles minimize the maximum velocity, some profile minimize acceleration, while other profiles tend to make a tradeoff between the maximum velocity and acceleration. If we take a standard motion with stroke 1 and motion time 1 sec., the following table can be generated:

profile	order	vmax	amax	j(0)	j(1/2)
Flat	0	0	0	0	0

Ramp	1	1	infinite	infinite	0
Trapezoidal	2	2	4	infinite	-infinite
Partial Trapezoidal1	2	1.67	4.17	infinite	0
Geneva Mechanism	2	2.41	8.49	infinite	-118.5
Sine	2	1.57	4.93	infinite	-15.5
Cubic	3	2	4	32	-32
Partial Cubic3	3	1.67	5.55	55.6	0
Cycloidal	3	2	6.28	39.5	-39.5
Modified Sine	3	1.76	5.53	69.4	-23.2
Modified Trapezoidal	3	2	4.88	61.4	-61.4
MSC50	3	1.26	9.20	173.6	0
MSC%4	3	1.37	7.20	113.1	0
3-4-5 Polynomial	3	1.88	5.77	60	-30
1-3-5-7-9 Polynomial5	3/4	2.05	10.25	BB	BM

1: Parameter CV = 20%

2: For  $l_w \gg l_c$  the Crank Rod profile equals the sine profile, for  $l_w > l_c$  performance deteriorates.

3: Parameter CV = 20%, CA = 20%

4: Parameter n = 30%, alpha = 10%

5: Parameter BB = 30%, BM = 10%

Here  $j(0)$  is the initial jerk/yerk (derivative of acceleration) and  $j(1/2)$  the crossover (halftime) jerk.

## Servo Motor Editor

The 20-sim Servo Motor Editor is a tool to generate dynamic models of servo motors for the use in 20-sim. These models describe the complete dynamic behaviour of servo motors, including the electrical, mechanical and thermal behaviour. The following classes of motors are supported in the editor:

1. Brush DC
2. Brushless DC (trapezoidal EMC and square wave currents)
3. AC synchronous (sinusoidal EMC and sinusoidal currents)
4. AC synchronous linear (sinusoidal EMC and sinusoidal currents)



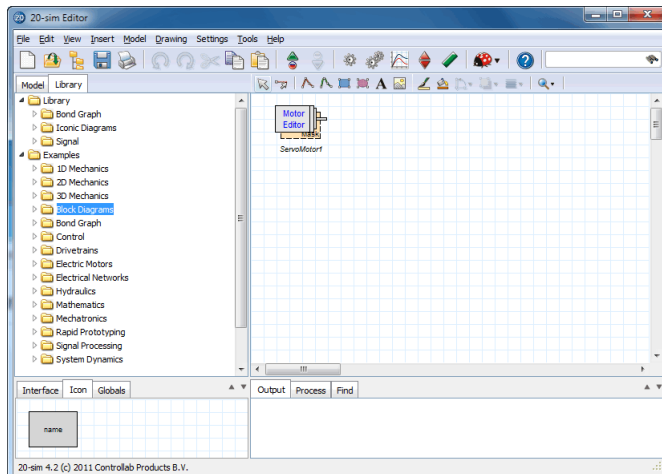
The dynamic models are generated automatically from data files containing commercially available motors, but you can also enter your own motor parameters. The following motors are available on data files:

1. The complete Maxon 2005 / 2006 program.
2. The complete Tecnotion 2006 program.
3. The Faulhaber 2006 program.

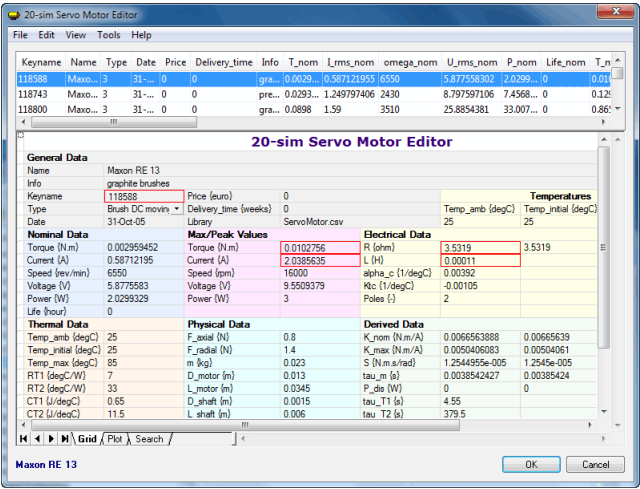
In the first part of these help files, the use of the 20-sim Servo Motor Editor is explained. The Editor uses a data table with motor parameters of commercial servo motors. You can select any motor from the table, inspect the corresponding torque speed curve and let the Servo Motor Editor generate a 20-sim dynamic model from the parameters.

The second part of these help files, explains the operating principles of the motors. A good indication of the performance of permanent magnet motors can be given by the torque speed plot. Various curves of the torque speed plot and how this can be used to choose the proper motor for a given task. An important part of the torque speed plot is the maximum continuous torque. It is the maximum torque that a motor can deliver without overheating. This curve is based on a thermal model of the motor, which is also explained.

The 20-sim Servo Motor Editor is part of the Mechatronics Toolbox of 20-sim. You can open the editor by selecting the **Servo Motor Editor** command (**Tools - Mechatronics** Toolbox). If you have a valid license, a servo motor model will be inserted:



Normally the editor will be opened automatically. If this does not happen, force the editor to open by clicking the Go Down button. This Editor looks like:

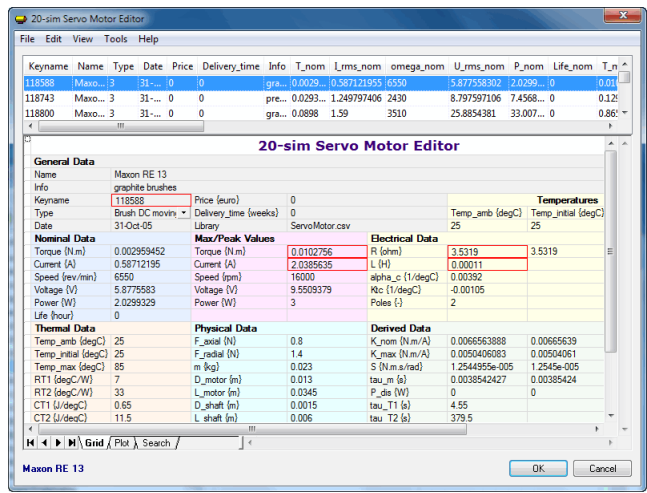


The top of the editor shows a list of motors. You can select one of the motors from the list by selecting it with your mouse pointer. The selected motor is shown with the blue line. The parameters of the selected motor are shown below the list.

To see the torque speed plot of the selected motor, click the *Plot* tab at the bottom of the editor. To find a motor based on specific searching conditions, click the *Search* tab. By clicking the *OK* button, a dynamic model will be created automatically, based on the selected motor in the list.

Using the Edit menu, new motors can be added to the list or deleted. By double clicking the mouse pointer on a parameter value, it can be changed.

If you open the Servo motor Editor, default data from file *ServoMotor.csv* is shown. You can open other data files by using the file menu.



Currently the following data files are available:

1. *ServoMotor.csv*: A selection of various motors to show the capabilities of the Servo Motor Editor.
2. *Maxon 2006.cse*: The complete list of Maxon motors, program 2005 / 2006.
3. *Tecnotion 2006.cse*: The complete list of Tecnotion motors, program 2006.
4. *Faulhaber 2006.cse*: Most of the Faulhaber motors, program 2006.

Unfortunately not all motor suppliers use the same parameters in the data sheets. Therefore the Servo Motor Editor uses the most common parameters as described in this section. All parameters are defined using a motor temperature and ambient temperature of 25° C.

**General Data**

This general section contains the unique identifier of the motor (Keyname) and some additional data, which can be filled in freely.

Name	The name of the motor
Info	Additional Info
Keyname	A unique name (no duplicates allowed in the motor list) to identify the motor.
Type	The motor type: <ol style="list-style-type: none"><li>1. AC Synchronous</li><li>2. Brush DC Iron</li><li>3. Brush DC moving coil</li><li>4. Brush DC Disc Rotor</li></ol>

- 5. AC Synchronous Linear
- 6. Brushless DC

In the Editor, you can select from a drop down list. In the data file (see next section, the corresponding numbers are used).

Date	Date at which the motor info was entered
Price	The price of the motor
Delivery Time	Delivery Time
Library	The name of the data file that is used

**Nominal Data**

Many data sheets describe the nominal operating point of a motor. The nominal operation point is characterized by a fixed current that is supplied to a motor with an initial temperature of 25° C that will result in a heating up of the coils to the exactly the maximum temperature. Because a current alone is not enough to describe the state of a motor, the operating point is always given at a certain speed. Although the other parameters (torque and power) can be derived from the current and speed they are usually printed in most data sheets.

Torque [N.m]or Force[N]	Torque or force at nominal operation.
Current [A] or [Arms]	Current at nominal operation.
Speed [rpm]or [m/s]	Speed at nominal operation.
Voltage [V] or [Vrms]	Voltage at nominal operation.
Power [W]	The output power at nominal operation.
Life [hour]	Expected Lifetime of the motor under normal operation.

As described, the definition of current and voltage depends on the selected motor:

motor	current	voltage
1. AC Synchronous	rms phase current (A)	rms phase to phase voltage (V)
2. Brush DC Iron	current (A)	voltage (V)
3. Brush DC moving coil	current (A)	voltage (V)
4. Brush DC Disc Rotor	current (A)	voltage (V)
5. AC Synchronous Linear	rms phase current (A)	rms phase to phase voltage (V)
6. Brushless DC	peak current (A)	peak phase to phase voltage (V)

**Max/Peak Values**

The maximum parameters indicate the maximum performance of the motor and are used to show the limits in the torque speed plot as explained in chapter 3. The parameters do not indicate an operating point on the torque speed curve. The maximum parameters are preferably measured at a temperature of 25° C.

Torque [N.m]or Force[N]	The maximum short-time or torque or force (also known as stall torque).
Current [A] or [Arms]	The maximum short-time current.
Speed [rpm]or [m/s]	The maximum speed.
Voltage [V] or [Vrms]	Maximum short-time voltage.
Power [W]	The maximum short time power.

The currents and voltages are defined the same as for the nominal parameters.

### Electrical Data

R [ohm]	The resistance at 25° C.
L [H]	The terminal inductance.
alpha_c [1/degC]	The temperature dependency of the coil resistance.
ktc [1/degC ]	The temperature dependency of the magnets.
poles [-] or pitch[m]	The number of poles (always an even number) or pole pitch (distance N-N poles).

As described, the definition of resistance and inductance depends on the selected motor:

motor	resistance	inductance
1. AC Synchronous	phase to phase resistance (ohm)	phase to phase inductance (H)
2. Brush DC Iron	resistance (ohm)	inductance (H)
3. Brush DC moving coil	resistance (ohm)	inductance (H)
4. Brush DC Disc Rotor	resistance (ohm)	inductance (H)
5. AC Synchronous Linear	phase to phase resistance (ohm)	phase to phase inductance (H)
6. Brushless DC	phase to phase resistance (ohm)	phase to phase inductance (H)

### Mechanical Data

The mechanical data describes the motor inertia and losses.

J_rotor [kg.m2] or m_motor [kg]	The rotor inertia or the the moving mass of the motor.
d [N.m.s/rad]or [N.s/m]	Mechanical damping and eddy current losses.
T_fric [N.m] or [N]	Mechanical friction and hysteresis losses.
T_cog [N.m] or [N]	The amplitude of the cogging torque.

### Thermal Data

The thermal data is used for the thermal model as explained in chapter 4. Zero values for the thermal resistances are replaced by a small value ( $1e-2$ ) to prevent division by zero.

Temp_amb [degC]	The ambient temperature.
Temp_initial [degC]	The initial temperature of the coils and housing.
Temp_max [degC]	The maximum coil temperature.
RT1 [degC/W]	The thermal resistance between rotor and stator.
RT2 [degC/W]	The thermal resistance between stator and environment.
CT1 [J/degC]	Thermal capacity of the rotor.
CT2 [J/degC]	Thermal capacity of the stator.

### Physical Data

This section describes the motor dimensions and maximal load.

F_axial [N]	The maximum axial force applied to the motor shaft.
F_radial [N]	The maximum radial force applied to the motor shaft.
m [kg]	The motor weight.
D_motor [m]	The motor diameter.
L_motor [m]	The motor length.
D_shaft [m]	The shaft diameter.
L_shaft [m]	The shaft length.

### Derived Data

These are values that can be found in many data sheets. They are useful for selection criteria when searching for motors.

K_nom [N.m/A], [N.m/Arms] or [N/Arms]	The torque constant or force constant at 25°C and nominal currents.
K_max [N.m/A], [N.m/Arms] or [N/Arms]	The torque constant or force constant at 25°C and at peak currents.
S [N.m.s/rad] or [N.s/m]	The steepness.
tau_m [s]	The mechanical time constant ( $J_{\text{rotor}}/S$ or $m_{\text{motor}}/S$ ).
P_dis [W]	The maximal continuous dissipation.

tau_T1 [s]	The thermal time constant of the rotor (RT1*CT1).
tau_T2 [s]	The thermal time constant of the stator (RT2*CT2).

### Additional Data

20-sim model []	Not implemented yet.
-----------------	----------------------

When you enter a new motor, not all parameters have to be filled in. In this section the critical and non critical parameters are listed.

### Critical

Only a few parameters are critical. I.e. they are necessary to generate a 20-sim dynamic model.

Keyname	A unique name to identify the motor.
Type	The motor type.
Maximum Torque or Force	The maximum short-time or torque or force.
Maximum Current	The maximum short-time current.
R	The resistance at 25° C.
L	The terminal inductance.
J_rotor or m_motor	The rotor inertia or the the moving mass of the motor.

### Desired

Some parameters are desired. I.e. they add more detail to the model:

Nominal Torque or Force	Torque or force at nominal operation.
Nominal Current	Current at nominal operation.
Nominal Speed	Speed at nominal operation.
alpha_c	The temperature dependency of the coil resistance.
ktc	The temperature dependency of the magnets.
poles or pitch	The number of poles (always an even number) or pole pitch (distance N-N poles).

d	Mechanical damping and eddy current losses.
T_fric	Mechanical friction and hysteresis losses.
T_cog	The amplitude of the cogging torque.
Temp_amb	The ambient temperature.
Temp_initial	The initial temperature of the coils and housing.
Temp_max	The maximum coil temperature.
RT1	The thermal resistance between rotor and stator.
RT2	The thermal resistance between stator and environment.
CT1	Thermal capacity of the rotor.
CT2	Thermal capacity of the stator.

If you do not know the values of these parameters, fill in zero. 20-sim will automatically change some into small numbers to prevent division by zero. Because the nominal torque and current are used to derive the torque constant at nominal operation, they will be replaced by the maximum current and torque if you fill in a zero value.

### Torque Speed Plot

Some parameters will add more detail to the torque speed plot:

Speed	The maximum speed.
Voltage	Maximum short-time voltage.
Power	The maximum short time power.

### Additional

The remaining parameters are not used in the torque speed plot or the 20-sim model. They are useful for selection criteria when searching motors. If you do not know the values of these parameters, fill in zero.

If you have selected a motor, clicking the OK button will close the editor and generate a dynamic model. The model will be filled with the parameters from the selected motor and is ready for the use in a simulation. The model contains a number of variables that may be useful to show in a simulation plot.

### General Part

R	resistance at simulated (fluctuating) temperature
K	torque constant at simulated (fluctuating) temperature



u_rms_ff	effective terminal (phase-phase) voltage
u_tt_ff	maximum terminal (phase-phase)
i_tt	maximum phase current
phi	shaft angle

### Thermal part

Temp_coil	coil temperature
Temp_housing	housing temperature

### Torque speed plot

omega_range	speed ranging from zero to over 5% of maximum speed
T_range	torque ranging from zero to over 5% of maximum torque
Torquemax	maximum torque
Speedmax	maximum speed
T_max_power	torque at maximum power
T_max_current	torque at maximum current
T_max_outputpower	line of maximum output torque
T_max_voltage	torque at maximum voltage
T_max_efficiency	line of torque at maximum efficiency
T_100	maximum allowable continuous torque, (i.e. a 100% duty cycle)
T_50	maximum allowable torque for a 50% duty cycle
T_25	maximum allowable torque for a 25% duty cycle
T_10	maximum allowable torque for a 10% duty cycle
T_abs	absolute output (load) torque
omega_abs	absolute velocity

The motor parameters are visible in the Grid tab. These parameters are stored in a coma separated data file (extension .csv) or in an encrypted coma separated data file (extension .cse).

By default, the file `ServoMotor.csv` is shown. Using the File menu you can store and open csv files. The csv files can be edited with the *Servo Motor Editor* or an external spreadsheet program like OpenOffice. In *OpenOffice Calc* the file looks like:

A	B	C	D	E	F	G	H	I	J
Keyname	Name	Type	Date	Price	Delivery_time	Info	T_nom	I_rms_nom	omega
				euro	weeks		N.m	A	rev/min
							F_nom	I_nom	v_nom
							N	A	m/s
motor key	motor name	motor type	date of file	motor price	average delivery time	motor information	nominal torque	nominal current	nominal speed
118588	Maxon RE 13	3	31/10/05	0	stock	graphite brushes	0	0.59	
118743	Maxon RE 25	3	31/10/05	0	stock	precious metal brushes	0.03	1.25	
118800	Maxon RE 36	3	31/10/05	0	stock	graphite brushes	0.09	1.59	
118821	Maxon RE 75	3	31/10/05	0	stock	graphite brushes	0.84	7.23	
252463 s	Maxon EC 45	1	31/10/05	0	stock	sine commutation	0.31	3.56	
167131 s	Maxon EC 60	1	31/10/05	0	stock	sine commutation	0.72	4.33	
252463 b	Maxon EC 45	6	31/10/05	0	stock	block commutation	0.3	4.36	
167131 b	Maxon EC 60	6	31/10/05	0	stock	block commutation	0.69	5.3	
TL 30 N	Tecnotion TL 30 N	5	08/11/05	0		0 iron core	1050	9.4	
TL 30 S	Tecnotion TL 30 S	5	08/11/05	0		0 iron core	1050	23	
UM 12 N	Tecnotion UM 12 N	5	08/11/05	0		0 ironless	116	3.2	
UM 12 S	Tecnotion UM 12 S	5	08/11/05	0		0 ironless	116	5.8	

The top 5 rows contain the description of the motor parameters and the corresponding units. The first and second row are used for rotation motors and the third and fourth row are used for linear (translation) motors. The fifth row contains the parameter names.

The other rows contain the motor parameters. The meaning of these parameters is described in the previous sections. Please use the following guidelines when editing data files:

1. Never change the first five lines
2. Do not use duplicate names in the first column (keyname)
3. Do use commas
4. Do not use strange formatting (in Excel use the General format)
5. Do not enter extra columns
6. Do not enter other information in additional rows or columns. The Servo Motor Editor will try to read all cells and halt if the content is not according to the specifications.
7. Do not add comment.
8. The last column entry (20-sim) should contain one white space character.
9. Store as comma separated file.

## File

20-sim 3.6\Tools\Servo Motor Dynamics\Maxon 2006.cse

## Date

November 2005

## More information

[www.maxonmotors.com](http://www.maxonmotors.com)

## Description

The data file Maxon 2006.cse contains the complete set of Maxon motors, program 2005 / 2006. Most of the data has been extracted from the Maxon data sheets. The tables below shows the 20-sim names and the corresponding data sheet names. Some parameters were not available in the data sheets and have been given by the Maxon motor company. These parameters are indicated as *Given by Maxon*. Some parameters were calculated. These are indicated as *Calculated*.

## DC motors

### Servo Motor Editor

#### General Data

Name	Motor Series
Keyname	Maxon Order Number
Info	Additional Information
Type	DC
Date	21 October 2005
Price	-
Delivery Time	stock / standard / special
Library	Maxon 2006.cse

#### Nominal Data

Torque	Max. continuous torque
Current	Max. continuous current
Speed	No load speed divided by 2
Voltage	Calculated
Power	Calculated

#### Max/Peak Data

Torque	Stall torque
Current	Starting current
Power	Assigned Power Rating
Voltage	Calculated*
Speed	Max. permissible speed

#### Thermal Data

Temp_amb	Set to 25
Temp_initial	Set to 25
Temp_max	Maximum rotor temperature
RT1	Thermal resistance rotor-housing
RT2	Thermal resistance housing-ambient
CT1	Calculated
CT2	Given by Maxon

#### Physical Data

F_axial	Maximum Axial load
F_Radial	Maximum radial load
m	Weight of motor
D_motor	Diameter of motor
L_motor	Length of motor
D_shaft	Diameter shaft
L_shaft	Length Shaft

### Maxon Data Sheets

**Electrical Data**

R	Terminal resistance
L	Terminal inductance
alpha_c	Given by Maxon
Ktc	Given by Maxon
Poles	Number of poles

**Mechanical Data**

J_rotor	Rotor inertia
d	Given by Maxon
T_fric	Given by Maxon
T_cog	0

**Derived Data**

K_nom	Calculated
K_max	Calculated
S_nom	Calculated
P_dis	Calculated

\* In the data sheets Maxon only gives a nominal voltage. According to Maxon higher operating voltages are permissible provided that other limits are not exceeded. Therefore the maximum voltage is chosen equal to the voltage that is needed to run a motor with zero load at maximum speed.

**EC motors with block commutation**

Maxon EC motors can be driven by block commutation and sine commutation. The Maxon data sheets give the parameters for block commutation. To distinguish between block commutation and sine commutation the character **b** or **s** is added to the keyname.

**Servo Motor Editor****General Data**

Name	Motor Series
Keyname	Maxon Order Number + b
Info	Additional Information
Type	Brushless DC
Date	21 October 2005
Price	-
Delivery Time	stock / standard / special
Library	Maxon 2006.csv

**Nominal Data**

Torque	Calculated
Current	Max. continuous current
Speed	Nominal speed
Voltage	Calculated
Power	Calculated

**Max/Peak Data**

Torque	Stall torque
Current	Calculated
Power	Assigned Power Rating
Voltage	Calculated*
Speed	Max. permissible speed

**Thermal Data****Maxon Data Sheets**

Temp_amb	Set to 25
Temp_initial	Set to 25
Temp_max	Maximum rotor temperature
RT1	Thermal resistance rotor-housing
RT2	Thermal resistance housing-ambient
CT1	Calculated
CT2	Calculated

**Physical Data**

F_axial	Maximum Axial load
F_Radial	Maximum radial load
m	Weight of motor
D_motor	Diameter of motor
L_motor	Length of motor
D_shaft	Diameter shaft
L_shaft	Length Shaft

**Electrical Data**

R	Terminal resistance phase to phase
L	Terminal inductance phase to phase
alpha_c	Given by Maxon
Ktc	Given by Maxon
Poles	Number of poles

**Mechanical Data**

J_rotor	Rotor inertia
d	Given by Maxon
T_fric	Given by Maxon
T_cog	0

**Derived Data**

K_nom	Calculated
K_max	Calculated
S_nom	Calculated
P_dis	Calculated

\* In the data sheets Maxon only gives a nominal voltage. According to Maxon higher operating voltages are permissible provided that other limits are not exceeded. Therefore the maximum voltage is chosen equal to the voltage that is needed to run a motor with zero load at maximum speed.

**EC motors with sine commutation**

Maxon EC motors can be driven by block commutation and sine commutation. The Maxon data sheets give the parameters for block commutation. The parameters for sine commutation can be calculated from the block commutation parameters. To distinguish between block commutation and sine commutation the character **b** or **s** is added to the keyname.

**Servo Motor Editor****General Data**

Name	Motor Series
Keyname	Maxon Order Number + s
Info	Additional Information
Type	AC Synchronous
Date	21 October 2005
Price	-

**Maxon Data Sheets**

Delivery Time	stock / standard / special
Library	Maxon 2006.csv
<b>Nominal Data</b>	
Torque	Calculated
Current	Calculated
Speed	Nominal speed
Voltage	Calculated
Power	Calculated
<b>Max/Peak Data</b>	
Torque	Calculated
Current	Calculated
Power	Assigned Power Rating
Voltage	Calculated*
Speed	Calculated
<b>Thermal Data</b>	
Temp_amb	Set to 25
Temp_initial	Set to 25
Temp_max	Maximum rotor temperature
RT1	Thermal resistance rotor-housing
RT2	Thermal resistance housing-ambient
CT1	Calculated
CT2	Calculated
<b>Physical Data</b>	
F_axial	Maximum Axial load
F_Radial	Maximum radial load
m	Weight of motor
D_motor	Diameter of motor
L_motor	Length of motor
D_shaft	Diameter shaft
L_shaft	Length Shaft
<b>Electrical Data</b>	
R	Terminal resistance phase to phase
L	Terminal inductance phase to phase
alpha_c	Given by Maxon
Ktc	Given by Maxon
Poles	Number of poles
<b>Mechanical Data</b>	
J_rotor	Rotor inertia
d	Given by Maxon
T_fric	Given by Maxon
T_cog	0
<b>Derived Data</b>	
K_nom	Calculated
K_max	Calculated
S_nom	Calculated
P_dis	Calculated

\* In the data sheets Maxon only gives a nominal voltage. According to Maxon higher operating voltages are permissible provided that other limits are not exceeded. Therefore the maximum voltage is chosen equal to the voltage that is needed to run a motor with zero load at maximum speed.

**File**

20-sim 3.6\Tools\Servo Motor Dynamics\Tecnotion 2006.cse

**Date**

November 2006

**More information**[www.tecnotion.com](http://www.tecnotion.com)**Description**

The data file Tecnotion 2006.cse contains the complete set of Tecnotion motors, program 2006. Most of the data has been extracted from the Tecnotion data sheets. The tables below shows the 20-sim names and the corresponding data sheet names. Some parameters were not available in the data sheets and have been given by the Tecnotion motor company. These parameters are indicated as *Given by Tecnotion*. Some parameters were calculated. These are indicated as *Calculated*.

**Important:** The nominal data and the default value of the thermal resistance RT2 are calculated for **air cooling**. The value for RT2 can be changed using a slider. **If water cooling is used, change the value of RT2 to its minimum value.**

**Servo Motor Editor****Tecnotion Data Sheets****General Data**

Name  
Keyname  
Info  
Type  
Date  
Price  
Delivery Time  
Library

Motor Series  
Order Number  
Additional Information  
AC Synchronous Linear  
21 October 2005  
-  
-  
Tecnotion 2006.cse

**Nominal Data**

Force  
Current  
Speed  
Voltage  
Power

Continuous Force (air cooled\*)  
Continuous Current (air cooled\*)  
0 m/s  
Calculated  
-

**Max/Peak Data**

Force  
Current  
Power  
Voltage  
Speed

Ultimate Force / Peak Force  
Ultimate Current / Peak Current  
Calculated  
Max. voltage ph-ph  
Maximum speed

**Thermal Data**

Temp\_amb  
Temp\_initial  
Temp\_max  
RT1  
RT2  
CT1

Set to 25  
Set to 25  
Maximum Temperature  
Thermal Resistance coil - housing  
Calculated\*  
Given by Tecnotion

CT2	Given by Tecnotion
<b>Physical Data</b>	
F_axial	-
F_Radial	-
m	-
D_motor	-
L_motor	-
D_shaft	-
L_shaft	-
	-
<b>Electrical Data</b>	
R	2 * Resistance per phase
L	2 * Induction per phase
alpha_c	0.004
Ktc	0
Pitch	Magnet Pitch NN
<b>Mechanical Data</b>	
m_motor	Weight of Coilunit
d	Given by Tecnotion
F_fric	-
F_cog	0
<b>Derived Data</b>	
K_nom	Calculated
K_max	Calculated
S_nom	Calculated
P_dis	Calculated

\* Note: The nominal data and the default value of the thermal resistance RT2 are calculated for **air cooling**. The value for RT2 can be changed using a slider. **If water cooling is used, change the value of RT2 to its minimum** value.

## File

20-sim 3.6\Tools\Servo Motor Dynamics\Faulhaber 2006.cse

## Date

February 2006

## More information

[www.faulhaber-group.com](http://www.faulhaber-group.com) or [www.minimotor.ch](http://www.minimotor.ch)

## Description

The data file Faulhaber 2006.cse contains the most of the Faulhaber servo motors, program 2006. Most of the data has been extracted from the Faulhaber data sheets. The tables below shows the 20-sim names and the corresponding data sheet names. Some parameters were not available in the data sheets and have been given by Faulhaber. These parameters are indicated as *Given by Faulhaber*. Some parameters were calculated. These are indicated as *Calculated*.



**DC motors****Servo Motor Editor****General Data**

Name  
 Keyname  
 Info  
 Type  
 Date  
 Price  
 Delivery Time  
 Library

**Nominal Data**

Torque  
 Current  
 Speed  
 Voltage  
 Power

**Max/Peak Data**

Torque  
 Current  
 Power  
 Voltage  
 Speed

**Thermal Data**

Temp\_amb  
 Temp\_initial  
 Temp\_max  
 RT1  
 RT2  
 CT1  
 CT2

**Physical Data**

F\_axial  
 F\_Radial  
 m  
 D\_motor  
 L\_motor  
 D\_shaft  
 L\_shaft

**Electrical Data**

R  
 L  
 alpha\_c  
 Ktc  
 Poles

**Mechanical Data**

J\_rotor  
 d  
 T\_fric

**Faulhaber Data Sheets**

Motor Name  
 Faulhaber Order Number  
 Additional Information  
 DC  
 23 February 2006  
 -  
 -  
 Faulhaber 2006.cse

Calculated  
 Current up to  
 No load speed divided by 2  
 Calculated  
 Calculated

Stall torque  
 Calculated  
 Output Power  
 Nominal Voltage  
 No-load speed

Set to 25  
 Set to 25  
 Maximum coil temperature  
 Thermal resistance rotor – housing Rth1  
 Thermal resistance housing-ambient Rth1  
 Calculated  
 Calculated

Maximum Axial load  
 Maximum radial load  
 Weight of motor  
 Diameter of motor  
 Length of motor  
 Diameter shaft  
 Length Shaft

Terminal resistance  
 Rotor Inductance  
 Temperature coefficient of resistance of copper  
 Given by Faulhaber  
 Given by Faulhaber

Rotor inertia  
 Friction torque, dynamic  
 Friction torque, static

T_cog	0
<b>Derived Data</b>	
K_nom	Calculated
K_max	Calculated
S_nom	Calculated
P_dis	Calculated

## DC Brushless motors with block commutation

### Servo Motor Editor

#### General Data

Name  
Keyname  
Info  
Type  
Date  
Price  
Delivery Time  
Library

#### Nominal Data

Torque  
Current  
Speed  
Voltage  
Power

#### Max/Peak Data

Torque  
Current  
Power  
Voltage  
Speed

#### Thermal Data

Temp\_amb  
Temp\_initial  
Temp\_max  
RT1  
RT2  
CT1  
CT2

#### Physical Data

F\_axial  
F\_Radial  
m  
D\_motor  
L\_motor  
D\_shaft  
L\_shaft

#### Electrical Data

### Faulhaber Data Sheets

Motor Name  
Faulhaber Order Number  
Additional Information  
DC Brushless  
23 February 2006  
-  
-  
Faulhaber 2006.cse

Torque up to  
Current up to  
At speed  
Calculated  
Calculated

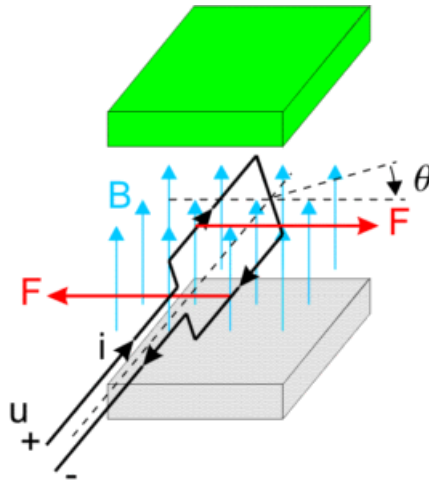
Stall torque  
Calculated  
Output Power  
Nominal Voltage  
No-load speed

Set to 25  
Set to 25  
Maximum coil temperature  
Thermal resistance rotor – housing Rth1  
Thermal resistance housing-ambient Rth1  
Calculated  
Calculated

Maximum Axial load  
Maximum radial load  
Weight of motor  
Diameter of motor  
Length of motor  
Diameter shaft  
Length Shaft

R	Terminal resistance
L	Rotor Inductance
alpha_c	Temperature coefficient of resistance of copper
Ktc	Given by Faulhaber
Poles	Given by Faulhaber
<b>Mechanical Data</b>	
J_rotor	Rotor inertia
d	Friction torque, dynamic
T_fric	Friction torque, static
T_cog	0
<b>Derived Data</b>	
K_nom	Calculated
K_max	Calculated
S_nom	Calculated
P_dis	Calculated

When permanent magnets are used in a motor, a magnetic field will be present with a magnetic flux density  $B$ . Suppose an electric coil is placed in this magnetic field. When an electric current  $i$  is forced to flow through this coil, a force acting on the coil will occur.



The resulting torque can be found as:

$$T = K_{tc}(\theta) \cdot i$$

where  $K_{tc}(q)$  denotes the transfer of current to torque. It is a function of the angle, shape of the coil, magnetic field density, current distribution etc. When the current is kept equal to zero and we start to rotate the coil, a voltage will be induced. This voltage is called the electromotive force (EMF) and can be found as:

$$EMF = K_{ec}(\theta) \cdot \omega$$

where  $K_{ec}(q)$  denotes the transfer of speed to voltage. It is also function of the angle, shape of the coil, magnetic field density, current distribution etc. For an ideal coil the input power should be equal to the output power

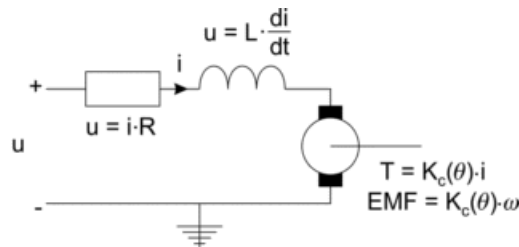
$$P_{in} = EMF \cdot i = K_{ec}(\theta) \cdot \omega \cdot \frac{T}{K_{tc}(\theta)} = \omega \cdot T = P_{out}$$

and thus

$$K_{tc}(\theta) = K_{ec}(\theta) = K_c(\theta)$$

In most literature the  $K_c(q)$  is calculated out of the magnetic field and coil distribution. Here it is simply assumed to be given and is called the **torque function**.

In normal operation a coil will have a resistance and inductance. A basic coil model is thus equal to:



By a proper design of the motor, i.e. geometry of the coil windings, magnets etc., the torque function  $K_c(q)$  can be given a particular shape. Then by proper manipulation of the current a positive torque can be created during the whole rotation of the coil. All permanent magnet motors are based on this principle.

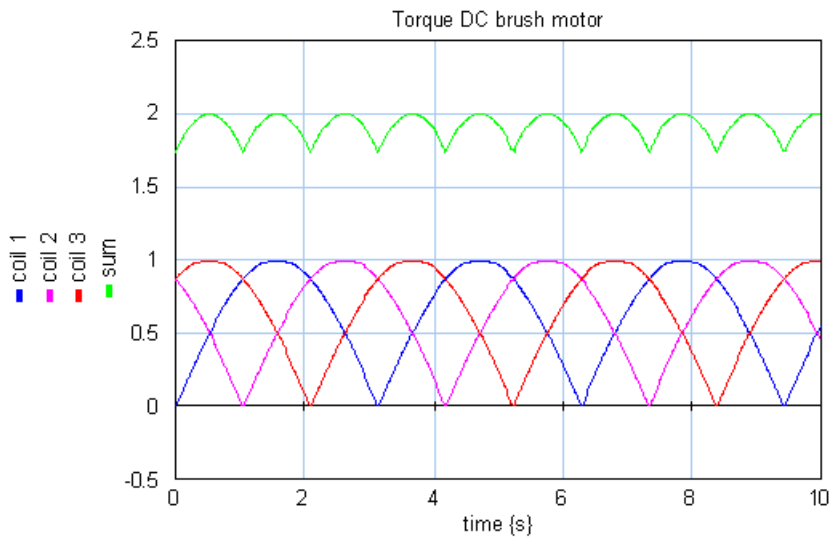
In DC motors, the torque function  $K_c(q)$  is sinusoidal:

$$K_c(\theta) = \hat{K}_c \cdot \sin(\theta)$$

In DC motors a constant current is supplied. Through a process called commutation, the coil is connected the other way around (i.e the current changes sign) when the coil function crosses zero. The resulting torque will then always be positive but will vary between zero and maximum:

$$T = i(\theta) \cdot \hat{K}_c \cdot \sin(\theta) = \hat{i} \cdot \hat{K}_c \cdot \text{abs}(\sin(\theta))$$

By combining coils, the resulting torque variation or *ripple* will decrease. The graph below shows the resulting torque when three coils are used.



The more coils are used the more the torque ripple decreases.

number of coils	torque ripple (top-top)
3	14%
5	5%
7	2.5%
9	1.5%
11	1%

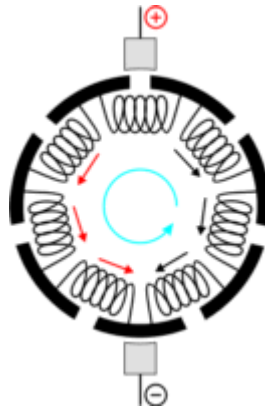
If we neglect the torque ripple, we get the common DC motor equations:

$$T = K \cdot i$$

$$EMF = K \cdot \omega$$

**Commutation**

In practical motors, the rotor is equipped with a commutator. A commutator consists of insulated collector bars that are connected with the coils. Each coil is connected with one end to a collector and the next end to the neighboring collector. A pair of brushes is used to connect an outside current source to the collectors.



Every rotation the current changes sign twice, resulting in a continuous positive torque addition of every coil.

### Limits

Commutation is the largest limiting factor in DC motor performance. Sparks between the brushes and the collectors are the main causes for brush wear. There are several causes for sparking, which limit the maximum speed, current, voltage and power of a brush DC motor.

When the brush leaves a collector, the current has to be reversed. The time that is needed to reverse the current depends directly on the current amplitude and thus on the generated torque. Because the time that is available depends on the motor speed, the result is a limit on the power that can be generated.

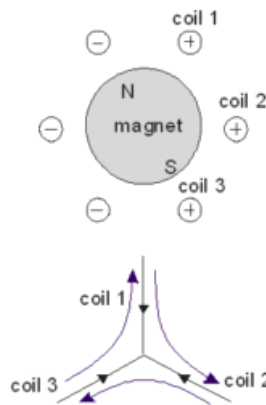
Another limitation of the motor speed is due to imperfect dimensions of the collectors. Differences in height of a few microns may cause the brushes to jump at high speeds.

Just a small part of the contact area of a brush and collector is actually used for the current transfer. As a result highly localized, short time "hot spots" develop. When the currents get greater than permitted, local temperatures occur that lead to material evaporation.

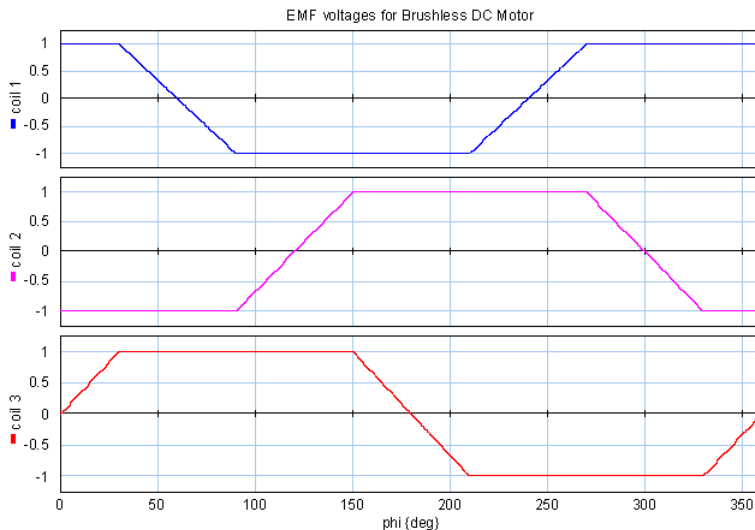
Above a voltage of 15 to 18V experience shows that the air will experience ionization phenomena, which leads to arcing. This arc extends from one collector bar to another. When enough voltage is applied, the arc will extend several collector bars and reach the other brush, leading to serious damage. The maximum motor voltage is therefore the result of multiplying the number of collector bars between the brushes and the maximum collector bar voltage.

Permanent magnets can lose their strength when operating above temperatures of 60 °C and suppressed by a high external magnetic field. Such a field can occur when large current changes occur. Therefore the maximum current of a motor should be limited.

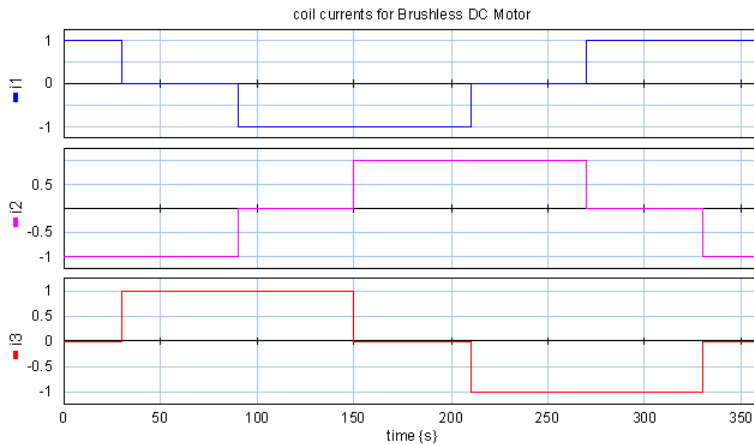
Given motor with three coils, where the coils are mounted in the stator with a spatial displacement of 120°. The coils are connected in a star-formation as shown in the figure below.



In Brushless DC motors, the coils and magnets are designed so that a trapezoidal torque function  $K_c(q)$  is found as shown below:



To get a constant torque each coil current is a block wave as shown in the figure below. Although the current is thus alternating, the term DC is used to distinguish this type of motor from motors that used a sinusoidal current. The block wave current is provided through "electronic commutation". The current is generated by a three phase amplifier that gets the exact switching points from a motor controller.



As can easily be seen from the graphs, the resulting torque is constant and twice the current times the amplitude of the coil function:

$$T = 2 \cdot \hat{i}_c \cdot \hat{K}_c$$

To get an equivalent of the coil model we can write this equation as:

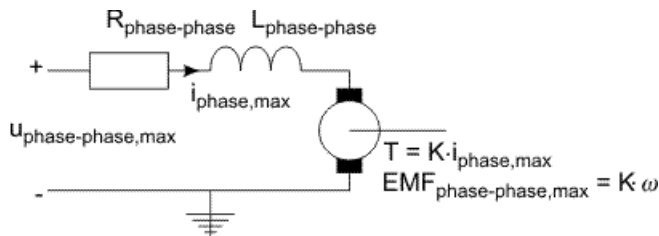
$$T = K \cdot i_{\text{phase,max}}$$

We have to realize that here  $i$  is not a constant current anymore but the maximum coil current! Because the coil current is the current of one of the three phases, in literature  $i$  is mostly written as the **maximum phase current**. It is the maximum current that can be measured at each of the three terminals of the motor.

In a derivation that goes beyond the scope of this introduction (see Compter, 2004), it can be shown that the electromotive force can be found as:

$$EMF_{\text{phase-phase,max}} = K \cdot \omega$$

Here the electromotive force is defined as the maximum induced voltage between two phases. The resulting motor model is shown below:



The voltage of the motor model is commonly known as the **maximum phase to phase voltage**. It is the maximum voltage that can be measured between any pair of two terminals. The **phase to phase resistance** and **phase to phase inductance** are defined equivalent as the resistance and inductance that can be measured between any pair of two terminals.

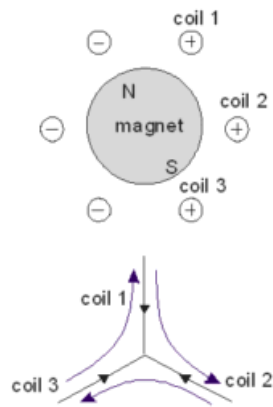


Limits

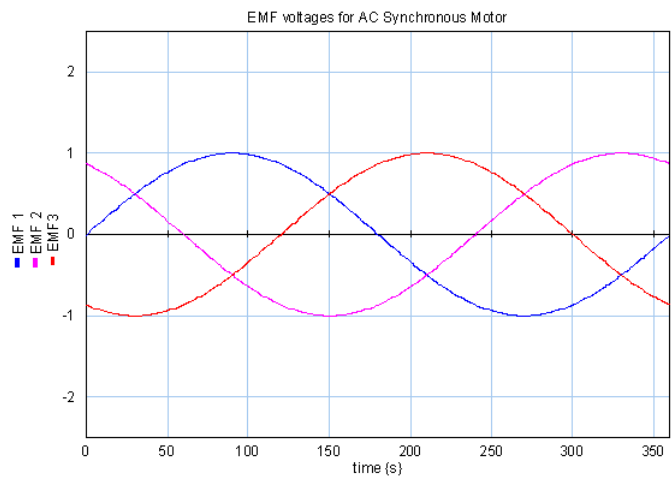
Brushless DC motors have no mechanical commutation, and therefore do not suffer from the limits caused by mechanical commutation. Consequently Brushless DC motors can run at much higher speeds and are not limited by a maximum voltage. The speed of Brushless DC motors is only limited by the bearings.

Just like brush DC motors the magnets impose an upper limit for the current and torque in a Brushless DC motor.

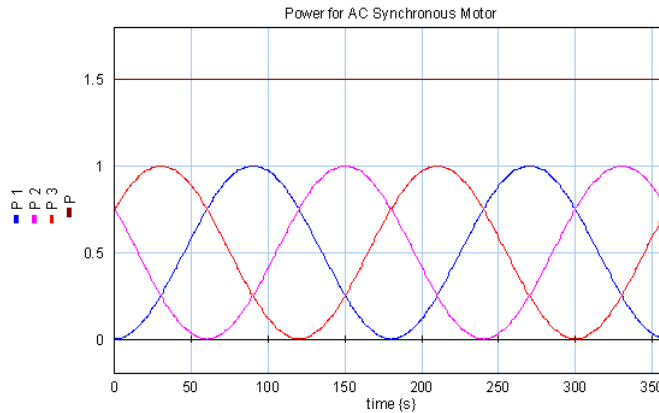
AC synchronous motors use the same principle as Brushless DC-motors. The coils are also mounted in the stator with a spatial displacement of 120°.



The coils and magnets are designed so that a sinusoidal torque function  $Kc(q)$  is found as shown below:



To get a constant torque each coil current is a sinusoidal wave as shown in the figure below.



As can be seen from the graph, the resulting torque is constant and one and a half times the current times the amplitude of the coil function:

$$T_a = \frac{3}{2} \cdot \hat{K}_c \cdot \hat{i}_c$$

To get an equivalent of the coil model we can write this equation as:

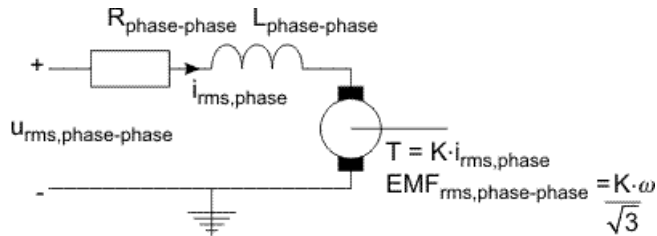
$$T = K \cdot i_{rms,phase}$$

We have to realize that here  $i$  is not a constant current anymore but the root mean square coil current! Because the coil current is the current of one phase in literature  $i$  is mostly denoted as the **rms phase current**. It is the rms current that can be measured at each of the three terminals of the motor.

In a derivation that goes beyond the scope of this introduction (see Compter, 2004), it can be shown that the electromotive force can be found as:

$$EMF_{rms,phase-phase} = \frac{K}{\sqrt{3}} \cdot \omega$$

Here the electromotive force is defined as the induced rms voltage between two phases. The resulting motor model is shown below:



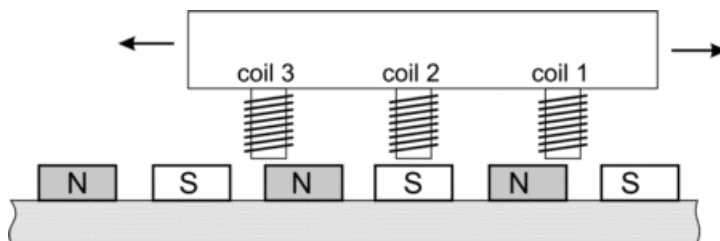
The voltage of the motor model is mostly denoted as the **rms phase to phase voltage**. It is the rms voltage that can be measured between any pair of two terminals. The **phase to phase resistance** and **phase to phase inductance** are defined equivalent as the resistance and inductance that could be measured between any pair of two terminals.

### Limits

AC synchronous motors have no mechanical commutation, and therefore do not suffer from the limits caused by mechanical commutation. Consequently AC synchronous motors can run at much higher speeds and are not limited by a maximum voltage. The speed of AC synchronous motors is only limited by the bearings.

Just like brush DC motors the magnets impose an upper limit for the current and torque in a AC synchronous motor.

The working principle of linear motors is exactly the same as for rotary motors. Magnets are placed on a flat surface, as shown in the figure below. A carriage holding the coils can run over the magnets.



When the carriage runs over the magnets an electromotive voltage will be induced:

$$u = K_c(x) \cdot v$$

with  $K_c(x)$  the **force function** of the coil. It is a function of the carriage position, shape of the coil, magnetic field density, current distribution etc. The force function in a linear motor is equivalent to the torque function of a rotary motor. When a current runs through the coil a force results:

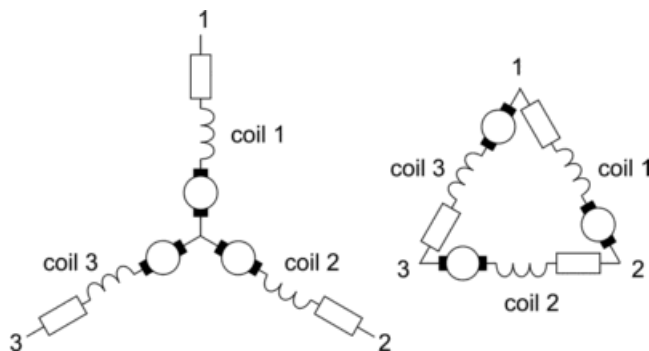
$$F = K_c(x) \cdot i$$

The principle for linear motor is the same as the principle of rotary motors. By a proper design of the motor, i.e. geometry of the coil windings, magnets etc., the force function  $K_c(x)$  can be given a particular shape. By proper manipulation of the current a positive force can be created during the movement of the carriage. Because mechanical commutation is not very useful for linear movements, linear motors use electronic commutation. Like their rotary counterparts, linear motors can be driven by block shape currents (Brushless DC Linear) and sinusoidal currents (AC Synchronous Linear).

### Limits

The limits for linear motors are equal to the Brushless DC and AC synchronous motors when torque is replaced by force and angular speed by linear speed.

Brushless DC motors and AC synchronous motors use three phase currents to connect to three groups of coils. The connection can be made use a star network or a delta network. Compared to star networks, in a delta network less voltage and more current is needed to produce the same amount of torque. For amplifiers the maximum current is directly related to the costs. That is why delta networks are only used in special cases where higher speeds than normal are required.



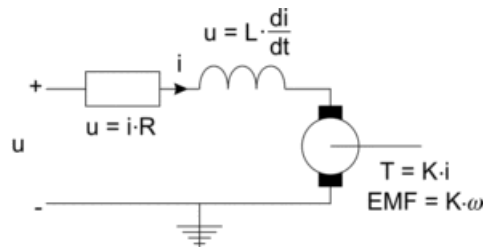
In 20-sim the electrical resistance and inductance are measured between the terminals (e.g. between 1 and 2 or 2 and 3 or 3 and 1). This is known as the **terminal resistance** and **inductance** or as the **phase to phase resistance** and **inductance**. There are two reasons for using terminal values. Most motor suppliers give the terminal values in their data sheet and by using terminal values the same dynamic model can be used for star networks and delta networks.

If the motor supplier gives coil values instead of terminal values, you have to calculate them by hand. The relation between the terminal values and the coil values is:

$$R_Y = 2 \cdot R_{coil} \quad R_\Delta = \frac{2}{3} \cdot R_{coil}$$

$$L_Y = 2 \cdot R_{coil} \quad L_\Delta = \frac{2}{3} \cdot R_{coil}$$

The DC motor model can serve as a prototype model for all permanent magnet motors.



Although the models for DC Brushless and AC synchronous motors are slightly different, the DC motor model is still very useful to explain their operation. In this chapter the DC motor model will be used to derive the torque speed plot of a motor and show the use of the torque speed plot for motor selection.

The working principle for all permanent magnet motors is the same: get a constant torque by manipulation of the coil function and the current. The relation between the torque and current is:

$$T = K_T \cdot i$$

The constant  $K_T$  is generally known as the **torque constant**. The relation between the induced current and the rotational speed is:

$$EMF = K_e \cdot \omega$$

The constant  $K_e$  is generally known as the **voltage constant**. For DC motors the torque constant and voltage constant have the same value. Therefore the subscripts T and e are usually omitted. The total voltage can be described as:

$$u = i \cdot R + L \cdot \frac{di}{dt} + K \cdot \omega$$

If we assume the current is changing only very slowly, the current derivative can be neglected:

$$i = \frac{u - K \cdot \omega}{R}$$

With the torque equation:

$$T = K \cdot i$$

this leads to

$$T = \frac{K \cdot (u - K \cdot \omega)}{R}$$

The torque at zero speed (**stall torque**) is found as

$$T_{stall} = \frac{K \cdot u}{R}$$

which enables us to write the torque as:

$$T = T_{stall} - \frac{K^2}{R} \cdot \omega = T_{stall} - S \cdot \omega$$

where S is commonly known as the **steepness**. The steepness has many definitions:

$$S = \frac{T^2}{i^2 \cdot R} = \frac{K^2}{R} = \frac{\Delta T}{\Delta \omega}$$

The speed where the current is zero (no load speed) is equal to

$$\omega_0 = \frac{u}{K}$$

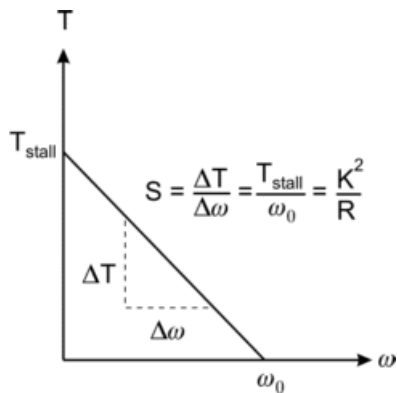
The relation between stall torque and no load speed is obvious:

$$T_{stall} = S \cdot \omega_0$$

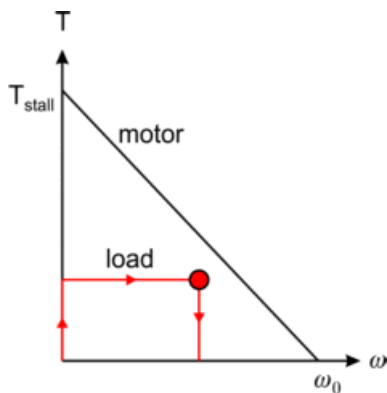
which leads to the general torque equation:

$$T = S \cdot (\omega_0 - \omega)$$

This equation can be displayed graphically and is commonly known as the torque speed plot. The graph shows the generated torque as a function of the speed. For constant voltages a straight line from the stall torque to the no load speed is found. The slope of the line is equal to the steepness S.



The torque speed plot is a useful representation of a motor because we can draw the desired load torque in this plot and to see if the motor is able to produce this torque. In the figure below the load curve is shown in red. It is a constant torque applied to a load, which makes it accelerate until a certain velocity is reached and the torque gets zero.



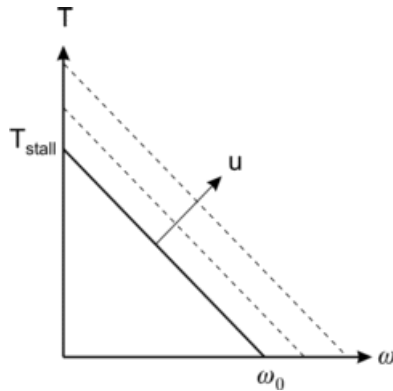
The red dot indicates the point of maximum load power. This point is important because it indicates the maximum power that the motor has to deliver.

To find out if a motor is sufficient, we have to plot the motor limits in the torque speed plot. In the previous chapter we have described the following limits:

Limit	Brush DC
torque / current	✓
speed	✓
power	✓
voltage	✓

### Maximum Voltage

For higher voltages, a higher stall torque and no load speed is found but the steepness does not change.

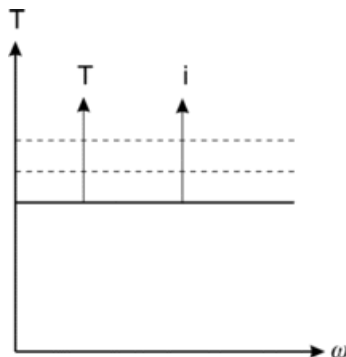


### Maximum Torque / Maximum Current

In many data sheets a maximum torque is given. This is directly connected with a maximum current limit through the equation:

$$i = \frac{T}{K}$$

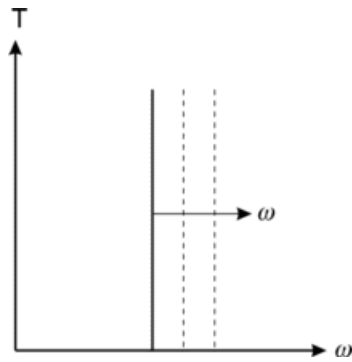
So both the maximum current and the maximum torque appear as horizontal lines in the torque speed plot.



### Maximum Velocity

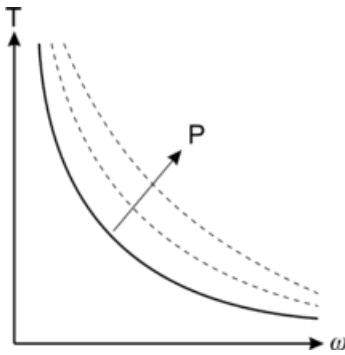
The maximum velocity can be directly indicated in the torque speed plot as a vertical line.



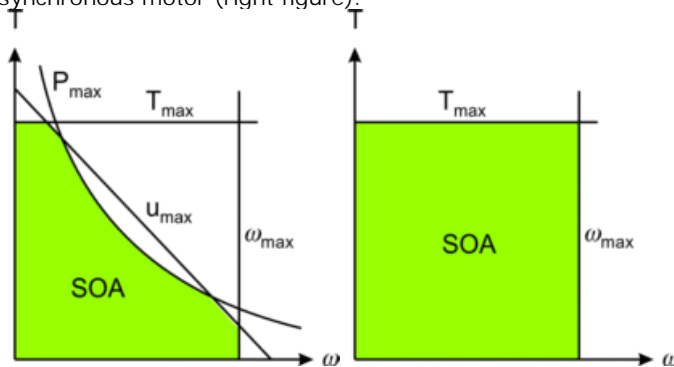


### Maximum Power

The line of maximum power can be indicated as a parabola in the torque speed plot.



If the limits are plotted in the torque speed plot, an Area of Safe Operation is found. For a proper motor, the torque speed curve of the load should be inside the **Safe Operating Area (SOA)**. The figures below show the safe operating areas for the various motor types. Brush DC-motors (left figure) have a safe operating area that is more limited than Brushless DC motors and AC synchronous motor (right figure).



In practice motor suppliers of Brushless DC motors and AC synchronous motors may impose limits on the maximum voltage and power. This is mostly done to prevent heating up the motor too quickly during continuous operation, or material limits. This makes the Safe Operating Area of these motors look like that of a DC motor. Compared to DC motors, Brushless DC motors and AC synchronous motors will always allow higher torques and speeds because of the absence of mechanical commutation.

Every motor will experience losses, which results in a temperature rise. The maximum allowed temperature is limited by the magnets, the oil in the bearings and the mechanical behaviour of the brushes. Analysis of the cause of losses is therefore important for the correct choice of a motor.

### Electric Dissipation

All motor coils have resistance and will therefore generate heat. The heat flow generated is equal to:

$$dQ = \frac{1}{\Delta T} \int_0^{\Delta T} i^2 \cdot R dt = \frac{R}{\Delta T} \int_0^{\Delta T} i^2 dt$$

which can also be written as:

$$dQ = i_{rms}^2 \cdot R$$

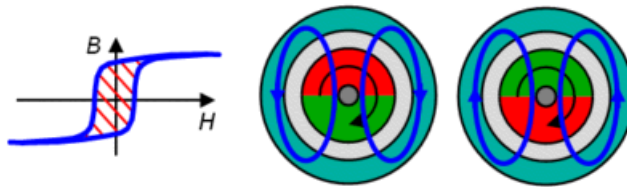
with *irms* the **root mean square** current:

$$i_{rms} = \sqrt{\frac{1}{\Delta T} \int_0^{\Delta T} i^2 dt}$$

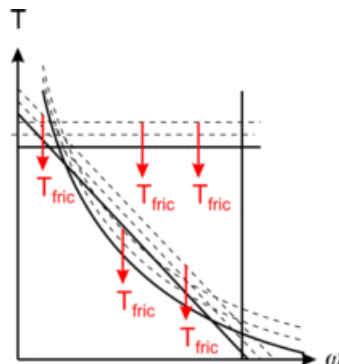
For constant DC currents the root mean square value is equal to the current itself. For sinusoidal currents, the root mean square value is equal to the amplitude of the current times the square root of 2.

### Hysteresis losses

In all motors except from hollow rotor motors, the magnets move with respect to the iron core of the motor. This results in a reversing magnetic field in the iron which leads to hysteresis.

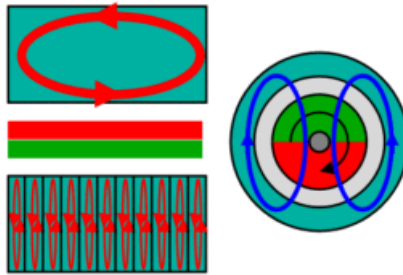


Each rotation produces an energy loss proportional to the area of the hysteresis curve (B/H). The power loss due to hysteresis is proportional to the motor speed and can therefore be represented as a friction torque. Due to this friction torque the motor can produce less output torque. This friction torque can therefore be represented in the torque speed plot as a drop down of all curves.

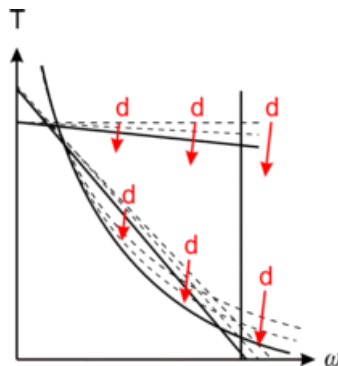


### Eddy Current losses

A reversing magnetic field in iron also leads to an induced voltage. The resistance of the iron determines the resulting currents in the iron. These currents are named eddy currents.



Eddy currents heat up the iron because of its resistance. If a massive iron return is used large eddy currents will be induced with high power losses. Therefore in most motors laminated is applied, which reduce eddy currents by decreasing the path length and thus lead to smaller power losses. The power loss due to eddy currents is proportional to the square of the motor speed and can therefore be modeled as mechanical damping. Damping will decrease the performance of the motor. It can be represented in the torque speed plot as a falling down of curves that increases with the speed.



### Cogging

In a permanent magnet motors cogging torque manifests itself by the tendency of the rotor to align in a number of stable positions when unexcited. The cogging torque can be described as:

$$T_{cog} = \hat{T}_{cog} \cdot \sin\left(\frac{p \cdot \theta}{2}\right)$$

where  $q$  is the motor angle and  $p$  the number of poles. Although cogging does not consume power and is not visible in the torque speed plot, under dynamic conditions it may cause undesirable speed pulsation and also may induce vibrations and acoustic noise.

### Mechanical Losses

Mechanical losses in motors are caused by bearings, brushes and air friction. Only when an air fan is mounted air friction becomes significant. The effects of brushes and bearings can be represented by coulomb friction and damping.

## Temperature

As a result of the heat flow, the motor will warm up leading to two major effects. First of all the coil resistance will increase. Because all coils are made of copper, the temperature dependency of the coil resistance can be written as:

$$R_T = R_{25} \cdot \left(1 + 0.004 \cdot (T_{coil} - 25)\right)$$

where  $R_{25}$  is the coil resistance at room temperature (25 degrees centigrade) and  $T_{coil}$  the actual coil temperature in degrees centigrade. As a result of the increase of motor temperature, the performance of the magnets will decrease. The result is a decrease of the torque constant :

$$K_T = K_{25} \cdot \left(1 + ktc \cdot (T_{magnet} - 25)\right)$$

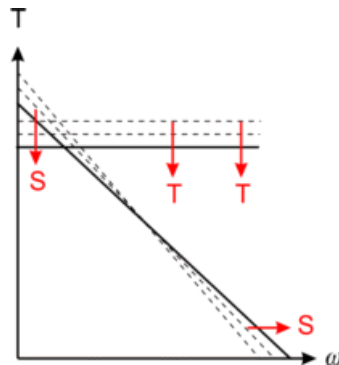
where  $K_{25}$  is the torque constant at room temperature (25 degrees centigrade),  $T_{magnet}$  the actual magnet temperature in degrees centigrade and  $ktc$  the temperature dependency of the used magnet.

Magnets	ktc
Ferrites	-0.002
Nd <sub>2</sub> Fe <sub>14</sub> B	-0.0013
SmCo	-0.0005
AlNiCo	-0.0002

Because the steepness is directly dependent of the torque constant and motor resistance

$$S = \frac{K^2}{R}$$

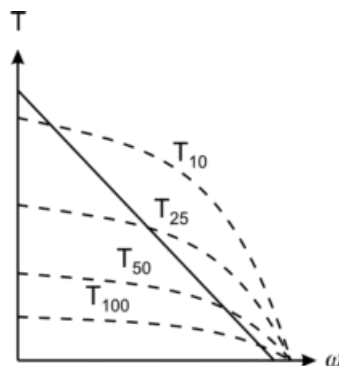
an increase of temperature will lead to a decrease of the steepness. The results of a temperature increase can therefore be shown in the torque speed plot indirectly through the decrease of the maximum torque and steepness.



### Thermal Duty Cycle

Motor losses result in an increase of the temperature. During short term operation the temperature increase will be limited. During long-term operation, the generated heat and the amount of heat that can be removed via the air and motor mounting determine the temperature increase.

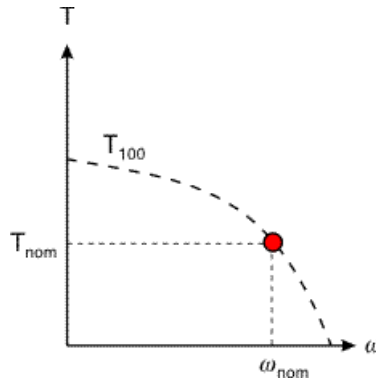
In most motors, the largest portion of the generated heat is caused by electric dissipation. The generated heat is therefore directly proportional to the current and thus the torque. Imagine a motor in long-term operation generating a constant torque. A small torque will lead to only a moderate increase of the motor temperature, but there will be a certain torque where the generated heat leads to an increase of the maximum motor temperature. This is called the **maximum continuous torque** or the **100% Thermal Duty Cycle (TDC)**. The line of the maximum continuous torque can be shown in the torque speed plot and is often denoted as T100. For lower speeds the T100 curve will be straight because the heat generation mainly depends on electric dissipation. For higher speeds the T100 curve will decrease because eddy current losses start to become significant.



If the motor is in continuous operation, but a constant torque is just delivered 50% of the time, a higher torque is permissible. This torque is denoted as T50 and sometimes called the 50% thermal duty cycle. In a similar way T25 and T10 are defined.

## Nominal Operating Point

Many motor manufacturers give in their data sheets a nominal or continuous current at a certain speed. This indicates an operating point on the T100 curve. The nominal or continuous current is the current that continuously be continuously be supplied to the motor at the given speed, which will result in a heating up of the coils to the maximum temperature.



The nominal operating point is always based on a certain ambient temperature. In the 20-sim Servo Motor Editor an ambient temperature of 25 °C is used.

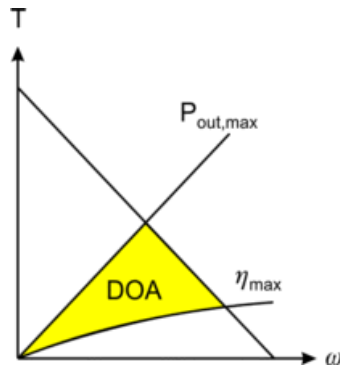
The choice of the speed for the nominal operation point is arbitrary. Some motor suppliers use the speed that results in a maximum power output at the motor shaft. Some motor suppliers use a speed that is half of the maximum allowed speed.

The purpose of a motor is to deliver power to a load. Given a certain voltage  $u$ , the delivered power is equal to the torque times the speed:

$$P = S \cdot \left( \frac{u}{K} - \omega \right) \cdot \omega$$

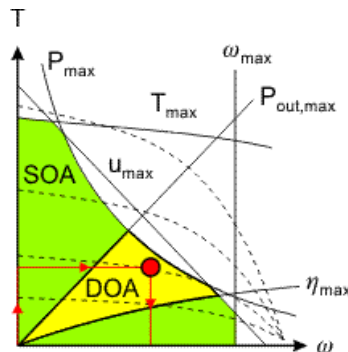
The maximum delivered power  $P_{out,max}$  for a given voltage can be found by differentiating this function and setting it to zero. The result will be a specific torque and speed. If this process is repeated for other voltages, a line of points where maximum power is delivered will result.

The efficiency  $h$  of a motor is defined as the net output power divided by the input power. For a given voltage, the maximum efficiency can be found just like the maximum power and will lead to a certain torque and speed. By repeating this procedure for other voltages, a line of points where maximum efficiency is obtained will result.



The resulting lines of maximum power and maximum efficiency can be shown in the torque speed plot. Choosing a good motor is always a compromise between efficiency and output power. A good choice is to choose a motor that has the major part of the load curve inside the lines of maximum power and maximum efficiency. This area is called the Desired Operating Area.

If we combine the results of the previous sections, a torque speed plot results as shown below. The arrows indicate the load curve with the circle as point of maximum load power. The **Safe Operating Area** shows the limits of operation due to motor specific parameters such as the maximum torque and speed.



The lines of maximum output power and maximum efficiency are the edges of the **Desired Operating Area**. The procedure for choosing a proper motor is:

1. Determine the load curve and the point of maximum load power.
2. Determine the duty cycle  $d$  (the percentage of the time that torque is required) and estimate the corresponding  $Td$  line with help of the shown  $T100$ ,  $T50$ ,  $T25$  and  $T10$  lines.
3. Select a motor such that the following demands are satisfied:
  - The load curve is completely beneath the  $Td$  line (no overheating).
  - The complete load curve is in the Safe Operating Area.
  - The point of maximum load power is in the Desired Operating Area.



- The point of maximum load power is as close to maximum voltage line as possible (we want to choose the smallest motor that can do the job).
- The load curve is as much in the Desired Operating Area as possible.

Every motor generates heat, even when at zero speed, and this will lead to an increase of the motor temperature. Especially when running in continuous operation, there is a good change that a motor, which is perfectly capable of generating the needed output power, will heat up beyond its thermal limit and break down.

As explained in the previous section the thermal limit is indicated in the torque speed curve by the maximum continuous torque line. To generate such a line, a thermal model is used. This thermal model is also part of the dynamic model that is used in 20-sim. This section describes the thermal model of permanent magnets motors.

In standard brush DC motors the coils are part of the rotor. To create a thermal model, various components will be identified first.

### Heat Generation

Heat is generated in the motor at every place where energy is lost: coils, bearings, iron etc. Because the main source of energy loss is in the coils due to the coil resistance, we start at the coils. The coils act as a heat source and generate a heat flow equal to:

$$dQ = i^2 \cdot R$$

### Thermal Capacity

The rotor package, consisting of the coils and possibly iron and other material, will heat up due to the generated heat. The temperature increase depends on the generated heat  $dQ$ , the heat capacity of the rotor  $C_{coil}$  and the transfer of heat to the stationary housing of the motor  $dQ_{coil-housing}$ :

$$T_{coil} = \frac{1}{C_{coil}} \cdot \int dQ - dQ_{coil-housing} dt$$

### Thermal Resistance

The heat flow from the coils to the housing  $dQ_{coil-housing}$  depends on the temperature difference between the rotor and the housing and the thermal resistance  $R_{coil-housing}$  :

$$dQ_{coil-housing} = \frac{(T_{coil} - T_{housing})}{R_{coil-housing}}$$

### Thermal Capacity

Like the rotor, the housing will also heat up. The temperature increase depends on the heat coming from the rotor  $dQ_{rotor-stator}$ , the heat capacity of the housing  $C_{housing}$  and the transfer of heat to the environment  $dQ_{housing-amb}$ :

$$T_{stator} = \frac{1}{C_{housing}} \cdot \int dQ_{coil-housing} - dQ_{housing-amb} dt$$

### Thermal Resistance

The heat flow from the stator to the environment stator  $dQ_{housing-amb}$  depends on the temperature difference between the housing and the environment and the thermal resistance  $R_{housing-amb}$ :

$$dQ_{housing-amb} = \frac{(T_{housing} - T_{amb})}{R_{housing-amb}}$$

The thermal resistance  $R_{housing-amb}$  depends on the motor mounting and external cooling. In most data sheets, a value for the thermal resistance can be found based on standard motor mounting.

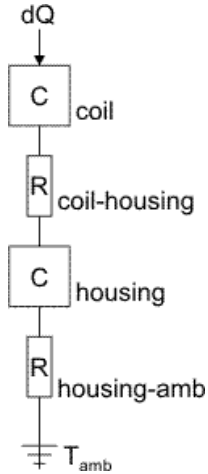
### Environment

The environment is supposed to have a fixed temperature  $T_{amb}$ .

The same components as found for the DC brush motor can be found for other motor types. We only have to realize that for Brushless DC motors and AC Synchronous motors the coils are mounted on the housing. This means the thermal resistance  $R_{coil-housing}$  is relatively small and excess heat can be transferred relatively easy. Therefore these motors are very robust for overheating.

In AC synchronous linear motors, the coils are mounted are part of a platform, on which the load can be attached. To get the same thermal model we consider the platform to be the housing. Depending on the type of motor the housing can have a medium thermal capacity (iron core motors) or a very small thermal capacity (ironless motors). Because the all excess heat has to be removed through the air, linear motors will heat up easily. That is why sometimes forced cooling (water) is applied.

If we combine all components we get the complete thermal model. It can be represented as shown in the figure below.



The values for thermal capacities and resistances can be found in most data sheets. These values are, however based on general conditions. The value of the thermal resistance *R<sub>housing-amb</sub>* can vary considerably, based on the specific mounting of the motor and use of passive or active cooling. Most motor suppliers will indicate the how the thermal parameters were derived and how the motor should be mounted to meet the general conditions.

## 8.6 Real-Time Toolbox

### Introduction

The Real Time toolbox of 20-sim allows you to create C-code out of any 20-sim model for the use in real-time applications:

1. Create ANSI-C code for use in a real-time environment.
2. Create Matlab / Simulink S-functions for the use in the Matlab Real-Time Workshop.

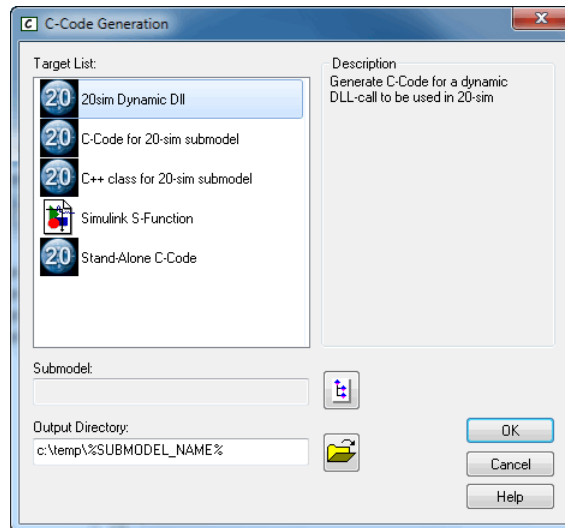
The generation of Matlab / Simulink code is can be performed using the Export command of the Editor File menu. You can also use the C-code generation command of the Simulator **Tools** menu.

The generation of C-code can be done with the C-code generation command of the Simulator **Tools** menu.

### C-Code Generation

20-sim has a C-Code Generator which automatically converts a complete 20-sim model or submodel into C-Code. The application can be used to generate Matlab™/Simulink™ S-Functions, to generate Stand-Alone executables or to generate input/output functions for use in other C and C++ programs. The ANSI C-Code Generator can be opened from the

Simulator (**Tools** menu, **C-Code Generation** command).



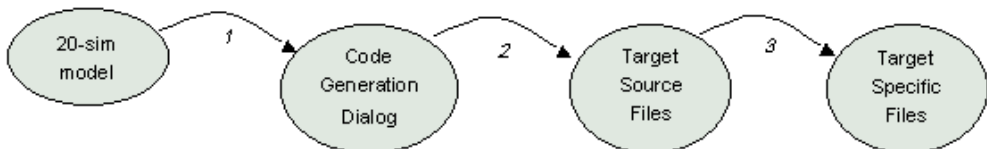
- Depending on the target selected, 20-sim will generate specific C-code.
- You can add more targets by adding paths in the General Properties.

## Overview

The modeling and simulation package 20-sim is capable of generating ANSI C-Code for several targets. Possible targets are Stand-Alone C, a C-Function, or a Simulink S-Function. Since 20-sim generates well-documented ANSI C-Code, it is easy for a user to make modifications or extensions to the generated code by hand. However it is also possible to fully define your own code target using C-Code templates, and to make modifications in these templates, so the resulting source code is tailor made for your application.

## General Structure

The code generation process of 20-sim typically has the following structure:



## Step 1

1. The process starts with a model and simulation in 20-sim.
2. In the 20-sim Simulator, the user selects the **C-Code Generation** command from the **Tools** menu.
3. 20-sim collects information about the current model.

4. A target configuration file is read that specifies the different code generation targets that exist.
5. The **C-code generation dialog** is opened, allowing the user to specify the target to use.

## Step 2

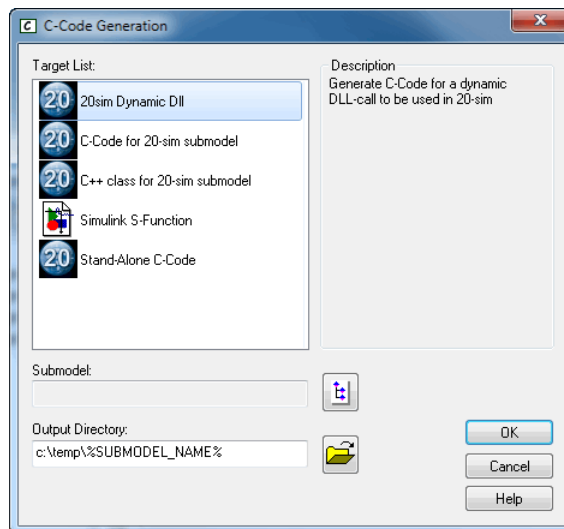
1. The selected target refers to specific template files (source files) in a target specific subdirectory.
2. 20-sim adapts these template files with the model information and generated code for the model.

## Step 3

1. The resulting files are placed in a destination directory.
2. These files are now specific for the target and the model.
3. If desired, 20-sim can call additional commands for further processing (f.i. make, run etc).

## Code Generation Dialog

After 20-sim reads the target configuration file, the code generation dialog is shown with the information of this file:



The target list shows the names of the available targets. When a selection is made, the description of the selected target is given at the right. A submodel can be selected when the target requires this. The output directory can be overruled.

## Targets

The user can create own targets. All targets are defined in the target definition file `Targets.ini`. This file has a typical INI-file structure and starts with a section that simply enumerates which targets exist. Each target then has its own section that holds the remaining information, like a short description of the target, the name of the template directory, the names of the template source files, additional commands to perform, etc. The following keywords may appear in a target section:

## Templates

Each target can point to a set of template files that are used to create C-Code with. Own template files can be created by the user, with the help of the most powerful feature of 20-sim C-Code generation: the use of tokens! A token is a placeholder for model-dependent information. For instance in the C-Code Generation Dialog, the target destination directory contains the name of the selected submodel (e.g. `c:\temp\%SUBMODEL_NAME%`) by default. Since this information is not yet known when the `targets.ini` file is created, a specific token that refers to this name is used instead. A complete description of predefined tokens is described in the section about Available 20-sim Tokens.

## Generation Result

After the tokens in the target template files are replaced, the resulting target and model specific files will be placed in the destination directory. If commands are specified in the `Targets.ini` file, these commands are performed. This allows the user to call scripts automatically. E.g. for automatic compilation, linking and running of the code in a certain target environment.

The user can create own targets. All targets are defined in the target definition file `Targets.ini`. This file has a typical INI-file structure and starts with a section that simply enumerates which targets exist. Each target then has its own section that holds the remaining information, like a short description of the target, the name of the template directory, the names of the template source files, additional commands to perform, etc. The following keywords may appear in a target section:

### **targetName**

= "string"

The name that will appear in the 20-sim C-Code Generation Dialog.

### **iconFile**

= "string"

The name of an icon file (.ico) that contains an icon to appear in the 20-sim C-Code Generation Dialog.

### **description**

= "string"

The string that will appear in the description field in the 20-sim C-Code Generation Dialog.

### **templateDirectory**

= "string"

Here the path name where the template files for the c-code can be found can be specified. The default name is the target name in the CCode directory of 20-sim. If no full path is specified, the Ccode directory in 20-sim is taken as a starting point.

**templateFiles**

=filename1; filename2; filename3...

A list of files, semicolon-separated, that specify the files that are generated in the targetDirectory.

**targetDirectory**

= "string"

This holds the default target directory where the files will be generated. This directory name will appear in the 20-sim dialog box when C-Code is generated and can be overruled by the user.

**submodelSelection**

=TRUE (default)

=FALSE

Determines whether C-Code is generated for the complete 20-sim model, or that a submodel selection is required.

**preCommand**

= "string"

A command which will be executed in the target directory before that the C-Code will be generated.

**postCommand**

= "string"

A command which will be executed in the target directory after that the C-Code has been generated. For example a "make" command can be given to automatically compile the generated code for the specific target.

**newLineCharacter**

=0	CRLF (0x0d0a = DOS Standard)
=1	CR (0x0d = Macintosh Standard)
=2	LF (0x0a = Unix Standard)

Enter a number for the kind of newline character that should be used.

**%KEYWORD%**

=value

This (re)defines the keyword "KEYWORD" and gives it the contents "value". Own keywords can be defined in this manner as well.

**example:**

```
%XX_TIME%=someTime
```

will redefine the time variable with the value "someTime"

## Example

A valid Targets.ini file (defining three targets) may look like below. The file may also contain specific 20-sim tokens (%MODEL\_NAME%) that are described later on.

```
; Possible targets for 20-sim C-Code Generation
;
[targets]
StandAloneC
CFunction
20simDLL
Simulink

; Generate Stand-Alone C-Code for the complete 20-sim model
;
[StandAloneC]
targetName="Stand-Alone C-Code"
iconFile="20sim.ico"
description="Use this target when testing the complete 20-sim model as a single process."
SubmodelSelection=FALSE
templateDirectory="StandAloneC"
templateFiles=xxfuncs.c;xxfuncs.h;xxinteg.c;xxinteg.h;xxinverse.c
templateFiles=xxmain.c;xxmatrix.c;xxmatrix.h;xxmodel.c;xxmodel.h
templateFiles=xxtypes.h;%MODEL_NAME%.dsp;%MODEL_NAME%.dsw
targetDirectory="c:\temp\%MODEL_NAME%"

; Generate C-Code for a selected Submodel
;
[CFunction]
targetName="C-Code for 20-sim submodel"
iconFile="20sim.ico"
description="This is the C-Code as it was generated for a submodel in 20-sim version 3.1"
templateDirectory="CFunction"
templateFiles=xxfuncs.c;xxfuncs.h;xxinteg.c;xxinteg.h;xxinverse.c
templateFiles=xxmain.c;xxmatrix.c;xxmatrix.h;xxmodel.c;xxmodel.h
templateFiles=xxsubmod.c;xxsubmod.h;xxtypes.h;%SUBMODEL_NAME%.dsp;%
SUBMODEL_NAM
E%.dsw
targetDirectory="c:\temp\%SUBMODEL_NAME%"

; Generate C-Code for a dynamic DLL-call to be used in 20-sim
;
[20simDLL]
targetName="20sim Dynamic Dll"
iconFile="20sim.ico"
description="Generate C-Code for a dynamic DLL-call to be used in 20-sim"
templateDirectory="20simDLL"
templateFiles=xxfuncs.c;xxfuncs.h;xxinverse.c
templateFiles=xxmatrix.c;xxmatrix.h;xxmodel.c;xxmodel.h
templateFiles=xxtypes.h;%SUBMODEL_NAME%.c
templateFiles=%SUBMODEL_NAME%.dsw;%SUBMODEL_NAME%.dsp;%SUBMODEL_NAME%
.emx
targetDirectory="c:\temp\%SUBMODEL_NAME%"
```



```
; Generate C-Code for a Simulink S-Function
;
[Simulink]
targetName="Simulink S-Function"
iconFile="mdl.ico"
description="This generates C-Code for a submodel to be used in Matlab/Simulink"
templateDirectory="Simulink"
templateFiles=%SUBMODEL_NAME%.c; xxinverse.c; xxmatrix.c; xxmatrix.h
templateFiles=xxmexfcs.c; xxmextps.h; xxtypes.h; %SUBMODEL_NAME%_.mdl
targetDirectory=c:\temp\%SUBMODEL_NAME%
postCommand=mex %SUBMODEL_NAME%.c
```

Both the target configuration file and the code generation dialog revealed the most important part of the 20-sim code generation process, the use of tokens!

A token is a placeholder for model-dependent information. For instance in the code generation dialog, the target destination directory contains the name of the selected submodel by default. Since this information is not yet known when the `targets.ini` file is created, a specific token that refers to this name is used instead.

The idea is to create targets from template source files that contain tokens instead of actual model-dependent information (like equations, names, parameters, inputs etc). The files that are specified in a target section will be scanned for these tokens and tokens will be replaced by the corresponding model-dependent information.

### Predefined variable names

The following variables should be declared in the C-Code template, because 20-sim uses these names in the generation of the equations:

**c:** constant array  
**P:** parameters array  
**V:** variables array  
**s:** states array  
**R:** rates array  
**M:** matrix array  
**U:** unnamed variables array  
**F:** favorite variables array  
**f:** favorite parameters array

Note that these parameters are case-sensitive!

### Model Data

The following tokens will be replaced by numbers indicating the number of model parameters etc., typically used in memory allocation parts and loops.

<b>%NUMBER_CONSTANTS</b>	The number of constants in the model
<b>%</b>	The number of parameters in the model
<b>%</b>	The number of variables in the model
<b>NUMBER_PARAMETERS</b>	The number of states in the model
<b>%</b>	The number of inputs of the model
	The number of outputs of the model

**%NUMBER\_VARIABLES** The number of matrices used in the model  
**%** The number of unnamed variables in the model  
**%NUMBER\_STATES%** The number of favorite parameters in the model  
**%NUMBER\_INPUTS%** The number of favorite variables in the model  
**%NUMBER\_OUTPUTS%** The size of the largest workarray necessary in calculating some  
**%NUMBER\_MATRICES** matrix functions  
**%**  
**%NUMBER\_UNNAMED%**  
**%**  
**NUMBER\_FAVORITE\_PA**  
**RAMETERS%**  
**%**  
**NUMBER\_FAVORITE\_VA**  
**RIABLES%**  
**%WORK\_ARRAY\_SIZE**  
**%**

The following tokens are already reserved for future use:

**%NUMBER\_DEPSTATES** The number of dependent states in the model  
**%** The number of algebraic loop variables pairs in the model  
**%NUMBER\_ALGLOOPS** The number of constraint variable pairs in the model  
**%** The number of import variables in the model  
**%** The number of export variables in the model  
**NUMBER\_CONSTRAINTS**  
**%**  
**%NUMBER\_IMPORTS%**  
**%NUMBER\_EXPORTS%**

Example

### Variable name arrays

If you want to use parameters etc. that are specific to a model you can use arrays of names using the following tokens:

**%CONSTANT\_NAMES%** All the constants used in the model.  
**%PARAMETER\_NAMES** All the parameters used in the model.  
**%** All the variables used in the model.  
**%VARIABLE\_NAMES%** All the states used in the model.  
**%STATE\_NAMES%** All the rates used in the model.  
**%RATE\_NAMES%** All the dependent states used in the model.  
**%DEPSTATE\_NAMES%** All the dependent rates used in the model.  
**%DEPRATE\_NAMES%** All the algebraic loop variables used in the model.

**%ALGLOOP\_NAMES%** All the constraint variables used in the model.  
**%CONSTRAINT\_NAMES** All the inputs used in the model.  
**%** All the outputs used in the model.  
**%INPUT\_NAMES%** All the matrices used in the model.  
**%OUTPUT\_NAMES%** All the favorite parameters used in the model.  
**%MATRIX\_NAMES%** All the favorite variables used in the model.  
**%**  
**FAVORITE\_PARAMETER**  
**\_NAMES%**  
**%**  
**FAVORITE\_VARIABLE\_N**  
**AMES%**

Example

### Initialization code

An important part of a model are the parameters, initial values states etc. To match these with the generated model code and use the correct values the following tokens can be used:

**%INITIALIZE\_CONSTANTS%**  
**%INITIALIZE\_PARAMETERS%**  
**%INITIALIZE\_MATRICES%**  
**%INITIALIZE\_STATES%**  
**%INITIALIZE\_DEPSTATES%**  
**%INITIALIZE\_ALGLOOPS%**  
**%INITIALIZE\_CONSTRAINTS%**  
**%INITIALIZE\_INPUTS%**  
**%INITIALIZE\_OUTPUTS%**  
**%INITIALIZE\_FAVORITE\_PARS%**  
**%INITIALIZE\_FAVORITE\_VARS%**

Example

### Equations

The following tokens can be used to place 20-sim simulation model equations into the C-Code:

**%INITIAL\_EQUATIONS** Equations that should be calculated once for initialization of the  
**%** model  
**%STATIC\_EQUATIONS** Equations that should be calculated once  
**%**  
**%INPUT\_EQUATIONS%** Equations that should be calculated once at the beginning of  
every simulation step  
**%** Equations that calculates the dynamic part of the model,  
**DYNAMIC\_EQUATIONS** calculates the rates  
**%**

**%OUTPUT\_EQUATIONS** Equations that should be calculated once at the end of every simulation step

**%OUTPUT2\_EQUATIONS** Reduced set of equations that should be calculated at the end of every simulation step

**%FINAL\_EQUATIONS%** Equations that should be calculated once for termination of the model

### Inputs/Outputs

To match model inputs and model outputs to for example sensor signals and actuator signals you can use:

**%INPUT\_TO\_VARIABLE\_EQUATIONS%**  
**%VARIABLE\_TO\_OUTPUT\_EQUATIONS%**  
**%ALIAS\_EQUATIONS%**  
**%FAVORITE\_PARS\_EQUATIONS%**  
**%FAVORITE\_VARS\_EQUATIONS%**

Example

### Additional tokens

**%INTEGRATION\_METHOD\_NAME%** A string representing the name of the selected integration method, for now only Euler, RungeKutta4 and Discrete are available.

**%XX\_TIME%** The name of the simulation time variable (combined with %VARPREFIX%)

**%XX\_INITIALIZE%** The name of the variable that indicates the initialization phase (combined with %VARPREFIX%).

**%START\_TIME%** Start time of the simulation (floating point notation).

**%FINISH\_TIME%** Finish time of the simulation (floating point notation).

**%TIME\_STEP\_SIZE%** Step size of the simulation (floating point notation).

**%MODEL\_IS\_DISCRETE** Either TRUE or FALSE, depending if the model is discrete in time or continuous in time.

### Experiment Tokens

Tokens which hold information about the model, experiment, user and system:

**%FILE\_NAME%** The file name of the generated C-Code.

**%MODEL\_FILE%** The complete path and file name of the original 20-sim model.

**%MODEL\_NAME%** The name of the 20-sim model out of which C-Code was generated.

**%SUBMODEL\_NAME%** The name of the 20-sim submodel out of which C-Code was generated.

**%EXPERIMENT\_NAME%** The name of the 20-sim submodel out of which C-Code was generated.

**%GENERATION\_TIME%** The time taken to generate the C-Code.

<b>%GENERATION_DATE%</b>	The experiment name accompanying the 20-sim (sub)model.
<b>%GENERATION_BUILD</b>	The time of C-Code generation.
<b>%</b>	The date of C-Code generation.
<b>%GENERATION_DIR%</b>	The 20-sim version and build number.
<b>%USER_NAME%</b>	The directory where the generated C-Code files are stored.
<b>%COMPANY_NAME%</b>	The user name given in the 20-sim license.
<b>%20SIM_DIR%</b>	The company name given in the 20-sim license.
	The directory where 20-sim is installed.

## 8.7 Time Domain Toolbox

### Time Domain Toolbox

The Time Domain Toolbox contains powerful tools to inspect the behaviour of your model using time domain simulation.

- *Parameter sweep*: Perform a number of simulation runs, while changing model parameters.
- *Optimization*: Optimize a given result by changing parameters.
- *Curve Fitting*: Fit your model to a given result by changing parameters.
- Tolerance Analysis
  - *Sensitivity*: Change parameters by a given percentage and monitor results.
  - *Monte Carlo*: Change parameters statistically and monitor results.
  - *Variation Analysis*: Find the statistical range of parameters to yield a given result.
- *External DLL*: Let the multiple run be controlled by a user-defined function in a DLL.

### Procedure

1. From the **Toolbox** menu select the **Time Domain Toolbox** and then the tool that you want to use.
2. This will open the *Multiple Run Wizard*. Follow the instructions and after all settings have been entered, close the wizard.
3. Select the **Multiple Run** command from the **Simulation** menu to perform the specified analysis.
4. After simulation is completed a special window will open to showing the results. If it is not available, you can always open this window, by selecting the **Multiple Run Results** command of the **View** Menu.

### Multiple Run Wizard

All tools of the Time Domain Toolbox are started use the Multiple Run Wizard. You can open this Wizard directly by selecting the **Multiple Run** command from the **Properties** menu.

## Parameter Sweep

Using the Parameter Sweep option of the *Time Domain Toolbox*, you can perform a predefined number of simulation runs with variation of parameters / initial values.

### Parameters / Initial Values

1. From the **Tools** menu select the **Time Domain Toolbox** and then **Parameter Sweep**.

A window will open, asking you which parameters / initial values should be changed during the multiple simulations:

Name	Type	Minimum	Maximum	Sweep	
Lever\L/v	Parameter	0.1	2	Linear	
Bellows\K/k	Parameter	10	500	Linear	

2. Add the parameters / initial values of your choice:
3. Click the **Next** button.

### Result

A window opens asking you which result (optional) should be shown after the simulations:

Result

Parameter Sweep: Choose the result you would like to monitor (optional).

Result = Function (var1 - var2)

var1  
Variable: Criterium1\output Clear  
Choose Variable

var2  
Variable: Clear  
Value: ☐ 0 Choose Variable

Function  
☒ End Value   
☐ Sum Absolute Value   
☐ Integral Absolute Value (Euler)  
☐ Sum Square Value   
☐ Integral Square Value (Euler)

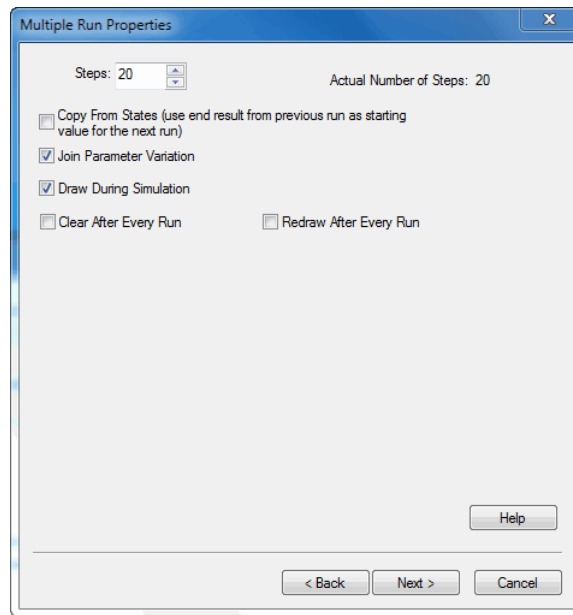
Help

< Back Next > Cancel

4. If you do not want to use a result after simulation, enter nothing here. If you like to present a result after the simulation, enter it here using the various options of the window.
5. Click the **Next** button.

### Run options

A window will open, asking some simulation run options:



You can select the following items:

- **Steps:** Number of simulations runs.
- **Copy from States:** Use the result of the previous simulation runs as the starting value numerical output of the parameter sweep.
- **Join Parameter Variation:** Change all parameters simultaneously.
- **Clear After Every Run:** Clear the simulation plot when a new simulation run starts.
- **Redraw After Every Run:** Update the scaling after every run.

6. Select the desired run options and click the **Next** button.

A window will open with a summary of the chosen options. If you are not satisfied you can use the **Back** button to go to a previous window and change settings.

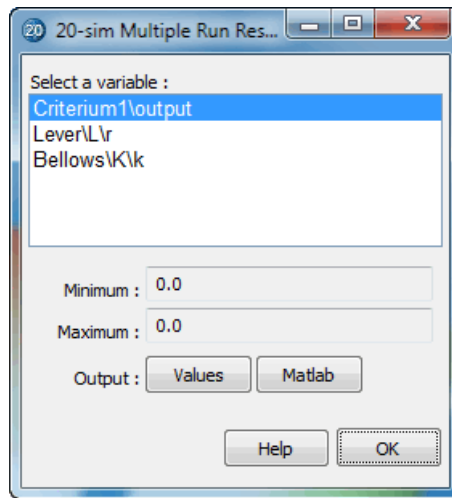
7. Click the **Finish** button to close the **Multiple Run Wizard**.

8. From the **Simulation** menu click the **Multiple Run** command to perform the Parameter Sweep.

### Parameter Sweep Results

After simulation has been done, a Multiple Run Results window will open, showing the minimum and maximum value of the result and chosen parameters:





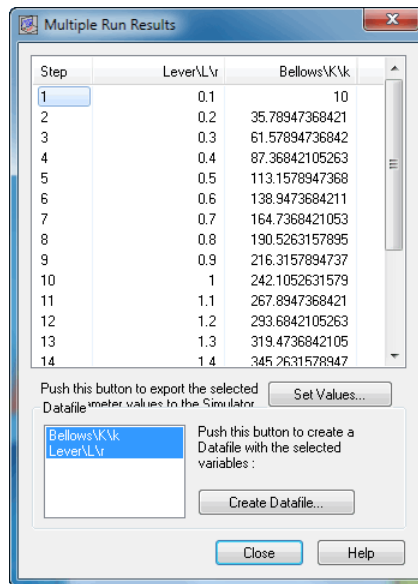
You can select the following items:

- **Values:** Choose this button to open the list that shows the numerical output of the parameter sweep.
- **Matlab:** Export the results to Matlab.
- **OK:** Close the Multiple Run Results Window.

You can always re-open the Multiple Run Results window, by selecting the **Multiple Run Results** command of the **View** Menu.

9. By choosing the Values button, a new window is opened, showing the numerical results of the parameter sweep.

In the **Results** list of this window the subsequent runs are shown and (if available) the value of the chosen result:



You can select the following items:

- **Set Values:** Choose the values of the selected run, as new parameter values of your model.
- **Create Datafile:** Use this button to store the values of the selected variables on file. Use the control-key and shift-key to make multiple selections.

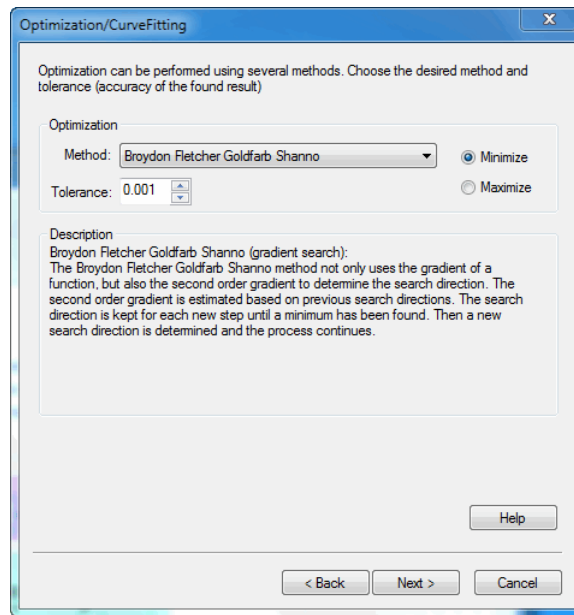
## Optimization

Using the Optimization option of the *Time Domain Toolbox*, you can optimize a given result using variation of parameters / initial values.

### Optimization Method

1. From the **Tools** menu select the **Time Domain Toolbox** and then Optimization.

A window opens asking you which optimization method should used:



2. Select the Optimization method that should be used.
3. Select the Tolerance (accuracy of the found optimum) that should be used and click **Next.**

### Parameters / Initial Values

A window opens asking you which parameters / initial values should be varied during optimization:

Parameters/Initial values

Optimization: Choose the parameters/initial values that may be changed by the optimization method.

Parameter/Initial Values

Name	Type	Minimum	Maximum
control\kp	Parameter	0.1	5
control\tauD (s)	Parameter	0.1	5

Add Add Group Delete

Minimum: 0.1 Maximum: 5

Nominal Value: 2

Help

< Back Next > Cancel

4. Add the parameters / initial values of your choice:
5. Click the **Next** button.

## Result

A window opens asking you which result should optimized:

Result

Optimization: Choose the result that should be optimized by the optimization method.

Result = Function (var1 - var2)

var1

Variable: CostFunction\output Clear

Choose Variable

var2

Variable: Clear

Value: ☐ 0 Choose Variable

Function

☒ End Value ☐ Sum Absolute Value ☐ Integral Absolute Value (Euler)

☐ Sum Square Value ☐ Integral Square Value (Euler)

Help

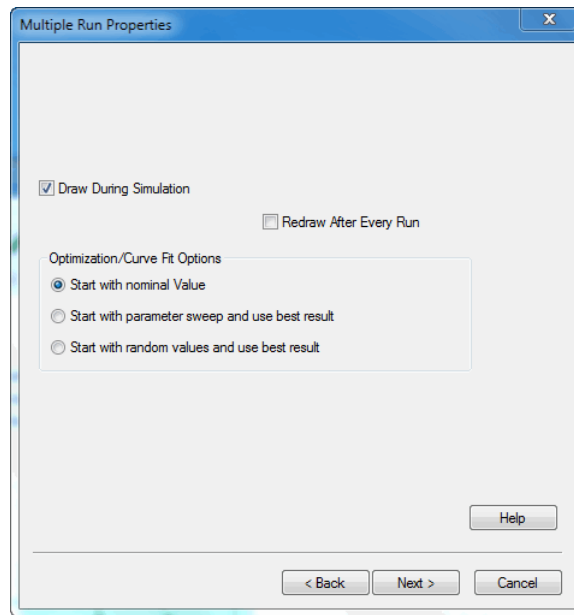
< Back Next > Cancel

6. Enter the result here using the various options of the window.

7. Click the **Next** button.

### Run options

A window opens asking some simulation run options:



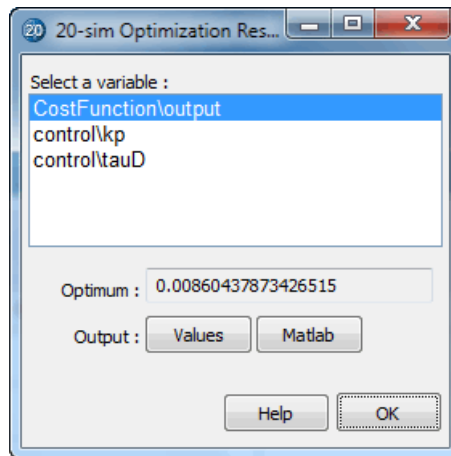
8. Select the desired run options and click the **Next** button.

A window opens with a summary of the chosen options. If you are not satisfied you can use the **Back** button to go to a previous window and change settings.

9. Click the **Finish** button to close the **Multiple Run** Wizard.
10. From the **Simulation** menu click the **Multiple Run** command to perform the Optimization.

### Optimization Results

After simulation has been done, an Optimization Results window will open, showing the optimum value of the result and corresponding parameters:



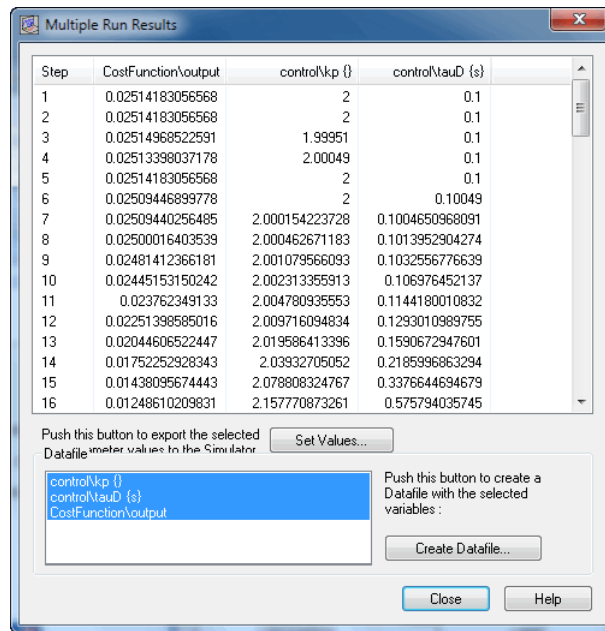
You can select the following items:

- **Values:** Choose this button to open the list that shows the numerical output of the optimization runs.
- **Matlab:** Export the results to Matlab.
- **OK:** Close the Optimization Results Window.

You can always re-open the Multiple Run Results window, by selecting the **Multiple Run Results** command of the **View** Menu.

11. By choosing the **Values** button, a new window is opened, showing the numerical results of the parameter sweep.

In the **Results list** of this window the subsequent runs are shown and (if available) the value of the chosen result:



You can select the following items:

- **Set Values:** Choose the values of the selected run, as new parameter values of your model.
- **Create Datafile:** Use this button to store the values of the selected variables on file. Use the control-key and shift-key to make multiple selections.

## Optimization Methods

In the Multiple Run Wizard you have to specify a result which will be optimized. The result is a function of model variables and the simulation run:

$$result = f(i, v1, v2, \dots)$$

with  $i$  the number of the simulation run. You also have to specify the parameters that should be varied to find the optimum result. We can group these parameters in a parameter vector:

$$parameter\ vector = p(i)$$

with again  $i$  the number of the simulation run. All methods in 20-sim for finding an optimum of the result use the same iterative process:

1. The initial parameter vector is determined, e.g.  $p(1)$  and the corresponding function value  $f(1)$ .
2. A search direction  $r(1)$  and a stepsize  $s(1)$  are determined.
3. Perform a new simulation run to find the parameter vector  $p(2) = p(1) + s(1)*r(1)$ .
4. Calculate  $f(2)$ .
5. When the  $f(2)$  is smaller than  $f(1)$  and the difference between the two is smaller than a given tolerance, stop the process. The optimum has been found.



6. When the  $f(2)$  is smaller than  $f(1)$  and the difference between the two is larger than a given tolerance, proceed the process at step 2
7. Otherwise a new stepsize and/or a new search direction are determined and the process is proceeded at step 3.

The choice of the stepsize is of importance for the speed and accuracy of the search process. A small stepsize will make the optimization process last very long. A large stepsize will make it less accurate. Most methods will therefore use a variable stepsize.

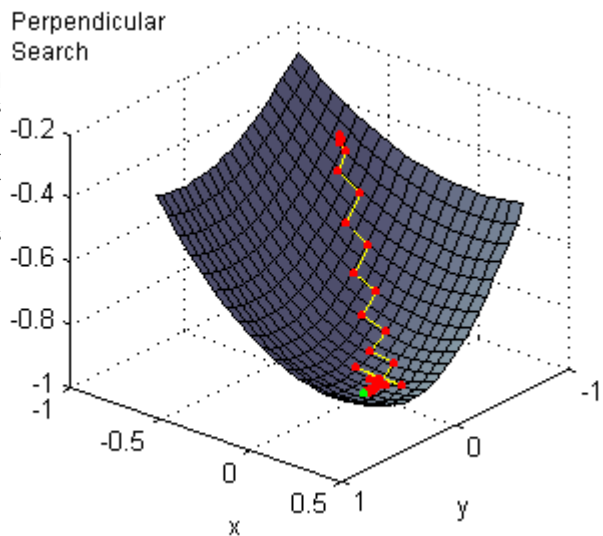
Of equal importance is the proper choice of the search direction. Methods for finding the search direction, can be divided in two groups: direct search methods and gradient search methods. The gradient of a function, is its slope at a certain point. Gradient search methods use this slope to find the optimal direction of search.

## Methods

The optimization methods that are supported in 20-sim will now be explained. The pictures at the right visualize the methods with two varying parameters  $x$  (horizontal) and  $y$  (horizontal) and the corresponding result (vertical).

### 1. Perpendicular Search (direct search)

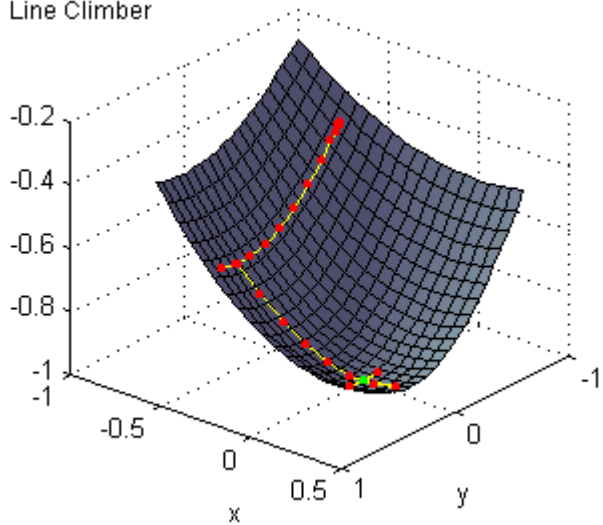
The perpendicular search method uses a search direction that is always perpendicular to the parameter axis. This means that only one parameter at a time is varied. All other parameters keep the same value. After one step, a next parameter is taken and the process continues.



## 2. Line Climber (direct search)

The line climber method uses a search direction that is always perpendicular to the parameter axis. This means that only one parameter at a time is varied. All other parameters keep the same value. After a minimum has been found the next parameter is varied and the process continues.

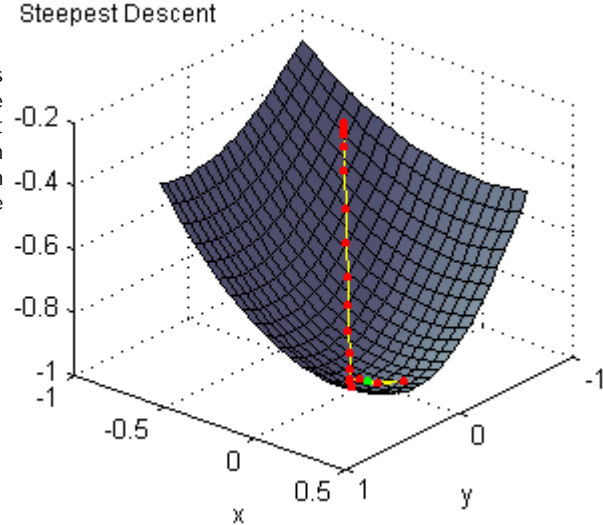
Line Climber



## 3. Steepest Descent (gradient search)

The steepest descent method starts its search in the direction of the steepest slope. This direction is kept for each new step until a minimum has been found. Then a new search direction is determined and the process continues.

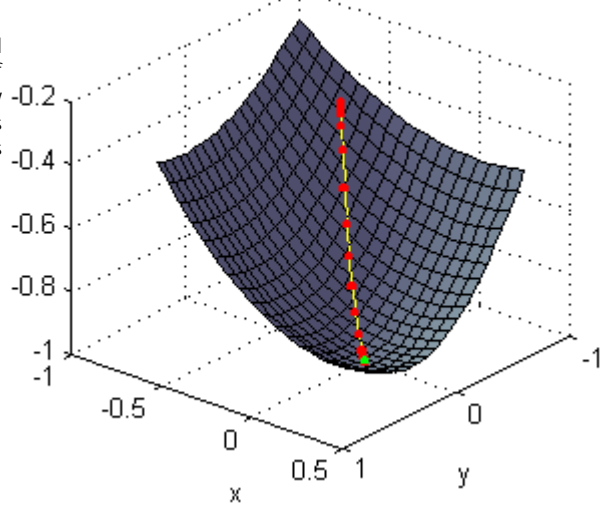
Steepest Descent



#### 4. Continuous Descent (gradient search)

The continuous descent method starts its search in the direction of the steepest slope. After each new step a new search direction is determined and the process continues.

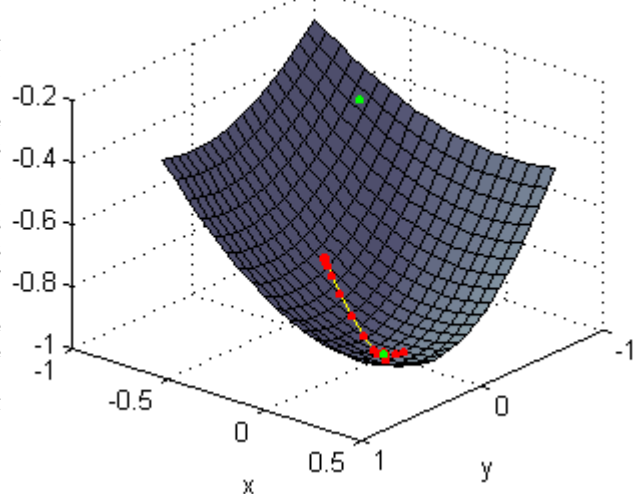
Continuous Descent



#### 5. Newton Raphson (gradient search)

The Newton Raphson method not only uses the gradient of a function, but also the second order gradient to determine the search direction. This direction is kept for each new step until a minimum has been found. Then a new search direction is determined and the process continues. Note: The method only converges for a positive second order gradient, i.e. near the minimum. This is shown in the figure to the right. For  $x = -0.7$  and  $y = -0.9$  the method does not converge. For  $x = -0.5$  and  $y = -0.3$  the method does converge.

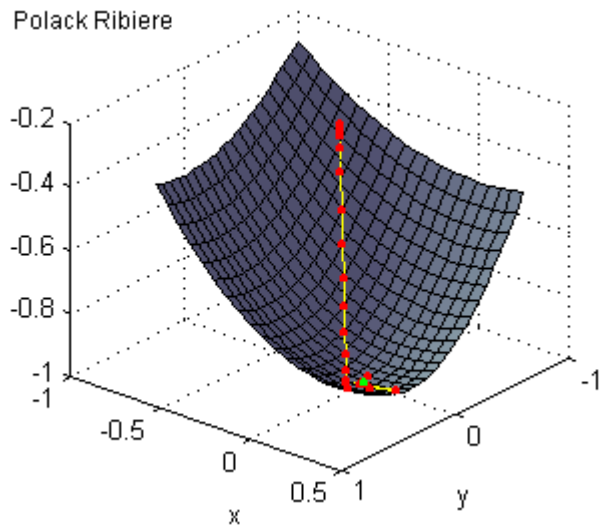
Newton Raphson



## 6. Polack Ribiere (gradient search)

The Polack Ribiere method not only uses the gradient of a function, but also the second order gradient to determine the search direction. The second order gradient is estimated based on previous search directions. The search direction is kept for each new step until a minimum has been found. Then a new search direction is determined and the process continues.

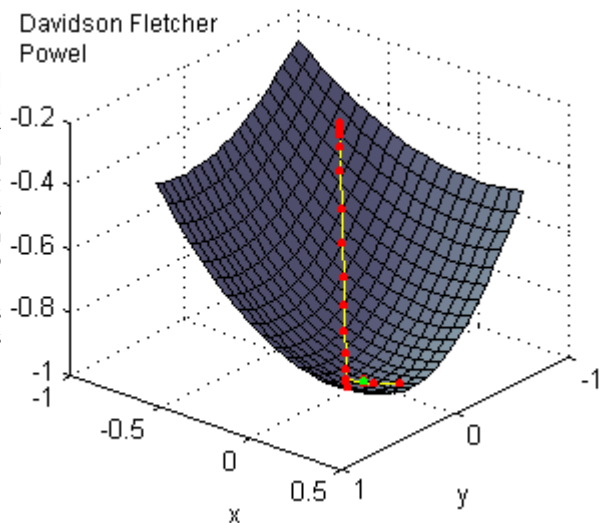
Polack Ribiere



## 7. Davidson Fletcher Powell (gradient search)

The Davidson Fletcher Powell method not only uses the gradient of a function, but also the second order gradient to determine the search direction. The second order gradient is estimated based on previous search directions. The search direction is kept for each new step until a minimum has been found. Then a new search direction is determined and the process continues.

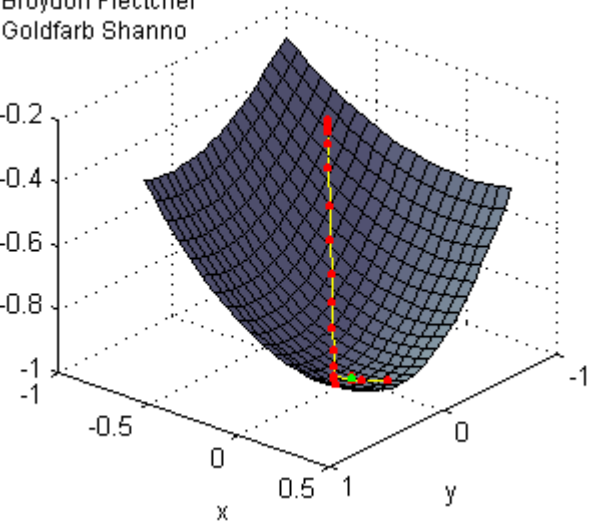
Davidson Fletcher Powell



**8. Broydon Fletcher Goldfarb Shanno (gradient search)**

The Broydon Fletcher Goldfarb Shanno method not only uses the gradient of a function, but also the second order gradient to determine the search direction. The second order gradient is estimated based on previous search directions. The search direction is kept for each new step until a minimum has been found. Then a new search direction is determined and the process continues.

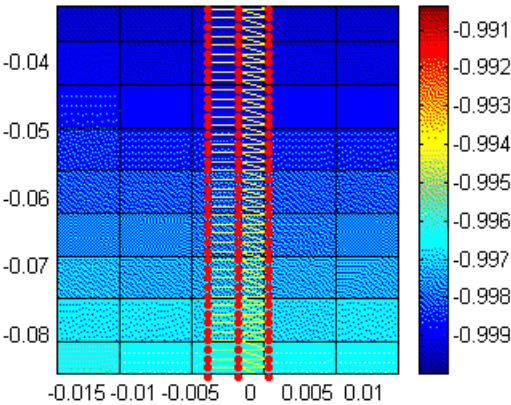
Broydon Fletcher  
Goldfarb Shanno



**What method should be used?**

There is no general answer to this question. Some remarks can however be made:

- 1. Gradient search methods (3 to 8), need more steps (note that each step means a simulation run) to determine the gradient. The Newton Raphson methods needs the most steps, because this method also needs additional steps for the determination of the second order gradient.
- 2. When the direction of the slope is not exactly the same as the search direction, direct search methods (1 and 2) may start to bounce, i.e. continuously change direction while making little progress. this is shown in the figure below:



Users are therefore advised to use methods 1 and 2 only for optimizations with one parameter, and use the methods 7 and 8 for optimizations with more parameters. Use the other methods for checking the results or educational purposes.

More information on these methods can be found in:

Bazaraa, M.S., Sherali, H.D., Shetty C.M. (1990), *Nonlinear Programming, Theory and Algorithms*, John Wiley & Sons Inc. New York, ISBN 0-471-59973-5.

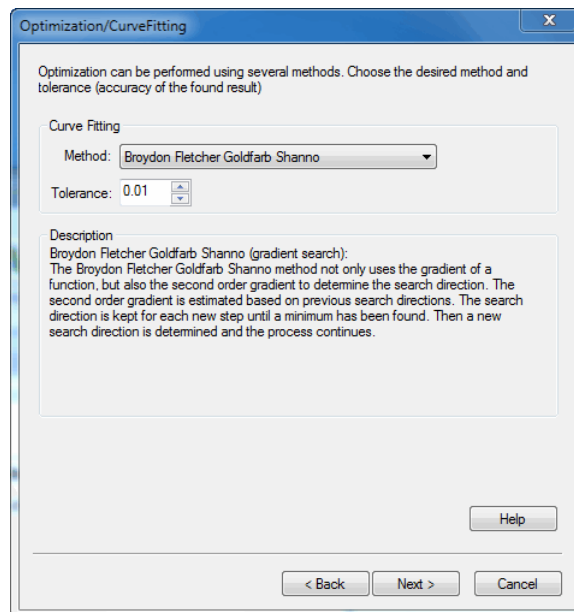
## Curve Fitting

Using the Parameter Sweep option of the *Time Domain Toolbox*, you can fit your model to a given result using variation of parameters / initial values.

### Optimization Method

1. From the **Tools** menu select the **Time Domain Toolbox** and then **Curve Fitting**.

A window opens asking you which optimization method should used for curve fitting:



2. Select the Optimization method that should be used.
3. Select the Tolerance (accuracy of the found fit) that should be used and click **Next**.

### Parameters / Initial Values

A window opens asking you which parameters / initial values should be varied during curve fitting:

Parameters/Initial values

Curve Fitting: Choose the parameters/initial values that can be changed to find an optimal fit.

Parameter/Initial Values

Name	Type	Minimum	Maximum
Model\omega	Parameter	0.1	100
Model\zeta	Parameter	0.1	10

Add Add Group Delete

Minimum: 0.1 Maximum: 100

Nominal Value: 2

Help

< Back Next > Cancel

4. Add the parameters / initial values of your choice:

5. Click the **Next** button.

### Result

A window opens asking you which result should be minimized to fit your model (variable 1) to a given result (variable 2):

Result

Curve Fitting: Choose the function that should be minimized to fit var1 to var2.

Result = Function (var1 - var2)

var1

Variable: ModelResponse\plot Clear

Choose Variable

var2

Variable: PlantResponse\plot Clear

Value: 0 Choose Variable

Function

☐ End Value
 ☐ Sum Absolute Value
 ☒ Integral Absolute Value (Euler)
 ☐ Sum Square Value
 ☐ Integral Square Value (Euler)

Help

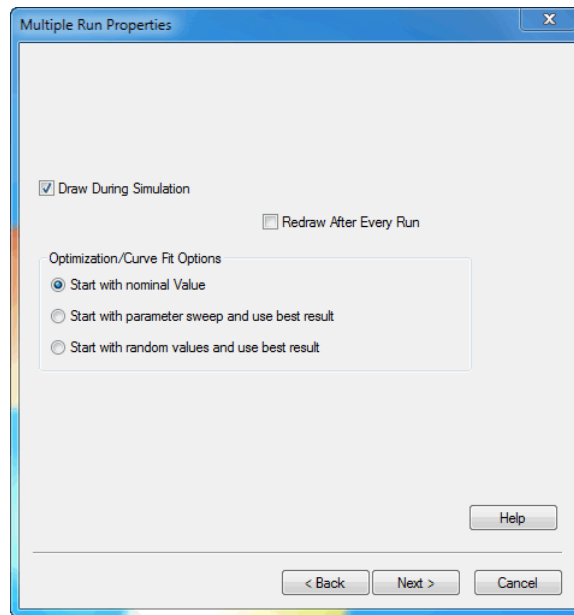
< Back
Next >
Cancel

6. Enter the result here using the various options of the window.
7. Click the **Next** button.

### Run options

A window opens asking some simulation run options:





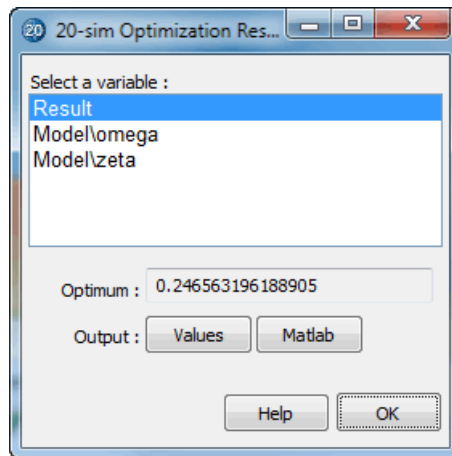
8. Select the desired run options and click the **Next** button.

A window opens with a summary of the chosen options. If you are not satisfied you can use the Back button to go to a previous window and change settings.

9. Click the **Finish** button to close the **Multiple Run Wizard**.
10. From the **Simulation** menu click the **Multiple Run** command to perform the Curve Fitting.

### Optimization Results

After simulation has been done, the Optimization Results window will open, showing the minimum value of the result and corresponding parameters:



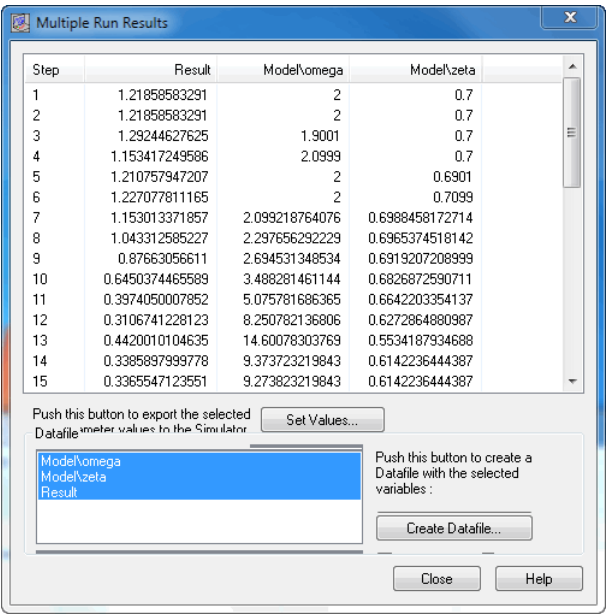
You can select the following items:

- **Values:** Choose this button to open the list that shows the numerical output of the curve fitting runs.
- **Matlab:** Export the results to Matlab.
- **OK:** Close the Optimization Results Window.

You can always re-open the **Multiple Run Results** window, by selecting the **Multiple Run Results** command of the **View** Menu.

11. By choosing the **Values** button, a new window is opened, showing the numerical results of the parameter sweep.

In the **Results list** of this window the subsequent runs are shown and the value of the chosen result:



You can select the following items:

- **Set Values:** Choose the values of the selected run, as new parameter values of your model.
- **Create Datafile:** Use this button to store the values of the selected variables on file. Use the control-key and shift-key to make multiple selections.

**Sensitivity Analysis**

Using the Tolerance Analysis option of the Multiple Run Wizard, you can analyze the effects of variation of parameters / initial values on the performance of your model. Three methods of Tolerance analysis are supported in the Multiple Run Wizard. One of these methods is Sensitivity analysis.

Sensitivity analysis starts with a simulation run with nominal parameter values. After the run a given result is monitored (*r*). Then, one by one, each parameter (*pi*) is changed with a given percentage (*to pi + dpi*) and a simulation run is performed. After the simulation run the changed result is monitored (*r + dri*). After all the runs, the results are displayed as sensitivities, where sensitivity is defined as the change in result divided by the change in parameter:

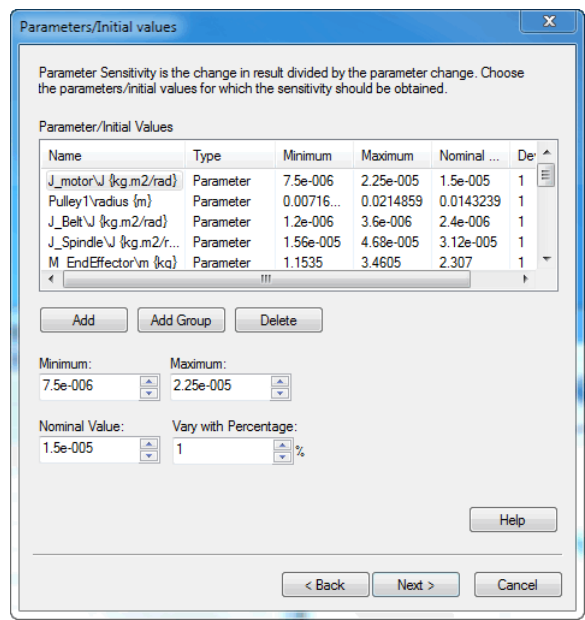
$$Si = dri / dpi$$

A large sensitivity means that the result is highly dependant of the parameter value. This can be used for optimization (change the parameter value) or design (change the design to make it less dependant of the parameter).

**Parameters / Initial Values**

1. From the **Tools** menu select the **Time Domain Toolbox** and then **Sensitivity Analysis**.

A window opens asking you which parameters / initial values should be changed for the Sensitivity analysis:



- 3. Add the parameters / initial values of your choice:
- 4. Click the **Next** button.

**Result**

A window opens asking you which result should be monitored for the sensitivity:

Result

Sensitivity Analysis: Choose the result that should be monitored.

Result = Function (var1 - var2)

var1

Variable:

var2

Variable:

Value: ☒ 0

Function

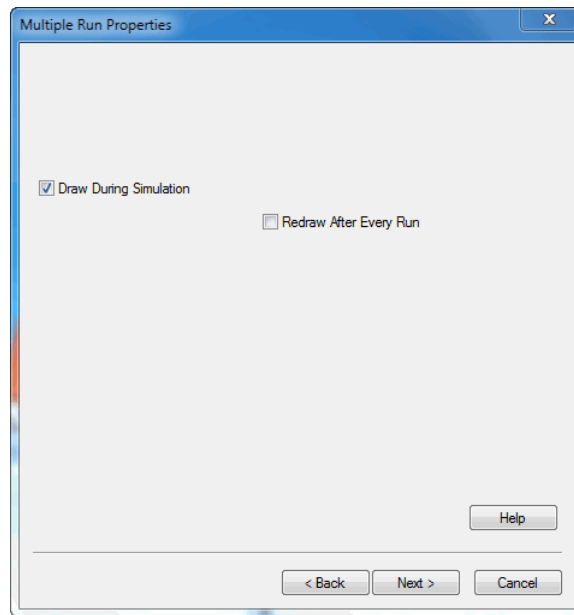
☒ End Value ☐ Sum Absolute Value ☐ Integral Absolute Value (Euler)

☐ Sum Square Value ☐ Integral Square Value (Euler)

5. Enter the result here using the various options of the window.
6. Click the **Next** button.

### Run options

A window opens asking some simulation run options:



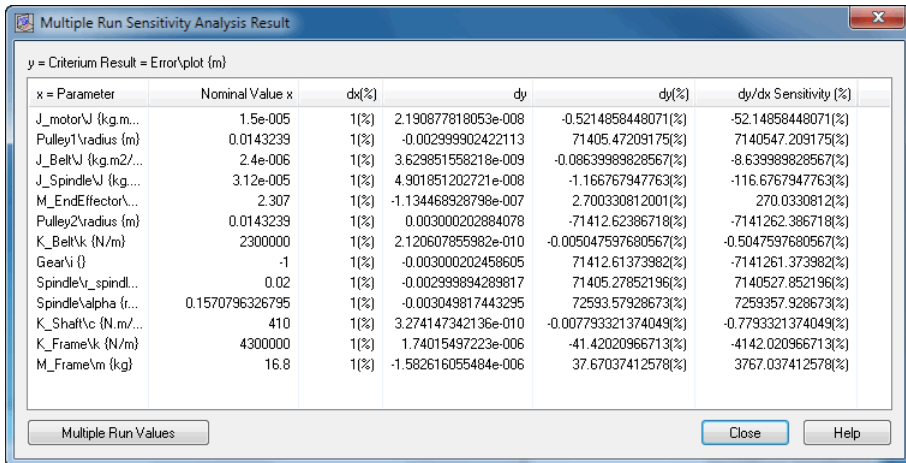
7. Select the desired run options and click the **Next** button.

A window opens with a summary of the chosen options. If you are not satisfied you can use the **Back** button to go to a previous window and change settings.

8. Click the **Finish** button to close the Multiple Run Wizard.
9. From the **Simulation** menu click the **Multiple Run** command to perform the Sensitivity Analysis.

### Sensitivity Analysis Results

After simulation has been done, a Sensitivity Analysis Results window will open, showing the sensitivities:



y = Criterion Result = Error\plot (m)

x = Parameter	Nominal Value x	dx(%)	dy	dy(%)	dy/dx Sensitivity (%)
J_motor\J {kg.m...}	1.5e-005	1(%)	2.190877818053e-008	-0.5214858448071(%)	-52.14858448071(%)
Pulley1\radius (m)	0.0143239	1(%)	-0.002999902422113	71405.47209175(%)	7140547.209175(%)
J_Belt\J {kg.m2/...	2.4e-006	1(%)	3.629851558218e-009	-0.08639989828567(%)	-8.639989828567(%)
J_Spindle\J {kg...	3.12e-005	1(%)	4.901851202721e-008	-1.166767947763(%)	-116.6767947763(%)
M_EndEffector\...	2.307	1(%)	-1.134468928798e-007	2.700330812001(%)	270.0330812(%)
Pulley2\radius (m)	0.0143239	1(%)	0.003000202884078	-71412.62386718(%)	-7141262.386718(%)
K_Belt\k {N/m}	2300000	1(%)	2.120607855982e-010	-0.005047597680567(%)	-0.5047597680567(%)
Gear\i {}	-1	1(%)	-0.003000202458605	71412.61373982(%)	-7141261.373982(%)
Spindle\spindl...	0.02	1(%)	-0.002999894289817	71405.27852196(%)	7140527.852196(%)
Spindle\alpha (r...	0.1570796326795	1(%)	-0.003049817443295	72593.57928673(%)	7259357.928673(%)
K_Shaf\c {N.m/...	410	1(%)	3.274147342136e-010	-0.007793321374049(%)	-0.7793321374049(%)
K_Frame\k {N/m}	4300000	1(%)	1.74015497223e-006	-41.42020966713(%)	-4142.020966713(%)
M_Frame\m (kg)	16.8	1(%)	-1.582616055484e-006	37.67037412578(%)	3767.037412578(%)

Multiple Run Values Close Help

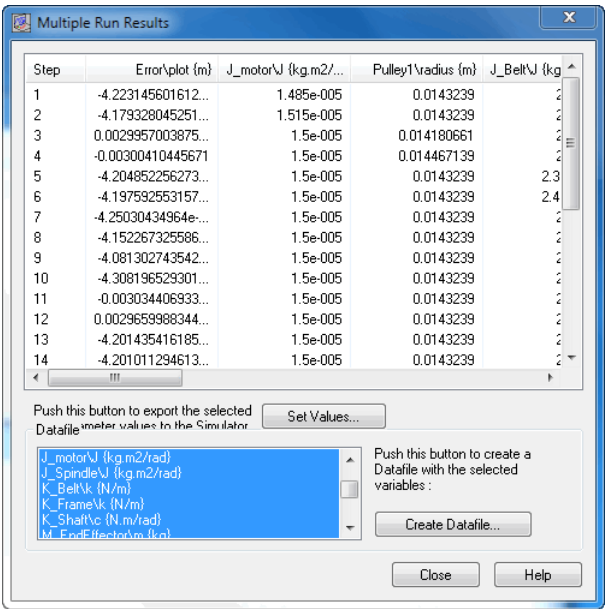
You can select the following items:

- **Multiple Run Values:** Choose this button to open the list that shows the output of the various runs performed during the sensitivity analysis.
- **Close:** Close the Sensitivity Analysis Results Window.

You can always re-open the *Multiple Run Results* window, by selecting the *Multiple Run Results* command of the View Menu.

- By choosing the **Multiple Run Values** button, a new window is opened, showing output of the various runs performed during the sensitivity analysis:

In the *Results list* of this window the subsequent runs are shown and the corresponding sensitivities.



You can select the following items:

- **Set Values:** Choose the values of the selected run, as new parameter values of your model.
- **Create Datafile:** Use this button to store the values of the selected variables on file. Use the control-key and shift-key to make multiple selections.

Monte Carlo Analysis

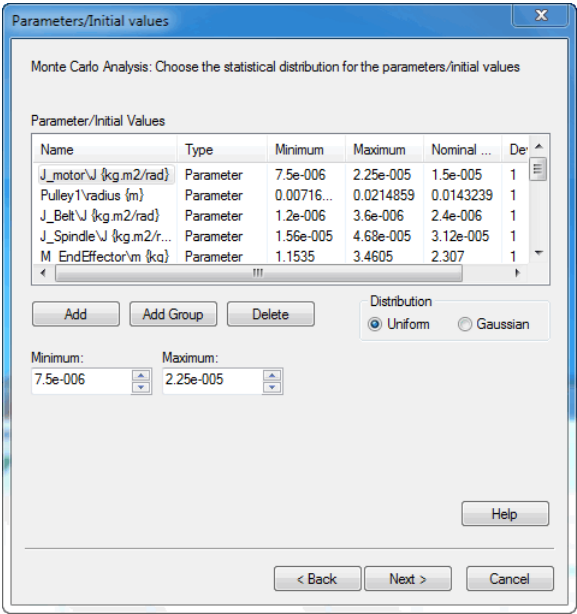
Using the Tolerance Analysis option of the Multiple Run Wizard, you can analyze the effects of variation of parameters / initial values on the performance of your model. Three methods of Tolerance analysis are supported in the Multiple Run Wizard. One of these methods is Monte Carlo Analysis. Using Monte Carlo analysis, you can perform a predefined number of simulation runs with variation of parameter values according to a predefined distribution function.

Parameters / Initial Values

1. From the **Tools** menu select the **Time Domain Toolbox** and then **Monte Carlo Analysis**.

A window opens asking you which parameters / initial values should be varied for the Monte Carlo analysis:





- 2. Add the parameters / initial values of your choice:
- 3. Click the **Next** button.

**Result**

A window opens asking you which result should be monitored during the Monte Carlo Analysis:

Result

Monte Carlo Tolerance Analysis: Choose the result that should be monitored.

Result = Function (var1 - var2)

var1  
Variable: Error\plot Clear  
Choose Variable

var2  
Variable: Clear  
Value: 0 Choose Variable

Function  
☒ End Value   
 ☐ Sum Absolute Value   
 ☐ Integral Absolute Value (Euler)  
☐ Sum Square Value   
 ☐ Integral Square Value (Euler)

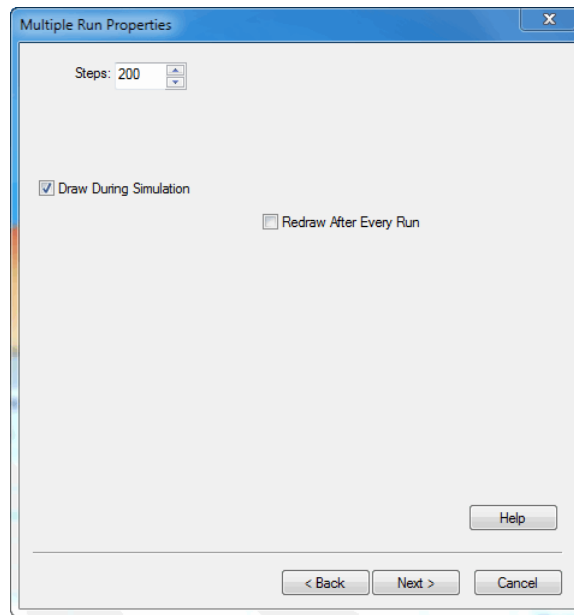
Help

< Back Next > Cancel

4. Enter the result here using the various options of the window.
5. Click the **Next** button.

### Run options

A window opens asking some simulation run options:



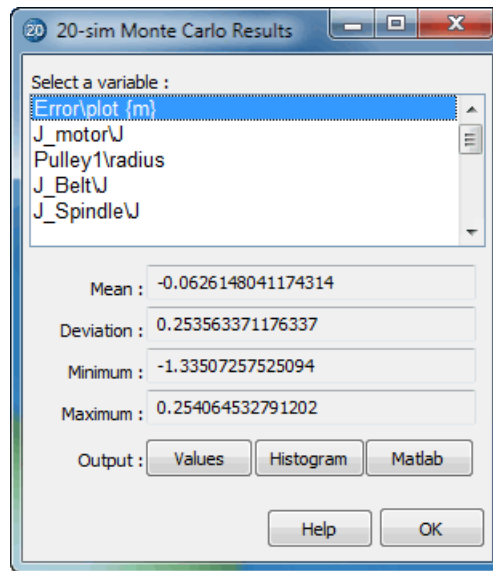
6. Select the desired run options and click the **Next** button.

A window opens with a summary of the chosen options. If you are not satisfied you can use the **Back** button to go to a previous window and change settings.

7. Click the **Finish** button to close the Multiple Run Wizard.
8. From the **Simulation menu** click the **Multiple Run** command to perform the Monte Carlo Analysis.

### Monte Carlo Analysis Results

After simulation has been done, a Monte Carlo Analysis Results window will open, showing the results:

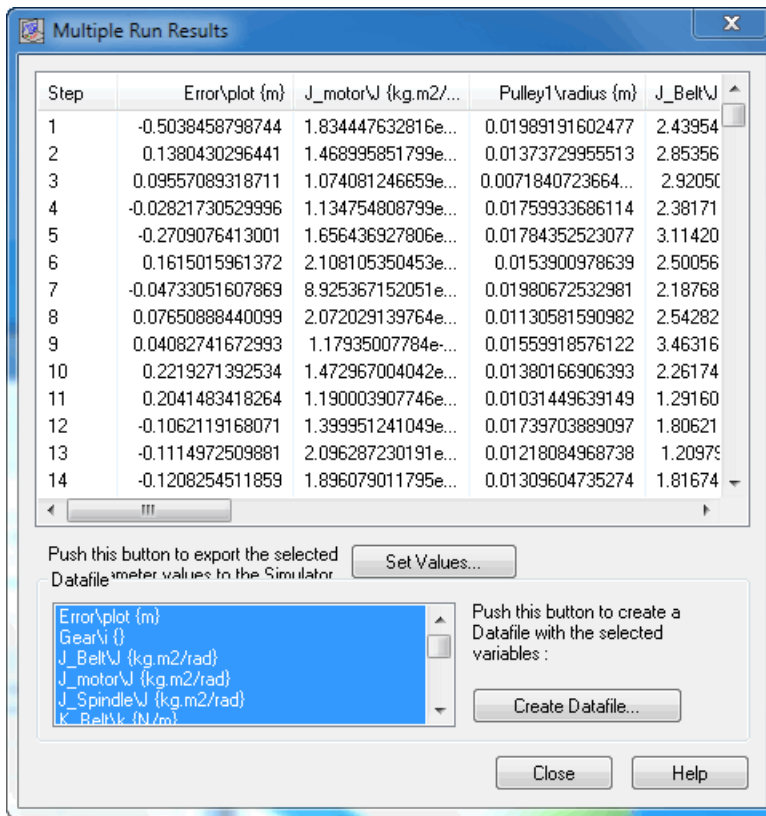


You can select the following items:

- **Values:** Choose this button to open the list that shows the output of the various runs performed during the Monte Carlo analysis.
- **Histogram:** Choose this button to open a histogram of the selected item.
- **Matlab:** Export the results to Matlab.
- **OK:** Close the Multiple Run Results Window.

You can always re-open the **Multiple Run Results** window, by selecting the **Multiple Run Results** command of the **View** Menu.

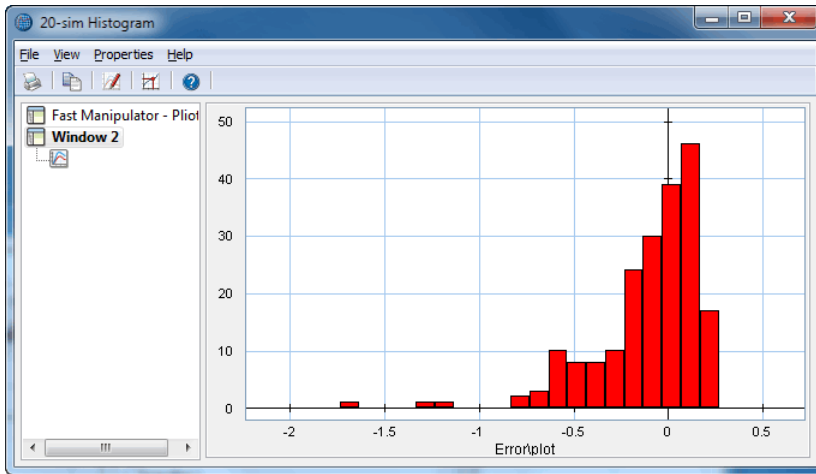
9. By choosing the **Multiple Run Values** button, a new window is opened, showing output of the various runs performed during the Monte Carlo analysis.



You can select the following items:

- **Set Values:** Choose the values of the selected run, as new parameter values of your model.
- **Create Datafile:** Use this button to store the values of the selected variables on file. Use the control-key and shift-key to make multiple selections.

By choosing the **Histogram** button, a new window is opened, showing distribution of the result variable:



## Variation Analysis

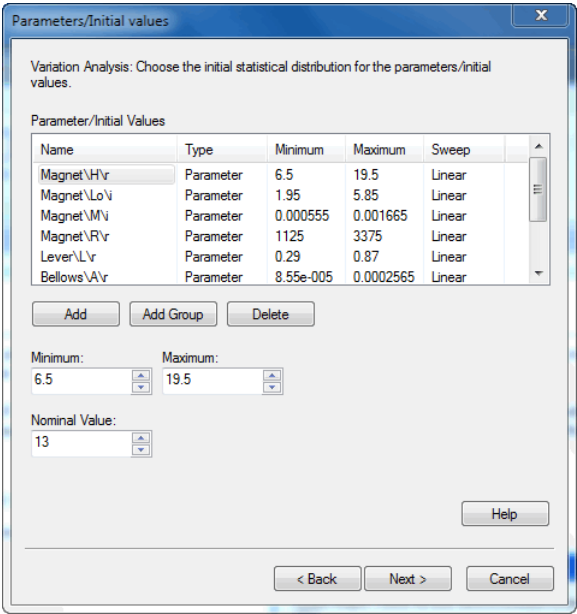
Using the Tolerance Analysis option of the Multiple Run Wizard, you can analyze the effects of variation of parameters / initial values on the performance of your model. Three methods of Tolerance analysis are supported in the Multiple Run Wizard. One of these methods is Variation Analysis.

Using Variation analysis, you can perform a predefined number of simulation runs with variation of parameter values according to a predefined distribution function. During the runs a given result is monitored. After the runs the statistical range of the result is presented. You can restrict the parameter distributions to get the result between desired bounds.

### Parameters / Initial Values

1. From the **Tools** menu select the **Time Domain Toolbox** and then **Variation Analysis**.

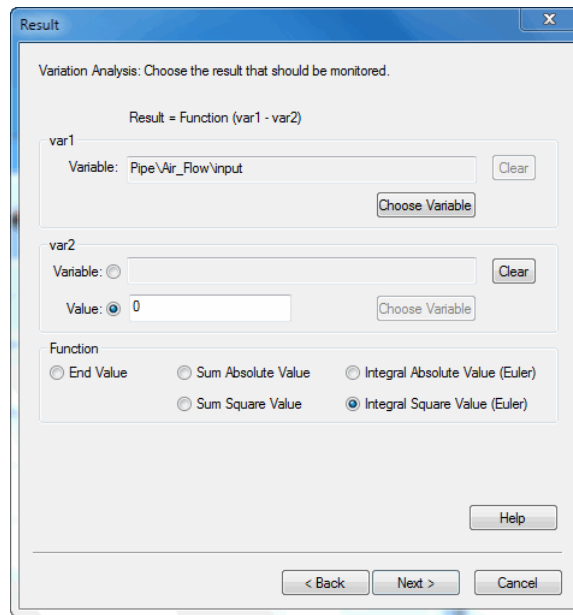
A window opens asking you which parameters / initial values should be varied for the Variation analysis:



- 2. Add the parameters / initial values of your choice:
- 3. Click the **Next** button.

**Result**

A window opens asking you which result should be monitored during the Variation Analysis:

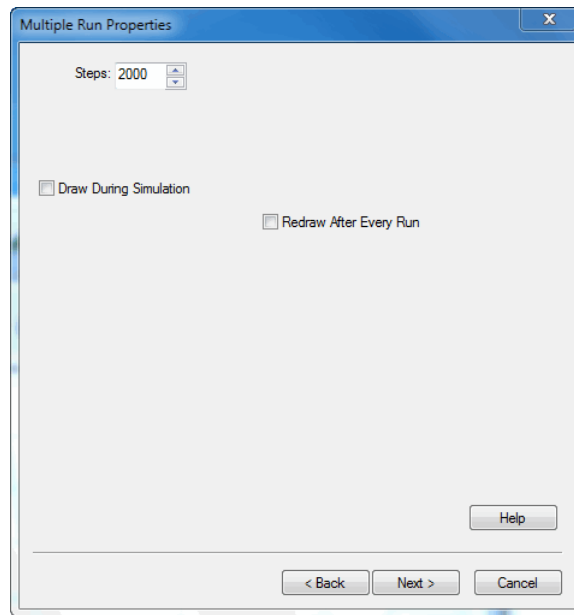


4. Enter the result here using the various options of the window.
5. Click the **Next** button.

### Run options

A window opens asking some simulation run options:





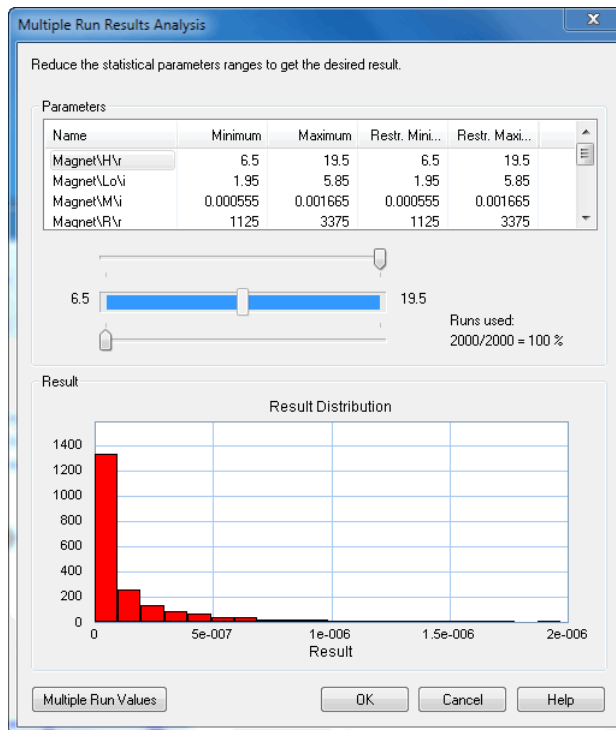
6. Select the desired run options and click the **Next** button.

A window opens with a summary of the chosen options. If you are not satisfied you can use the **Back** button to go to a previous window and change settings.

7. Click the **Finish** button to close the **Multiple Run Wizard**.
8. From the **Simulation** menu click the **Multiple Run command** to perform the Variation Analysis.

### Variation Analysis Results

After simulation has been done, a Variation Analysis Results window will open, showing the results. A histogram shows the distribution of the result. Using the slider bar you can see how restraining the distribution of the parameters effects the distribution of the result.

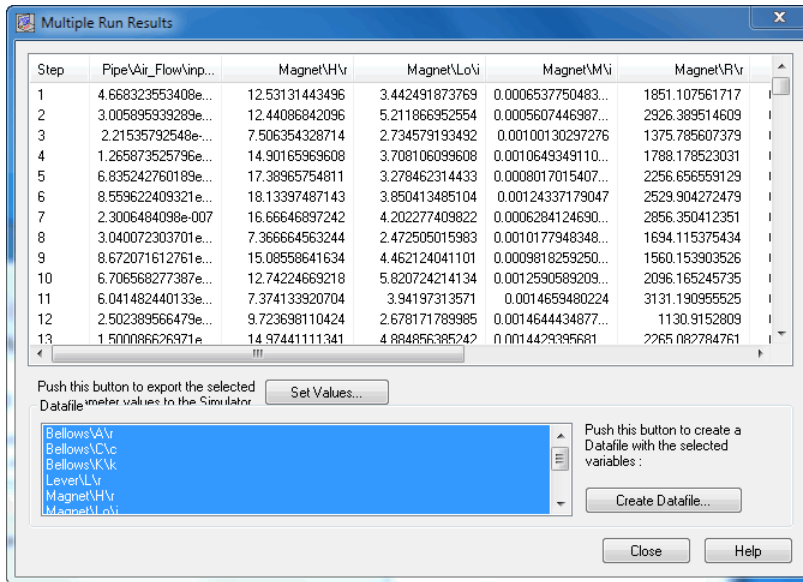


You can select the following items:

- **Slider Bar**: Select a parameter and restrict its distribution with the slider bar. You will see the histogram showing the result change.
- **Multiple Run Values**: Choose this button to open the list that shows the output of the various runs performed during the Variation Analysis.
- **OK**: Close the Multiple Run Results Window.

You can always re-open the Multiple Run Results window, by selecting the **Multiple Run Results** command of the **View** Menu.

9. By choosing the **Multiple Run Values** button, a new window is opened, showing output of the various runs performed during the Variation analysis:



You can select the following items:

- **Set Values:** Choose the values of the selected run, as new parameter values of your model.
- **Create Datafile:** Use this button to store the values of the selected variables on file. Use the control-key and shift-key to make multiple selections.

## External DLL

You can analyze the effects of variation of parameters / initial values using your own method with the use of an external DLL-function. Ask Controllab Products for details.

## Cost Function

In the Multiple Run Wizard, the Result window allows you to define a result (the *Cost Function*) that will be used during simulations (Optimization, Curve Fitting) and displayed after the simulations runs (Parameter sweep, Optimization, Curve Fitting, Sensitivity, Monte Carlo, Variation Analysis, External DLL).

The result can be a function of one or two variables. Instead of the second variable an (offset) value can be entered.

### Items

- **Choose Variable:** Select this button to select a model variable
- **Clear:** Use this button the remove a chosen model variable.
- **Function:**
  - **End value:** The value at the end of the simulation run.
  - **Sum Absolute Value:** The sum of all absolute values during a simulation run.
  - **Sum Square Value:** The sum of all values squared during a simulation run.
  - **Integral Absolute Value:** The integral of all absolute values during a simulation run (uses Euler integration).
  - **Integral Square Value:** The integral of all values squared during a simulation run (uses Euler integration).

### User Defined Cost Function

You can easily use your own *Cost Function* for the result variable:

1. Create your own cost function in the model.
2. Use the **Choose** button to select as var1 the output of your function.
3. Set *var2* to a zero value.

4. Choose **End Value** to prevent further operations on your function.

## 9 Library

### 9.1 Bond Graph

#### Bond Graph Models

Bond graphs are a network-like description of physical systems in terms of ideal physical processes. With the bond graph method we split up the system characteristics into an (imaginary) set of separate elements. Each element describes an idealized physical process. To facilitate drawing of bond graphs, the common elements are denoted by special symbols. This library contains all kind of bond graph elements. If you want to know more about modeling with bond graphs, please have a look at the modeling tutorial.

The standard library contains single dimensional bond graph elements. The 2d Library contains elements with multi-bonds of size 2 and the 3d library contains elements with multi-bonds of size 3.

#### C

##### Library

Bond Graph

##### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams, Bond Graphs.

##### Description

This model represents a power continuous storage element. The element has a preferred effort out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred flow out causality. The constitutive equations then contain a derivation.

effort out causality (preferred):

```
state = int(p.f) + state(0);
p.e = state/c;
output = state;
```

flow out causality:

```
state = c*p.e;
p.f = d state / dt;
output = state;
```

##### Interface

##### Ports

p

##### Description

Input port of the storage element.

##### Causality

preferred effort out

A flow out causality results in a derivative constitutive equation.

##### Outputs

output                      The output signal is equal to the state.

## Parameters

c The storage element constant.

### Initial Values

state(0)	The initial value of the storage element.
----------	---

**CC**

## Library

## Bond Graph

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model represents a two port C-element. Normally the equation of a two port C-element is written in vector notation as:

$$p.e = (1/C)*p.f$$

When the C matrix is singular simulation will not be possible. Therefore the element is described in a safer notation as:

$$p.e = A * p.f, \text{ with } A = (1/C);$$

Both ports have a preferred effort out causality:

```
state1 = int (p1.f);
state2 = int (p2.f);
p1.e = a11*state1 + a12*state2;
p2.e = a21*state1 + a22*state2;
```

## Interface

Ports	Description
p1, p2	Input ports of the storage element.
<b>Causality</b>	
preferred effort out p1	A flow out causality results in a derivative constitutive equation.
preferred effort out p2	
<b>Outputs</b>	
state1	
state2	
<b>Parameters</b>	
a11, a12, a21, a22	The storage element constants.

**Initial Values**

state1\_initial                      The initial values of the storage element.  
 state2\_initial

**EffortSensor****Library**

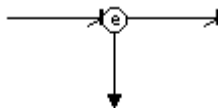
System , Bond Graph

**Use**

**Domains:** Continuous. **Size:** [n,m]. **Kind:** Bond Graphs.

**Description**

This model can be inserted in any bond to yield the effort of that bond as an output signal.



To ensure success, use drag and drop to place the sensor exactly on top in the middle of the bond. As a result the model will be automatically connected.

**Interface****Ports**

p1, p2                      Input and output port of the effort sensor.

**Outputs**

effort                      Effort of the bond.

**EnergySensor****Library**

System , Bond Graph

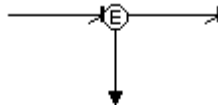
**Use**

**Domains:** Continuous. **Size:** [n,m]. **Kind:** Bond Graphs.

**Description**

This model can be inserted in any bond to yield the energy that is carried through that bond as an output signal.





To ensure success, use drag and drop to place the sensor exactly on top in the middle of the bond. As a result the model will be automatically connected.

### Interface

#### Ports

p1, p2 Input and output port of the energy sensor.

#### Outputs

E Energy carried through the bond.

## FlowSensor

### Library

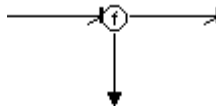
System , Bond Graph

### Use

**Domains:** Continuous. **Size:** [n,m]. **Kind:** Bond Graphs.

### Description

This model can be inserted in any bond to yield the flow of that bond as an output signal.



To ensure success, use drag and drop to place the sensor exactly on top in the middle of the bond. As a result the model will be automatically connected.

### Interface

#### Ports

p1, p2 Input and output port of the flow sensor.

#### Outputs

flow Flow of the bond.

## GY

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal gyrator, a power continuous relation between the effort of one port and the flow of the other port and vice-versa. The model can have both ports with an effort out causality or both ports with a flow out causality:

effort out causality:

$$\begin{aligned}p1.e &= r * p2.f; \\p2.e &= r * p1.f;\end{aligned}$$

flow out causality:

$$\begin{aligned}p1.f &= 1/r * p2.e; \\p2.f &= 1/r * p1.e;\end{aligned}$$

### Interface

#### Ports

p1, p2

#### Description

Input and output port of the gyrator.

#### Causality

p1 equal p2

The causality of both ports must be equal.

#### Parameters

r

Gyration ratio.

## I

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model represents a power continuous storage element. The element has a preferred flow out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred effort out causality. The constitutive equations then contain a derivation.

flow out causality (preferred):

```

state = int(p.e) + state(0);
p.f = state/i;
output = state;

```

effort out causality:

```

state = i*p.f;
p.e = d state / dt;
output = state;

```

## Interface

### Ports

p

### Description

Input port of the storage element.

### Causality

preferred flow out

An effort out causality results in a derivative constitutive equation.

### Outputs

output

The output signal is equal to the state.

### Parameters

i

The storage element constant.

### Initial Values

state(0)

The initial value of the storage element.

## IC

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model is a combination of an I storage element and a C storage element. Consequently the constitutive equation must be written as a matrix-vector multiplication. The constitutive equation of this element is given below:

```

state1 = int(p1.f);
state2 = int(p2.e);
p1.e = state1*a11 + state2*a21;
p2.f = state1*a21 + state2*a22;
output2 = state1;
output2 = state2;

```

The Maxwell reciprocity demands  $a_{12} = a_{21}$ . Therefore only 3 matrix parameters are necessary.

## Interface

### Ports

p1,p2

### Description

Input ports of the storage element.

### Causality

fixed effort out p1

fixed flow out p2

### Outputs

output1, output2

The output signals are equal to the states.

### Parameters

a11,a21,a22

The storage element constants.

### Initial Values

state1(0), state2(0)

The initial values of the storage element.

## MGY

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal modulated gyrator, a power continuous relation between the effort of one port and the flow of the other port and vice-versa. The gyration ratio can be set to a certain (fluctuating) value, given by an input signal. The model can have both ports with an effort causality or both ports with a flow causality:

effort out causality:

$$\begin{aligned} p1.e &= input * p2.f; \\ p2.e &= input * p1.f; \end{aligned}$$

flow out causality:

$$\begin{aligned} p1.f &= 1/input * p2.e; \\ p2.f &= 1/input * p1.e; \end{aligned}$$

## Interface

### Ports

p1, p2

### Description

Input and output port of gyrator.

### Causality

p1 equal p2

The causality of both ports must be equal.

**Inputs**

input	Modulated gyration ratio.
-------	---------------------------

**MR****Library**

Bond Graph

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.**Description**

This model represents a linear friction/resistor equation. It can have an effort as well as a flow causality. In that case the constitutive equation, as shown below, is simply inverted. The friction/resistor parameter can be set to a (fluctuating) value, given by an input signal.

effort out causality:

$$p.e = input * p.f$$

flow out causality:

$$p.f = p.e / input$$

**Interface****Ports**

p

**Description**

Input port of the R-element.

**Causality**

indifferent

**Inputs**

input	The (modulated) friction/resistor parameter.
-------	--

**MSe****Library**

Bond Graph

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.**Description**

This model represents an ideal modulated effort source. The effort can be set to a (fluctuating) value given by an input signal. The flow is indifferent.

$$p.e = input;$$

## Interface

### Ports

p

### Description

Output port of the effort source.

### Causality

fixed effort out

### Inputs

input

Modulation signal.

## MSf

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal modulated flow source. The flow can be set to a (fluctuating) value given by an input signal. The effort is indifferent.

$$p.f = input;$$

## Interface

### Ports

p

### Description

Output port of the flow source.

### Causality

fixed flow out

### Inputs

input

Modulation signal.

## MTF

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal modulated transformer. The model represents a power continuous relation between the efforts and flows of both its ports. The transform ratio can be set to a certain (fluctuating) value, given by an input signal. The causality is always mixed: one port has an effort out causality while the other has a

flow out causality:

$$\begin{aligned} p1.e &= input * p2.e; \\ p2.f &= input * p1.f; \end{aligned}$$

or:

$$\begin{aligned} p2.e &= 1/input * p1.e; \\ p1.f &= 1/input * p2.f; \end{aligned}$$

## Interface

### Ports

p1, p2

### Description

Input and output port of the transformer.

### Causality

p1 notequal p2

### Inputs

input

Modulated transform ratio.

## OneJunction

### Library

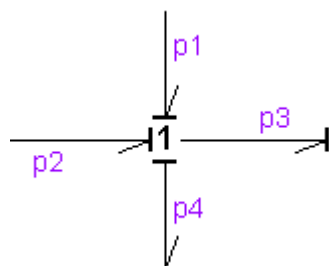
Bond Graph

### Use

**Domains:** Continuous. **Size:** [n,m]. **Kind:** Bond Graphs.

### Description

This junction represents a power continuous (no energy storage, dissipation or generation) connection of elements. The sum of the efforts on all ports is zero and the flows on all ports are equal. The constitutive equations are for example:



$$p1.e + p2.e - p3.e - p4.e = 0;$$

$$p1.f = p2.f = p3.f = p4.f;$$

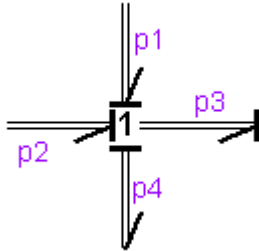
$$flow = p4.f;$$

A one junction has only one initial port p defined. Because any number of bonds may be connected, successive connected bonds are named p1, p2, p3 etc.

The plus or minus signs of the effort equation depend on the direction of the bonds. A bond pointing towards the one junction results in a plus sign and vice-versa. Only one port of a one junction may determine the flow. In the example port p4 determines the flow.

## Multi Bonds

Bonds with a size larger than one (multi bonds) can also be connected to a one junction. All connected bonds, however, must have the same size.



$$p1.e + p2.e - p3.e + p4.e = 0;$$

$$p1.f = p2.f = p3.f = p4.f;$$

$$flow = p4.f;$$

Naming conventions are equal to those of the single bond (size 1) junctions. Successive connected bonds are named p1, p2, p3 etc. To denote single elements of a multibond, matrix notation is used. E.g. the effort of bond number 3 of a multibond p2 can be denoted as p2.e[3] (columnvector notation) or p2.e[3,1] (matrix notation).

## Interface

### Ports

p[any]

### Description

Any number of ports may be connected.

### Causality

1\_effort p

Only one port may have an effort out causality (as seen from the element).

### Outputs

flow

The output signal is equal to the flow of the ports.

### Limitations

All connected bonds must have the same size.

## OneJunction-Activity

### Library

Bond Graph

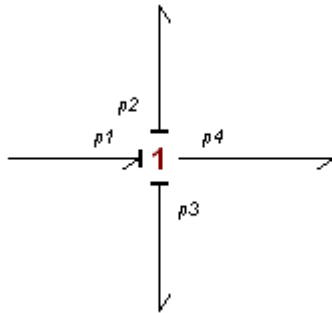
### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This junction is equal to a normal one junction but monitors the powerflows through the connected bonds. If you use this junction and connect some bonds, it could look like the figure below. The bond numbers are important for identification. You can see them by clicking **Port Names** from the **View** menu.





The constitutive equations for this example are:

$$\begin{aligned} p1.e - p2.e - p3.e - p4.e &= 0; \\ p1.f &= p2.f = p3.f = p4.f; \\ flow &= p4.f; \end{aligned}$$

The powerflows through the junction are monitored:

$$power = p.e .* p.f;$$

Note that power is a vector with a size equal to the number of bonds that are attached to the junction. The first element of the vector is the power of the first bond (*p1* in the example figure), the second element is the power of the second bond (*p2* in the example figure) and so on. To see which bonds are active and which bonds are not, the activity is calculated:

$$activity = int(abs(power));$$

To get an easy comparison, the relative activity is calculated:

$$\begin{aligned} maximum\_activity &= max(activity); \\ relative\_activity &= activity ./ maximum\_activity \end{aligned}$$

## Interface

### Ports

p[any]

### Description

Any number of ports may be connected.

### Causality

1\_effort p

Only one port may have a effort out causality (as seen from the element).

### Outputs

flow

The output signal is equal to the effort of the ports.

### Variables

power

Vector of which the elements are the powers of the connected bonds.

activity

Vector of which the elements are the integrated absolute powers of the connected bonds.

**relative\_activity** Vector of which the elements are the relative activities of the connected bonds.

### Limitations

All connected bonds must have size 1.

## PowerSensor

### Library

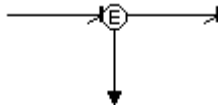
System , Bond Graph

### Use

**Domains:** Continuous. **Size:** [n,m]. **Kind:** Bond Graphs.

### Description

This model can be inserted in any bond to yield the power that is carried through that bond as an output signal.



To ensure success, use drag and drop to place the sensor exactly on top in the middle of the bond. As a result the model will be automatically connected.

### Interface

#### Ports

p1, p2 Input and output port of the power sensor.

#### Outputs

E Power carried through the bond.

## Power Splitter

### Library

System , Bond Graph

### Use

**Domains:** Continuous. **Size:** n-D. **Kind:** Bond Graphs.

## Description

This model can be used to split a multi-bond into single bonds or vice versa. **Default 2** bonds can be connected. Use the right mouse menu and choose *Edit Implementation* to change the number of bonds.

## Interface

### Inputs/Outputs

P(any)	Multi-bond (dimension $[n,m]$ ).
p	single bonds (a total of $n*m$ )

### Note

The multi-bond and corresponding single bonds must have opposite orientations. I.e. when the multi-bond is pointing **towards** the the power-splitter, all single bonds must point **from** the power splitter and when the multi-bond is pointing **from** the the power-splitter, all single bonds must point towards the signal splitter.

## PSensor

### Library

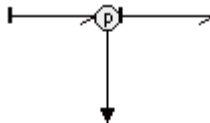
System , Bond Graph

### Use

**Domains:** Continuous. **Size:**  $[n,m]$ . **Kind:** Bond Graphs.

### Description

This model can be inserted in any bond to yield the integral of the effort of that bond as an output signal.



To ensure success, use drag and drop to place the sensor exactly on top in the middle of the bond. As a result the model will be automatically connected.

## Interface

### Ports

p1, p2	Input and output port of the flow sensor.
--------	---

### Outputs

p	Integral of the effort of the bond.
---	-------------------------------------



$$p.f = p.e/r;$$

## Interface

### Ports

p

### Description

Input port of the R-element.

### Causality

indifferent

### Parameters

r

The friction/resistor parameter.

## Se

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal effort source. The effort can be set to a certain constant value, the flow is indifferent.

$$p.e = s;$$

### Ports

p

### Description

Output port of the effort source.

### Causality

fixed effort out

### Parameters

s

The constant value of the generated effort

## Sf

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal flow source. The flow can be set to a certain constant value, the effort is indifferent.

$$p.f = s;$$

## Interface

### Ports

p

### Description

Output port of the flow source.

### Causality

fixed flow out

### Parameters

s

The constant value of the generated flow.

## SGY

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal gyrator with gyration ratio 1. The model represents a one to one power continuous relation between the effort of one port and the flow of the other port and vice-versa. The model can be used to transform a C element into a I element etc. The model can have both ports with an effort causality or both ports with a flow causality:

#### effort out causality:

$$\begin{aligned} p1.e &= p2.f; \\ p2.e &= p1.f; \end{aligned}$$

#### flow out causality:

$$\begin{aligned} p1.f &= p2.e; \\ p2.f &= p1.e; \end{aligned}$$

## Interface

### Ports

p1, p2

### Description

Input and output port of the gyrator.

### Causality

p1 equal p2

## STF

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal transformer with transform ratio 1. The model has no real effect but allows for domain changes (one port having another domain as the other). The model represents a power continuous relation between the efforts and flows of both its ports. The causality is always mixed: one port has an effort causality while the other has a flow causality:

$$\begin{aligned} p1.e &= p2.e \\ p2.f &= p1.f \end{aligned}$$

or:

$$\begin{aligned} p2.e &= p1.e \\ p1.f &= p2.f \end{aligned}$$

### Interface

#### Ports

p1, p2

#### Description

Input and output port of the simple transformer.

#### Causality

p1 notequal p2

The causality of both ports must be different.

## TF

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This model represents an ideal transformer. The model represents a power continuous relation between the efforts and flows of both its ports. The causality is always mixed: one port has an effort causality while the other has a flow causality:

$$\begin{aligned} p1.e &= r * p2.e \\ p2.f &= r * p1.f \end{aligned}$$

or:

$$p2.e = 1/r * p1.e$$

$$p1.f = 1/r * p2.f$$

## Interface

### Ports

p1, p2

### Description

Input and output port of the transformer.

### Causality

p1 notequal p2

The causality of both ports must be different.

### Parameters

r

Transform ratio

## ZeroJunction

### Library

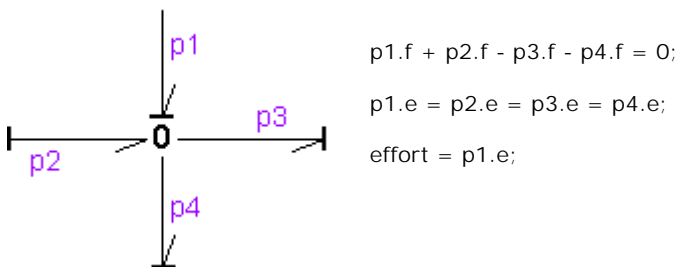
Bond Graph

### Use

**Domains:** Continuous. **Size:** [n,m]. **Kind:** Bond Graphs.

### Description

This junction represents a power continuous (no energy storage, dissipation or generation) connection of elements. The sum of the flows on all ports is zero and the efforts on all ports are equal. The constitutive equations are for example:



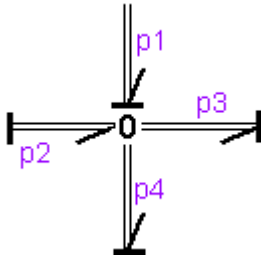
A zero junction has only one initial port p defined. Because any number of bonds may be connected, successive connected bonds are named p1, p2, p3 etc.

The plus or minus signs of the flow equation depend on the direction of the bonds. A bond pointing towards the zero junction results in a plus sign and vice-versa. Only one port of a zero junction may determine the effort. In the example port p1 determines the effort.



## Multi Bonds

Bonds with a size larger than one (multi bonds) can also be connected to a zero junction. All connected bonds, however, must have the same size.



$$p1.f + p2.f - p3.f + p4.f = 0;$$

$$p1.e = p2.e = p3.e = p4.e;$$

$$\text{effort} = p1.e;$$

Naming conventions are equal to those of the single bond (size 1) junctions. Successive connected bonds are named p1, p2, p3 etc. To denote single elements of a multibond, matrix notation is used. E.g the effort of bond number 3 of a multibond p2 can be denoted as p2.e [3] (columnvector notation) or p2.e[3,1] (matrix notation).

## Interface

### Ports

p[any]

### Description

Any number of ports may be connected.

### Causality

1\_flow p

Only one port may have a flow out causality (as seen from the element).

### Outputs

effort

The output signal is equal to the effort of the ports.

### Limitations

All connected bonds must have the same size.

## ZeroJunction-Activity

### Library

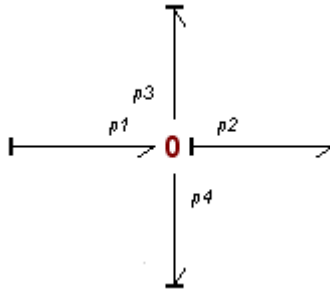
Bond Graph

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Bond Graphs.

### Description

This junction is equal to a normal zero junction but monitors the powerflows through the connected bonds. If you use this junction and connect some bonds, it could look like the figure below. The bond numbers are important for identification. You can see them by clicking **Port Names** from the **View** menu.



The constitutive equations for this example are:

$$\begin{aligned} p1.f - p2.f - p3.f - p4.f &= 0; \\ p1.e &= p2.e = p3.e = p4.e; \\ output &= p2.e; \end{aligned}$$

The powerflows through the junction are monitored:

$$power = p.e . * p.f;$$

Note that power is a vector with a size equal to the number of bonds that are attached to the junction. The first element of the vector is the power of the first bond (p1 in the example figure), the second element is the power of the second bond (p2 in the example figure) and so on. To see which bonds are active and which bonds are not, the activity is calculated:

$$activity = int(abs(power));$$

To get an easy comparison, the relative activity is calculated:

$$\begin{aligned} maximum\_activity &= max(activity); \\ relative\_activity &= activity ./ maximum\_activity \end{aligned}$$

## Interface

### Ports

p[any]

### Description

Any number of ports may be connected.

### Causality

1\_flow p

Only one port may have a flow out causality (as seen from the element).

### Outputs

effort

The output signal is equal to the effort of the ports.

### Variables

power

Vector of which the elements are the powers of the connected bonds.

activity

Vector of which the elements are the integrated absolute powers of the connected bonds.

`relative_activity` Vector of which the elements are the relative activities of the connected bonds.

### Limitations

All connected bonds must have size 1.

## 3d

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model is the multiport equivalent of the single C storage element. Consequently the constitutive equation must be written as a matrix-vector multiplication. The element has a preferred effort out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred flow out causality. The constitutive equations then contain a derivation, which can only be simulated when the Backward Differentiation Formula integration algorithm is available:

effort out causality (preferred):

$$\begin{aligned} state &= \text{int}(p.f) + state(0); \\ p.e &= \text{inverse}(C)*state; \\ outp &= state; \end{aligned}$$

flow out causality:

$$\begin{aligned} state &= C*p.e; \\ p.f &= d \text{ state} / dt; \\ output &= state; \end{aligned}$$

### Interface

#### Ports

`p[3]`

#### Description

Input port of the storage element (columnvector with size 3).

#### Causality

preferred effort out

A flow out causality results in a derivative constitutive equation.

**Outputs**

output[3]                      The output signal is equal to the state (columnvector with size 3).

**Parameters**

C[3,3]                      The storage element constants (matrix of size [3,3]).

**Initial Values**

state(0)[3]                      The initial values of the storage element (columnvector with size 3).

**Limitations**

The preferred equation contains an inverted C matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

**Library**

Bond Graph

**Use**

**Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.

**Description**

This model is the multiport equivalent of the single gyrator. Consequently the constitutive equation must be written as a matrix-vector multiplication. The model can have both ports with an effort out causality or both ports with a flow out causality:

effort out causality:

$$\begin{aligned} p1.e &= \text{transpose}(R) * p2.f; \\ p2.e &= R * p1.f; \end{aligned}$$

flow out causality:

$$\begin{aligned} p1.f &= \text{inverse}(\text{transpose}(R)) * p2.e; \\ p2.f &= \text{inverse}(R) * p1.e; \end{aligned}$$

**Interface****Ports**

p1[3], p2[3]

**Description**

Input and output port of the gyrator (columnvectors with size 3).

**Causality**

$p_1$  equal  $p_2$

The causality of both ports must be equal.

### Parameters

$R[3]$

Gyrator ratio (matrix of size  $[3,3]$ ).

### Limitations

The flow out equations contain an inverted  $R$  matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model is the multiport equivalent of the single  $I$  storage element. Consequently the constitutive equation must be written as a matrix-vector multiplication. The element has a preferred flow out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred effort out causality. The constitutive equations then contain a derivation, which can only be simulated when the Backward Differentiation Formula integration algorithm is available:

flow out causality (preferred):

```
state = int(p.e) + state(0);
p.f = inverse(I)*state;
output = state;
```

effort out causality:

```
state = I*p.f;
p.e = d state / dt;
output = state;
```

## Interface

### Ports

p[3]

### Description

Input port of the storage element (columnvector with size 3).

### Causality

preferred effort out

A flow out causality results in a derivative constitutive equation.

### Outputs

output[3]

The output signal is equal to the state (columnvector with size 3).

### Parameters

I[3,3]

The storage element constants (matrix of size [3,3]).

### Initial Values

state(0)[3]

The initial values of the storage element (columnvector with size 3).

### Limitations

The preferred equation contains an inverted I matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single modulated gyrator. Consequently the constitutive equation must be written as a matrix-vector multiplication. The gyration ratio can be set to a certain (fluctuating) value, given by an input signal. The model can have both ports with an effort out causality or both ports with a flow out causality:

effort out causality:

$$\begin{aligned} p1.e &= \text{transpose}(r) * p2.f; \\ p2.e &= r * p2.f; \end{aligned}$$

flow out causality:

$$p1.f = \text{inverse}(\text{transpose}(r)) * p2.e;$$

$$p2.f = \text{inverse}(r) * p1.e;$$

## Interface

### Ports

p1[3], p2[3]

### Description

Input and output port of the gyrator (columnvectors with size 3).

### Causality

p1 equal p2

The causality of both ports must be equal.

### Inputs

r[3,3]

Modulated gyration ratio (size [3,3]).

### Limitations

The flow out equations contain a matrix inversion of the modulation signal. The elements of this input signal should always have non-singular values.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single dissipative element. Consequently the constitutive equation must be written as a matrix-vector multiplication. This model can have an effort out as well as a flow out causality. In the last case the constitutive equation, as shown below, is simply inverted. The friction/resistor parameter can be set to a (fluctuating) value, given by an input signal.

effort out causality:

$$p.e = r * p.f;$$

flow out causality:

$$p.f = \text{inverse}(r) * p.e;$$

## Interface

### Ports

p[3]

### Description

Input port of the R-element (columnvector with size 3).

### Causality

indifferent

### Input

r[3,3]

The (modulated) friction/resistor parameter (size [3,3]).

### Parameters

R

The friction parameters (matrix of size [3,3])

### Limitations

The flow out equation contains an inverted R matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single modulated effort source. The effort can be set to a (fluctuating) value given by an input signal. The flow is indifferent.

$$p.e = input;$$

### Ports

p[3]

### Description

Output port of the effort source (columnvector with size 3).

### Causality

fixed effort out

### Inputs

input[3]

Modulation signal (columnvector with size 3).



**Library**

Bond Graph

**Use****Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.**Description**

This model is the multiport equivalent of the single modulated flow source. The flow can be set to a (fluctuating) value given by an input signal. The flow is indifferent.

$$p.f = input;$$

**Ports**

p[3]

**Description**

Output port of the flow source (columnvector with size 3).

**Causality**

fixed flow out

**Inputs**

input[3]

Modulation signal (columnvector with size 3).

**Library**

Bond Graph

**Use****Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.**Description**

This model is the multiport equivalent of the single modulated transformer. Consequently the constitutive equation must be written as a matrix-vector multiplication. The transform ratio can be set to a certain (fluctuating) value, given by an input signal. The causality is always mixed: one port has an effort out causality while the other has a flow out causality:

$$\begin{aligned} p1.e &= transpose(r) * p2.e; \\ p2.f &= r * p1.f; \end{aligned}$$

or:

$$\begin{aligned} p2.e &= inverse(transpose(r)) * p1.e; \\ p1.f &= inverse(r) * p2.f; \end{aligned}$$

## Interface

### Ports

p1[3], p2[3]

### Description

Input and output port of the gyrator (columnvectors with size 3).

### Causality

p1 notequal p2

### Inputs

r[3,3]

Modulated transform ratio (size [3,3]).

### Limitations

The second set of equations contain a matrix inversion of the modulation signal. The elements of this input signal should always have non-singular values.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single dissipative element. Consequently the constitutive equation must be written as a matrix-vector multiplication. This model can have an effort out as well as a flow out causality. In the last case the constitutive equation, as shown below, is simply inverted.

effort out causality:

$$p.e = R*p.f;$$

flow out causality:

$$p.f = inverse(R)*p.e;$$

## Interface

### Ports

p[3]

### Description

Input port of the R-element (columnvector with size 3).

### Causality

indifferent

### Parameters

R The friction parameters (matrix of size [3,3])

### Limitations

The flow out equation contains an inverted R matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model is the multiport equivalent of the single effort source. The effort can be set to a certain constant value, the flow is indifferent.

$$p.e = S;$$

### Ports

p[3]

### Description

Output port of the effort source (columnvector with size 3).

### Causality

fixed effort out

### Parameters

S[3]

The constant value of the generated effort (columnvector with size 3).

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model is the multiport equivalent of the single flow source. The effort can be set to a certain constant value, the flow is indifferent.

$$p.f = S;$$

**Ports**

p[3]

**Description**

Output port of the flow source (columnvector with size 3).

**Causality**

fixed flow out

**Parameters**

s[3]

The constant value of the generated flow (columnvector with size 3).

**Library**

Bond Graph

**Use**

**Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.

**Description**

This model is the multiport equivalent of the single symplectic gyrator. Consequently the constitutive equation must be written as a matrix-vector multiplication. This model represents an ideal gyrator with gyration ratio equal to the identity matrix. The model represents a one to one power continuous relation between the effort of one port and the flow of the other port and vice-versa. The model can be used to transform a C-3 element into a I-3 element etc. The model can have both ports with an effort causality or both ports with a flow causality:

effort out causality:

$$p1.e = p2.f;$$

$$p2.e = p1.f;$$

flow out causality:

$$p1.f = p2.e;$$

$$p2.f = p1.e;$$

**Interface****Ports**

p1[3], p2[3]

**Description**

Input and output port of the gyrator (columnvectors with size 3).

**Causality**

p1 equal p2

The causality of both ports must be equal.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single symplectic transformer. This model represents an ideal transformer with a transform ratio equal to the identity matrix. The model represents a one to one power continuous relation between the effort of one port and the flow of the other port and vice-versa. The causality is always mixed: one port has an effort causality while the other has a flow causality:

$$\begin{aligned} p1.e &= p2.e; \\ p2.f &= p1.f; \end{aligned}$$

or:

$$\begin{aligned} p2.e &= p1.e \\ p1.f &= p2.f \end{aligned}$$

### Interface

#### Ports

p1[3], p2[3]

#### Description

Input and output port of the transformer (columnvectors with size 3).

#### Causality

p1 notequal p2

The causality of both ports must be different.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 3-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single transformer. Consequently the constitutive equation must be written as a matrix-vector multiplication. The causality is always mixed: one port has an effort causality while the other has a flow causality:

$$\begin{aligned} p1.e &= \text{transpose}(R) * p2.e; \\ p2.f &= R * p1.f; \end{aligned}$$

or:

$$p2.e = \text{inverse}(\text{transpose}(R)) * p1.e$$

$$p1.f = \text{inverse}(R) * p2.f$$

## Interface

### Ports

p1[3], p2[3]

### Description

Input and output port of the transformer (columnvectors with size 3).

### Causality

p1 notequal p2

The causality of both ports must be different.

### Parameters

R[3,3]

Transform ratio (matrix of size [3,3]).

### Limitations

The lower set of equations contain an inverted R matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## 2d

### Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model is the multiport equivalent of the single C storage element. Consequently the constitutive equation must be written as a matrix-vector multiplication. The element has a preferred effort out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred flow out causality. The constitutive equations then contain a derivation, which can only be simulated when the Backward Differentiation Formula integration algorithm is available:

effort out causality (preferred):

$$state = \text{int}(p.f) + state(0);$$

$$p.e = \text{inverse}(C) * state;$$

$$outp = state;$$

flow out causality:

```

state = C*p.e;
p.f = d state / dt;
output = state;

```

## Interface

### Ports

p[2]

### Description

Input port of the storage element (columnvector with size 2).

### Causality

preferred effort out

A flow out causality results in a derivative constitutive equation.

### Outputs

output[2]

The output signal is equal to the state (columnvector with size 2).

### Parameters

C[2,2]

The storage element constants (matrix of size [2,2]).

### Initial Values

state(0)[2]

The initial values of the storage element (columnvector with size 2).

## Limitations

The preferred equation contains an inverted C matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## Library

Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

## Description

This model is the multiport equivalent of the single gyrator. Consequently the constitutive equation must be written as a matrix-vector multiplication. The model can have both ports with an effort out causality or both ports with a flow out causality:

effort out causality:

$$\begin{aligned}
 p1.e &= \text{transpose}(R) * p2.f; \\
 p2.e &= R * p1.f;
 \end{aligned}$$

flow out causality:

$$\begin{aligned} p1.f &= \text{inverse}(\text{transpose}(R)) * p2.e; \\ p2.f &= \text{inverse}(R) * p1.e; \end{aligned}$$

## Interface

### Ports

p1[2], p2[2]

### Description

Input and output port of the gyrator (columnvectors with size 2).

### Causality

p1 equal p2

The causality of both ports must be equal.

### Parameters

R[2]

Gyrator ratio (matrix of size [2,2]).

## Limitations

The flow out equations contain an inverted R matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## Library

Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Block Diagrams, Bond Graphs.

## Description

This model is the multiport equivalent of the single I storage element. Consequently the constitutive equation must be written as a matrix-vector multiplication. The element has a preferred flow out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred effort out causality. The constitutive equations then contain a derivation, which can only be simulated when the Backward Differentiation Formula integration algorithm is available:

flow out causality (preferred):

$$\begin{aligned} \text{state} &= \text{int}(p.e) + \text{state}(0); \\ p.f &= \text{inverse}(I) * \text{state}; \\ \text{output} &= \text{state}; \end{aligned}$$



effort out causality:

$$\begin{aligned} \text{state} &= I * p.f; \\ p.e &= d \text{ state} / dt; \\ \text{output} &= \text{state}; \end{aligned}$$

## Interface

### Ports

p[2]

### Description

Input port of the storage element (columnvector with size 2).

### Causality

preferred effort out

A flow out causality results in a derivative constitutive equation.

### Outputs

output[2]

The output signal is equal to the state (columnvector with size 2).

### Parameters

I[2,2]

The storage element constants (matrix of size [2,2]).

### Initial Values

state(0)[2]

The initial values of the storage element (columnvector with size 2).

## Limitations

The preferred equation contains an inverted I matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## Library

Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

## Description

This model is the multiport equivalent of the single modulated gyrator. Consequently the constitutive equation must be written as a matrix-vector multiplication. The gyration ratio can be set to a certain (fluctuating) value, given by an input signal. The model can have both ports with an effort out causality or both ports with a flow out causality:

effort out causality:

$$p1.e = \text{transpose}(r) * p2.f;$$

$$p2.e = r * p2.f;$$

flow out causality:

$$\begin{aligned} p1.f &= \text{inverse}(\text{transpose}(r)) * p2.e; \\ p2.f &= \text{inverse}(r) * p1.e; \end{aligned}$$

## Interface

### Ports

p1[2], p2[2]

### Description

Input and output port of the gyrator (columnvectors with size 2).

### Causality

p1 equal p2

The causality of both ports must be equal.

### Inputs

r[2,2]

Modulated gyration ratio (size [2,2]).

## Limitations

The flow out equations contain a matrix inversion of the modulation signal. The elements of this input signal should always have non-singular values.

## Library

Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

## Description

This model is the multiport equivalent of the single dissipative element. Consequently the constitutive equation must be written as a matrix-vector multiplication. This model can have an effort out as well as a flow out causality. In the last case the constitutive equation, as shown below, is simply inverted. The friction/resistor parameter can be set to a (fluctuating) value, given by an input signal.

effort out causality:

$$p.e = r*p.f;$$

flow out causality:

$$p.f = \text{inverse}(r)*p.e;$$

## Interface

### Ports

p[2]

### Description

Input port of the R-element (columnvector with size 2)

### Causality

indifferent

### Input

r[2,2]

The (modulated) friction/resistor parameter (size [2,2]).

### Parameters

R

The friction parameters (matrix of size [2,2]).

### Limitations

The flow out equation contains an inverted R matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single modulated effort source. The effort can be set to a (fluctuating) value given by an input signal. The flow is indifferent.

$$p.e = \text{input};$$

### Ports

p[2]

### Description

Output port of the effort source (columnvector with size 2).

### Causality

fixed effort out

## Inputs

input[2]	Modulation signal (columnvector with size 2).
----------	---

## Library

## Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single modulated flow source. The flow can be set to a (fluctuating) value given by an input signal. The flow is indifferent.

*p.f* = *input*;

## Ports

p[2]

### Description

Output port of the flow source (columnvector with size 2).

## Causality

fixed flow out

## Inputs

`input[2]` Modulation signal (columnvector with size 2).

## Library

## Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

### Description

This model is the multiport equivalent of the single modulated transformer. Consequently the constitutive equation must be written as a matrix-vector multiplication. The transform ratio can be set to a certain (fluctuating) value, given by an input signal. The causality is always mixed: one port has an effort out causality while the other has a flow out causality:

```
p1.e = transpose(r) * p2.e;
p2.f = r * p1.f;
```

or:

$$p2.e = \text{inverse}(\text{transpose}(r)) * p1.e;$$

$$p1.f = \text{inverse}(r) * p2.f;$$

## Interface

### Ports

p1[2], p2[2]

### Description

Input and output port of the gyrator (columnvectors with size 2).

### Causality

p1 notequal p2

### Inputs

r[2,2]

Modulated transform ratio (size [2,2]).

## Limitations

The second set of equations contain a matrix inversion of the modulation signal. The elements of this input signal should always have non-singular values.

## Library

Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

## Description

This model is the multiport equivalent of the single dissipative element. Consequently the constitutive equation must be written as a matrix-vector multiplication. This model can have an effort out as well as a flow out causality. In the last case the constitutive equation, as shown below, is simply inverted.

effort out causality:

$$p.e = R * p.f;$$

flow out causality:

$$p.f = \text{inverse}(R) * p.e;$$

## Interface

### Ports

### Description

p[2] Input port of the R-element (columnvector with size 2)

### Causality

indifferent

### Parameters

R The friction parameters (matrix of size [2,2]).

### Limitations

The flow out equation contains an inverted R matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## Library

Bond Graph

### Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Block Diagrams, Bond Graphs.

### Description

This model is the multiport equivalent of the single effort source. The effort can be set to a certain constant value, the flow is indifferent.

$$p.e = S;$$

### Ports

p[2]

### Description

Output port of the effort source (columnvector with size 2).

### Causality

fixed effort out

### Parameters

S[2] The constant value of the generated effort (columnvector with size 2).

**Library**

Bond Graph

**Use****Domains:** Continuous. **Size:** 2-D. **Kind:** Block Diagrams, Bond Graphs.**Description**

This model is the multiport equivalent of the single flow source. The effort can be set to a certain constant value, the flow is indifferent.

$$p.f = S;$$

**Ports**

p[2]

**Description**

Output port of the flow source (columnvector with size 2).

**Causality**

fixed flow out

**Parameters**

s[2]

The constant value of the generated flow (columnvector with size 2).

**Library**

Bond Graph

**Use****Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.**Description**

This model is the multiport equivalent of the single symplectic gyrator. Consequently the constitutive equation must be written as a matrix-vector multiplication. This model represents an ideal gyrator with gyration ratio equal to the identity matrix. The model represents a one to one power continuous relation between the effort of one port and the flow of the other port and vice-versa. The model can be used to transform a C-2 element into a I-2 element etc. The model can have both ports with an effort causality or both ports with a flow causality:

effort out causality:

$$\begin{aligned} p1.e &= p2.f; \\ p2.e &= p1.f; \end{aligned}$$

flow out causality:

$$p1.f = p2.e;$$

$$p2.f = p1.e;$$

## Interface

### Ports

p1[2], p2[2]

### Description

Input and output port of the gyrator (columnvectors with size 2).

### Causality

p1 equal p2

The causality of both ports must be equal.

## Library

Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

## Description

This model is the multiport equivalent of the single simple transformer. This model represents an ideal transformer with a transform ratio equal to the identity matrix. The model has no real effect but allows for domain changes (one port having another domain as the other). The model represents a power continuous relation between the efforts and flows of both its ports. The causality is always mixed: one port has an effort causality while the other has a flow causality:

$$p1.e = p2.e;$$

$$p2.f = p1.f;$$

or:

$$p2.e = p1.e$$

$$p1.f = p2.f$$

## Interface

### Ports

p1[2], p2[2]

### Description

Input and output port of the transformer (columnvectors with size 2).

### Causality



p1 notequal p2

The causality of both ports must be different.

## Library

Bond Graph

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Bond Graphs.

## Description

This model is the multiport equivalent of the single transformer. Consequently the constitutive equation must be written as a matrix-vector multiplication. The causality is always mixed: one port has an effort causality while the other has a flow causality:

$$p1.e = transpose(R) * p2.e;$$

$$p2.f = R * p1.f;$$

or:

$$p2.e = inverse(transpose(R)) * p1.e$$

$$p1.f = inverse(R) * p2.f$$

## Interface

### Ports

p1[2], p2[2]

### Description

Input and output port of the transformer (columnvectors with size 2).

### Causality

p1 notequal p2

The causality of both ports must be different.

### Parameters

R[2,2]

Transform ratio (matrix of size [2,2]).

### Limitations

The lower set of equations contain an inverted R matrix. The elements of this matrix should be chosen with care to prevent this matrix from becoming singular.

## 9.2 Iconic Diagrams

### Iconic Diagrams

The Iconic Diagram library contains components which are very useful for modeling physical systems. The following libraries are available.

- Electric
- Hydraulics
- Mechanical
- Thermal

### Electric

The Electric library contains components which are very useful for modeling electrical systems. The library contains the following sections:

- Actuators
- Components
- Sources

### Library

Iconic Diagrams\Electric\Actuators  
Iconic Diagrams\Mechanical\Translation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model represents a piezo actuator. The actuator translates a voltage difference at port *p1* to a mechanical position difference between the base at port *p2* and the end effector at port *p3*.

Although the underlying equations of this model are equal to the equations of the *CMAStrecher.emx* model, the default parameter values are typical for bending.

### Interface

Ports	Description
p	Translation port.
<b>Causality</b>	
fixed force out	
<b>Input</b>	
C	Capacitance [F]
KF	Voltage to force conversion factor [N/V]
m	Equivalent mass [kg]
k	Stiffness [N/m]

B	Relative damping ratio []
KB	Force to voltage conversion factor [V/N]

## Library

Iconic Diagrams\Electric\Actuators

Iconic Diagrams\Mechanical\Translation\Actuators

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

## Description

This model represents a piezo actuator. The actuator translates a voltage difference at port *p1* to a mechanical position difference between the base at port *p2* and the end effector at port *p3*.

Although the underlying equations of this model are equal to the equations of the CMABender.emx model, the default parameter values are typical for stretching.

## Interface

Ports	Description
p	Translation port.
<b>Causality</b>	
fixed force out	
<b>Input</b>	
C	Capacitance [F]
KF	Voltage to force conversion factor [N/V]
m	Equivalent mass [kg]
k	Stiffness [N/m]
B	Relative damping ratio []
KB	Force to voltage conversion factor [V/N]

## Library

Iconic Diagrams\Electric\Actuators

Iconic Diagrams\Mechanical\Electric

## Implementations

Default  
IR

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric, Electric).

**Description - Default**

This models represents an ideal DC-motor with no energy loss. The electric port has separate high and low terminals. The equations are

$$\begin{aligned} p1.i &= p1\_high.i = p1\_low.i; \\ p1.u &= p1\_high.u - p1\_low.u; \end{aligned}$$

The model can have mixed forms of causality

$$\begin{aligned} p1.u &= k * p2.omega; \\ p2.T &= k * p1.i; \end{aligned}$$

or:

$$\begin{aligned} p2.omega &= p1.u / k; \\ p1.i &= p2.T / k; \end{aligned}$$

**Interface - Default**

Ports	Description
p1_high, p1_low	Both terminals of the Electric port p1.
p2	Rotation port.

**Causality**

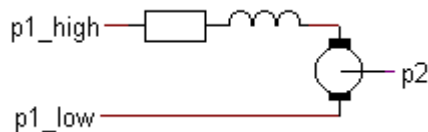
mixed	See equations above.
-------	----------------------

**Parameters**

k	motor constant [Nm/A]
---	-----------------------

**Description - IR**

This models represents an ideal DC-motor with inductance and resistance.



The electric port has separate high and low terminals. The equations are

$$\begin{aligned} p1.i &= p1\_high.i = p1\_low.i; \\ p1.u &= p1\_high.u - p1\_low.u; \end{aligned}$$

**Interface - IR**

Ports	Description
-------	-------------

p1\_high, p1\_low Both terminals of the Electric port p1.  
 p2 Rotation port.

### Causality

mixed See equations above.

### Parameters

k motor constant [Nm/A]  
 L motor inductance [H]  
 R motor resistance [Ohm]

## Library

Iconic Diagrams\Electric\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

### Description

This model represents an ideal capacitor. The element has a preferred voltage out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred current out causality. The constitutive equations then contain a derivation. The port p of the inductor model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p\_high.i = p\_low.i; \\ p.u &= p\_high.u - p\_low.u; \end{aligned}$$

voltage out causality (preferred):

$$p.u = (1/C) * \text{int}(p.i);$$

current out causality:

$$p.i = C * \text{ddt}(p.u);$$

### Interface

#### Ports

p\_high, p\_low

#### Description

Both terminals of the Electric port p.

#### Causality

preferred voltage out

A current out causality results in a derivative constitutive equation.

#### Parameters

C capacitance [F]

### Initial Values

p.u\_initial The initial charge of the capacitor [V].

## Library

Iconic Diagrams\Electric\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric), Block Diagrams.

### Description

This model translates a current to an output signal. It has a voltage out causality. The port p of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p\_high.i = p\_low.i; \\ p.u &= p\_high.u - p\_low.u; \\ p.u &= 0; \\ i &= p.i; \end{aligned}$$

## Interface

### Ports Description

p\_high, p\_low Both terminals of the Electric port p.

### Causality

fixed voltage out

### Output

i Current [A].

## Library

Iconic Diagrams\Electric\Components

## Implementations

Default  
Exponential

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

### Description - Default

This is an ideal electrical diode. The model is a switch which is open when the voltage drop  $v < 0$  and closed when the voltage drop  $v > 0$ . The heart of the model consist of a resistance that is changed by the input voltage from almost zero (on) to a very large value (off). By proper selection of the on and off resistances, they can be effectively zero and infinity in comparison to other circuit elements. The port p of the diode model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p\_high.i = p\_low.i; \\ p.u &= p\_high.u - p\_low.u; \end{aligned}$$

#### voltage out causality:

$$\begin{aligned} R &= \text{if } p.i > 0 \text{ then } Ron \text{ else } Roff \text{ end}; \\ p.u &= R * p.i; \end{aligned}$$

#### current out causality:

$$\begin{aligned} R &= \text{if } p.u > 0 \text{ then } Ron \text{ else } Roff \text{ end}; \\ p.i &= p.u / R; \end{aligned}$$

### Interface - Default

Ports	Description
p_high, p_low	Both terminals of the Electric port p.
<b>Causality</b>	
indifferent p	
<b>Parameters</b>	
Ron	Resistance when diode is turned on [Ohm]
Roff	Resistance when diode is turned off [Ohm]

### Description - Exponential

This is an electrical diode described by an exponential expression. The port p of the diode model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p\_high.i = p\_low.i \\ p.u &= p\_high.u - p\_low.u \\ uT &= (k * T) / e; \\ p.i &= Is * (\exp(p.u / uT) - 1); \end{aligned}$$

with k the Boltzmann constant ( $k = 1.380658e-23$  {J/K})

### Interface - Exponential

Ports	Description
p_high, p_low	Both terminals of the Electric port p.
<b>Causality</b>	
indifferent p	

**Parameters**

T	operating temperature [K]
Is	reverse saturation current [A]

**Library**

Iconic Diagrams\Electric\Components

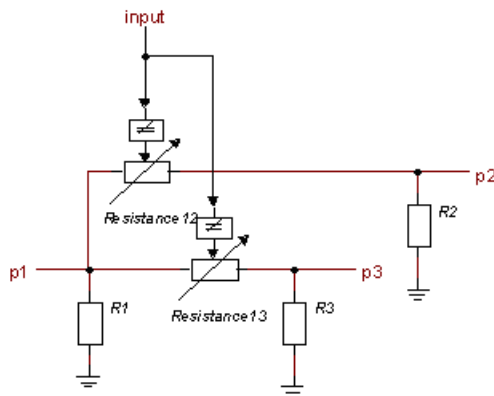
**Implementations**

Level  
Amplitude

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).**Description - Level**

This model represents an almost ideal switch. The switch connects port *p1* with *p2* when the input signal is larger than the threshold value *vt* and connects port *p1* with *p3* when the input signal is smaller or equal to the threshold value *vt*.

The heart of the model consist of two resistances that can be changed by an input signal from almost zero (on) to a very large value (off). By proper selection of the on and off resistances, they can be effectively zero and infinity in comparison to other circuit elements.

*Layout of the switch model.*

The equations of the resistances are:

$$R = \text{if input} > vt \text{ then } Ron \text{ else } Roff \text{ end};$$

$$p.u = R * p.i;$$

**Interface - Level****Ports**

p1, p2, p3

**Description**

The electric ports (Electric).



input                      The switching signal.

### Causality

indifferent p1, p2,  
p3

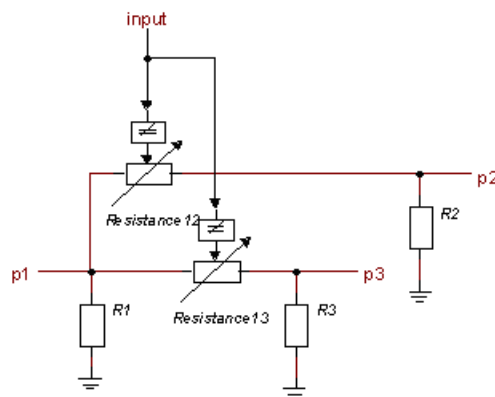
### Parameters

R1\R	Ground resistance at port 1 [Ohm]
R2\R	Ground resistance at port 2 [Ohm]
R3\R	Ground resistance at port 3 [Ohm]
Resistance12\Ron	Resistance between p1 and p2 when switch is turned on [Ohm]
Resistance12\Roff	Resistance between p1 and p2 when switch is turned off [Ohm]
Resistance12\vt	Threshold value between p1 and p2, switch is turned on when input > Resistance12\vt
Resistance13\Ron	Resistance between p1 and p3 when switch is turned on [Ohm]
Resistance13\Roff	Resistance between p1 and p3 when switch is turned off [Ohm]
Resistance13\vt	Threshold value between p1 and p3, switch is turned on when input > Resistance13\vt

### Description - Amplitude

This model represents an almost ideal switch. The switch connects port *p1* with *p2* when the absolute value of the input signal is larger than the threshold value *Resistance12\vt* and connects port *p1* with *p3* when the absolute value of the input signal is smaller or equal to the threshold value *Resistance13\vt*.

The heart of the model consist of two resistances that can be changed by an input signal from almost zero (on) to a very large value (off). By proper selection of the on and off resistances, they can be effectively zero and infinity in comparison to other circuit elements.



*Layout of the switch model.*

The equations of the resistances are:

$$R = \text{if } \text{input} > vt \text{ then } R_{on} \text{ else } R_{off} \text{ end};$$

$$p.u = R * p.i;$$

## Interface - Amplitude

### Ports Description

p1, p2, p3      The electric ports (Electric).  
input            The switching signal.

### Causality

indifferent p1, p2,  
p3

### Parameters

R1\R	Ground resistance at port 1 [Ohm]
R2\R	Ground resistance at port 2 [Ohm]
R3\R	Ground resistance at port 3 [Ohm]
Resistance12\Ron	Resistance between p1 and p2 when switch is turned on [Ohm]
Resistance12\Roff	Resistance between p1 and p2 when switch is turned off [Ohm]
Resistance12\vt	Threshold value between p1 and p2, switch is turned on when $\text{abs}(\text{input}) > \text{Resistance12\vt}$
Resistance13\Ron	Resistance between p1 and p3 when switch is turned on [Ohm]
Resistance13\Roff	Resistance between p1 and p3 when switch is turned off [Ohm]
Resistance13\vt	Threshold value between p1 and p3, switch is turned on when $\text{abs}(\text{input}) > \text{Resistance13\vt}$

## Note

To get a simple switching behavior, pay attention to chose the parameters *Resistance12\vt* and *Resistance13\vt* equal. When these parameters are not chosen equal a more complex switching behavior can be obtained.

## Library

Iconic Diagrams\Electric\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

### Description

This model represents the ground (voltage = 0). The model has only one initial port p defined. Because any number of connections can be made, successive ports are named p1, p2, p3 etc. which gives the constitutive equations:

$$p1.u = p2.u = \dots = pn.u = 0;$$

$$p1.i = \text{free}; p2.i = \text{free}; \dots; pn.i = \text{free};$$

## Interface

Ports	Description
p [any]	Any number of connections can be made (Electric).
<b>Causality</b>	
Fixed voltage out	All ports have a fixed voltage out causality.

## Library

Iconic Diagrams\Electric\Components

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

## Description

This model represents an ideal electrical inductance. The element has a preferred current out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred voltage out causality. The constitutive equations then contain a derivation. The port p of the inductor model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p\_high.i = p\_low.i; \\ p.u &= p\_high.u - p\_low.u; \end{aligned}$$

### current out causality (preferred):

$$p.i = (1/L) \text{int}(p.u);$$

### voltage out causality:

$$p.u = L * \text{ddt}(p.i);$$

## Interface

Ports	Description
p_high, p_low	Both terminals of the Electric port p.
<b>Causality</b>	
preferred current out	An voltage out causality results in a derivative constitutive equation.
<b>Parameters</b>	
L	Inductance [H]
<b>Initial Values</b>	
p.i_initial	The initial flux in the inductor.

**Library**

Iconic Diagrams\Electric\Components

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

**Description**

This node model represents a structural connection between two or more branches of an electrical circuit. The model has only one initial port *p* defined. Because any number of connections can be made, successive ports are named *p*1, *p*2, *p*3 etc.

**Interface**

Ports	Description
<i>p</i> [any]	Any number of connections can be made.

**Library**

Iconic Diagrams\Electric\Components

**Implementations**

Default  
Universal

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

**Description - Default**

This model represents an ideal operational amplifier. The input resistance is infinite and the output resistance is zero. The port *p\_in* of the OpAmp model has separate high and low terminals:

$$\begin{aligned} p\_in.u &= p\_in\_high.u - p\_in\_low.u; \\ p\_in\_high.i &= p\_in\_low.i = p\_in.i = 0; \\ p\_out.u &= A * p\_in.u; \end{aligned}$$

**Interface - Default**

Ports	Description
<i>p_in_high</i> ,	Both terminals of the input port <i>p_in</i> (Electric).
<i>P_in_low</i>	
<i>p_out</i>	Output port (Electric).

**Causality**

fixed current out  
*p\_in*

fixed voltage out

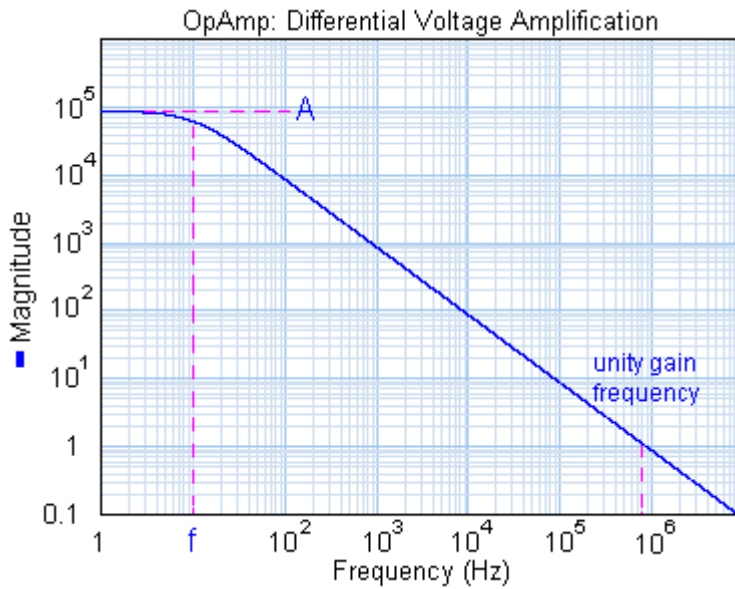
p\_out

### Parameters

A                      Amplification []

### Description - Universal

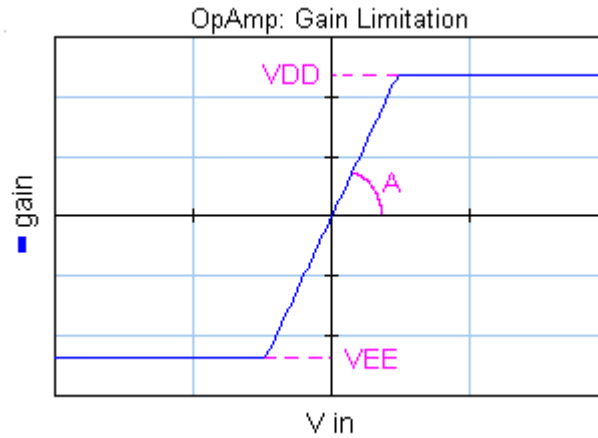
This model represents an operational amplifier with a first order decreasing voltage amplification.



The amplification is parameterized by a DC-gain ( $A$ ) and a cut-off frequency ( $f$ ). This yields a unity gain frequency of:

$$\text{unity gain frequency} = A \cdot f;$$

The gain is limited to yield an output that is between the positive ( $V_{DD}$ ) and negative ( $V_{EE}$ ) supply voltage.



The input resistance is infinite and the output resistance is equal to the parameter  $R$ . The port  $p\_in$  of the OpAmp model has separate high and low terminals:

$$\begin{aligned} p\_in.u &= p\_in\_high.u - p\_in\_low.u \\ p\_in\_high.i &= p\_in\_low.i = p\_in.i = 0; \\ p\_out.u &= A_{diff} * p\_in.u - R * p\_out.u; \end{aligned}$$

where  $A_{diff}$  is a dynamic gain according to the bode and gain plot.

## Interface - Universal

### Ports

$p\_in\_high$ ,	Both terminals of the input port $p\_in$ (Electric).
$p\_in\_low$	Output port (Electric).
$p\_out$	

### Causality

fixed current out  
 $p\_in$   
 preferred voltage  
 out  $p\_out$

### Parameters

$A$	DC gain or DC Amplification
$f$	Cut-off frequency [Hz]
$V_{DD}$	Positive supply voltage [V], choose $V_{DD} > V_{EE}$ !
$V_{EE}$	Negative supply voltage [V], choose $V_{DD} > V_{EE}$ !
$R$	Output impedance [Ohm]

## Library

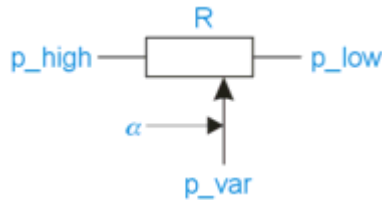
Iconic Diagrams\Electric\Components

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

## Description

This model represents an ideal potentiometer.



It can have various forms of causality. The equations are:

$$\begin{aligned} R1 &= (1 - \alpha) * R; \\ R2 &= \alpha * R; \\ p\_high.u - p\_var.u &= p\_high.i * R1; \\ p\_var.u - p\_low.u &= p\_low.i * R2; \\ p\_high.i + p\_var.i &= p\_low.i; \end{aligned}$$

where alpha denotes the position of the indicator and can vary from zero to one.

## Interface

Ports	Description
p_high, p_low	Both terminals of the resistor.
p_var	Indicator terminal.
<b>Causality</b>	
indifferent	
<b>Parameters</b>	
R	Resistance [Ohm].
alpha	Indicator position ( $0 \leq \alpha \leq 1$ ).

## Library

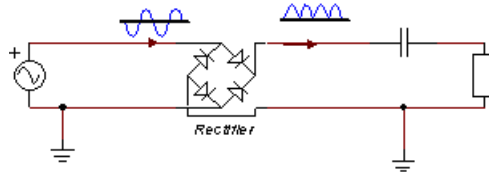
Iconic Diagrams\Electric\Components

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

## Description

This model represents an diode bridge rectifier consisting of a set four diodes. Given an alternating input current, the bridge produces an output current which is always positively oriented and has the same amplitude as the input current. The bridge behavior is ideal. No diode characteristics are implemented and no power is dissipated.



A circuit with a diode bridge rectifier.

## Interface

Ports	Description
p1_high, p1_low	Both terminals of the Electric input port p1.
p2_high, p2_low	Both terminals of the Electric output port p2.

## Causality

p1 not equal p2

## Library

Iconic Diagrams\Electric\Components

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

## Description

This model represents an ideal electrical resistor. It can have an voltage out as well as a current out causality. In the last case the constitutive equation, as shown below, is simply inverted. The port p of the damper model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p_{high}.i = p_{low}.i; \\ p.u &= p_{high}.u - p_{low}.u; \end{aligned}$$

Voltage out causality:

$$p.u = R * p.i;$$

Current out causality:

$$p.i = p.u / R;$$



## Interface

Ports	Description
p_high, p_low	Both terminals of the Electric port p.
<b>Causality</b>	
indifferent	
<b>Parameters</b>	
R	Resistance [Ohm].

## Library

Iconic Diagrams\Electric\Components

## Implementations

Level  
Amplitude

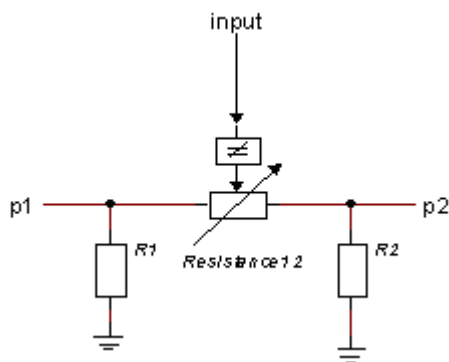
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

## Description - Level

This model represents an almost ideal switch. The switch is turned on when the input signal is larger than the threshold value  $v_t$  and it is turned off when the input signal is smaller or equal to the threshold value  $v_t$ .

The heart of the model consist of a resistance that can be changed by an input signal from almost zero (on) to a very large value (off). By proper selection of the on and off resistances, they can be effectively zero and infinity in comparison to other circuit elements.



*Layout of the switch model.*

The equations of the resistance are:

```
R = if input > vt then Ron else Roff end;
p.u = R * p.i;
```

## Interface - Level

Ports	Description
p1, p2	Both electric ports (Electric).
input	The switching signal.

### Causality

indifferent p1, p2

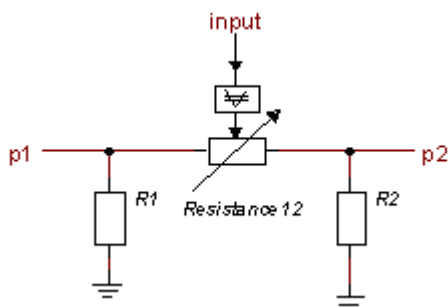
### Parameters

R1\R	Ground resistance at port 1 [Ohm]
R2\R	Ground resistance at port 2 [Ohm]
Resistance12\Ron	Resistance when switch is turned on [Ohm]
Resistance12\Roff	Resistance when switch is turned off [Ohm]
Resistance12\vt	Threshold value, switch is turned on when input > vt

## Description - Amplitude

This model represents an almost ideal switch. The switch is turned on when the amplitude of the input signal is larger than the threshold value  $vt$  and it is turned off when the amplitude of the input signal is smaller or equal to the threshold value  $vt$ .

The heart of the model consist of a resistance that can be changed by an input signal from almost zero (on) to a very large value (off). By proper selection of the on and off resistances, they can be effectively zero and infinity in comparison to other circuit elements.



Layout of the switch model.

The equations of the resistance are:

```
R = if abs(input) > vt then Ron else Roff end;
p.u = R * p.i;
```

## Interface - Amplitude

Ports	Description
-------	-------------

p1, p2                      Both electric ports (Electric).  
input                        The switching signal.

### Causality

indifferent p1,p2

### Parameters

R1\R                        Ground resistance at port 1 [Ohm]  
R2\R                        Ground resistance at port 2 [Ohm]  
Resistance12\Ron        Resistance when switch is turned on [Ohm]  
Resistance12\Roff       Resistance when switch is turned off [Ohm]  
Resistance12\vt        Threshold value, switch is turned on when  $\text{abs}(\text{input}) > \text{vt}$

## Library

Iconic Diagrams\Electric\Components

### Implementations

Default  
Induction

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

### Description - Default

This models represents an ideal transformer. The transformer does not have internal resistors, capacitance or inductance. The causality of this model is always mixed: one port has a voltage causality while the other has a current out causality:

$$\begin{aligned} p\_1.u &= n * p\_2.u; \\ p\_2.i &= n * p\_1.i; \end{aligned}$$

or:

$$\begin{aligned} p\_2.u &= 1/n * p\_1.u; \\ p\_1.i &= 1/n * p\_2.i; \end{aligned}$$

### Interface - Default

Ports	Description
p_1,p_2	Electrical ports

**Causality**

p\_small    notequal

p\_large

### Parameters

n                      turns ratio []

### Description - Induction

This models represents a transformer with inductance and mutual inductance. The equations are:

$$\begin{aligned} p\_1.u &= L1 * ddt(p\_1.i) + M * ddt(p\_2.i); \\ p\_2.u &= M * ddt(p\_1.i) + L2 * ddt(p\_2.i); \end{aligned}$$

### Interface - Induction

Ports	Description
p_1, p_2	Electrical ports

### Causality

indifferent

### Parameters

L1	Primary inductance [H]
L2	Secondary Inductance [H]
M	Coupling Inductance [H]

## Library

Iconic Diagrams\Electric\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric), Block Diagrams.

### Description

This model translates a voltage difference to an output signal. It has a current out causality. The port p of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p\_high.i = p\_low.i; \\ p.u &= p\_high.u - p\_low.u; \\ p.i &= 0; \\ u &= p.u; \end{aligned}$$

### Interface

Ports	Description
p_high, p_low	Both terminals of the Electric port p.

### Causality

fixed current out

### Output

u                      Voltage [V].

## Library

Iconic Diagrams\Electric\Sources

## Implementations

Voltage

Current

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

## Description - Voltage

This model represents an ideal voltage controlled current source. Both ports of the model have separate high and low terminals:

$$\begin{aligned} p\_in.u &= p\_in\_high.u - p\_in\_low.u; \\ p\_in\_high.i &= p\_in\_low.i = p\_in.i; \\ p\_out.u &= p\_out\_high.u - p\_out\_low.u = 0 \\ p\_out\_high.i &= p\_out\_low.i = p\_in.i; \end{aligned}$$

The equations of this model are:

$$\begin{aligned} p\_in.i &= 0; \\ p\_out.i &= p\_in.u; \\ p\_out.u &= \text{indifferent}; \end{aligned}$$

## Interface - Voltage

Ports	Description
p_in_high,	Both terminals of the input port p_in (Electric).
P_in_low	
p_out_high,	Both terminals of the output port p_out (Electric).
P_out_low	

## Causality

fixed current out

p\_in

fixed current out

p\_out

### Description - Current

This model represents an ideal current controlled current source. Both ports of the model have separate high and low terminals:

$$\begin{aligned} p\_in.u &= p\_in\_high.u - p\_in\_low.u; \\ p\_in\_high.i &= p\_in\_low.i = p\_in.i; \\ p\_out.u &= p\_out\_high.u - p\_out\_low.u = 0 \\ p\_out\_high.i &= p\_out\_low.i = p\_in.i; \end{aligned}$$

The equations of this model are:

$$\begin{aligned} p\_in.u &= 0; \\ p\_out.i &= p\_in.i; \\ p\_out.u &= \text{indifferent}; \end{aligned}$$

### Interface - Current

Ports	Description
p_in_high,	Both terminals of the input port p_in (Electric). Both terminals of the output port p_out (Electric).
P_in_low	
p_out_high,	
P_out_low	

#### Causality

fixed voltage out  
p\_in  
fixed current out  
p\_out

### Library

Iconic Diagrams\Electric\Sources

### Implementations

Voltage  
Current  
PI  
KP

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

### Description - Voltage

This model represents an ideal voltage controlled voltage source. Both ports of the model have separate high and low terminals:

$$\begin{aligned}
p\_in.u &= p\_in\_high.u - p\_in\_low.u; \\
p\_in\_high.i &= p\_in\_low.i = p\_in.i; \\
p\_out.u &= p\_out\_high.u - p\_out\_low.u = 0 \\
p\_out\_high.i &= p\_out\_low.i = p\_in.i;
\end{aligned}$$

The equations of this model are:

$$\begin{aligned}
p\_in.i &= 0; \\
p\_out.u &= p\_in.u; \\
p\_out.i &= \text{indifferent};
\end{aligned}$$

## Interface - Voltage

### Ports

p_in_high,	Both terminals of the input port p_in (Electric).
P_in_low	Both terminals of the output port p_out (Electric).
p_out_high,	
P_out_low	

### Causality

fixed current out  
p\_in  
fixed voltage out  
p\_out

## Description - Current

This model represents an ideal current controlled voltage source. Both ports of the model have separate high and low terminals:

$$\begin{aligned}
p\_in.u &= p\_in\_high.u - p\_in\_low.u; \\
p\_in\_high.i &= p\_in\_low.i = p\_in.i; \\
p\_out.u &= p\_out\_high.u - p\_out\_low.u = 0 \\
p\_out\_high.i &= p\_out\_low.i = p\_in.i;
\end{aligned}$$

The equations of this model are:

$$\begin{aligned}
p\_in.u &= 0; \\
p\_out.u &= p\_in.i; \\
p\_out.i &= \text{indifferent};
\end{aligned}$$

## Interface - Current

### Ports

p_in_high,	Both terminals of the input port p_in (Electric).
P_in_low	Both terminals of the output port p_out (Electric).
p_out_high,	
P_out_low	

### Causality

fixed voltage out

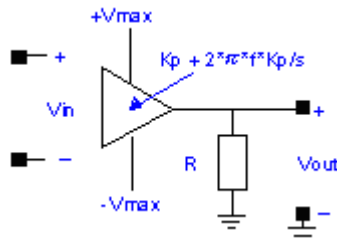
p\_in

fixed voltage out

p\_out

### Description - PI

This model represents a voltage controlled voltage source. The output voltage is connected to the input voltage through a PI-controller and limited to a maximum and minimum value of  $\pm V_{max}$ . The output voltage is subjected to an output resistance  $R$ .



Both ports of the model have separate high and low terminals:

$$\begin{aligned} p\_in.u &= p\_in\_high.u - p\_in\_low.u; \\ p\_in\_high.i &= p\_in\_low.i = p\_in.i; \\ p\_out.u &= p\_out\_high.u - p\_out\_low.u = 0 \\ p\_out\_high.i &= p\_out\_low.i = p\_in.i; \end{aligned}$$

### Interface - PI

#### Ports

p\_in\_high,

p\_in\_low

p\_out\_high,

p\_out\_low

#### Description

Both terminals of the input port p\_in (Electric).

Both terminals of the output port p\_out (Electric).

#### Causality

fixed current out

p\_in

fixed voltage out

p\_out

#### Parameters

Kp

Proportional gain []

f

Integration frequency [Hz]

Vmax

Maximum output voltage [V]

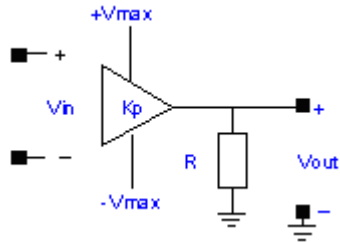
R

Output resistance [Ohm]



## Description - KP

This model represents a voltage controlled voltage source. The output voltage is proportional to the input voltage and is limited to a maximum and minimum value of  $\pm V_{max}$ . The output voltage is subjected to an output resistance  $R$ .



Both ports of the model have separate high and low terminals:

$$\begin{aligned} p\_in.u &= p\_in\_high.u - p\_in\_low.u; \\ p\_in\_high.i &= p\_in\_low.i = p\_in.i; \\ p\_out.u &= p\_out\_high.u - p\_out\_low.u = 0 \\ p\_out\_high.i &= p\_out\_low.i = p\_in.i; \end{aligned}$$

## Interface - KP

### Ports

p\_in\_high,  
p\_in\_low

### Description

Both terminals of the input port p\_in (Electric).

p\_out\_high,  
p\_out\_low

Both terminals of the output port p\_out (Electric).

### Causality

fixed current out

p\_in

fixed voltage out

p\_out

### Parameters

Kp	Proportional gain []
Vmax	Maximum output voltage [V]
R	Output resistance [Ohm]

## Library

Iconic Diagrams\Electric\Sources

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

## Description

This model represents an ideal current source with a constant current. The current can be set to a certain constant value, the voltage is indifferent. The port  $p$  of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p\_high.i = p\_low.i; \\ p.u &= p\_high.u - p\_low.u; \end{aligned}$$

$$\begin{aligned} p.u &= \text{indifferent}; \\ p.i &= i; \end{aligned}$$

## Interface

Ports	Description
p_low, p_high	Both terminals of the Electric port p.
<b>Causality</b>	
fixed current out	
<b>Parameters</b>	
i	Current [A].

## Library

Iconic Diagrams\Electric\Sources

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric), Block Diagrams.

## Description

This model represents an ideal current source with a variable current. The current can be set to a (fluctuating) value given by the input signal  $i$ , the voltage is indifferent.

$$p.i = i;$$

## Interface

Ports	Description
p	Electric port.
<b>Causality</b>	
fixed current out	
<b>Input</b>	
i	Current [A].

**Library**

Iconic Diagrams\Electric\Sources

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric), Block Diagrams.

**Description**

This model represents an ideal voltage source with a variable voltage. The voltage can be set to a (fluctuating) value given by the input signal  $u$ , the current is indifferent.

$$p.u = u;$$

**Interface**

Ports	Description
p	Electric port.

**Causality**

fixed voltage out

**Input**

u	Voltage [V].
---	--------------

**Library**

Iconic Diagrams\Electric\Sources

**Implementations**

DC

AC

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

**Description - DC**

This model represents an ideal voltage source with a constant voltage. The voltage can be set to a certain constant value, the current is indifferent. The port  $p$  of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.i &= p\_high.i = p\_low.i; \\ p.u &= p\_high.u - p\_low.u; \end{aligned}$$

*p.i = indifferent;*  
*p.u = u;*

## Interface - DC

Ports	Description
p	Both terminals of the Electric port p.

### Causality

fixed voltage out

### Parameters

u	Voltage [V].
---	--------------

## Description - AC

This model represents an ideal voltage source with a sinusoidal voltage. The voltage can be set to a certain constant value, the current is indifferent. The port *p* of the model has separate high and low terminals. The equations are:

*p.i = p\_high.i = p\_low.i;*  
*p.u = p\_high.u - p\_low.u;*

*p.i = indifferent;*  
*p.u = U\*sin(2\*pi\*f\*time);*

## Interface - AC

Ports	Description
p	Both terminals of the Electric port p.

### Causality

fixed voltage out

### Parameters

U	Voltage amplitude [V].
f	Voltage frequency [Hz]

## Hydraulics

The 20-sim Hydraulics library contains components to model the dynamic behavior of hydraulic circuits. Most components have lumped volumes to ensure a seamless connection with other components. Therefore almost all components can be connected arbitrarily. Care has to be taken that physically relevant circuits are created.

The elementary components (without lumped volumes) are stored in the basic libraries. These models should only be used by experienced modelers who want to create their own library components.

Hydraulic components can easily be coupled to other library models. The pumps and motors have a rotation port that can be coupled to models of the Rotation library. The cylinder models have a translation port that can be coupled to models of the Translation library. Some models have a variable input that can be coupled to models of the Signal library.

To get a good impression of the use the components of this library, have a look at the example circuits.

### Ports

Every library component has one or more hydraulic connectors, which are called ports in 20-sim. Ports always have two variables: pressure [Pa] and volume flow [m<sup>3</sup>/s]. The following ports a and b are usually provided:

a

a.p                      Pressure in [Pa] with respect to atmospheric pressure (p stands for pressure)

.

a.phi                    Volume flow [m<sup>3</sup>/s], positive if oil is entering the component at port a (phi stands for flow).

b

b.p                      Pressure in [Pa] with respect to atmospheric pressure (p stands for pressure)

.

b.phi                    Volume flow [m<sup>3</sup>/s], negative if oil is entering the component at port b (phi stands for flow).

### Pressure

The 20-sim hydraulics library uses the common definition of pressure in Pa:

$$1 \text{ Pa} = 1 \text{ N/m}^2 = 1\text{e-}5 \text{ bar}$$

The air pressure at sea level is taken as the zero value:

$$0 \text{ Pa} = \text{air pressure}$$

Consequently the pressure for liquid oil that starts to vaporize is negative. In 20-sim the default value of the vapour pressure is:

$$p_{\text{vapour}} = -0.999\text{e}5 \text{ Pa}$$

The vapour pressure is the minimum pressure. Some models have a safeguard on the pressure to prevent it to become smaller. You can change the value of the vapour pressure but take care that always a value is chosen that is smaller than zero. Otherwise some of the models will not work correctly.

### Bulk modulus

No liquid is fully incompressible. The compliance characteristics of the oil in a hydraulic system is a vital parameters affecting the response. The effect of compressibility is incorporated by entering the bulk modulus of the fluid:

$$dp = -B*dV/V$$

Here  $dp$  is the pressure,  $V$  the volume and  $B$  the bulk modulus. For small pressure variations the compressibility effect may be rewritten as:

$$p = B/V * \int(flow)$$

The bulk modulus is a very uncertain parameter. It depends on the percentage of air dissolved in the fluid, the pressure and the temperature. In most textbooks a value of 1.5 to 1.75 [GPa] is used. 20-sim uses a default value of 1.6 [GPa]. If fluid should be simulated at elevated temperatures or with a high percentage of air dissolved, you should use a smaller value for the bulk modulus.

### Units

20-sim uses SI-units for the hydraulic components. If you want to use other units select them in the Parameters Editor or the Variables Chooser.

### Laminar flow

Many hydraulic models have a laminar (leakage) flow:

$$flow = G * dp$$

with  $G$  the flow conductance and  $dp$  the pressure difference. The table below shows the flow rates for various conductance values and pressure differences of 10 [bar] and 400 [bar].

G m <sup>3</sup> /s.Pa	P Pa	P bar	flow m <sup>3</sup> /s	flow l/min
1.0e-14	1.0e6	10	2.89e-8	0.002
1.0e-14	4.0e7	400	1.82e-7	0.01
1.0e-12	1.0e6	10	1.44e-6	0.09
1.0e-12	4.0e7	400	9.12e-6	0.6
1.0e-10	1.0e6	10	1.44e-4	9
1.0e-10	4.0e7	400	9.12e-4	55
1.0e-8	1.0e6	10	2.89e-3	173
1.0e-8	4.0e7	400	1.82e-2	1095

If the flow rate is very small (leakage flow), choose  $G$  below 1.0e-14 [m<sup>3</sup>/s.Pa]. If the flow rate is very large (open connection to a tank), choose  $G$  1.0e-9 or higher if desired.

### Turbulent flow

Some hydraulic models have a turbulent (orifice) flow described by:

$$flow = Cd * A * \sqrt{2 / \rho * dp}$$

with  $Cd$  the discharge coefficient,  $A$  the orifice area,  $\rho$  the fluid density and  $dp$  the pressure difference. Except for small pressure around zero, the discharge coefficient is constant. In most textbooks a value of 0.6 is recommended. The table below shows the flow rates for various orifice areas and pressure differences of 10 [bar] and 400 [bar].

Cd m <sup>3</sup> /s.Pa	A m <sup>2</sup>	rho kg/m <sup>3</sup>	dp Pa	dp bar	flow m <sup>3</sup> /s	flow l/min
0.6	1.0e-9	865	1.0e6	10	1.0e-8	0.0006
0.6	1.0e-9	865	4.0e7	400	4.0e-7	0.024
0.6	5.0e-8	865	1.0e6	10	1.0e-6	0.06
0.6	5.0e-8	865	4.0e7	400	4.0e-5	2.4
0.6	5.0e-6	865	1.0e6	10	1.0e-4	6
0.6	5.0e-6	865	4.0e7	400	4.0e-3	240
0.6	1.0e-4	865	1.0e6	10	1.0e-2	600
0.6	1.0e-4	865	4.0e7	400	4.0e-1	24000

If the flow rate is very small (leakage flow) choose A smaller than 1.0e-9 [m2]. If the flow rate should be very large (open connection) choose A equal to 1.0e-4 or higher if desired. For very small pressure differences the flow will become laminar and the discharge coefficient will drop. For such cases, specialized models should be applied. If they are not available, use a laminar flow model with a small conductance value.

### Simulation

Hydraulic circuits can be simulated with all the available integration methods. In practice the default integration method (BDF) will give the most accurate and quickest response. Take care with hydraulic circuits that will give high pressure peaks and small flow rates. These circuits are sometimes hard to simulate. In practice high pressure peaks should be reduced with pressure relief valves to avoid damage. Fortunately adding pressure relief valves will in most cases improve the simulation response.

### Disclaimer

All models have been tested with standard configurations. This will however not ensure that valid results will be found at all times. For example temperature effects are not included and certain parameter values will lead to unstable simulations. Therefore any application of the library without validation of the user is at its own risk!

### Literature

The 20-sim hydraulic library has been based on the following literature:

P. Dransfield, Hydraulic Control Systems - Design and Analysis of Their Dynamics, Springer 1981, ISBN 3-540-10890-4.

P. Beater, Entwurf Hydraulischer Maschinen, Modelbildung, Stabilitätsanalyse und Simulation hydrostatischer Antriebe und Steuerungen, Springer 1999, ISBN 3-540-65444-5.

The models have been designed as close as possible to the Modelica hydraulic library ([www.modelica.org](http://www.modelica.org)). To compare both libraries the example model Closed Circuit Drive Train.emx has been added.

## Library

Iconic Diagrams\Hydraulics\Components

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description

When a fluid flow changes speed, a force is needed to accelerate the fluid. This force is equal to the acceleration multiplied by the mass of the fluid.

$$F = m * dv/dt$$



The fluid mass is equal to the pipe area multiplied by the pipe length and the fluid density:

$$m = A * l * \rho$$

The force will result in a pressure differential:

$$F = A * dp = A * (p_a - p_b)$$

We can rewrite the formulas as

$$dp = \rho * l * dv/dt$$

and by introducing the fluid flow  $\phi$ :

$$v = \phi/l$$

we get the formula for an hydraulic inertia:

$$dp = (\rho * l / A) * d\phi/dt$$

## Interface

### Ports

pa, pb

### Description

Both terminals of the hydraulic inertia.

### Causality

fixed pressure out

pa

fixed pressure out

pb



**Parameters**

$\rho$	Mass density of the fluid [kg/m <sup>3</sup> ].
$d$	pipe diameter [m]
$l$	pipe length [m]

**Library**

Iconic Diagrams\Hydraulics\Components

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

**Description**

This node model represents a connection between two or more lines of an hydraulic circuit. The model has only one initial port  $p$  defined. Because any number of connections can be made, successive ports are named  $p_1$ ,  $p_2$ ,  $p_3$  etc.

**Interface****Ports****Description**

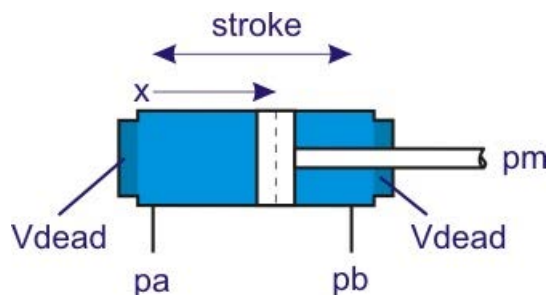
$p$  [any] Any number of connections can be made.

**Library**

Iconic Diagrams\Hydraulics\Cylinders\Basic Cylinders

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics/Translational).

**Description**

This is an ideal model of cylinder with no mass and no friction. The volume of the chambers is given by:

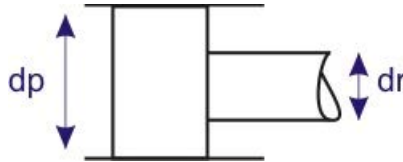
$$V_a = V_{dead} + A_a \cdot (x + x_{initial})$$

$$V_b = V_{dead} + A_b \cdot (stroke - x - x_{initial})$$

with  $A_a$  the piston area and  $A_b$  the effective area at the rod side.  $x$  is the piston position and  $V_{dead}$  the initial volume when piston position is zero. The piston areas  $A_a$  and  $A_b$  are related to the piston diameter  $dp$  and rod diameter  $dr$  by:

$$A_a = \pi \cdot dp^2 / 4$$

$$A_b = \pi \cdot dp^2 / 4 - \pi \cdot dr^2 / 4$$



There is no restriction on the travel of the piston. Only a warning is given when the maximum stroke is exceeded or the piston position gets negative.

## Interface

### Ports

pa, pb  
pm

### Description

hydraulic port  
translation port

### Causality

preferred pressure out pa  
preferred force out pm

### Parameters

Vdead	rest volume of oil in cylinder chamber when closed [N.s/m]
B	effective bulk modulus [Pa]
stroke	stroke length [m]
x_initial	starting position of piston [m]
dp	piston diameter [m]
dr	rod diameter [m]

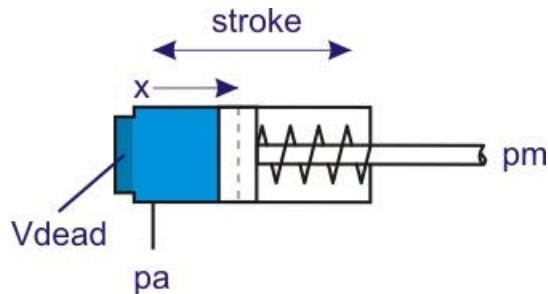
## Library

Iconic Diagrams\Hydraulics\Cylinders\Basic Cylinders

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics/Translational).

## Description



This is an ideal model of a single acting cylinder with no mass and no friction and a return spring to drive the cylinder back when there is no pressure in the chamber. The volume of the chamber is given by:

$$V = V_{dead} + Aa \cdot (x + x_{initial})$$

with  $Aa$  the piston area,  $x$  the piston position and  $V_{dead}$  the initial volume when piston position is zero. The piston area  $Aa$  is related to the piston diameter  $dp$  by:

$$Aa = \pi \cdot dp^2 / 4$$



The driving force of the return spring is determined by two parameters: the force for piston position zero ( $F_{spr\_min}$ ) and the force when the piston is at the other side ( $F_{spr\_max}$ ). The spring constant ( $kspr$ ) and initial spring position ( $x0$ ) are calculated out of these parameters by:

$$kspr = (F_{spr\_max} - F_{spr\_min}) / stroke$$

$$x0 = -F_{spr\_min} / kspr$$

There is no restriction on the travel of the piston. Only a warning is given when the maximum stroke is exceeded or the piston position gets negative.

## Interface

### Ports

pa

### Description

hydraulic port

pm translation port

### Causality

preferred pressure out pa

preferred force out pm

### Parameters

Vdead rest volume of oil in cylinder chamber when closed [N.s/m]

B effective bulk modulus [Pa]

stroke stroke length [m]

x\_initial starting position of piston [m]

dp piston diameter [m]

Fspr\_min minimum return spring force (at x = 0) [N]

Fspr\_max maximum return spring force (at x = stroke) [N]

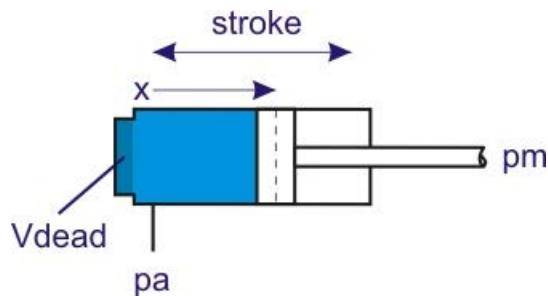
### Library

Iconic Diagrams\Hydraulics\Cylinders\Basic Cylinders

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics/Translational).

### Description

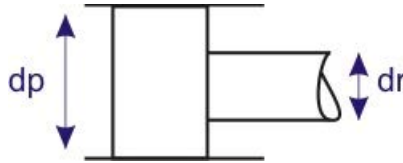


This is an ideal model of a single acting cylinder with no mass and no friction. The volume of the chamber is given by:

$$V = V_{dead} + Aa \cdot (x + x_{initial})$$

with  $Aa$  the piston area,  $x$  the piston position and  $V_{dead}$  the initial volume when piston position is zero. The piston area  $Aa$  is related to the piston diameter  $dp$  by:

$$Aa = \pi * dp^2 / 4$$



There is no restriction on the travel of the piston. Only a warning is given when the maximum stroke is exceeded or the piston position gets negative.

## Interface

### Ports

pa

pm

### Description

hydraulic port

translation port

### Causality

preferred pressure out pa

preferred force out pm

### Parameters

Vdead

rest volume of oil in cylinder chamber when closed [N.s/m]

B

effective bulk modulus [Pa]

stroke

stroke length [m]

x\_initial

starting position of piston [m]

dp

piston diameter [m]

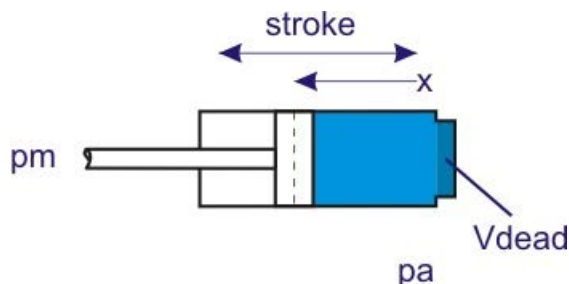
## Library

Iconic Diagrams\Hydraulics\Cylinders\Basic Cylinders

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics/Translational).

### Description

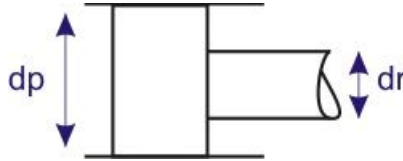


This is an ideal model of a single acting cylinder with no mass and no friction. The volume of the chamber is given by:

$$V = V_{dead} + Aa \cdot (x + x_{initial})$$

with  $Aa$  the piston area,  $x$  the piston position and  $V_{dead}$  the initial volume when piston position is zero. The piston area  $Aa$  is related to the piston diameter  $dp$  by:

$$Aa = \pi \cdot dp^2 / 4$$



There is no restriction on the travel of the piston. Only a warning is given when the maximum stroke is exceeded or the piston position gets negative.

## Interface

### Ports

pa

pm

### Description

hydraulic port

translation port

### Causality

preferred pressure out pa

preferred force out pm

### Parameters

Vdead

rest volume of oil in cylinder chamber when closed [N.s/m]

B

effective bulk modulus [Pa]

stroke

stroke length [m]

x\_initial

starting position of piston [m]

dp

piston diameter [m]

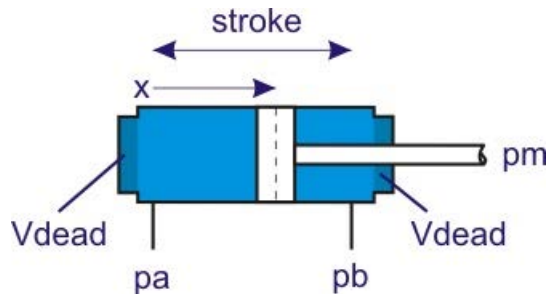
## Library

Iconic Diagrams\Hydraulics\Cylinders

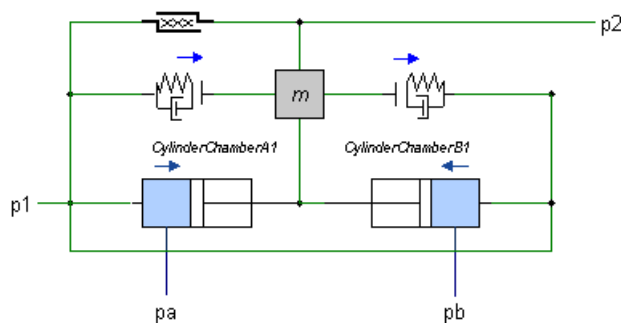
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics/Translational).

## Description



This is the extended model of a double acting cylinder with mass, friction and end stops.



The volume of the chambers is given by:

$$V_a = V_{dead} + A_a \cdot (x + x_{initial})$$

$$V_b = V_{dead} + A_b \cdot (stroke - x - x_{initial})$$

with  $A_a$  the piston area and  $A_b$  the effective area at the rod side.  $x$  is the piston position and  $V_{dead}$  the initial volume when piston position is zero. The piston areas  $A_a$  and  $A_b$  are related to the piston diameter  $dp$  and rod diameter  $dr$  by:

$$A_a = \pi \cdot dp^2 / 4$$

$$A_b = \pi \cdot dp^2 / 4 - \pi \cdot dr^2 / 4$$



The travel of the piston is restricted. At the cylinder heads two collision models prevent the piston from traveling any further. The friction between the piston and the cylinder walls is modeled by static and viscous friction.

## Interface

### Ports

pa, pb  
pm

### Description

hydraulic ports  
translation port

### Causality

preferred pressure out pa  
preferred force out pm

### Parameters

Vdead	rest volume of oil in cylinder chamber when closed, [m <sup>3</sup> ]
B	effective bulk modulus [Pa]
stroke	stroke length [m]
x_initial	starting position of piston [m]
dp	piston diameter [m]
dr	rod diameter [m]
mass	rod and piston mass [kg]
kc	stiffness during collision with cylinder heads [N/m]
dc	damping during collision with cylinder heads [N.s/m]
Fc	static friction [N]
dv	viscous friction coefficient [N.s/m]
slope	steepness of the static friction curve []

### Note

When a the cylinder piston collides with the cylinder heads, simulation may get very slow or even become unstable. In these cases you are advised to use the BDF-method with default settings. Try to change the absolute integration error until a stable simulation is obtained!



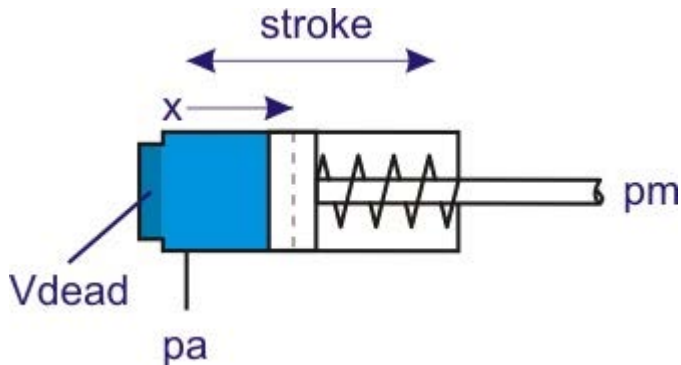
## Library

Iconic Diagrams\Hydraulics\Cylinders

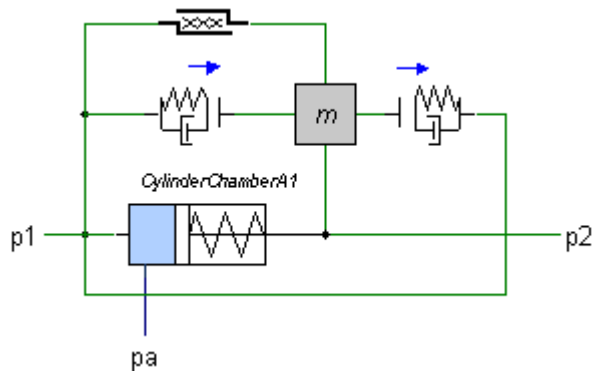
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics/Translational).

## Description



This is the extended model of a single acting cylinder with mass, friction, end stops and a return spring to drive the cylinder back when there is no pressure in the chamber.

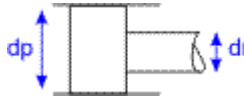


The volume of the chamber is given by:

$$V = V_{dead} + Aa \cdot (x + x_{initial})$$

with  $Aa$  the piston area,  $x$  the piston position and  $V_{dead}$  the initial volume when piston position is zero. The piston area  $Aa$  is related to the piston diameter  $dp$  by:

$$Aa = \pi * dp^2 / 4$$



The driving force of the return spring is determined by two parameters: the force for piston position zero (*Fspr\_min*) and the force when the piston is at the other side (*Fspr\_max*). The spring constant (*kspr*) and initial spring position (*x0*) are calculated out of these parameters by:

$$kspr = (Fspr\_max - Fspr\_min) / stroke$$

$$x0 = -Fspr\_min / kspr$$

The travel of the piston is restricted. At the cylinder heads two collision models prevent the piston from traveling any further. The friction between the piston and the cylinder walls is modeled by static and viscous friction.

## Interface

### Ports

pa	hydraulic port
pm	translation port

### Causality

preferred pressure out pa  
preferred force out pm

### Parameters

Vdead	rest volume of oil in cylinder chamber when closed [m3]
B	effective bulk modulus [Pa]
stroke	stroke length [m]
x_initial	starting position of piston [m]
dp	piston diameter [m]
mass	rod and piston mass [kg]
kc	stiffness during collision with cylinder heads [N/m]
dc	damping during collision with cylinder heads [N.s/m]
Fc	static friction [N]
dv	viscous friction coefficient [N.s/m]
slope	steepness of the static friction curve []

### Note

When a the cylinder piston collides with the cylinder heads, simulation may get very slow or even become unstable. In these cases you are advised to use the BDF-method with default settings. Try to change the absolute integration error until a stable simulation is obtained!

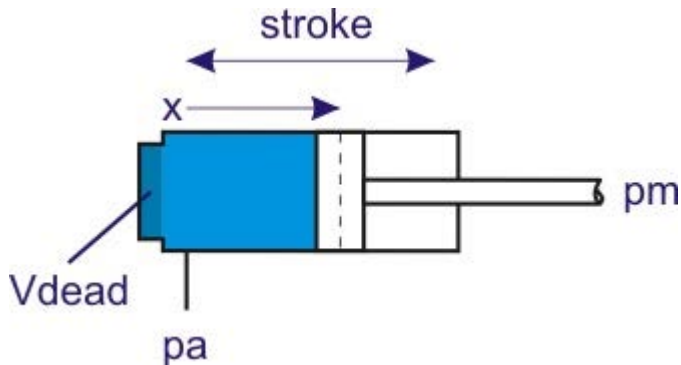
## Library

Iconic Diagrams\Hydraulics\Cylinders

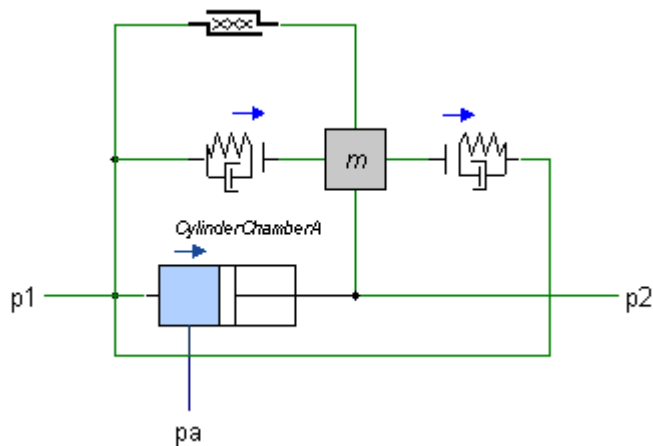
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics/Translational).

## Description



This is the extended model of a single acting cylinder with mass, friction and end stops.

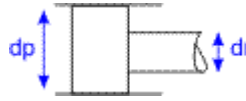


The volume of the chamber is given by:

$$V = V_{dead} + Aa \cdot (x + x_{initial})$$

with  $Aa$  the piston area,  $x$  the piston position and  $V_{dead}$  the initial volume when piston position is zero. The piston area  $Aa$  is related to the piston diameter  $dp$  by:

$$Aa = \pi * dp^2 / 4$$



The travel of the piston is restricted. At the cylinder heads two collision models prevent the piston from traveling any further. The friction between the piston and the cylinder walls is modeled by static and viscous friction.

## Interface

### Ports

pa	hydraulic port
pm	translation port

### Causality

preferred pressure out pa  
preferred force out pm

### Parameters

Vdead	rest volume of oil in cylinder chamber when closed [m3]
B	effective bulk modulus [Pa]
stroke	stroke length [m]
x_initial	starting position of piston [m]
dp	piston diameter [m]
mass	rod and piston mass [kg]
kc	stiffness during collision with cylinder heads [N/m]
dc	damping during collision with cylinder heads [N.s/m]
Fc	static friction [N]
dv	viscous friction coefficient [N.s/m]
slope	steepness of the static friction curve []

### Note

When a the cylinder piston collides with the cylinder heads, simulation may get very slow or even become unstable. In these cases you are advised to use the BDF-method with default settings. Try to change the absolute integration error until a stable simulation is obtained!

**Library**

Iconic Diagrams\Hydraulics\Pumps\Basic Pumps

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

**Description**

This model describes an ideal motor with an axial speed that is proportional to the input flow rate:

$$p_a.\phi = p_b.\phi = i * p_{rot}.\omega;$$

$$i = D / (2 * \pi);$$

The torque is equal to:

$$p.T = i * (p_a.p - p_b.p);$$

If the port pressure is smaller than the vapour pressure ( $p < p_{vapour}$ ), the flow is zero. If the port pressure becomes larger than the vapour pressure the flow gradually grows to its normal value, until the atmospheric pressure ( $p = 0$ ) is reached.

**Interface**

Ports	Description
pa	inlet port (hydraulic)
pb	outlet port (hydraulic)
p_rot	axis (rotation)

**Causality**

fixed volume flow  
 out pa  
 fixed volume flow  
 out pb  
 fixed torque out  
 p\_rot

**Parameters**

D displacement per revolution [m3]

## Library

Iconic Diagrams\Hydraulics\Pumps\Basic Pumps

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description

This model describes an ideal pump with a displacement that is proportional to the speed of the input axis:

$$\begin{aligned} p_a.\phi &= p_b.\phi = i * p_{rot}.\omega; \\ i &= D / (2*\pi); \end{aligned}$$

The torque is equal to:

$$p.T = i*(p_a.p - p_b.p);$$

If the inlet pressure is smaller than the vapour pressure ( $p < p_{vapour}$ ), the flow is zero. If the inlet pressure is larger than the vapour pressure the flow gradually grows to its normal value, until the atmospheric pressure ( $p = 0$ ) is reached.

### Interface

Ports	Description
pa	inlet port (hydraulic)
pb	outlet port (hydraulic)
p_rot	axis (rotation)

### Causality

fixed volume flow  
out pa  
fixed volume flow  
out pb  
preferred angular  
velocity out p\_rot

### Parameters

D displacement per revolution [m<sup>3</sup>]

## Library

Iconic Diagrams\Hydraulics\Pumps\Basic Pumps

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description

This model represents an ideal flow source with a fixed flow given by the parameter phi:

$$p.\phi = \phi;$$

The model has no leakage.

## Interface

### Ports Description

p

### Causality

fixed volume flow

out p

### Parameters

phi Volume flow [m<sup>3</sup>/s]

## Library

Iconic Diagrams\Hydraulics\Pumps\Basic Pumps

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description

This model represents an ideal flow source with a variable flow that is given by input signal *phi*:

$$p.\phi = \phi;$$

The model has no leakage.

## Interface

### Ports Description

p

### Causality

fixed volume flow

out p

### Input

phi Volume flow [m<sup>3</sup>/s]

**Library**

Iconic Diagrams\Hydraulics\Pumps\Basic Pumps

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

**Description**

This model represents an ideal pressure source with a fixed pressure given by the parameter pressure:

$$p.p = pressure;$$

The model has no leakage.

**Interface**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p	
---	--

**Causality**

fixed pressure out

**Input**

pressure	Pressure [Pa]
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**Library**

Iconic Diagrams\Hydraulics\Pumps\Basic Pumps

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

**Description**

This model represents an ideal pressure source with a fixed pressure given by the parameter pressure:

$$p.p = pressure;$$

The model has no leakage.

**Interface**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p	
---	--

**Causality**

fixed pressure out

**Parameters**

p	Pressure [Pa]
---	---------------



## Library

Iconic Diagrams\Hydraulics\Pumps\Basic Pumps

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description

This model describes an ideal motor with an axial speed that is proportional to the input flow rate:

$$p_a.\phi = p_b.\phi = i * p_{rot}.\omega;$$

$$i = D * c / (2*\pi);$$

The torque is equal to:

$$p.T = i*(p_a.p - p_b.p);$$

The displacement is controllable by the input signal c. For a positive rotation of the driving axis the flow is:

$$\begin{array}{ll} c \geq 1 & \text{maximum flow from port 1 to port 2} \\ c = 0 & \text{zero flow} \\ c \leq -1 & \text{maximum flow from port 2 to port 1} \end{array}$$

If the port pressure is smaller than the vapour pressure ( $p < p_{vapour}$ ), the flow is zero. If the port pressure becomes larger than the vapour pressure the flow gradually grows to its normal value, until the atmospheric pressure ( $p = 0$ ) is reached.

## Interface

Ports	Description
pa	inlet port (hydraulic)
pb	outlet port (hydraulic)
p_rot	axis (rotation)

## Causality

fixed volume flow  
out pa  
fixed volume flow  
out pb  
fixed torque out  
p\_rot

## Input

c relative displacement

## Parameters

D displacement per revolution [m3]

## Library

Iconic Diagrams\Hydraulics\Pumps\Basic Pumps

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description

This model describes an ideal pump with a displacement that is proportional to the speed of the input axis:

$$\begin{aligned} p_a.\phi &= p_b.\phi = i * p_{rot}.\omega; \\ i &= D * c / (2 * \pi); \end{aligned}$$

The torque is equal to:

$$p.T = i * (p_b.p - p_a.p);$$

The displacement is controllable by the input signal  $c$ . For a positive rotation of the driving axis the flow is:

$$\begin{aligned} c &\geq 1 && \text{maximum flow from port 1 to port 2} \\ c &= 0 && \text{zero flow} \\ c &\leq -1 && \text{maximum flow from port 2 to port 1} \end{aligned}$$

If the port pressure is smaller than the vapour pressure ( $p < p_{vapour}$ ), the flow is zero. If the port pressure is larger than the vapour pressure the flow gradually grows to its normal value, until the atmospheric pressure ( $p = 0$ ) is reached.

## Interface

Ports	Description
$p_a$	inlet port (hydraulic)
$p_b$	outlet port (hydraulic)
$p_{rot}$	axis (rotation)

## Causality

fixed volume flow  
out  $p_a$   
fixed volume flow  
out  $p_b$   
fixed torque out  
 $p_{rot}$

## Input

$c$  relative displacement

## Parameters

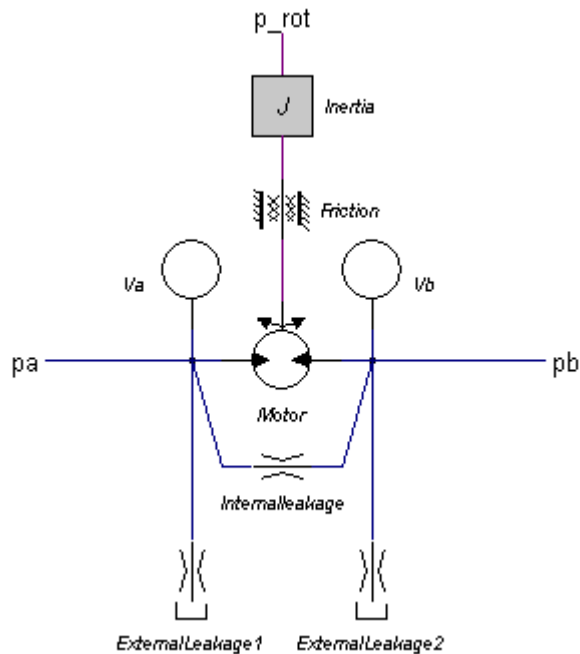
$D$  displacement per revolution [m<sup>3</sup>]

## Library

Iconic Diagrams\Hydraulics\Pumps

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).



## Description

This model describes an motor with internal and external leakage and an axial speed that is proportional to the input flow rate:

$$p_a.\phi = p_b.\phi = i * p_{rot}.\omega;$$

$$i = D / (2 * \pi);$$

The actual flows at the inlet and outlet port may be slightly different because of the flow into the lumped volumes and the leakage flows. The leakage flows are modeled by laminar resistances. The torque is equal to:

$$p.T = i * (p_a.p - p_b.p);$$

If the port pressure is smaller than the vapour pressure ( $p < p_{vapour}$ ), the flow is zero. If the port pressure is larger than the vapour pressure the flow gradually grows to its normal value, until the atmospheric pressure ( $p = 0$ ) is reached.

## Interface

### Ports

pa	inlet port (hydraulic)
pb	outlet port (hydraulic)
p_rot	axis (rotation)

### Causality

preferred pressure out pa  
 preferred pressure out pb  
 preferred angular velocity out  
 p\_rot

### Parameters

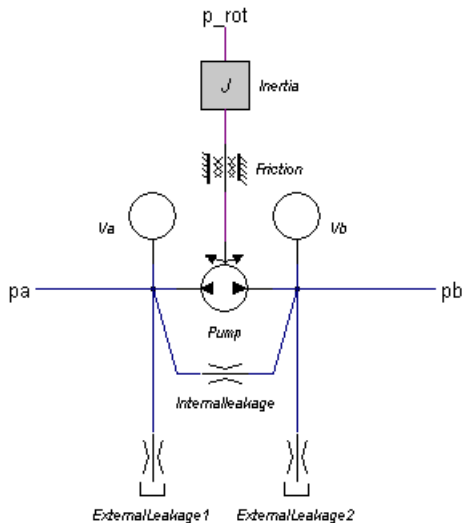
ExternalLeakage1\p_preload	Tank pressure [Pa]
ExternalLeakage1\G	Conductance of laminar resistance [m3/s.Pa]
ExternalLeakage2\p_preload	Tank pressure [Pa]
ExternalLeakage2\G	Conductance of laminar resistance [m3/s.Pa]
InternalLeakage\G	Conductance of laminar resistance [m3/s.Pa]
Va\V	Volume of oil under pressure [m3]
Va\B	Effective bulk modulus [Pa]
Va\p_initial	The starting pressure of the volume [Pa]
Vb\V	Volume of oil under pressure [m3]
Vb\B	Effective bulk modulus [Pa]
Vb\p_initial	The starting pressure of the volume [Pa]
Motor\D	Displacement per revolution [m3]
Friction\d	Damping [N.m.s/rad]
Inertia\J	Moment of inertia [kg.m2]

Library

Iconic Diagrams\Hydraulics\Pumps

Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).



Description

This model describes a pump with internal and external leakage and a displacement that is proportional to the speed of the input axis:

$$i = D * c / (2 * \pi);$$
$$pa.\phi = pb.\phi = i * p\_rot.\omega;$$

The actual flows at the inlet and outlet port may be slightly different because of the flow into the lumped volumes and the leakage flows. The leakage flows are modeled by laminar resistances. The torque of the pump is equal to:

$$p.T = i * (pa.p - pb.p);$$

If the inlet pressure is smaller than the vapour pressure( $p < p\_vapour$ ), the flow is zero. If the inlet pressure becomes larger than the vapour pressure the flow gradually grows to its normal value, until the atmospheric pressure ( $p = 0$ ) is reached.

Interface

Ports

pa  
pb

Description

inlet port (hydraulic)  
outlet port (hydraulic)

p\_rot axis (rotation)

## Causality

preferred pressure out pa

preferred pressure out pa

preferred angular velocity out

p\_rot

## Parameters

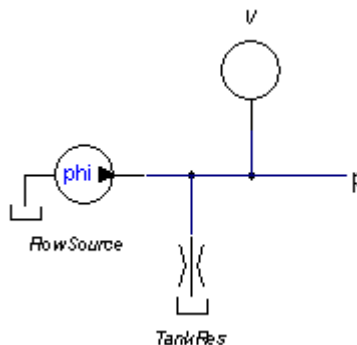
ExternalLeakage1\p_preload	Tank pressure [Pa]
ExternalLeakage1\G	Conductance of laminar resistance [m <sup>3</sup> /s.Pa]
ExternalLeakage2\p_preload	Tank pressure [Pa]
ExternalLeakage2\G	Conductance of laminar resistance [m <sup>3</sup> /s.Pa]
InternalLeakage\G	Conductance of laminar resistance [m <sup>3</sup> /s.Pa]
Va\V	Volume of oil under pressure [m <sup>3</sup> ]
Va\B	Effective bulk modulus [Pa]
Va\p_initial	The starting pressure of the volume [Pa]
Vb\V	Volume of oil under pressure [m <sup>3</sup> ]
Vb\B	Effective bulk modulus [Pa]
Vb\p_initial	The starting pressure of the volume [Pa]
Pump\D	Displacement per revolution [m <sup>3</sup> ]
Friction\d	Damping [N.m.s/rad]
Inertia\J	Moment of inertia [kg.m <sup>2</sup> ]

## Library

Iconic Diagrams\Hydraulics\Pumps

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).



### Description

This model represents a flow source with a fixed flow and leakage. The flow is given by the parameter *phi*:

$$p.\phi = \phi - G \cdot p;$$

The actual flow at the outlet port may be slightly different because of the flow into the lumped volume at the outlet port and the leakage flow.

## Interface

### Ports Description

p

### Causality

fixed volume flow out p

### Input

phi Volume flow [m3/s]

### Parameters

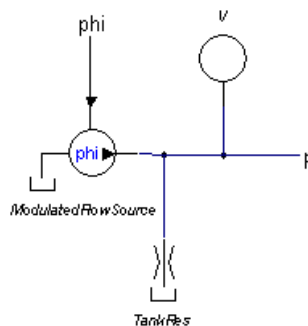
FlowSource\phi	Volume flow [m3/s]
TankRes\p_preload	Tank pressure [Pa]
TankRes\G	Conductance of laminar resistance [m3/s.Pa]
V\V	Volume of oil under pressure [m3]
V\B	Effective bulk modulus [Pa]
V\p_initial	The starting pressure of the volume [Pa]

## Library

Iconic Diagrams\Hydraulics\Pumps

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).



## Description

This model represents a flow source with a variable flow and leakage. The variable flow is given by an input signal:

$p.\phi = \phi - G \cdot p.p;$

The actual flow at the outlet port may be slightly different because of the flow into the lumped volume at the outlet port and the leakage flow.

**Interface**

Ports	Description
-------	-------------

p

**Causality**

fixed volume flow out p

**Input**

phi	Volume flow [m3/s]
-----	--------------------

**Parameters**

TankRes\p_preload	tank pressure [Pa]
TankRes\G	Conductance of laminar resistance [m3/s.Pa]
V\V	Volume of oil under pressure [m3]
V\B	Effective bulk modulus [Pa]
V\p_initial	The starting pressure of the volume [Pa]

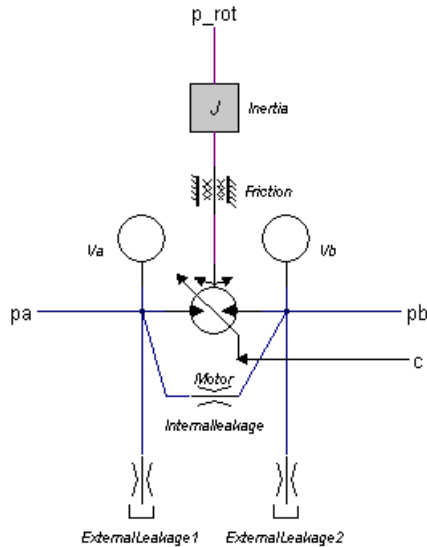


## Library

Iconic Diagrams\Hydraulics\Pumps

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).



## Description

This model describes an motor with internal and external leakage and an axial speed that is proportional to input flow rate:

$$p_a.\phi = p_b.\phi = i * p_{rot}.\omega;$$

$$i = D / (2 * \pi);$$

The actual flows at the inlet and outlet port may be slightly different because of the flow into the lumped volumes and the leakage flows. The leakage flows are modeled by laminar resistances. The torque is equal to:

$$p.T = i * (p_a.p - p_b.p);$$

The displacement is controllable by the input signal  $c$ . For a positive rotation of the driving axis the flow is:

$c \geq 1$	maximum flow from port 1 to port 2
$c = 0$	zero flow
$c \leq -1$	maximum flow from port 2 to port 1

If the port pressure is smaller than the vapour pressure ( $p < p_{\text{vapour}}$ ), the flow is zero. If the port pressure is larger than the vapour pressure the flow gradually grows to its normal value, until the atmospheric pressure ( $p = 0$ ) is reached.

## Interface

### Ports

pa	inlet port (hydraulic)
pb	outlet port (hydraulic)
p_rot	axis (rotation)

### Causality

preferred pressure out pa  
 preferred pressure out pb  
 preferred angular velocity out p\_rot

### Input

c	relative displacement
---	-----------------------

### Parameters

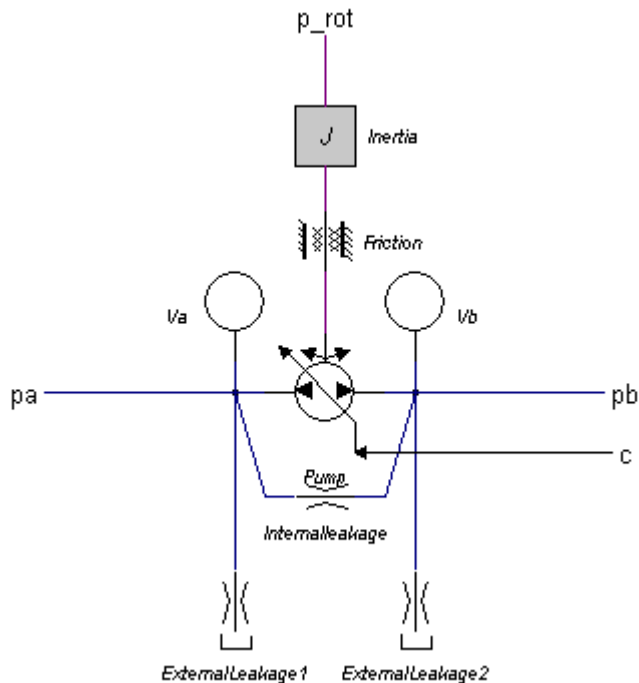
ExternalLeakage1\p_preload	Tank pressure [Pa]
ExternalLeakage1\G	Conductance of laminar resistance [m <sup>3</sup> /s.Pa]
ExternalLeakage2\p_preload	Tank pressure [Pa]
ExternalLeakage2\G	Conductance of laminar resistance [m <sup>3</sup> /s.Pa]
InternalLeakage\G	Conductance of laminar resistance [m <sup>3</sup> /s.Pa]
Va\V	Volume of oil under pressure [m <sup>3</sup> ]
Va\B	Effective bulk modulus [Pa]
Va\p_initial	The starting pressure of the volume [Pa]
Vb\V	Volume of oil under pressure [m <sup>3</sup> ]
Vb\B	Effective bulk modulus [Pa]
Vb\p_initial	The starting pressure of the volume [Pa]
Motor\D	Displacement per revolution [m <sup>3</sup> ]
Friction\d	Damping [N.m.s/rad]
Inertia\J	Moment of inertia [kg.m <sup>2</sup> ]

## Library

Iconic Diagrams\Hydraulics\Pumps

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).



## Description

This model describes a pump with internal and external leakage and a displacement that is proportional to the speed of the input axis:

$$i = D * c / (2 * \pi);$$

$$p_a.\phi = p_b.\phi = i * p\_rot.\omega;$$

The actual flows at the inlet and outlet port may be slightly different because of the flow into the lumped volumes and the leakage flows. The leakage flows are modeled by laminar resistances. The torque of the pump is equal to:

$$p.T = i * (p_a.p - p_b.p);$$

The displacement is controllable by the input signal  $c$ . For a positive rotation of the driving axis the flow is:

$c \geq 1$	maximum flow from port 1 to port 2
$c = 0$	zero flow

$c \leq -1$       *maximum flow from port 2 to port 1*

If the port pressure is smaller than the vapour pressure ( $p < p_{\text{vapour}}$ ), the flow is zero. If the port pressure becomes larger than the vapour pressure the flow gradually grows to its normal value, until the atmospheric pressure ( $p = 0$ ) is reached.

## Interface

### Ports

pa	inlet port (hydraulic)
pb	outlet port (hydraulic)
p_rot	axis (rotation)

### Causality

preferred pressure out pa  
 preferred pressure out pb  
 preferred angular velocity out p\_rot

### Input

c      relative displacement

### Parameters

ExternalLeakage1\p_preload	Tank pressure [Pa]
ExternalLeakage1\G	Conductance of laminar resistance [m3/s.Pa]
ExternalLeakage2\p_preload	Tank pressure [Pa]
ExternalLeakage2\G	Conductance of laminar resistance [m3/s.Pa]
InternalLeakage\G	Conductance of laminar resistance [m3/s.Pa]
Va\V	Volume of oil under pressure [m3]
Va\B	Effective bulk modulus [Pa]
Va\p_initial	The starting pressure of the volume [Pa]
Vb\V	Volume of oil under pressure [m3]
Vb\B	Effective bulk modulus [Pa]
Vb\p_initial	The starting pressure of the volume [Pa]
Pump\D	Displacement per revolution [m3]
Friction\d	Damping [N.m.s/rad]
Inertia\J	Moment of inertia [kg.m2]

## Library

Iconic Diagrams\Hydraulics\Restrictions

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description

This model describes the laminar flow through a component:

$$pa.\phi = pb.\phi = G \cdot (pa.p - pb.p);$$

The pressure at both ports has a lower limit which is equal to the vapour pressure. Therefore the actual equations used in this component are:

$$\begin{aligned} p1\_lim &= \text{if } pa.p < p\_vapour \text{ then } p\_vapour \text{ else } pa.p \text{ end;} \\ p2\_lim &= \text{if } pb.p < p\_vapour \text{ then } p\_vapour \text{ else } pb.p \text{ end;} \\ dp &= p1\_lim - p2\_lim; \\ pa.\phi &= G \cdot dp; \\ pb.\phi &= pa.\phi; \end{aligned}$$

There is no check on the validity of laminar flow in this component!

### Interface

Ports	Description
pa, pb	Both terminals of the hydraulic component.

### Causality

fixed volume flow  
out pa  
fixed volume flow  
out pb

### Parameters

G Conductance of laminar resistance [m<sup>3</sup>/s.Pa], G >= 0!.

## Library

Iconic Diagrams\Hydraulics\Restrictions

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

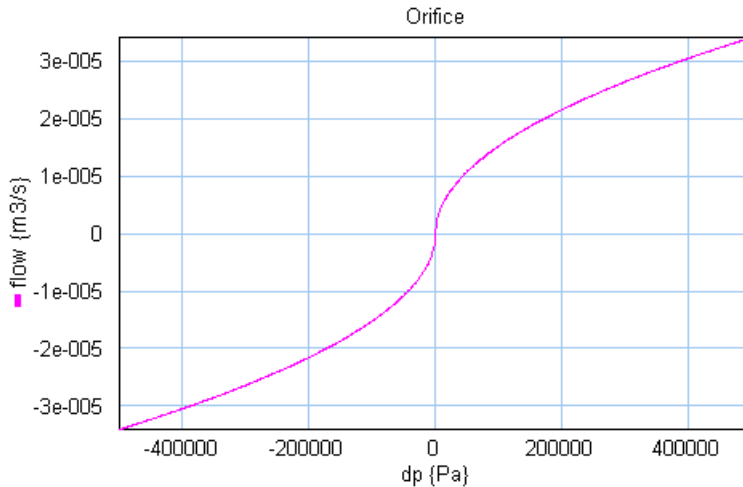
### Description

This model describes the laminar/turbulent flow through an orifice if no cavitation occurs. The flow depends on the pressure difference:

$$dp = pa.p - pb.p$$

$$phi = sign(dp) * Cd * A * sqrt( (2/rho) * abs(dp) ) + GLeak * dp;$$

Here  $Cd$  is the discharge coefficient which normally has a value between 0.55 and 0.7 and  $A$  is the area of the orifice opening.  $GLeak$  is the conductance of laminar leakage flow when the valve is closed.



The pressure at both ports has a lower limit that is equal to the vapour pressure. Therefore the actual equations used in this component are:

$$p1\_lim = \text{if } pa.p < p\_vapour \text{ then } p\_vapour \text{ else } pa.p \text{ end};$$

$$p2\_lim = \text{if } pb.p < p\_vapour \text{ then } p\_vapour \text{ else } pb.p \text{ end};$$

$$dp = p1\_lim - p2\_lim;$$

## Interface

### Ports

pa, pb

### Description

Both terminals of the hydraulic component.

### Causality

fixed volume flow

out pa

fixed volume flow

out pb

### Parameters

rho

Mass density of the fluid [kg/m³].

GLeak

Conductance of the laminar leakage flow [m³/s.Pa],  $GLeak \geq 0$ !

A

Orifice Area [m²],  $A \geq 0$ !

Cd

Discharge coefficient [].

## Library

Iconic Diagrams\Hydraulics\Restrictions

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description

This model describes the laminar flow through a component:

$$pa.\phi = pb.\phi = G \cdot (pa.p - pb.p);$$

The variable conductance  $G$  is given by an input signal. The pressure at both ports has a lower limit that is equal to the vapour pressure. Therefore the actual equations used in this component are:

$$\begin{aligned} p1\_lim &= \text{if } pa.p < p\_vapour \text{ then } p\_vapour \text{ else } pa.p \text{ end;} \\ p2\_lim &= \text{if } pb.p < p\_vapour \text{ then } p\_vapour \text{ else } pb.p \text{ end;} \\ dp &= p1\_lim - p2\_lim; \\ pa.\phi &= G \cdot dp; \\ pb.\phi &= pa.\phi; \end{aligned}$$

There is no check on the validity of laminar flow in this component!

### Interface

#### Ports

pa, pb

#### Description

Both terminals of the hydraulic component.

#### Causality

fixed volume flow

out pa

fixed volume flow

out pb

#### Input

$G$

Conductance of laminar resistance [ $\text{m}^3/\text{s} \cdot \text{Pa}$ ],  $G \geq 0$ .

## Library

Iconic Diagrams\Hydraulics\Restrictions

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

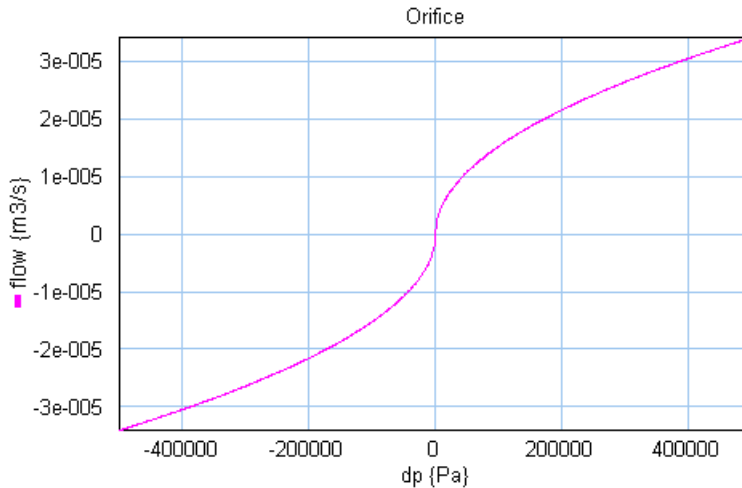
### Description

This model describes the laminar/turbulent flow through an orifice if no cavitation occurs. The flow depends on the pressure difference:

$$dp = pa.p - pb.p;$$

$$phi = sign(dp) * Cd * A * sqrt( (2/rho) * abs(dp) ) + GLeak * dp;$$

Here  $Cd$  is the discharge coefficient that normally has a value between 0.55 and 0.7 and  $A$  is the area of the orifice opening. The area  $A$  is given as an input signal.



The pressure at both ports has a lower limit that is equal to the vapour pressure. Therefore the actual equations used in this component are:

$$p1\_lim = \text{if } pa.p < p\_vapour \text{ then } p\_vapour \text{ else } pa.p \text{ end};$$

$$p2\_lim = \text{if } pb.p < p\_vapour \text{ then } p\_vapour \text{ else } pb.p \text{ end};$$

$$dp = p1\_lim - p2\_lim;$$

## Interface

### Ports

pa, pb

### Description

Both terminals of the hydraulic component.

### Causality

fixed volume flow

out pa

fixed volume flow

out pb

### Input

A

Orifice Area [m<sup>2</sup>],  $A \geq 0$ .

### Parameters

rho

Mass density of the fluid [kg/m<sup>3</sup>].

GLeak

Conductance of the laminar leakage flow [m<sup>3</sup>/s.Pa],  $GLeak \geq 0$ !

Cd

Discharge coefficient [],  $Cd \geq 0$ !



**Library**

Iconic Diagrams\Hydraulics\Sensors

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

**Description**

This model gives the measured flow as an output signal. The port p of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.\phi &= p_{\_high}.\phi = p_{\_low}.\phi; \\ p.p &= p_{\_high}.p - p_{\_low}.p; \\ p.p &= 0; \\ \phi &= p.\phi; \end{aligned}$$

The model has no leakage.

**Interface**

Ports	Description
-------	-------------

p	
---	--

**Causality**

fixed volume flow	
-------------------	--

out	
-----	--

**Output**

phi	Volume flow [m3/s]
-----	--------------------

**Library**

Iconic Diagrams\Hydraulics\Sensors

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

**Description**

This model gives the power that is tranferred over a hydraulic line:

$$\begin{aligned} p_{\_high}.p &= p_{\_low}.p; \\ p_{\_high}.\phi &= p_{\_low}.\phi; \\ P &= p_{\_high}.\phi * p_{\_high}.p; \end{aligned}$$

The model has no leakage.

**Interface**

Ports	Description
-------	-------------

p

**Causality**

indifferent

**Output**

P                      Power [W].

**Library**

Iconic Diagrams\Hydraulics\Sensors

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).**Description**

This model gives the measured pressure as an output signal:

$$\begin{aligned} pressure &= p.p; \\ p.phi &= 0; \end{aligned}$$

The model has no leakage.

**Interface**

Ports	Description
-------	-------------

p

**Causality**

fixed volume flow

out

**Output**

pressure                      Absolute velocity [m/s].

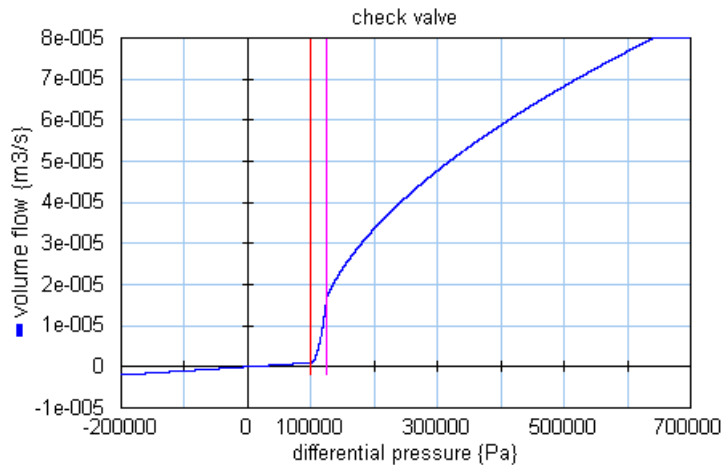
**Library**

Iconic Diagrams\Hydraulics\Valves\Basic Valves

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).**Description**

This model describes a spring-loaded check valve. The resistance depends on the pressure difference:

$dp < p_{closed} \Rightarrow$  valve closed, only leakage:  $pa.\phi = pb.\phi = dp * G_{Leak}$   
 $p_{closed} < dp < p_{open} \Rightarrow$  working range, i. e. valve partially opened  
 $p_{open} < dp \Rightarrow$  valve wide open:  $pa.\phi = pb.\phi = C_d * A * \sqrt{dp - p_{closed}}$ ;



## Interface

### Ports

pa, pb

### Description

Both terminals of the hydraulic component.

### Causality

fixed volume flow

out pa

fixed volume flow

out pb

### Parameters

pclosed

Valve is closed under this pressure [Pa].

popen

Valve is fully open above this pressure [Pa].

GLeak

Conductance of closed valve [m³/s.Pa].

A

Maximum valve area when the valve is open [m²],  $A \geq 0$ !

Cd

Discharge coefficient [].

## Library

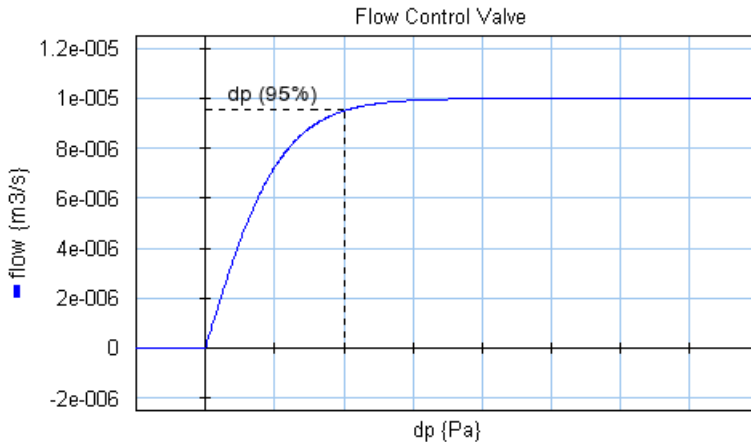
Iconic Diagrams\Hydraulics\Valves\Basic Valves

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description

Flow control valves have the purpose to provide a constant flow, independent of the downstream pressure. The flow is obtained by means of a pressure difference controller using the pressure drop over an orifice. Therefore flow control valves always need a certain pressure drop before the desired flow can be achieved.



In this model the flow is modeled by an tanh function. The pressure drop is defined as the pressure where 95% of the desired flow rate is achieved.

```

dp = pa.p - pb.p
phi = if dp > 0 then
  phi*arctanh( (arctan(0.95)/p_drop) * dp) + GLeak * dp;
else
  GLeak * dp
end;

```

Here *phi* is the desired flow and *p\_drop* is the 95% pressure drop. *GLeak* is the conductance of laminar leakage flow when the valve is closed. The pressure at both ports has a lower limit that is equal to the vapour pressure. Therefore the actual equations used in this model are:

```

p1_lim = if pa.p < p_vapour then p_vapour else pa.p end;
p2_lim = if pb.p < p_vapour then p_vapour else pb.p end;
dp = p1_lim - p2_lim;

```

## Interface

### Ports

pa, pb

### Description

Both terminals of the hydraulic component.

### Causality

fixed volume flow

out pa

fixed volume flow

out pb

### Parameters

phi	Desired flow [m3/s]
p_drop	pressure drop at 95% flow [Pa]
GLeak	Conductance of the laminar leakage flow [m3/s.Pa], GLeak >= 0!

### Library

Iconic Diagrams\Hydraulics\Valves\Basic Valves

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description

This model is equal to the four three way proportional valve model, except for the spool position. The spool position is rounded to 0, 1 or -1:

$$\begin{aligned} -0.5 < spoolpos < 0.5 &\Rightarrow pos = 0 \\ spoolpos \geq 0.5 &\Rightarrow pos = 1 \\ spoolpos \leq -0.5 &\Rightarrow pos = -1 \end{aligned}$$

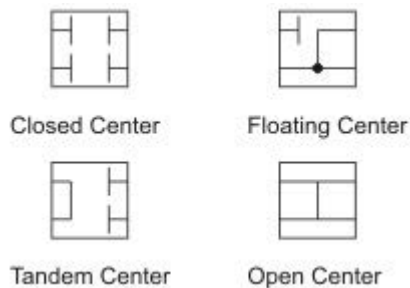
The spool dynamics is modeled by a second order transfer function:

$$sp = SO(f, d, discrete(pos))$$

which is characterized by the bandwidth ( $f$ ) and damping ( $d$ ).

### Implementation

The 4/3-way directional control valve is implemented with various spool centre configurations. The configurations are shown in the picture below:



When you drag and drop a model in the editor, you will be asked which implementation you want to choose. During modeling you can easily change the spool center configuration:

1. Select the valve model.
2. Click the right mouse button to open the right mouse menu.
3. Click *Edit Implementation* and choose another implementation.

## Interface

### Ports

pp, pt, pa, pb,

### Description

All terminals of the valve.

### Causality

fixed volume flow

out pp

fixed volume flow

out pt

fixed volume flow

out pa

fixed volume flow

out pb

### Inputs

spoolpos

position of the spool valve: 0 =closed, 1 = open

$0 \leq \text{spoolpos} \leq 1$

### Parameters

rho

Mass density of the fluid [kg/m<sup>3</sup>].

GLeak

Conductance of the laminar leakage flows [m<sup>3</sup>/s.Pa], GLeak  $\geq 0$ .

Amax

Maximum spool valve areas when the valves are open [m<sup>2</sup>], Amax  $> 0$ .

Cd

Discharge coefficient [], Cd  $> 0$ .

overlap

The valve overlaps in closed position [],  $-1 < \text{overlap} < 1$ .

f

Bandwidth of the spool dynamics [Hz], f  $> 0$ .

d

Damping of the spool dynamics [], d  $> 0$

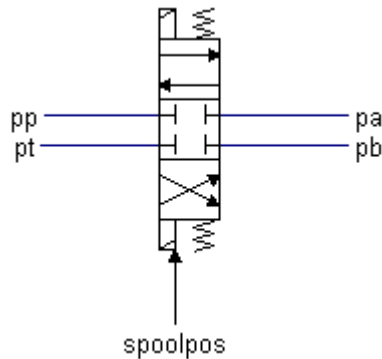
## Library

Iconic Diagrams\Hydraulics\Valves\Basic Valves

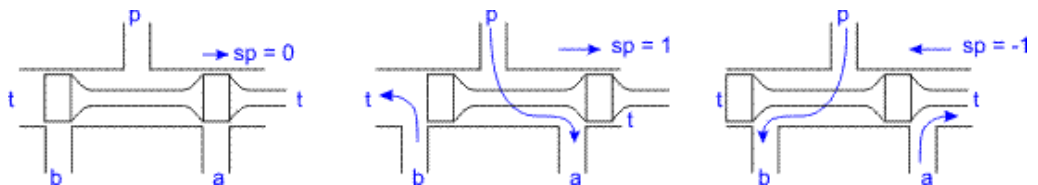
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description



This model describes a 4/3-way proportional control valve with second order spool dynamics.



The spool position is indicated by the variable  $sp$ :

$sp = -1$       Flow from  $p$  to  $b$  and  $a$  to  $t$

$-1 < sp < 0$       Partial flow from  $p$  to  $b$  and  $a$  to  $t$

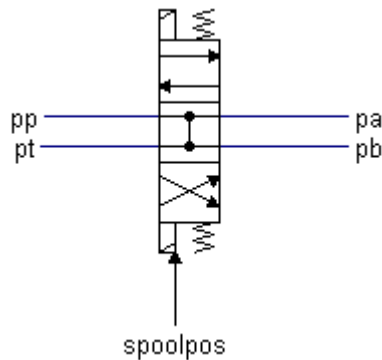
$sp = 0$       No flow

$0 < sp < 1$       Partial flow from  $p$  to  $a$  and  $b$  to  $t$

$sp = 1$       Flow from  $p$  to  $a$  and  $b$  to  $t$

The flow through the valves is described as laminar/turbulent flow through an orifice. A detailed description of the flow equations can be found in the description of the model `TwoTwoWayDirectionalValve`.

In the neutral spool position ( $sp = 0$ ) all valves are closed. A positive overlap indicates that the spool must travel a certain distance before the valves open. A negative overlap indicates that the valves are already open in the neutral position. A 4/3-way directional control valve with negative overlap could therefore also be indicated by the figure below.



The overlap is indicated by the parameter *overlap*, which is given as a fraction of the spool position. Note that overlap is only active in the neutral position. For the spool position equal to 1 or -1 the valves are completely open or completely closed.

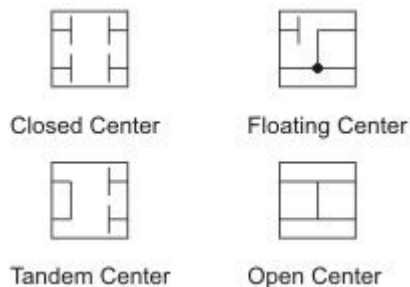
The spool position *sp* is a function of the input signal *spoolpos*:

$$sp = SO(f, d, \text{discrete}(\text{spoolpos}))$$

where *SO* is a second order transfer function to model the spool dynamics. The function is characterized by the bandwidth (*f*) and damping (*d*). The valve input position *spoolpos* should be limited to the range between -1 and 1.

## Implementation

The 4/3-way proportional control valve is implemented with various spool centre configurations. The configurations are shown in the picture below:



When you drag and drop a model in the editor, you will be asked which implementation you want to choose. During modeling you can easily change the spool center configuration:

1. Select the valve model.
2. Click the right mouse button to open the right mouse menu.
3. Click *Edit Implementation* and choose another implementation

## Interface

Ports	Description
-------	-------------



pp, pt, pa, pb, All terminals of the valve.

### Causality

fixed volume flow

out pp

fixed volume flow

out pt

fixed volume flow

out pa

fixed volume flow

out pb

### Inputs

spoolpos position of the spool valve: 0 =closed, 1 = open  
 $0 \leq \text{spoolpos} \leq 1$

### Parameters

rho Mass density of the fluid [kg/m<sup>3</sup>].

GLeak Conductance of the laminar leakage flows [m<sup>3</sup>/s.Pa], GLeak  $\geq 0$ .

Amax Maximum spool valve areas when the valves are open [m<sup>2</sup>], Amax  $> 0$ .

Cd Discharge coefficient [], Cd  $> 0$ .

overlap The valve overlaps in closed position [],  $-1 < \text{overlap} < 1$ .

f Bandwidth of the spool dynamics [Hz], f  $> 0$ .

d Damping of the spool dynamics [], d  $> 0$

## Library

Iconic Diagrams\Hydraulics\Valves\Basic Valves

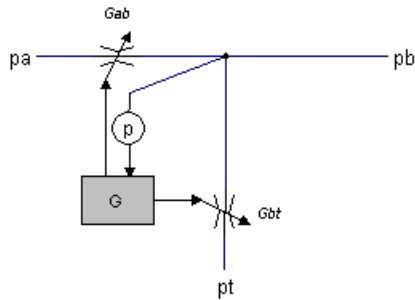
### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

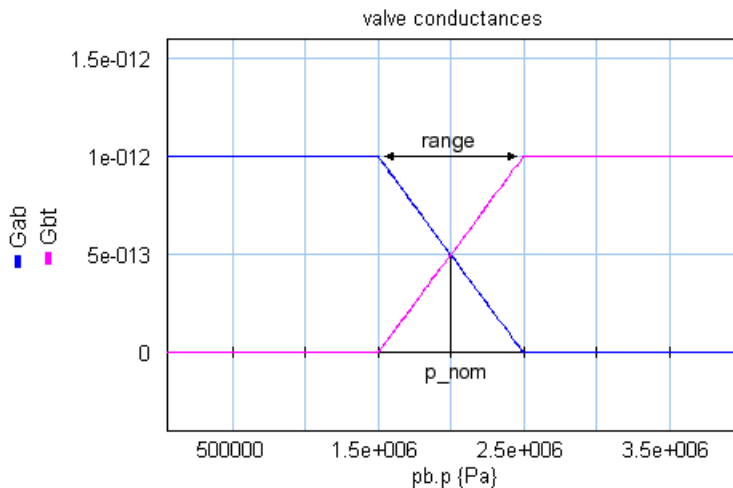
### Description

Pressure reducing valves have the purpose to provide a constant pressure ( $p_{nom}$ ), independent of the upstream pressure. They are used to limit the pressure of a primary circuit to a desired pressure for a secondary circuit.

The desired pressure ( $p_{nom}$ ) is obtained by means of a flow over a valve between an input port ( $pa$ ) and an output port ( $pb$ ). The valve is modeled by a variable conductance). Depending on the pressure downstream ( $pb.p$ ) the valve is opened (large conductance) or closed (zero conductance). Therefore pressure reducing valves always need a small flow to establish the correct downstream pressure.



When the downstream pressure ( $pb.p$ ) increases over the desired pressure a second valve opens to allow flow from the downstream port ( $pb$ ) to a third port ( $pt$ ). The third port is mostly connected to the tank.



The valves have a pressure region for opening an closing. This region is indicated by the parameter *range*.

## Interface

Ports	Description
pa	Upstream port
pb	Downstream port
pt	Relief port

## Causality

fixed volume flow  
out pa  
fixed volume flow  
out pb  
fixed volume flow  
out pt

### Parameters

$p\_nom$	Desired downstream pressure [Pa].
range	Range for opening and closing the valves [Pa].
$G_{ab}$	The maximum conductance from a to b [m <sup>3</sup> /s.Pa].
$G_{bt}$	The maximum conductance from b to t [m <sup>3</sup> /s.Pa].

### Library

Iconic Diagrams\Hydraulics\Valves\Basic Valves

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description

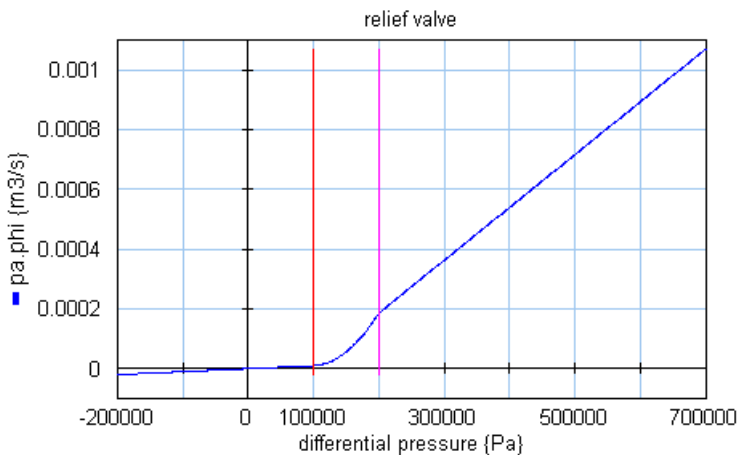
This model describes a pressure relief valve. The resistance depends on the pressure difference:

$$dp = p_a.p - p_b.p$$

$dp < p_{closed} \Rightarrow$  valve closed, only leakage:  $p_a.\phi_i = p_b.\phi_i = dp * G_{Leak}$

$p_{closed} < dp < p_{open} \Rightarrow$  working range, i. e. valve partially opened

$p_{open} < dp \Rightarrow$  valve wide open:  $p_a.\phi_i = p_b.\phi_i = dp * G_{Open}$



### Interface

#### Ports

$p_a$ ,  $p_b$

#### Description

Both terminals of the hydraulic component.

#### Causality

fixed volume flow

out pa

fixed volume flow

out pb

### Parameters

pclosed	Valve is closed under this pressure [Pa].
popen	Valve is fully open above this pressure [Pa].
GLeak	Conductance of closed valve [m3/s.Pa].
GOpen	Conductance of open valve [m3/s.Pa].

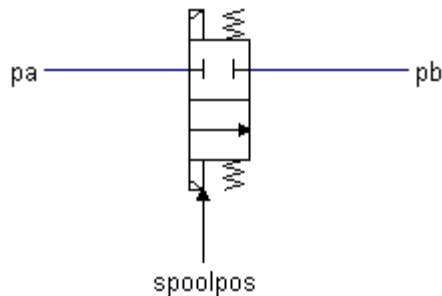
## Library

Iconic Diagrams\Hydraulics\Valves\Basic Valves

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description

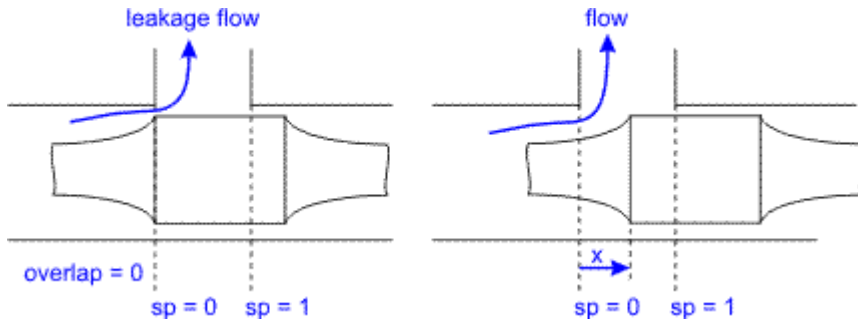


This model describes a 2/2-way directional control valve with second order spool dynamics. The flow through the valve is described as laminar/turbulent flow through an orifice:

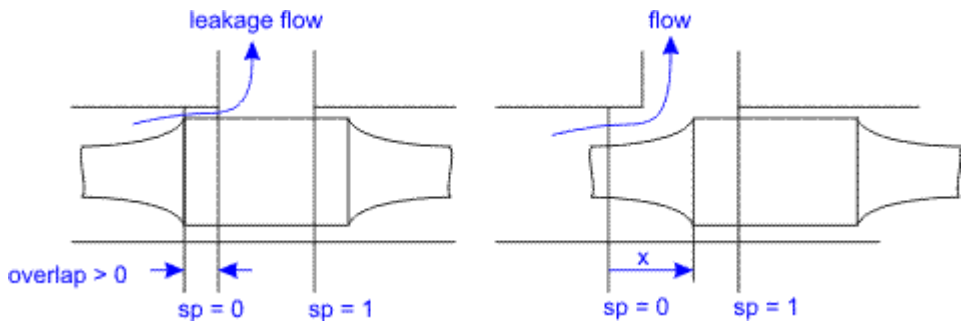
$$dp = pa.p - pb.p$$

$$phi = sign(dp) * Cd * A(sp) * sqrt( (2/rho) * abs(dp) ) + GLeak * dp;$$

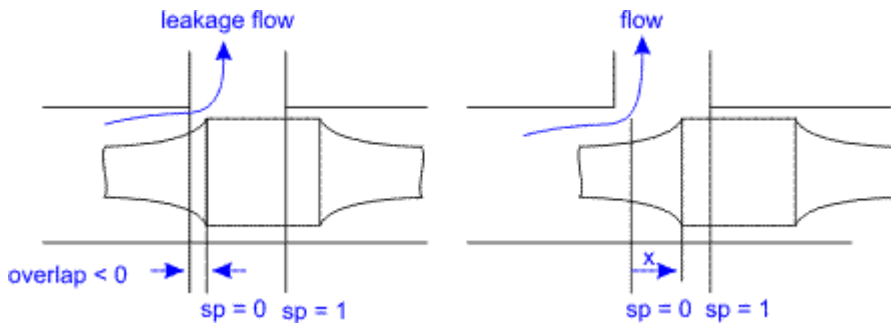
Here  $Cd$  is the discharge coefficient which normally has a value between 0.55 and 0.7.  $A(sp)$  is the area of the orifice opening.  $A(sp)$  depends linearly on the spool position  $sp$  and varies between 0 ( $sp = 0$ ) and the maximum area  $A_{max}$  ( $sp = 1$ ).  $GLeak$  is the conductance of laminar leakage flow when the valve is closed. The relative opening of the spool valve is indicated by  $sp$ . For a closed valve the spool position ( $sp$ ) is equal to zero and for an open valve the spool position ( $sp$ ) is equal to 1.



In the neutral spool position ( $sp = 0$ ) the valve is just closed. A positive overlap indicates that the spool must travel a certain distance before the valve opens.



A negative overlap indicates that the valve is already open in the neutral position.



The overlap is indicated by the parameter `overlap`, which is given as a fraction of the spool position.

The spool position  $sp$  is a function of the input signal `spoolpos`:

$$sp = SO(f, d, discrete(spoolpos))$$

where *SO* is a second order transfer function to model the spool dynamics. The function is characterized by the bandwidth (*f*) and damping (*d*). The model acts as a directional valve (a valve which is either open or closed) because the input signal *spoolpos* is rounded to 0 or 1:

$$\begin{aligned} \text{spoolpos} < 0.5 &=> 0 \\ \text{spoolpos} >= 0.5 &=> 1 \end{aligned}$$

The pressure at both ports has a lower limit which is equal to the vapour pressure. Therefore the actual equations used in this component are:

$$\begin{aligned} p_{a\_lim} &= \text{if } p_{a.p} < p_{\text{vapour}} \text{ then } p_{\text{vapour}} \text{ else } p_{a.p} \text{ end;} \\ p_{b\_lim} &= \text{if } p_{b.p} < p_{\text{vapour}} \text{ then } p_{\text{vapour}} \text{ else } p_{b.p} \text{ end;} \end{aligned}$$

## Interface

Ports	Description
pa, pb	Both terminals of the valve.

### Causality

fixed volume flow  
out pa  
fixed volume flow  
out pb

### Inputs

spoolpos	position of the spool valve
	spoolpos < 0.5 => valve is closed
	spoolpos >= 0.5 => valve is open

### Parameters

rho	Mass density of the fluid [kg/m3].
GLeak	Conductance of the laminar leakage flow [m3/s.Pa], GLeak >= 0.
Amax	Maximum spool valve area when the valve is open [m2], Amax > 0.
Cd	Discharge coefficient [], Cd > 0.
overlap	The valve overlap in closed position [], -1 < overlap < 1.
f	Bandwidth of the spool dynamics [Hz], f > 0.
d	Damping of the spool dynamics [], d > 0.

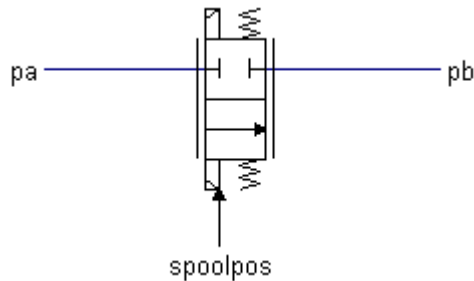
## Library

Iconic Diagrams\Hydraulics\Valves\Basic Valves

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description

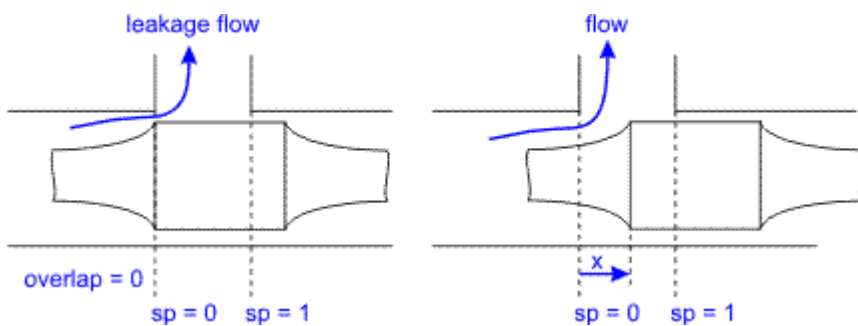


This model describes a 2/2-way proportional control valve with second order spool dynamics. The flow through the valve is described as laminar/turbulent flow through an orifice:

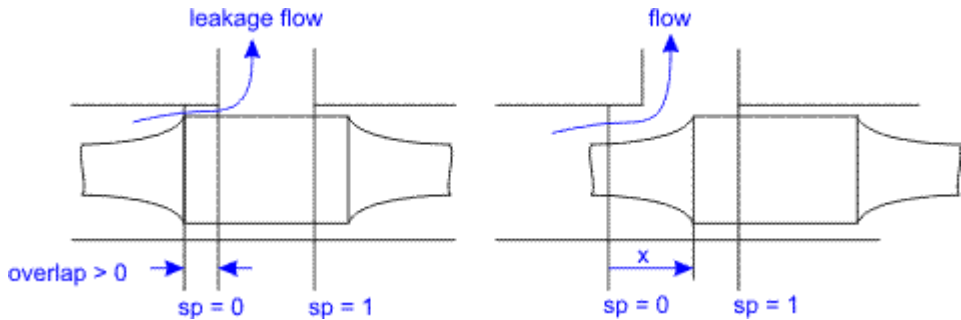
$$dp = pa.p - pb.p$$

$$phi = sign(dp) * Cd * A(sp) * sqrt( (2/rho) * abs(dp) ) + GLeak * dp;$$

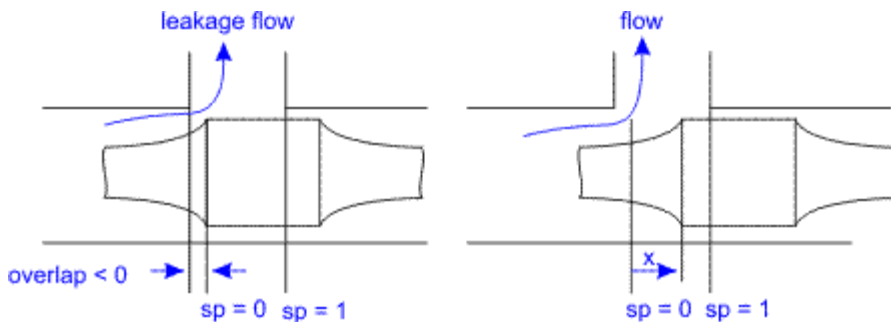
Here  $Cd$  is the discharge coefficient which normally has a value between 0.55 and 0.7.  $A(sp)$  is the area of the orifice opening.  $A(sp)$  depends linearly on the spool position  $sp$  and varies between 0 ( $sp = 0$ ) and the maximum area  $A_{max}$  ( $sp = 1$ ).  $GLeak$  is the conductance of laminar leakage flow when the valve is closed. The relative opening of the spool valve is indicated by  $sp$ . For a closed valve the spool position ( $sp$ ) is equal to zero and for an open valve the spool position ( $sp$ ) is equal to 1.



In the neutral spool position ( $sp = 0$ ) the valve is just closed. A positive overlap indicates that the spool must travel a certain distance before the valve opens.



A negative overlap indicates that the valve is already open in the neutral position.



The overlap is indicated by the parameter *overlap*, which is given as a fraction of the spool position.

The spool position *sp* is a function of the input signal *spoolpos*:

$$sp = SO(f, d, spoolpos)$$

where *SO* is a second order transfer function to model the spool dynamics. The function is characterized by the bandwidth (*f*) and damping (*d*). The valve input position *spoolpos* should be limited to the range between 0 and 1.

The pressure at both ports has a lower limit which is equal to the vapour pressure. Therefore the actual equations used in this component are:

$$\begin{aligned} pa\_lim &= \text{if } pa.p < p\_vapour \text{ then } p\_vapour \text{ else } pa.p \text{ end;} \\ pb\_lim &= \text{if } pb.p < p\_vapour \text{ then } p\_vapour \text{ else } pb.p \text{ end;} \end{aligned}$$

## Interface

### Ports

pa, pb

### Description

Both terminals of the valve.

### Causality



fixed volume flow

out pa

fixed volume flow

out pb

### Inputs

spoolpos                      position of the spool valve: 0 =closed, 1 = open  
 $0 \leq \text{spoolpos} \leq 1$

### Parameters

rho                      Mass density of the fluid [kg/m<sup>3</sup>].  
 GLeak                      Conductance of the laminar leakage flow [m<sup>3</sup>/s.Pa],  $GLeak \geq 0$ .  
 Amax                      Maximum spool valve area when the valve is open [m<sup>2</sup>],  $Amax > 0$ .  
 Cd                      Discharge coefficient [],  $Cd > 0$ .  
 overlap                      The valve overlap in closed position [],  $-1 < \text{overlap} < 1$ .  
 f                      Bandwidth of the spool dynamics [Hz],  $f > 0$ .  
 d                      Damping of the spool dynamics [],  $d > 0$ .

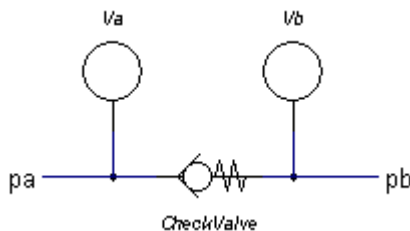
### Library

Iconic Diagrams\Hydraulics\Valves

### Use

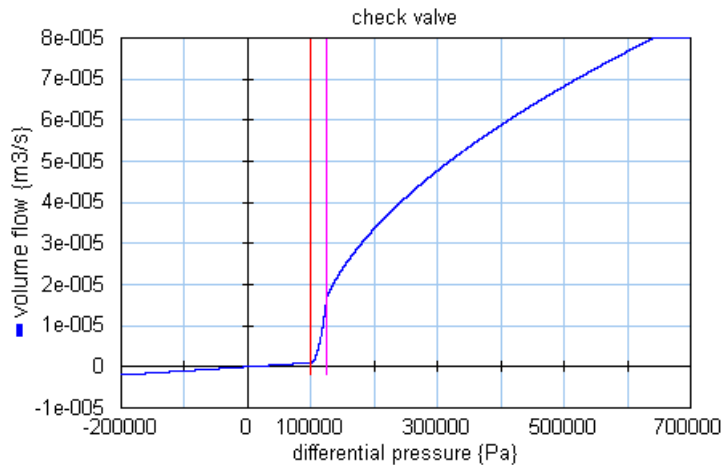
**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description



This model describes a spring-loaded check valve with lumped volumes. The resistance depends on the pressure difference:

$dp < p_{closed} \Rightarrow$  valve closed, only leakage:  $pa.\phi = pb.\phi = dp * G_{Leak}$   
 $p_{closed} < dp < p_{open} \Rightarrow$  working range, i. e. valve partially opened  
 $p_{open} < dp \Rightarrow$  valve wide open:  $pa.\phi = pb.\phi = K * \sqrt{dp - p_{closed}}$ ;



## Interface

### Ports

pa, pb

### Causality

preferred pressure out pa

preferred pressure out pb

### Parameters

CheckValve\pclosed

CheckValve\popen

CheckValve\GLeak

CheckValve\A

CheckValve\Cd

Va\V

Va\B

Va\p\_initial

Vb\V

Vb\B

Vb\p\_initial

### Description

Both terminals of the hydraulic component.

Valve is closed under this pressure [Pa].

Valve is fully open above this pressure [Pa].

Conductance of closed valve [m³/s.Pa].

Maximum valve area when the valve is open [m²],  $A \geq 0$ !

Discharge coefficient [].

Volume of oil under pressure [m³]

Effective bulk modulus [Pa]

The starting pressure of the volume [Pa]

Volume of oil under pressure [m³]

Effective bulk modulus [Pa]

The starting pressure of the volume [Pa]

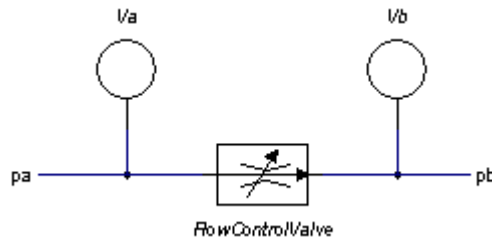
## Library

Iconic Diagrams\Hydraulics\Valves\Basic Valves

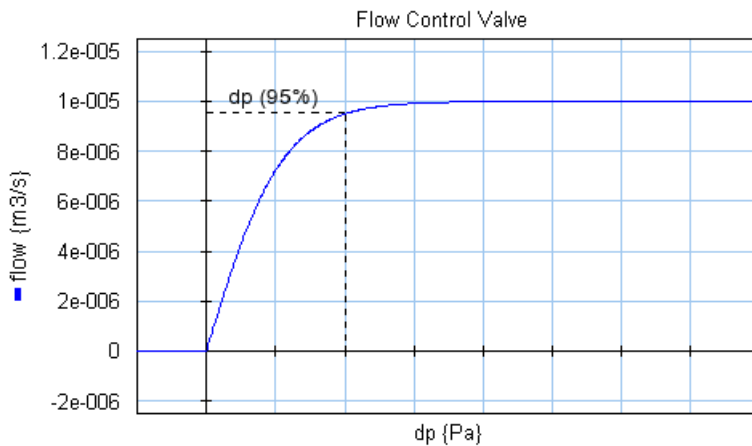
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description



This model describes a flow control valve with with lumped volumes.



In this model the flow is modeled by an *tanh* function. The pressure drop is defined as the pressure where 95% of the desired flow rate is achieved.

```

dp = pa.p - pb.p
phi = if dp > 0 then
  phi*arctanh( (arctan(0.95)/p_drop) * dp) + GLeak * dp;
else
  GLeak * dp
end;
```

Here *phi* is the desired flow and *p\_drop* is the 95% pressure drop. *GLeak* is the conductance of laminar leakage flow when the valve is closed. The pressure at both ports has a lower limit that is equal to the vapour pressure. Therefore the actual equations used in this model are:

```

p1_lim = if pa.p < p_vapour then p_vapour else pa.p end;
p2_lim = if pb.p < p_vapour then p_vapour else pb.p end;
dp = p1_lim - p2_lim;

```

## Interface

### Ports

pa, pb

### Description

Both terminals of the hydraulic component.

### Causality

fixed volume flow out pa

fixed volume flow out pb

### Parameters

FlowControlValve\phi	Desired flow [m3/s]
FlowControlValve\p_drop	pressure drop at 95% flow [Pa]
FlowControlValve\GLeak	Conductance of the laminar leakage flow [m3/s.Pa], GLeak >= 0!
Va\V	Volume of oil under pressure [m3]
Va\B	Effective bulk modulus [Pa]
Va\p_initial	The starting pressure of the volume [Pa]
Vb\V	Volume of oil under pressure [m3]
Vb\B	Effective bulk modulus [Pa]
Vb\p_initial	The starting pressure of the volume [Pa]

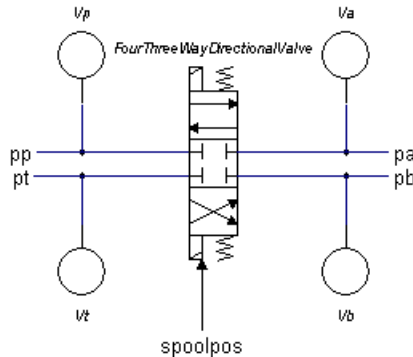
## Library

Iconic Diagrams\Hydraulics\Valves

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description



This model describes a 4/3-way directional control valve with second order spool dynamics and lumped volumes. The flow through the valves is described as laminar/turbulent flow through an orifice. A detailed description of the valve can be found in [FourThreeWayDirectionalValve.htm](#).

The spool position is indicated by the input spoolpos:

$sp = -1$       Flow from  $p$  to  $b$  and  $a$  to  $t$

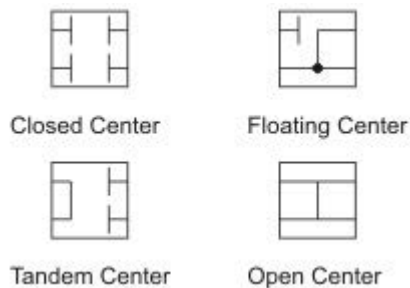
$sp = 0$         No flow

$sp = 1$         Flow from  $p$  to  $a$  and  $b$  to  $t$

Values between -1 and 0 or between 0 and 1 are rounded to the nearest value.

## Implementation

The 4/3-way proportional control valve is implemented with various spool center configurations. The configurations are shown in the picture below:



When you drag and drop a model in the editor, you will be asked which implementation you want to choose. During modeling you can easily change the spool center configuration:

1. Select the valve model.
2. Click the right mouse button to open the right mouse menu.
3. Click **Edit Implementation** and choose another implementation.

## Interface

### Ports

pp, pt, pa, pb

### Description

All terminals of the valve.

### Causality

preferred effort out pp

preferred effort out pt

preferred effort out pa

preferred effort out pb

### Inputs

spoolpos

position of the spool valve

spoolpos < 0.5 => valve is closed

spoolpos >= 0.5 => valve is open

### Parameters

FourThreeWayDirectionalValve\ Mass density of the fluid [kg/m<sup>3</sup>].

rho Conductance of the laminar leakage flow [m<sup>3</sup>/s.Pa], GLeak  
FourThreeWayDirectionalValve\ >= 0.

GLeak Maximum spool valve area when the valve is open [m<sup>2</sup>],  
FourThreeWayDirectionalValve\ Amax > 0.

Amax Discharge coefficient [], Cd > 0.

FourThreeWayDirectionalValve\ The valve overlap in closed position [], -1 < overlap < 1.

Cd Bandwidth of the spool dynamics [Hz], f > 0.

FourThreeWayDirectionalValve\ Damping of the spool dynamics [], d > 0.

overlap Volume of oil under pressure [m<sup>3</sup>]

FourThreeWayDirectionalValve\ Effective bulk modulus [Pa]

f The starting pressure of the volume [Pa]

FourThreeWayDirectionalValve\ Volume of oil under pressure [m<sup>3</sup>]

d Effective bulk modulus [Pa]

Va\V The starting pressure of the volume [Pa]

Va\B

Va\p\_initial

Vb\V

Vb\B

Vb\p\_initial

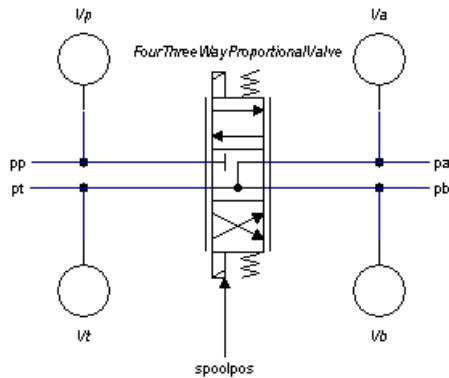
## Library

Iconic Diagrams\Hydraulics\Valves

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description



This model describes a 4/3-way proportional control valve with second order spool dynamics and lumped volumes. The flow through the valves is described as laminar/turbulent flow through an orifice. A detailed description of the valve can be found in [FourThreeWayProportionalValve.htm](#).

The spool position is indicated by the input *spoolpos*:

$sp = -1$       *Flow from p to b and a to t*

$-1 < sp < 0$       *Partial flow from p to b and a to t*

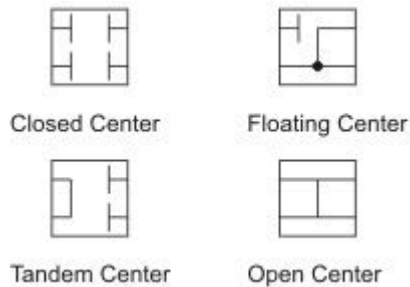
$sp = 0$       *No flow*

$0 < sp < 1$       *Partial flow from p to a and b to t*

$sp = 1$       *Flow from p to a and b to t*

## Implementation

The 4/3-way proportional control valve is implemented with various spool centre configurations. The configurations are shown in the picture below:



When you drag and drop a model in the editor, you will be asked which implementation you want to choose. During modeling you can easily change the spool center configuration:

1. Select the valve model.
2. Click the right mouse button to open the right mouse menu.
3. Click *Edit Implementation* and choose another implementation.

## Interface

### Ports

pp, pt, pa, pb

### Description

All terminals of the valve.

### Causality

preferred effort out pp  
preferred effort out pt  
preferred effort out pa  
preferred effort out pb

### Inputs

spoolpos value of the spool position

### Parameters

FourThreeWayProportionalValv	Mass density of the fluid [kg/m <sup>3</sup> ].
e\rho	Conductance of the laminar leakage flow [m <sup>3</sup> /s.Pa], GLeak
FourThreeWayProportionalValv	>= 0.
e\GLeak	Maximum spool valve area when the valve is open [m <sup>2</sup> ],
FourThreeWayProportionalValv	Amax > 0.
e\Amax	Discharge coefficient [], Cd > 0.
FourThreeWayProportionalValv	The valve overlap in closed position [], -1 < overlap < 1.
e\Cd	Bandwidth of the spool dynamics [Hz], f > 0.
FourThreeWayProportionalValv	Damping of the spool dynamics [], d > 0.
e\overlap	Volume of oil under pressure [m <sup>3</sup> ]
FourThreeWayProportionalValv	Effective bulk modulus [Pa]
e\fb	The starting pressure of the volume [Pa]
FourThreeWayProportionalValv	Volume of oil under pressure [m <sup>3</sup> ]
e\fb	Effective bulk modulus [Pa]



Va\V	The starting pressure of the volume [Pa]
Va\B	
Va\p_initial	
Vb\V	
Vb\B	
Vb\p_initial	

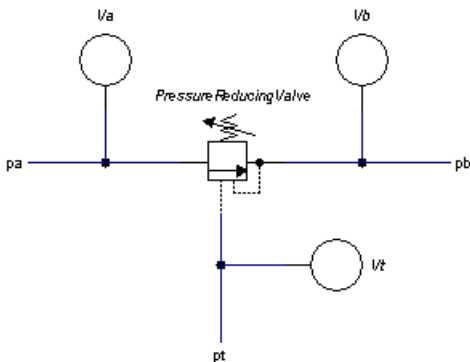
Library

Iconic Diagrams\Hydraulics\Valves

Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

Description



This model describes a pressure reducing valve with lumped volumes. Pressure reducing valves have the purpose to provide a constant pressure ( $p_{nom}$ ), independent of the upstreamstream pressure. They are used to limit the pressure of a primary circuit to a desired pressure for a secondary circuit.

Interface

Ports

pa, pb  
pt

Description

Both terminals of the hydraulic component.  
Pilot

Causality

fixed volume flow out pa  
fixed volume flow out pb

Parameters

FlowControlValve\phi	Desired flow [m3/s]
FlowControlValve\p_drop	pressure drop at 95% flow [Pa]
FlowControlValve\GLeak	

$V_a \backslash V$	Conductance of the laminar leakage flow [m <sup>3</sup> /s.Pa], $G_{Leak} \geq 0$ !
$V_a \backslash B$	
$V_a \backslash p\_initial$	Volume of oil under pressure [m <sup>3</sup> ]
$V_b \backslash V$	Effective bulk modulus [Pa]
$V_b \backslash B$	The starting pressure of the volume [Pa]
$V_b \backslash p\_initial$	Volume of oil under pressure [m <sup>3</sup> ]
	Effective bulk modulus [Pa]
	The starting pressure of the volume [Pa]

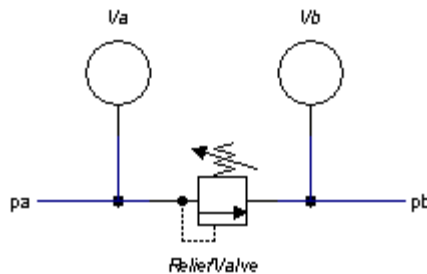
## Library

Iconic Diagrams\Hydraulics\Valves

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description



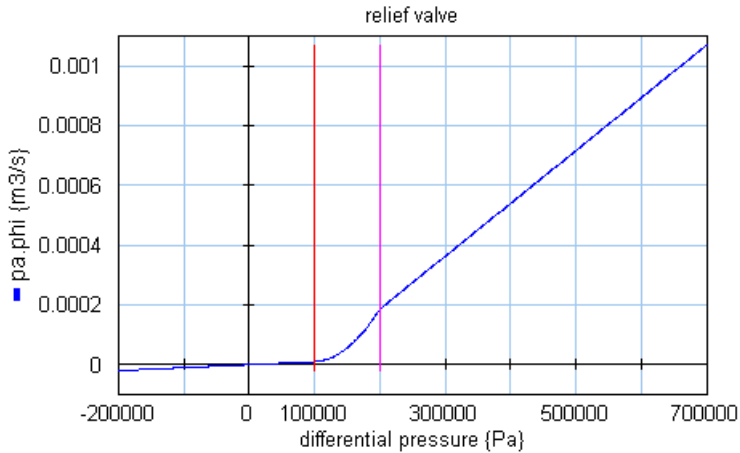
This model describes a pressure relief valve with lumped volumes. The resistance depends on the pressure difference:

$$dp = pa.p - pb.p$$

$dp < p_{closed} \Rightarrow$  valve closed, only leakage:  $pa.\phi = pb.\phi = dp * G_{Leak}$

$p_{closed} < dp < p_{open} \Rightarrow$  working range, i. e. valve partially opened

$p_{open} < dp \Rightarrow$  valve wide open:  $pa.\phi = pb.\phi = dp * G_{Open}$



## Interface

### Ports

pa, pb

### Causality

preferred pressure out pa

preferred pressure out pb

### Parameters

PressureReliefValve\pclosed

PressureReliefValve\popen

PressureReliefValve\GLeak

PressureReliefValve\GOpen

Va\V

Va\B

Va\p\_initial

Vb\V

Vb\B

Vb\p\_initial

### Description

Both terminals of the hydraulic component.

Valve is closed under this pressure [Pa].

Valve is fully open above this pressure [Pa].

Conductance of closed valve [m³/s.Pa].

Conductance of open valve [m³/s.Pa].

Volume of oil under pressure [m³]

Effective bulk modulus [Pa]

The starting pressure of the volume [Pa]

Volume of oil under pressure [m³]

Effective bulk modulus [Pa]

The starting pressure of the volume [Pa]

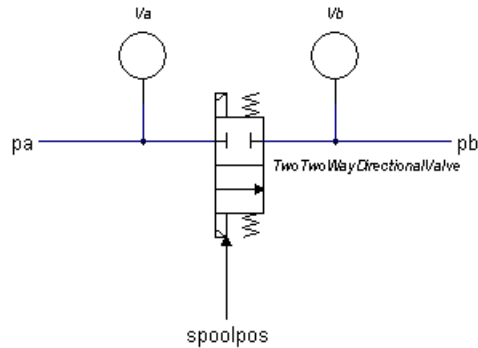
## Library

Iconic Diagrams\Hydraulics\Valves

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description



This model describes a 2/2-way directional control valve with second order spool dynamics and lumped volumes. The flow through the valve is described as laminar/turbulent flow through an orifice. A detailed description of the valve can be found in [TwoTwoWayDirectionalValve.htm](#).

## Interface

### Ports

pa, pb

### Description

Both terminals of the valve.

### Causality

preferred effort out pa

preferred effort out pb

### Inputs

spoolpos

position of the spool valve

spoolpos < 0.5 => valve is closed

spoolpos >= 0.5 => valve is open

### Parameters

TwoTwoWayDirectionalValve\rh Mass density of the fluid [kg/m<sup>3</sup>].

o Conductance of the laminar leakage flow [m<sup>3</sup>/s.Pa], GLeak

TwoTwoWayDirectionalValve\G >= 0.

Leak Maximum spool valve area when the valve is open [m<sup>2</sup>],

TwoTwoWayDirectionalValve\A Amax > 0.

max Discharge coefficient [], Cd > 0.

The valve overlap in closed position [], -1 < overlap < 1.

TwoTwoWayDirectionalValve\C	Bandwidth of the spool dynamics [Hz], $f > 0$ .
d	Damping of the spool dynamics [], $d > 0$ .
TwoTwoWayDirectionalValve\ov	Volume of oil under pressure [m3]
erlap	Effective bulk modulus [Pa]
TwoTwoWayDirectionalValve\f	The starting pressure of the volume [Pa]
TwoTwoWayDirectionalValve\d	Volume of oil under pressure [m3]
Va\V	Effective bulk modulus [Pa]
Va\B	The starting pressure of the volume [Pa]
Va\p_initial	
Vb\V	
Vb\B	
Vb\p_initial	

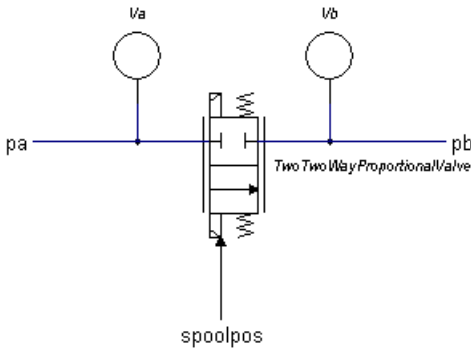
Library

Iconic Diagrams\Hydraulics\Valves

Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

Description



This model describes a 2/2-way proportional control valve with second order spool dynamics and lumped volumes. The flow through the valve is described as laminar/turbulent flow through an orifice. A detailed description of the valve can be found in [TwoTwoWayProportionalValve.htm](#).

Interface

Ports

pa, pb

Description

Both terminals of the valve.

Causality

preferred effort out pa

preferred effort out pb

### Inputs

spoolpos position of the spool valve: 0 = closed, 1 = open  
 $0 \leq \text{spoolpos} \leq 1$

### Parameters

TwoTwoWayDirectionalValve\rh Mass density of the fluid [kg/m<sup>3</sup>].  
 o Conductance of the laminar leakage flow [m<sup>3</sup>/s.Pa], GLeak  
 TwoTwoWayDirectionalValve\G  $\geq 0$ .  
 Leak Maximum spool valve area when the valve is open [m<sup>2</sup>],  
 TwoTwoWayDirectionalValve\A Amax  $> 0$ .  
 max Discharge coefficient [], Cd  $> 0$ .  
 TwoTwoWayDirectionalValve\C The valve overlap in closed position [],  $-1 < \text{overlap} < 1$ .  
 d Bandwidth of the spool dynamics [Hz], f  $> 0$ .  
 TwoTwoWayDirectionalValve\ov Damping of the spool dynamics [], d  $> 0$ .  
 erlap Volume of oil under pressure [m<sup>3</sup>]  
 TwoTwoWayDirectionalValve\fb Effective bulk modulus [Pa]  
 TwoTwoWayDirectionalValve\vd The starting pressure of the volume [Pa]  
 Va\V Volume of oil under pressure [m<sup>3</sup>]  
 Va\B Effective bulk modulus [Pa]  
 Va\p\_initial The starting pressure of the volume [Pa]  
 Vb\V  
 Vb\B  
 Vb\p\_initial

### Library

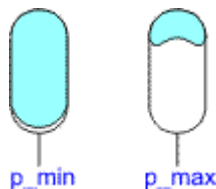
Iconic Diagrams\Hydraulic\Volumes

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

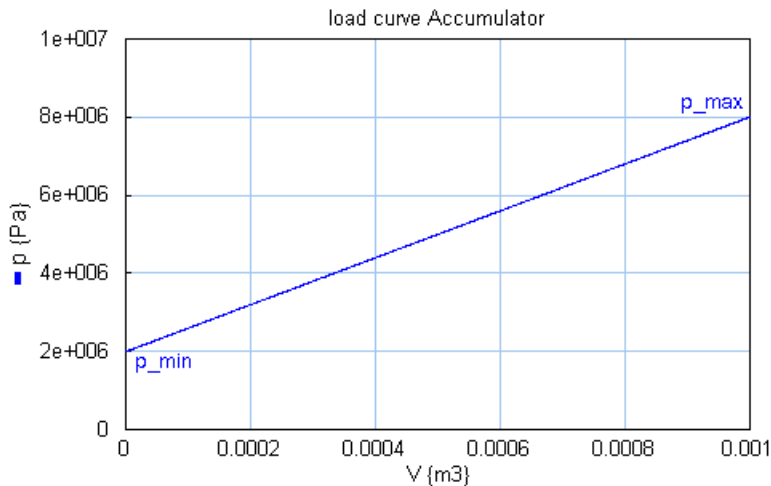
### Description

Hydraulic accumulators regulate the performance of a hydraulic system by providing an additional volume of system fluid, pressurized by an external gas supply.



A common accumulator consists of a volume of gas that is separated from the hydraulic fluid by a flexible diaphragm or a piston. The gas is pressurized to make it react against the fluid pressure. When the fluid pressure is low, the accumulator is completely filled by the gas volume. When the fluid pressure rises at a given minimum ( $p = p_{min}$ ) the gas volume starts to shrink until it reaches its smallest allowable volume ( $p = p_{max}$ ).

In this model the shape of the accumulator is supposed to be designed in such a way that the fluid volume is a linear function of the pressure, as shown in the figure below.



The pressure in this the model has a lower limit which is equal to the vapour pressure. Therefore the actual equations used in this component are:

$$p_{lim} = \text{if } p_a.p < p_{vapour} \text{ then } p_{vapour} \text{ else } p.p \text{ end}$$

### Interface

#### Ports Description

p

#### Causality

preferred pressure  
out

#### Parameters

p_vapour	vapour pressure [Pa].
G	conductance of the accumulator input [m3/s.Pa].
p_min	minimum gas pressure [Pa].

p\_max                      maximum gas pressure [Pa].

## Library

Iconic Diagrams\Hydraulic\Volumes

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description

This model represents a tank with a preload pressure against atmosphere. The default preload pressure of 0 [Pa] means that the tank has atmospheric pressure. A preload pressure of 1e5 [Pa] means that the tank has an absolute pressure of 2e5 [Pa] etc.

## Interface

### Ports                      Description

p

### Causality

fixed pressure out

### Parameters

p\_preload                      tank pressure [Pa]

## Library

Iconic Diagrams\Hydraulic\Volumes

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

## Description

This model represents a tank with a preload pressure against atmosphere and a resistance of the tank pipe. The default preload pressure of 0 [Pa] means that the tank has atmospheric pressure. A preload pressure of 1e5 [Pa] means that the tank has an absolute pressure of 2e5 [Pa] etc.

There is no check on the validity of laminar flow in this component!

## Interface

### Ports                      Description

p

### Causality

fixed volume flow

out p

### Parameters



p_preload	tank pressure [Pa]
G	Conductance of laminar resistance [m3/s.Pa]

## Library

Iconic Diagrams\Hydraulic\Volumes

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Hydraulics).

### Description

This model represents a lumped volume with a constant bulk modulus. If the calculated pressure falls below the vapour pressure the pressure is NOT limited to the vapour pressure.

### Interface

Ports	Description
-------	-------------

p

### Causality

preferred pressure

out

### Parameters

V	Volume of oil under pressure [m3]
B	Effective bulk modulus [Pa]
p_initial	The starting pressure of the volume [Pa]

## Mechanical

The Mechanical library contains components which are very useful for modeling mechanical systems. The library contains the following sections:

- Mechanics
  - Rotation
    - Actuators
    - Components
    - Friction
    - Gears
    - Sensors
  - Translation
    - 2D Small Rotation
    - 3D Small Rotation
    - Actuators
    - Components
    - Friction
    - Sensors
    - Transmission

### Library

Iconic Diagrams\Mechanical\Rotation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

### Description

This model represents an ideal actuator. An angular acceleration input signal is integrated to an angular velocity difference between its two terminals:

$$p\_high.\omega = p\_low.\omega + \text{int}(\alpha, \omega\_initial);$$

$$p\_low.T = p\_high.T = \text{indifferent};$$

### Interface

#### Ports

p\_high, p\_low

#### Description

Both terminals of the Rotation port p.

#### Causality

fixed          angular  
velocity out

**Input**

alpha                  Angular acceleration [rad/s<sup>2</sup>].

**Parameters**

omega\_initial          Initial angular velocity output of the integration [rad/s].

**Library**

Iconic Diagrams\Mechanical\Rotation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

**Description**

This model represents an ideal actuator. An angular acceleration input signal is integrated to an angular velocity at the rotation port. The actuator is mounted to the fixed world:

```
p.omega = int(alpha,omega_initial);
p.T = indifferent;
```

**Interface**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p	Rotation port.
---	----------------

**Causality**

fixed          angular  
velocity out

**Input**

alpha                  Angular acceleration [rad/s<sup>2</sup>].

**Parameters**

omega\_initial          Initial angular velocity at the port [rad/s].

**Note**

This model was named ServoMotor.emx in previous versions of 20-sim!

**Library**

Iconic Diagrams\Mechanical\Rotation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

**Description**

Industrial servo motors in the medium to high power range generally consist of an AC-electric and drive (the digital controlled current supply of the motor). The drive takes care of the correct supply of current to let the motor follow every desired path. Unfortunately the exact implementation and performance of drives and motors is one of the trade secrets of the commercial motor suppliers. Fortunately modern servo-motors are designed well enough to be described by general parameters that can be found in every data sheet.

The servo motor model describes a digitally controlled AC-motor that is described by general parameters. The model is suited for modeling machine dynamics, i.e. models where the machine behavior is the topic of interest and not the motor itself. For studying the exact motor behavior (temperature, wear, vibration etc.) other motor models should be used. A complete description of the motor is given in the second part of this topic.

**Interface****Ports**                      **Description**

p                              Rotation port.

**Causality**

preferred    angular  
velocity out p

**Inputs**

v                              velocity setpoint [rad/s]

**Parameters**

VelocityLimit\v\_ma Maximum motor speed (>0) [rad/s]

x                              Maximum allowed acceleration (>0) [rad/s<sup>2</sup>]

AccelerationLimit\alpha\_max Bandwidth drive (half of the sample frequency, >0) [Hz]

Proportional gain []

AccelerationLimit\tau\_e Integral time constant (>0) [s]

\_e                              Tracking time constant (>0) [s]

PI\K                              Maximum motor torque (>0) [Nm]

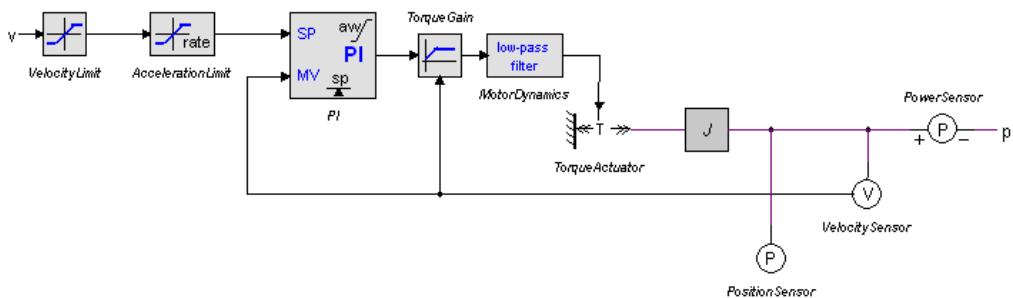
PI\Ti	Motor speed where torque gain starts to drop ( $>0$ ) [rad/s]
PI\Ta	
PI\T_max	
TorqueGain\vd	
TorqueGain\g0	Torque gain at zero motor speed ( $>0$ , choose equal to 1 to turn off torque gain drop [])
MotorDynamics\fc	Bandwidth drive and motor electronics [Hz]
Inertia\J	Motor inertia [ $\text{kg.m}^2/\text{rad}$ ]

**Variables** There are some variables that can be of interest when inspecting the servo performance:

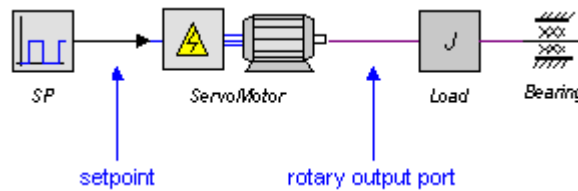
PI\error	The error between setpoint and motor velocity [rad/s].
PositionSensor\phi	Motor Angle [rad]
VelocitySensor\om	Motor Speed [rad/s]
ega	Motor Acceleration [rad/s <sup>2</sup> ]
Inertia\alpha	Output Torque [Nm].
PowerSensor\T	Output Power [W].
PowerSensor\P	

## Model

The complete servo motor model is shown below. Every block that is used to form this model will be explained in the next sections. The model has a velocity input signal  $v$  and a rotary output port  $p$ .



The servo motor model can be used in a machine model as shown in the example below.



## Blocks

### Velocity Limit

Most servo motors have a velocity limit to prevent the motor from damage. This limit can be set in the velocity VelocityLimit block. If no limit is known choose twice the nominal velocity.

### Acceleration Limit

To prevent the motor from damage, most servos have a maximum acceleration limit. This limit is very important in a model because it can seriously degrade the systems performance.

To find the acceleration, the derivative of the input must be calculated. This is done by means of a first order differentiation with bandwidth  $f_c$ . The bandwidth is equal to one half the of the sample frequency of the velocity control loop. Older drives may have loops that run on sample frequencies ranging from 100 Hz to 500 Hz. Modern drives can run the velocity control loop on sample frequencies of 2 kHz or more.

To switch the maximum acceleration limit off, choose the maximum acceleration parameter high enough and choose the bandwidth sufficiently high, preferably 10 times as large as the bandwidth  $f_e$  of the motor electronics (specified in the motor dynamics block).

### PI-Controller

Most servos will use velocity as the setpoint signal. To calculate the desired torque out of the velocity setpoint, PI-controllers are widely used. For many servos, the controller parameters can be changed by the user, but this is not a very easy task. Therefore these servos often offer automatic tuning facilities.

In 20-sim you can use the Optimization toolbox for automatic tuning. A good starting point is to take the error variable of the PI-controller and minimize it by changing the controller parameters  $K_p$ ,  $T_i$  and  $T_a$ . It is important to realize that automatic tuning will tune the controller parameters for a certain task. If you run another task, i.e. perform a simulation with another setpoint, the results may degrade. For varying tasks it is better to use parameters that give a good response over a wide area of loads. To help the user find good starting values, the table below shows some motors, loads and corresponding starting value for the controller parameters.

Motor				Load	controller		
Nominal Power [kW]	Nominal Torque [Nm]	Nominal Speed [rpm]	Peak Torque [Nm]	Load + Motor Inertia [kg.m2]	Kp	Ti	Ta
0.38	1.2	3000	4.6	0.005	250	0.1	0.1
1.13	3.6	3000	14	0.002	1000	0.4	0.4
7.54	24	3000	134	0.1	5000	2	2
11	36	3000	90	0.4	15000	6	6
55	177	3000	531	2	75000	30	30
560	1792	3000	6092.8	25	750000	300	300

The user has to find the load that should be driven in terms of the rotational inertia. If there is a gear that changes the rotary motion to a linear motion this means the load has to be divided by the square of the gear ratio to get the corresponding load in the rotational domain. Do not forget to add the inertia of the motor itself! For many gear ratios the load in terms of rotational inertia will be of the same magnitude as the motor inertia.

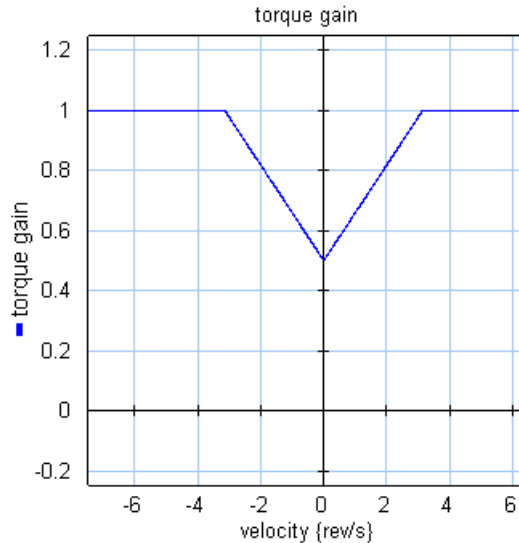
In this model PI-controller with an anti-windup facility is used. This controller is the heart of the servo motor model. It is therefore important to know something about PI-control. More information can be found in the PID controllers section of the library.

AC-motors have a limited output torque which is a complex function of the controller settings, the applied speed, duty cycle, temperature and more. In the servo motor model simply the torque limit of the PI-controller  $T_{max}$  is used which limits the generated torque to a maximum. Because this is a simplification of the real behavior, the maximum torque limit should only be used to inspect what happens to the system when the motor torque is approaching its maximum value. For a proper evaluation of its system, the user should also look at the unconstrained torque. Run a simulation and note the amount of time that the motor runs at a maximum torque. This is called the duty cycle. Every motor manual will have tables showing duty cycles and the corresponding chances of overheating.

### Torque Gain

Standard AC-motors, normally designed to run at base speeds between 850 to 3500 rpm, are not particularly well suited for low-speed operation, as their efficiency drops with the reduction in speed. They may also be unable to deliver sufficient smooth torque at low speeds.

An ideal motor will always have a torque gain of 1, i.e. an input signal of 1 Nm will always result in an output torque of 1 Nm. Most industrial motors have a torque gain that is only equal to 1 for higher speeds. At low speeds the torque gain will drop due to electronic limitations. This behavior is represented by the graph below. At speeds below a drop-off speed  $vd$  the torque gain drops linearly to a user defined zero speed torque gain  $g0$ . If no torque gain drop is desired, choose  $g0$  equal to 1.



### Motor Dynamics

The electrical circuits of the drive and wiring of the motor have a limited bandwidth. This is modeled with a first order low-pass filter with a bandwidth  $f_e$ . Typical motor bandwidths vary from 3 kHz to 20 kHz.

### Torque source

In the torque source block the torque signal is converted to an iconic diagram port p.

### Inertia

This block describes the rotor inertia. The equations of motion of the inertia are used to get the angular acceleration without needing derivatives.

### Sensors

Finally four sensors are available to plot the position, velocity, acceleration and output power.

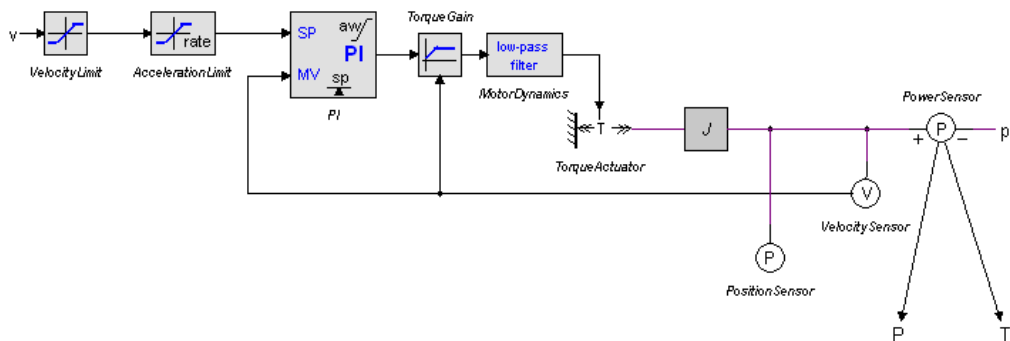
### Variables

There are some variables in the model that may be of special interest

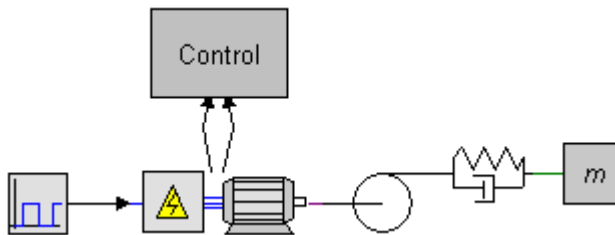
PI\error	The error between setpoint and motor velocity [rad/s].
PositionSensor\phi	Motor Angle [rad]
VelocitySensor\om	Motor Speed [rad/s]
ega	Motor Acceleration [rad/s <sup>2</sup> ]
Inertia\alpha	Output Torque [Nm].
PowerSensor\T	Output Power [W].
PowerSensor\P	



All these variables are output signals of their respective blocks. By inserting extra outputs in the servo motor model you can use as output signals for usage in other parts of your model. In the pictures below is shown how to define signals for the torque and power.



In the servo model define a torque and a power output and connect them.



One level higher you can use these signals for modeling, for example in a high level control unit.

## Library

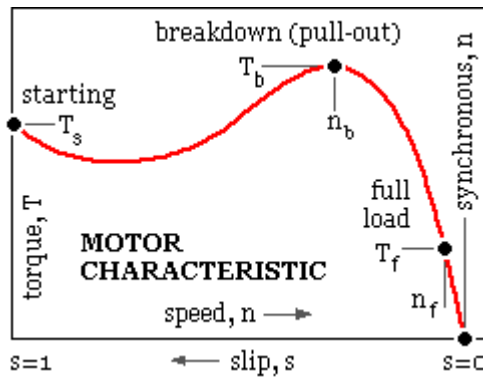
Iconic Diagrams\Mechanical\Rotation\Actuators

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description

This is a model of an industrial AC electric motor with squirrel cage rotor. The motor is not controlled by a power electric converter. Instead its performance is directly defined by a torque speed curve.



The torque speed curve is fully defined by the parameters shown in the picture. The synchronous speed is defined as:

$$n = 2 * \text{voltage frequency} / \text{no. of poles}$$

## Interface

### Ports

p

### Description

Output axis (Rotation)

### Parameters

Ts	start torque (zero speed) [Nm]
n	synchronous speed (zero torque) [rad/s]
Tm	maximum torque [Nm]
nm	speed at maximum torque [rad/s]
Tf	full load torque [Nm]
nf	speed at full load torque [rad/s]
J	motor inertia [ $\text{kgm}^2/\text{rad}$ ]

## Library

Iconic Diagrams\Electric\Actuators  
Iconic Diagrams\Mechanical\Electric

## Implementations

Default  
IR

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric, Electric).

**Description - Default**

This models represents an ideal DC-motor with no energy loss. The electric port has separate high and low terminals. The equations are

$$\begin{aligned} p1.i &= p1\_high.i = p1\_low.i; \\ p1.u &= p1\_high.u - p1\_low.u; \end{aligned}$$

The model can have mixed forms of causality

$$\begin{aligned} p1.u &= k * p2.omega; \\ p2.T &= k * p1.i; \end{aligned}$$

or:

$$\begin{aligned} p2.omega &= p1.u / k; \\ p1.i &= p2.T / k; \end{aligned}$$

**Interface - Default**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p1_high, p1_low	Both terminals of the Electric port p1.
p2	Rotation port.

**Causality**

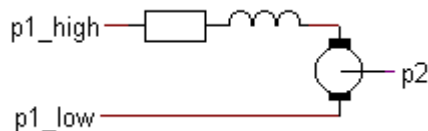
mixed	See equations above.
-------	----------------------

**Parameters**

k	motor constant [Nm/A]
---	-----------------------

**Description - IR**

This models represents an ideal DC-motor with inductance and resistance.



The electric port has separate high and low terminals. The equations are

$$\begin{aligned} p1.i &= p1\_high.i = p1\_low.i; \\ p1.u &= p1\_high.u - p1\_low.u; \end{aligned}$$

**Interface - IR**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p1\_high, p1\_low Both terminals of the Electric port p1.  
 p2 Rotation port.

### Causality

mixed See equations above.

### Parameters

k motor constant [Nm/A]  
 L motor inductance [H]  
 R motor resistance [Ohm]

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

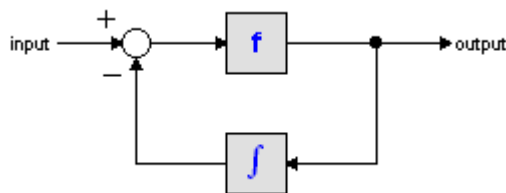
### Description

This model represents an ideal actuator. An angle input signal is differentiated by a state variable filter to an angular velocity difference between its two terminals:

$$p\_high.\omega = p\_low.\omega + d\phi/dt;$$

$$p\_low.T = p\_high.T = indifferent;$$

Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where  $f$  is the cut-off frequency. For very high values of  $f$ , the output becomes the pure derivative of the input. High values of  $f$ , however, increase simulations times. A good trade-off is a starting value of  $1e5$ .

### Interface

Ports	Description
-------	-------------

p\_high, p\_low Both terminals of the Rotation port p.

### Causality

fixed angular  
velocity out

### Input

phi Angle [rad].

### Parameters

f Cut-off frequency of the differentiation [Hz].

omega\_initial Initial angular velocity output of the differentiation [rad/s].

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

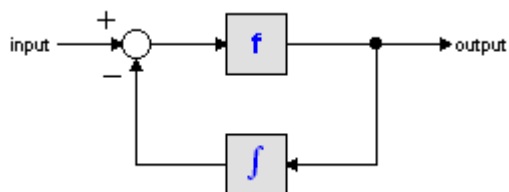
### Description

This model represents an ideal actuator. An angle input signal is differentiated by a state variable filter to an angular velocity at the rotation port. The actuator is mounted to the fixed world:

$$p.\omega = d\phi/dt;$$

$$p.T = \text{indifferent};$$

Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where  $f$  is the cut-off frequency. For very high values of  $f$ , the output becomes the pure derivative of the input. High values of  $f$ , however, increase simulations times. A good trade-off is a starting value of 1e5.

## Interface

Ports	Description
p	Rotation port.

## Causality

fixed      angular  
velocity out

## Input

phi      Angle [rad].

## Parameters

f      Cut-off frequency of the differentiation [Hz].  
omega\_initial      Initial angular velocity at the port [m/s].

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators  
Iconic Diagrams\Mechanical\Translation\Actuators

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

## Description

This is a masked model which opens the Servo Motor Editor when edited. The servo Motor Editor is a tool that can shows the torque speed plots numerous permanent magnet motors and can generate a dynamic model from any motor that you select. The following motor types are supported:

1. Brush DC
2. Brushless DC (trapezoidal EMC and square wave currents)
3. AC synchronous (sinusoidal EMC and sinusoidal currents)

## 4. AC synchronous linear (sinusoidal EMC and sinusoidal currents)

**Interface**

Depending on the type of motor that you have selected, the interface can vary:

**DC Brush**

Ports	Description
p	Rotation port.

**Causality**

fixed      rotational  
velocity out

**Input**

i                      The input current [A]

**DC Brushless**

Ports	Description
p	Rotation port.

**Causality**

fixed      rotational  
velocity out

**Input**

i                      The maximum input current [A]

**AC Synchronous**

Ports	Description
p	Rotation port.

**Causality**

fixed      rotational  
velocity out

**Input**

i\_rms                  The rms phase current [A]

**AC Synchronous Linear**

Ports	Description
p	Translation port.

**Causality**

fixed velocity out

## Input

**i<sub>rms</sub>**                      The rms phase current [A]

For more information on the parameters and variables of this model is referred to the Mechatronic Toolbox.

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators

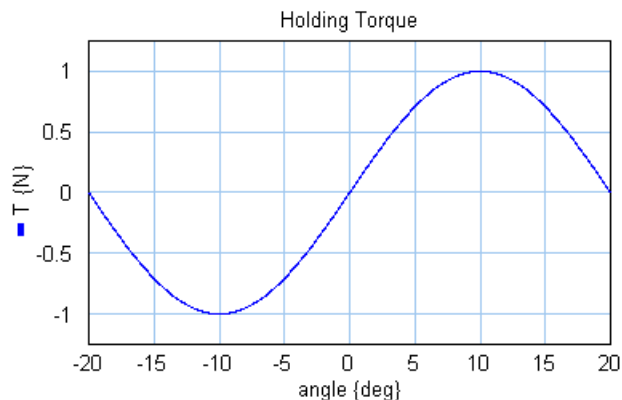
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description

A stepper motor is a device used to convert electrical pulses into discrete mechanical rotational movements. The minimum movement, invoked by one pulse, is called the *step angle*. The electrical pulses are mostly generated by a pulse generator that converts a setpoint change in a corresponding amount of pulses. This model describes a combination of a pulse generator and stepper motor.

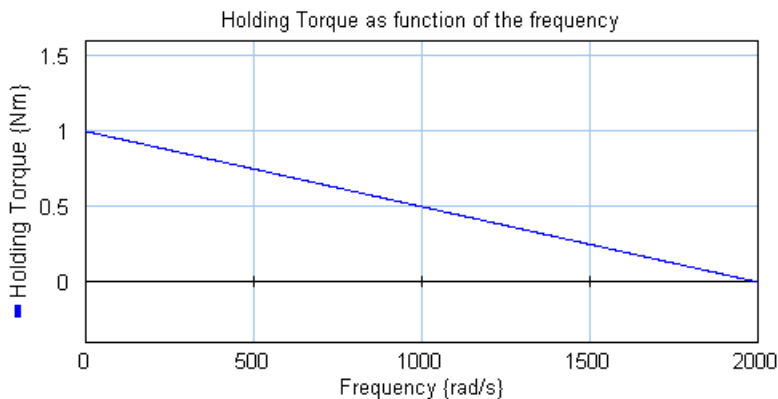
At standstill the torque required to deflect the motor a full step is called the *holding torque*. The holding torque normally is much higher than required to drive the load, and thus acts as a strong brake to hold the load. The holding torque as function of the output angle is shown in the graph below. Around zero angle the curves shows the behavior of a spring. By changing the input by one step, the force will increase to its maximum and move the the load.



*Motor torque as function of the angle (holding torque = 1 [N], step angle =  $[10^\circ]$ ).*

If the subsequent steps are generated fast enough the holding torque will start to decrease. The maximum holding torque as function of the rotation speed is shown in the figure below. This force curve is commonly describe as the *pull out* curve.





*Pull out curve: maximum generated torque as a function of the rotational speed.*

Ports	Description
input	Desired output angle.
p_out	Rotation port.
<b>Causality</b>	
fixed current out	
p_in	
preferred angular velocity out	p_out
<b>Inputs</b>	
input	Stepper motor input
<b>Parameters</b>	
step_angle	Minimum change of the output axis [deg].
tau	Time constant coil [s].
Th	Holding torque [Nm].
J	Inertia rotor [Nm^2]
B	Relative damping at the stepper motor resonance [].
fmax	Maximum frequency motor (frequency at which the torque gets zero) [rad/s].

**Library**  
Iconic Diagrams\Mechanical\Rotation\Actuators

**Use**  
**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description

This model represents an ideal actuator. The actuator applies a torque between its two terminals. This torque can be set to a certain constant value, the angular velocity is indifferent.

$$p\_high.T = p\_low.T = T$$

## Interface

Ports	Description
p_high, p_low	Both terminals of the Rotational port p.
<b>Causality</b>	
fixed torque out	
<b>Input</b>	
T	Torque [Nm].

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description

This model represents an ideal actuator. The actuator is mounted to the fixed world and applies a torque. The torque can be set to a certain constant value, the angular velocity is indifferent.

$$p.T = T;$$

## Interface

Ports	Description
p	Rotation port.
<b>Causality</b>	
fixed torque out	
<b>Parameters</b>	
T	Torque [Nm].

**Library**

Iconic Diagrams\Mechanical\Rotation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

**Description**

This model represents an ideal actuator. The actuator applies a torque between its two terminals. This torque can be set to a (fluctuating) value given by the input signal  $T$ , the angular velocity is indifferent.

$$p_{high}.T = p_{low}.T = T$$

**Interface**

Ports	Description
$p_{high}$ , $p_{low}$	Both terminals of the Rotation port p.
<b>Causality</b>	
fixed torque out	
<b>Input</b>	
$T$	Torque [Nm].

**Library**

Iconic Diagrams\Mechanical\Rotation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

**Description**

This model represents an ideal actuator. The actuator is mounted to the fixed world and applies a torque. The torque can be set to a (fluctuating) value given by the input signal  $T$ , the angular velocity is indifferent.

$$p.T = T;$$

**Interface**

Ports	Description
$p$	Rotation port.
<b>Causality</b>	

fixed torque out

### Input

T Torque [Nm].

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

This model represents an ideal actuator. The actuator applies an angular velocity difference between its two terminals. This angular velocity can be set to a constant value *omega*, the force is indifferent.

$$p\_low.\omega = p\_high.\omega + \omega$$

### Interface

#### Ports Description

p\_high, p\_low Both terminals of the Rotation port p.

#### Causality

fixed angular  
velocity out

#### Parameter

v Angular velocity [rad/s].

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

This model represents an ideal actuator. The actuator is mounted to the fixed world and applies an angular velocity. This angular velocity can be set to a certain constant value, the torque is indifferent.

$$p.\omega = \omega;$$

## Interface

### Ports

p                      Rotation port.

### Causality

fixed              angular  
velocity out

### Parameters

omega              Angular velocity [rad/s].

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

## Description

This model represents an ideal actuator. The actuator applies an angular velocity difference between its two terminals. This angular velocity can be set to a (fluctuating) value given by the input signal  $v$ , the force is indifferent.

$$p_{low}.\omega = p_{high}.\omega + \omega$$

## Interface

### Ports

p\_high, p\_low              Both terminals of the Rotation port p.

### Causality

fixed              angular  
velocity out

### Input

omega              Angular velocity [rad/s].

## Library

Iconic Diagrams\Mechanical\Rotation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

### Description

This model represents an ideal actuator. The actuator is mounted to the fixed world and applies an angular velocity. This angular velocity can be set to a (fluctuating) value given by the input signal *omega*, the torque is indifferent.

$$p.\omega = \omega;$$

### Interface

Ports	Description
p	Rotation port.
<b>Causality</b>	
fixed	angular
velocity out	
<b>Input</b>	
omega	Angular velocity [rad/s].

## Library

Iconic Diagrams\Mechanical\Rotation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

This model represents backlash by a spring damper system equivalent to the translational backlash model. The port p of this model has separate high and low terminals. The equations are:

$$\begin{aligned} p.T &= p_{high}.T = p_{low}.T \\ p.\omega &= p_{high}.\omega - p_{low}.\omega \end{aligned}$$

### Interface

Ports	Description
-------	-------------

p\_high, p\_low Both terminals of port p (Rotation).

### Causality

fixed torque out

### Parameters

s	Interval of the play [rad]
k1	Stiffness in the play [Nm/rad]
k2	Stiffness outside the play [Nm/rad]
d1	Damping inside the play [Nms/rad]
d2	Damping outside the play [Nms/rad]
ep	Relative round off (1e-6 -> sharp edges, 1e-2 -> smoother)

### Parameters

x_initial	Initial position in the play [rad], $-s/2 < x\_initial < s/2$
-----------	---

## Library

Iconic Diagrams\Mechanical\Rotation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

In this model bearing friction is represented as linear viscous friction. The model has only one initial port p defined. Because any number of connections can be made, successive ports are named p1, p2, p3 etc. 20-sim will automatically create equations such that the resulting torque  $p.T$  is equal to the sum of the torques of all connected ports p1 .. pn. The angular velocities of all connected ports are equal to  $p.\omega$ . The model can have an torque out as well as an angular velocity out causality. In the last case the constitutive equation, as shown below, is simply inverted:

$$\begin{aligned} p.T &= \text{sum}(p1.T, p2.T, ....) \\ p.\omega &= p1.\omega = p2.\omega = .... \end{aligned}$$

Torque out causality:

$$p.T = d * p.\omega;$$

Angular velocity out causality:

$$p.\omega = p.T / d;$$

## Interface

### Ports

p[any] Any number of connections can be made (Rotation).

### Description

### Causality

indifferent

### Parameters

d                      Damping [Nms/rad]

### Library

Iconic Diagrams\Mechanical\Rotation\Components

### Implementations

C

V

CV

SCVS

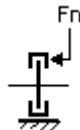
LuGre

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Introduction

The brake models represent a disk brake or other type of brake where a rotation is stopped by applying a friction force. The amount of friction depends on the normal force that is applied and the friction function that is used. The normal force is given by the input signal  $F_n$ . The brake is mounted to the fixed world.



The model has only one initial port  $p$  defined. Because any number of connections can be made, successive ports are named  $p1$ ,  $p2$ ,  $p3$  etc. 20-sim will automatically create equations such that the resulting torque  $p.T$  is equal to the sum of the torques of all connected ports  $p1 \dots pn$ . The angular velocities of all connected ports are equal to  $p.\omega$ .

$$p.T = \text{sum}(p1.T, p2.T, \dots)$$

$$p.\omega = p1.\omega = p2.\omega = \dots$$

Due to the use of normal force, the brake models all have a fixed torque out causality. The constitutive equations are therefore described as:

$$p.T = F_n * f(p.\omega);$$

with  $f$  the friction function.

### Description - C

This model represents a brake with braking force described as coulomb friction. The brake is mounted to the fixed world. The amount of friction depends on the normal force that is applied:

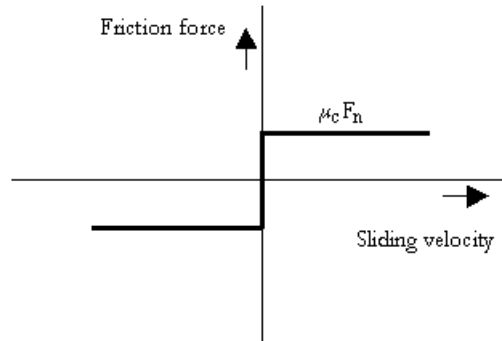


$$p.T = F_n * \mu_c * \tanh(\text{slope} * p.\omega);$$

$F_n$ : normal force (given by the input signal  $F_n$ )

$\mu_c$ : the coulomb friction coefficient

$\text{slope}$ : the steepness of the coulomb friction curve.



## Interface - C

### Ports

$p[\text{any}]$

### Description

Any number of connections can be made (Rotation).

### Causality

Fixed torque out

### Input

$F_n$  Normal force [N]

### Parameters

$\mu_c$  Coulomb friction coefficient [m]

$\text{slope}$  Steepness of Coulomb friction curve [s/rad]

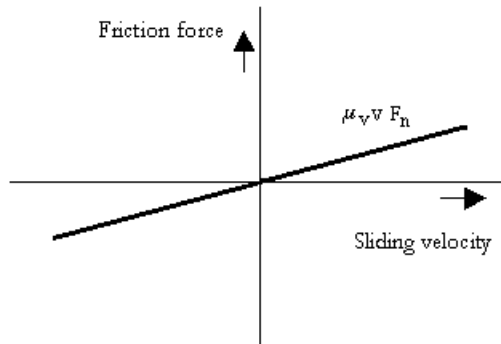
## Description - V

This model represents a brake with braking force described as viscous friction. The brake is mounted to the fixed world. The amount of friction depends on the normal force that is applied:

$$p.T = F_n * \mu_v * p.\omega;$$

$F_n$ : normal force (given by the input signal  $F_n$ )

$\mu_v$ : the viscous friction coefficient



### Interface - V

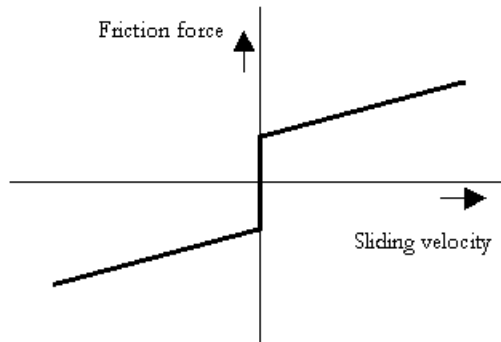
Ports	Description
p[any]	Any number of connections can be made (Rotation).
<b>Causality</b>	
Fixed torque out	
<b>Input</b>	
Fn	Normal force [N]
<b>Parameters</b>	
mu_v	Viscous friction coefficient [m.s/rad]

### Description - CV

This model represents a brake with braking force described as coulomb plus viscous friction. The brake is mounted to the fixed world. The amount of friction depends on the normal force that is applied:

$$p.T = F_n * (\mu_c * \tanh(\text{slope} * p.\omega) + \mu_v * p.\omega);$$

*Fn*: normal force (given by the input signal Fn)  
*mu\_v*: the viscous friction coefficient  
*mu\_c*: the coulomb friction coefficient  
*slope*: the steepness of the coulomb friction curve.



## Interface - CV

Ports	Description
p[any]	Any number of connections can be made (Rotation).

### Causality

Fixed torque out

### Input

Fn	Normal force [N]
----	------------------

### Parameters

mu_v	Viscous friction coefficient [ms/rad]
mu_cv	Coulomb friction coefficient [m]
slope	Steepness of Coulomb friction curve [s/rad]

## Description - SCVS

This model represents a brake with braking force described as static plus coulomb plus viscous plus Stribeck friction. The brake is mounted to the fixed world. The amount of friction depends on the normal force that is applied:

$$p.T = F_n * ((\mu_c + (\mu_s * \text{abs}(\tanh(\text{slope} * p.\omega)) - \mu_c) * \exp(-(p.\omega / v_{st})^2)) * \text{sign}(p.\omega) + \mu_v * p.\omega);$$

*Fn*: normal force (given by the input signal Fn)

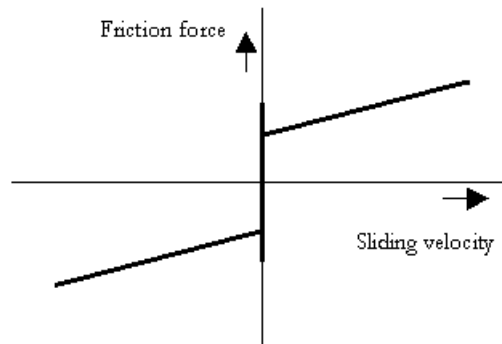
*mu\_s*: the static friction coefficient

*mu\_v*: the viscous friction coefficient

*mu\_c*: the coulomb friction coefficient

*slope*: the steepness of the coulomb and static friction curve.

*v\_st*: the characteristic Stribeck velocity.



### Interface - SCVS

Ports	Description
p[any]	Any number of connections can be made (Rotation).
<b>Causality</b>	
Fixed torque out	
<b>Input</b>	
Fn	Normal force [N]
<b>Parameters</b>	
mu_s	Static friction coefficient [m]
mu_v	Viscous friction coefficient [m.s/rad]
mu_cv	Coulomb friction coefficient [m]
slope	Steepness of Coulomb friction curve [s/rad]
v_st	Characteristic Stribeck velocity [rad/s]

### Description - LuGre

This model represents a brake with braking force described by the LuGre friction model. The brake is mounted to the fixed world. The amount of friction depends on the normal force that is applied:

$$p.T = FN * f\_lg(p.\omega);$$

*Fn*: normal force (given by the input signal Fn)

*f\_lg*: the LuGre friction model

### Interface - LuGre

Ports	Description
p[any]	Any number of connections can be made (Rotation).
<b>Causality</b>	
Fixed Torque out	

**Input**

$F_n$  Normal force [N]

**Parameters**

$\mu_c$  Coulomb friction coefficient  
 $\mu_s$  Static friction coefficient [m]  
 $\mu_v$  Viscous friction coefficient [ms/rad]  
 $v_{st}$  Characteristic Stribeck velocity [rad/s]  
 $\mu_k$  rotational stiffness coefficient at zero speed [m/rad]

Iconic Diagrams\Mechanical\Rotation\Components

**Implementations**

C  
V  
CV  
SCVS  
LuGre

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

**Introduction**

The clutch models model represent friction relative to other objects. The amount of friction depends on the normal force that is applied and the friction function that is used. The normal force is given by the input signal  $F_N$ .



The port  $p$  of the clutch model has separate high and low terminals. The equations are:

$$p.T = p_{high}.T = p_{low}.T$$

$$p.\omega = p_{high}.\omega - p_{low}.\omega$$

Due to the use of normal force, the clutch models all have a fixed torque out causality. The constitutive equations are therefore described as:

$$p.T = F_n * f(p.\omega);$$

with  $f$  the friction function.

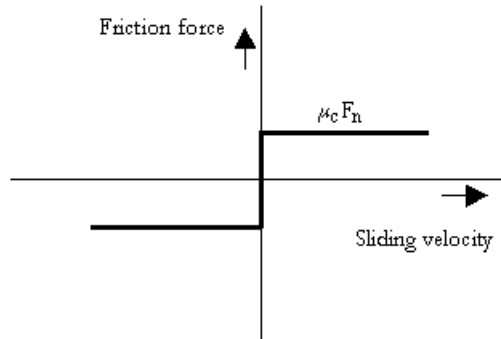
**Description - C**

This model represents bearing with friction force described as coulomb friction. The amount of friction depends on the normal force that is applied and the friction function that is used:

$$p.T = T_c * \tanh(\text{slope} * p.\omega);$$

$T_c$ : coulomb friction

*slope*: the steepness of the coulomb friction curve.



## Interface - C

### Ports

p Both terminals of port p (Rotation).

### Causality

Fixed torque out

### Input

$F_n$  Normal force [N]

### Parameters

$T_c$  Coulomb friction [N.m]

*slope* Steepness of Coulomb friction curve [s/rad]

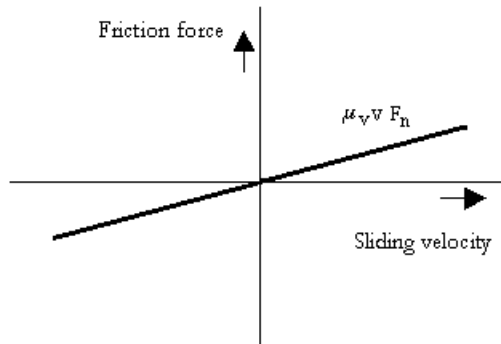
## Description - V

This model represents a clutch with friction force described as viscous friction. The amount of friction depends on the normal force that is applied and the friction function that is used:

$$p.T = F_n * \mu_{u\_v} * p.\omega;$$

$F_n$ : normal force (given by the input signal  $F_n$ )

$\mu_{u\_v}$ : the viscous friction coefficient



### Interface - V

Ports	Description
p_high, p_low	Both terminals of port p (Rotation).

#### Causality

Fixed torque out

#### Input

Fn	Normal force [N]
----	------------------

#### Parameters

mu_v	Viscous friction coefficient [m.s/rad]
------	--

### Description - CV

This model represents a clutch with friction force described as coulomb plus viscous friction. The amount of friction depends on the normal force that is applied and the friction function that is used:

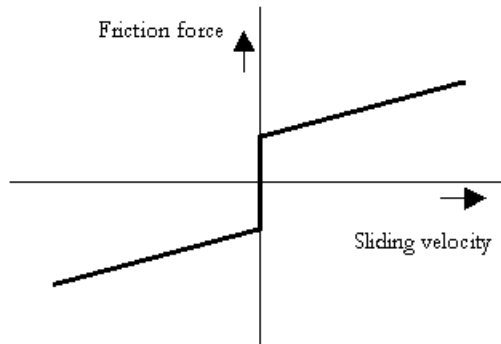
$$p.T = Fn*(Tc*\tanh(slope*p.\omega) + \mu_v*p.\omega);$$

*Fn*: normal force (given by the input signal Fn)

*mu\_v*: the viscous friction coefficient

*Tc*: the coulomb friction coefficient

*slope*: the steepness of the coulomb friction curve.



## Interface - CV

### Ports Description

p\_high, p\_low Both terminals of port p (Rotation).

### Causality

Fixed torque out

### Input

Fn Normal force [N]

### Parameters

mu\_v Viscous friction coefficient [m.s/rad]

Tc Coulomb friction [N.m]

slope Steepness of Coulomb friction curve [s/rad]

## Description - SCVS

This model represents a clutch with friction force described as static plus coulomb plus viscous plus Stribeck friction. The amount of friction depends on the normal force that is applied and the friction function that is used:

$$p.T = F_n * ((T_c + (\mu_{st} * \text{abs}(\tanh(\text{slope} * p.\omega)) - T_c) * \exp(-(p.\omega / v_{st})^2)) * \text{sign}(p.\omega) + \mu_v * p.\omega);$$

*Fn*: normal force (given by the input signal Fn)

*mu\_s*: the static friction coefficient

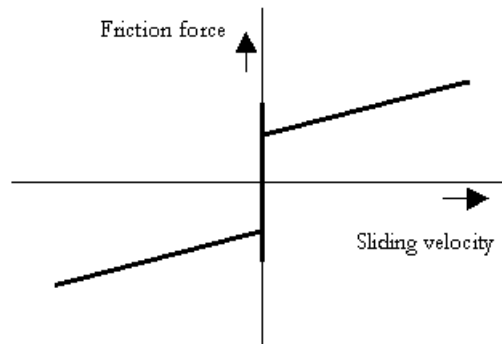
*mu\_v*: the viscous friction coefficient

*Tc*: the coulomb friction coefficient

*slope*: the steepness of the coulomb and static friction curve.

*v\_st*: the characteristic Stribeck velocity.





### Interface - SCVS

Ports	Description
p_high, p_low	Both terminals of port p (Rotation).

#### Causality

Fixed torque out

#### Input

Fn	Normal force [N]
----	------------------

#### Parameters

mu_s	Static friction coefficient [m]
mu_v	Viscous friction coefficient [m.s/rad]
Tc	Coulomb friction [N.m]
slope	Steepness of Coulomb friction curve [s/rad]
v_st	Characteristic Stribeck velocity [rad/s]

### Description - LuGre

This model represents a clutch with friction force described by the LuGre friction model. The amount of friction depends on the normal force that is applied and the friction function that is used:

$$p.T = FN * f_{lg}(p.\omega);$$

*Fn*: normal force (given by the input signal Fn)

*f<sub>lg</sub>*: the LuGre friction model

### Interface- LuGre

Ports	Description
p_high, p_low	Both terminals of port p (Rotation).

#### Causality

Fixed torque out

#### Input

$F_n$  Normal force [N]

### Parameters

$T_c$  Coulomb friction coefficient  
 $\mu_s$  Static friction coefficient [m]  
 $\mu_v$  Viscous friction coefficient [m.s/rad]  
 $v_{st}$  Characteristic Stribeck velocity [rad/s]  
 $\mu_k$  rotational stiffness coefficient at zero speed [m/rad]

### Library

Iconic Diagrams\Mechanical\Rotation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

This model represents a linear damper. It can have an torque out as well as an angular velocity out causality. In the last case the constitutive equation, as shown below, is simply inverted. The port  $p$  of the damper model has separate high and low terminals. The equations are:

$$p.T = p_{high}.T = p_{low}.T$$

$$p.\omega = p_{high}.\omega - p_{low}.\omega$$

Torque out causality:

$$p.T = d * p.\omega;$$

Angular velocity out causality:

$$p.\omega = p.T / d;$$

### Interface

#### Ports

$p_{high}$ ,  $p_{low}$

#### Description

Both terminals of the Rotation port  $p$ .

#### Causality

indifferent

#### Parameters

$d$  damping [Nms/rad]

## Library

Iconic Diagrams\Mechanical\Rotation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

This model represents the fixed world (angular velocity = 0). The model has only one initial port  $p$  defined. Because any number of connections can be made, successive ports are named  $p_1$ ,  $p_2$ ,  $p_3$  etc. which gives the constitutive equations:

$$p_1.\omega = p_2.\omega = \dots = p_n.\omega = 0;$$

$$p_1.T = \text{free}; p_2.T = \text{free}; \dots; p_n.T = \text{free};$$

### Interface

Ports	Description
-------	-------------

$p$ [any]	Any number of connections can be made.
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### Causality

Fixed angular velocity out  
All ports have a fixed angular velocity out causality.

Iconic Diagrams\Mechanical\Rotation\Components

## Implementations

C  
V  
CV  
SCVS  
LuGre

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Introduction

The friction model represent bearing friction with various friction models. The model have only one initial port  $p$  defined. Because any number of connections can be made, successive ports are named  $p_1$ ,  $p_2$ ,  $p_3$  etc. 20-sim will automatically create equations such that the resulting force  $p.F$  is equal to the sum of the forces of all connected ports  $p_1 \dots p_n$ . The velocities of all connected ports are equal to  $p.v$ .

$$p.F = \text{sum}(p_1.F, p_2.F, \dots)$$

$$p.v = p_1.v = p_2.v = \dots$$

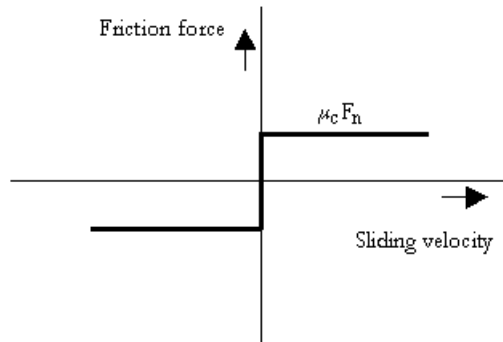
### Description - C

This model represents a bearing with friction torque described as coulomb friction:

$$p.T = T_c * \tanh(\text{slope} * p.\omega);$$

$T_c$ : the coulomb friction

$\text{slope}$ : the steepness of the coulomb friction curve.



## Interface - C

### Ports

$p[\text{any}]$

### Description

Any number of connections can be made (Rotation).

### Causality

Fixed torque out

### Parameters

$T_c$

Coulomb friction [N.m]

$\text{slope}$

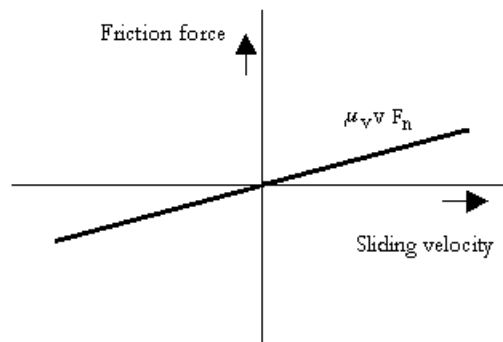
Steepness of Coulomb friction curve [s/rad]

## Description - V

This model represents a bearing with friction force described as viscous friction:

$$p.T = d * p.\omega;$$

$d$ : the viscous damping



## Interface - V

Ports	Description
p[any]	Any number of connections can be made (Rotation).

### Causality

Fixed torque out

### Input

Fn	Normal force [N]
----	------------------

### Parameters

mu_v	Viscous damping [N.m.s/rad]
------	-----------------------------

## Description - CV

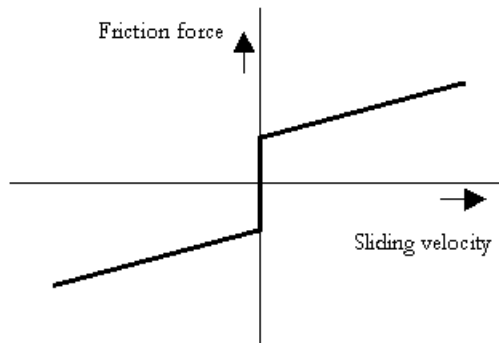
This model represents a bearing with friction force described as coulomb plus viscous friction:

$$p.T = T_c * \tanh(\text{slope} * p.\omega) + \mu_v * p.\omega;$$

*d*: the viscous damping

*T<sub>c</sub>*: the coulomb friction

*slope*: the steepness of the coulomb friction curve.



## Interface - CV

Ports	Description
p[any]	Any number of connections can be made (Rotation).

### Causality

Fixed torque out

### Input

Fn	Normal force [N]
----	------------------

### Parameters

mu_v	Viscous damping [N.m.s/rad]
------	-----------------------------

Tc	Coulomb friction [N.m]
slope	Steepness of Coulomb friction curve [s/rad]

### Description - SCVS

This model represents a bearing with friction force described as static plus coulomb plus viscous plus Stribeck friction:

$$p.T = ((Tc + (Tst * \text{abs}(\tanh(\text{slope} * p.\omega)) - Tc) * \exp(-(p.\omega / v_{st})^2)) * \text{sign}(p.\omega) + d * p.\omega);$$

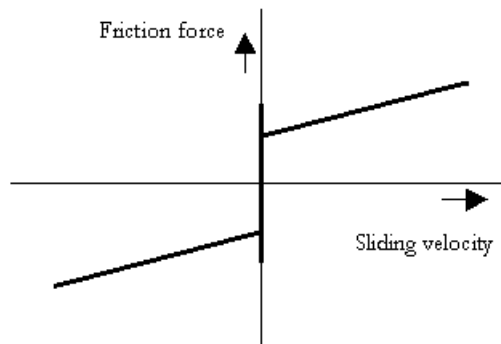
*Tst*: the static friction

*d*: the viscous damping

*Tc*: the coulomb friction

*slope*: the steepness of the coulomb and static friction curve.

*v<sub>st</sub>*: the characteristic Stribeck velocity.



### Interface - SCVS

Ports	Description
p[any]	Any number of connections can be made (Rotation).

#### Causality

Fixed torque out

#### Input

Fn	Normal force [N]
----	------------------

#### Parameters

Tst	Static friction [N.m]
d	Viscous damping [N.m.s/rad]
Tc	Coulomb friction [N.m]
slope	Steepness of Coulomb friction curve [s/rad]
v <sub>st</sub>	Characteristic Stribeck velocity [rad/s]

### Description - LuGre

This model represents a bearing with friction force described by the LuGre friction model:

$$p.T = f\_lg(p.\omega);$$

$f\_lg$ : the LuGre friction model

## Interface- LuGre

Ports	Description
p[any]	Any number of connections can be made (Rotation).
<b>Causality</b>	
Fixed torque out	
<b>Input</b>	
Fn	Normal force [N]
<b>Parameters</b>	
Tc	Coulomb friction [N.m]
mu_s	Static friction coefficient [m]
d	Viscous damping [N.m.s/rad]
v_st	Characteristic Stribeck velocity [rad/s]
c	Stiffness at zero speed [N.m/rad]

## Library

Iconic Diagrams\Mechanical\Rotation\Components

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description

This model represents an ideal rotational inertia. The element has a preferred angular velocity out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred torque out causality. The constitutive equations then contain a derivation. The model has only one initial port p defined. Because any number of connections can be made, successive ports are named p1, p2, p3 etc. 20-sim will automatically create equations such that the resulting torque  $p.T$  is equal to the sum of the torques of all connected ports p1 .. pn and that the angular velocities of all connected ports is equal to  $p.\omega$ .

$$p.T = \text{sum}(p1.T, p2.T, \dots)$$

$$p.\omega = p1.\omega = p2.\omega = \dots$$

angular velocity out causality (preferred):

$$\alpha = p.T/J;$$

$$p.\omega = \text{int}(\alpha);$$

$$\phi = \text{int}(p.\omega);$$

torque out causality:

```

alpha = ddt(p.omega);
p.T = J*alpha;
phi = int(p.omega);

```

## Interface

### Ports

p[any]

### Description

Any number of connections can be made (Rotation).

### Causality

preferred angular velocity out

An torque out causality results in a derivative constitutive equation.

### Variables

phi

angle [rad]

alpha

angular acceleration [rad/s<sup>2</sup>]

### Parameters

J

moment of inertia [kgm<sup>2</sup>]

### Initial Values

p.omega\_initial

The initial velocity of the inertia [rad/s].

phi\_initial

The initial angle of the inertia [rad].

## Library

Iconic Diagrams\Mechanical\Rotation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

This node model represents a structural connection between two (or more) shafts, where the velocity of all connected shafts is equal. The model has only one initial port p defined. Because any number of connections can be made, successive ports are named p1, p2, p3 etc.

## Interface

### Ports

p [any]

### Description

Any number of connections can be made (Rotation).



## Library

Iconic Diagrams\Mechanical\Rotation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

This model represents an ideal rotational spring. The element has a preferred torque out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred angular velocity out causality. The constitutive equations then contain a derivation. The port  $p$  of the spring model has separate high and low terminals. The equations are:

$$\begin{aligned} p.T &= p\_high.T = p\_low.T \\ p.\omega &= p\_high.\omega - p\_low.\omega \end{aligned}$$

torque out causality (preferred):

$$\begin{aligned} \phi &= \text{int}(p.\omega); \\ p.T &= c * \phi; \end{aligned}$$

angular velocity out causality:

$$\begin{aligned} p.\omega &= \text{ddt}(\phi); \\ \phi &= p.T/k; \end{aligned}$$

### Interface

#### Ports

$p\_high$ ,  $p\_low$

#### Description

Both terminals of the Rotational port  $p$ .

#### Causality

preferred torque out

An angular velocity out causality results in a derivative constitutive equation.

#### Variables

$\phi$

torsion of the spring [rad]

#### Parameters

$c$

Stiffness [Nm/rad]

#### Initial Values

$\phi\_initial$

The initial torsion of the spring [rad].

## Library

Iconic Diagrams\Mechanical\Rotation\Components

## Implementations

Default  
Stiffness  
Frequency

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description - Default

This model represents an ideal rotational spring with damper. The element has a preferred torque out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred angular velocity out causality. The constitutive equations then contain a derivation. The port  $p$  of the spring model has separate high and low terminals. The equations are:

$$\begin{aligned} p.T &= p\_high.T = p\_low.T \\ p.\omega &= p\_high.\omega - p\_low.\omega \end{aligned}$$

Torque out causality (preferred):

$$\begin{aligned} \phi &= \text{int}(p.\omega); \\ p.T &= c * \phi + d * p.\omega; \end{aligned}$$

Angular velocity out causality:

$$\begin{aligned} p.\omega &= \text{ddt}(\phi); \\ \phi &= (p.T - d * p.\omega) / c; \end{aligned}$$

## Interface - Default

### Ports

p\_high  
p\_low

### Description

Two ports of the spring (Rotation).

### Causality

preferred torque out

An angular velocity out causality results in a derivative constitutive equation.

### Variables

$\phi$  torsion of the spring [rad]

### Parameters

$c$  Rotational stiffness [Nm /rad]  
 $d$  Damping [Nms/rad]

### Initial Values

phi\_initial                      The initial torsion of the spring [rad].

### Description - Stiffness

This model represents an ideal rotational spring with damper. The damping value ( $d$ ) is calculated on the basis of a known stiffness ( $c$ ), relative damping ( $b$ ) and reference inertia ( $J$ ). The inertia is only used to compute the damping (no actual mass is used in this component).

The element has a preferred torque out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred angular velocity out causality. The constitutive equations then contain a derivation. The port  $p$  of the spring model has separate high and low terminals. The equations are:

$$\begin{aligned} p.T &= p\_high.T = p\_low.T \\ p.\omega &= p\_high.\omega - p\_low.\omega \end{aligned}$$

Torque out causality (preferred):

$$\begin{aligned} \phi &= \int(p.\omega); \\ p.F &= c * \phi + d * p.\omega; \\ d &= 2 * b * \sqrt{c * J}; \end{aligned}$$

Angular velocity out causality:

$$\begin{aligned} p.\omega &= \text{ddt}(\phi); \\ \phi &= (p.T - d * p.\omega) / c; \\ d &= 2 * b * \sqrt{c * J}; \end{aligned}$$

### Interface - Stiffness

#### Ports

p\_high  
p\_low

#### Description

Two ports of the spring (Rotation).

#### Causality

preferred torque out

An angular velocity out causality results in a derivative constitutive equation.

#### Variables

phi                      torsion of the spring [rad]  
d                        damping [Nms/rad]

#### Parameters

c                        Rotational stiffness [Nm /rad]  
b                        Relative damping []  
J                        Moment of inertia [kgm<sup>2</sup>]

#### Initial Values

phi\_initial            The initial torsion of the spring [rad].

## Description - Frequency

This model represents an ideal rotational spring with damper. The stiffness ( $c$ ) is calculated on basis of a known resonance frequency ( $f$ ). The damping value ( $d$ ) is calculated on the basis of the stiffness, relative damping ( $b$ ) and reference inertia ( $J$ ). The inertia is only used to compute the damping (no actual mass is used in this component).

The element has a preferred torque out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred angular velocity out causality. The constitutive equations then contain a derivation. The port  $p$  of the spring model has separate high and low terminals. The equations are:

$$\begin{aligned} p.T &= p\_high.T = p\_low.T \\ p.\omega &= p\_high.\omega - p\_low.\omega \end{aligned}$$

Torque out causality (preferred):

$$\begin{aligned} \phi &= \text{int}(p.\omega); \\ p.T &= c * \phi + d * p.\omega; \\ c &= J * (2 * \pi * f)^2; \\ d &= 2 * b * \sqrt{c * J}; \end{aligned}$$

Angular velocity out causality:

$$\begin{aligned} p.\omega &= \text{ddt}(\phi); \\ \phi &= (p.T - d * p.\omega) / c; \\ c &= J * (2 * \pi * f)^2; \\ d &= 2 * b * \sqrt{c * J}; \end{aligned}$$

## Interface - Frequency

### Ports

$p\_high$   
 $p\_low$

### Description

Two ports of the spring (Rotation).

### Causality

preferred torque out

An angular velocity out causality results in a derivative constitutive equation.

### Variables

$\phi$	torsion of the spring [rad]
$c$	rotational stiffness [Nm /rad]
$d$	damping [Nms/rad]

### Parameters

$f$	Resonance frequency [Hz]
$b$	Relative damping []
$J$	Moment of inertia [kgm <sup>2</sup> ]

### Initial Values

$\phi\_initial$	The initial torsion of the spring [rad].
-----------------	--

## Library

Iconic Diagrams\Mechanical\Rotation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

### Description

This model can be used to connect any open end of another model that is not connected to the fixed world. It generates a fixed torque of 0 N while the angular velocity is free:

$$\begin{aligned} p.\omega &= \text{indifferent}; \\ p.T &= 0; \end{aligned}$$

### Interface

Ports	Description
p	rotation port
<b>Causality</b>	
Fixed torque out	

## Library

Iconic Diagrams\Mechanical\Rotation\Gears

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation/Translation).

### Description

This models represents a belt and pulley. The connection to the pulley is through the rotation port  $p_{rot}$ . The connection to the belt is through the translation port  $p_{trans}$ . The model is ideal, i.e. there are no compliances or inertias. The causality of this model is always mixed: torque out & velocity out or angular velocity out & force out:

$$\begin{aligned} p_{rot}.T &= radius * p_{trans}.F \\ p_{trans}.v &= radius * p_{rot}.\omega \end{aligned}$$

or:

$$p\_trans.F = 1/radius * p\_rot.T$$

$$p\_rot.omega = 1/radius * p\_trans.v$$

## Interface

Ports	Description
p_rot	Rotation port.
p_trans	Translation port.

### Causality

p_rot	notequal
p_trans	

### Parameters

radius	pulley radius [m]
--------	-------------------

## Library

Iconic Diagrams\Mechanical\Rotation\Gears  
Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation/Translation).

## Description

This is a masked model which opens the Cam Wizard when edited. Depending on the selections entered, various cam motion profiles can be generated.

## Interface

Ports	Description
p_in	Driving axis (Rotation)
p_out	Output port with resulting motion (Rotation or Translation)

### Parameters

stroke	amplitude of resulting motion
start_angle	start angle motion
stop_angle	angle when the maximum is reached
return_angle	start angle of the return motion
end_angle	finish angle of the return motion

## Library

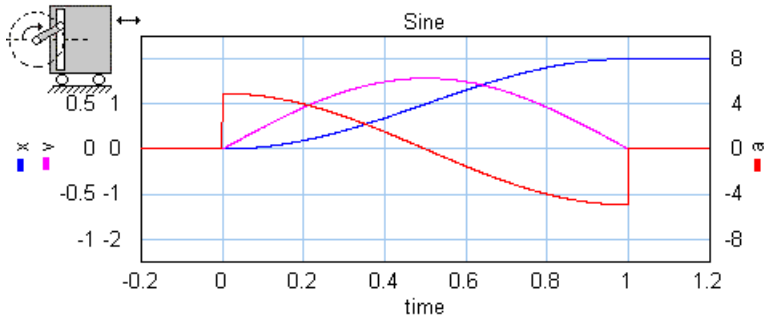
Iconic Diagrams\Mechanical\Rotation\Gears  
Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description

This models represents a cam and rod mechanism. If the input shaft is rotating with a constant speed, the output motion is a pure sinusoidal.



The mechanism is ideal, i.e., it does not have inertia, friction or geometrical limitations. It has one rotation port ( $p_{in}$ ) and one translation port ( $p_{out}$ ). The causality of this model is always mixed: one port has a force out causality while the other has a velocity out causality:

$$p_{in}.T = i * p_{out}.F$$

$$p_{out}.v = i * p_{in}.omega$$

The transmission ratio ( $i$ ) is the ratio of the velocities of both ports (in fact a sinusoidal function of the shaft angle).

## Interface

Ports	Description
$p_{in}$	Driving axis (Rotation)
$p_{out}$	Output port with resulting motion (Translation)

## Causality

fixed torque out

$p_{in}$

fixed velocity out

$p_{out}$

## Parameters

stroke                      Stroke of the translation port (is equal to half the length of the rod).

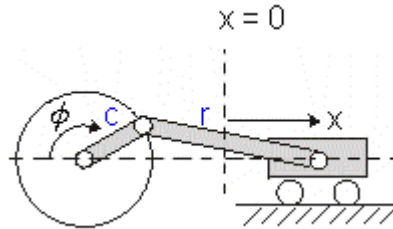
## Library

Iconic Diagrams\Mechanical\Rotation\Gears  
Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description



This model represents a crank and rod mechanism. The mechanism is ideal, i.e., it does not have inertia, friction or geometrical limitations. It has one rotation port (*p\_in*) and one translation port (*p\_out*). The causality of this model is always mixed: one port has a force out causality while the other has a velocity out causality:

$$p_{in}.T = i * p_{out}.F$$

$$p_{out}.v = i * p_{in}.omega$$

The transmission ratio (*i*) is the ratio of the velocities of both ports. It is a function of the shaft angle, the crank length and the rod length.

## Interface

Ports	Description
p_in	Driving axis (Rotation)
p_out	Output port with resulting motion (Translation)

### Causality

fixed torque out  
 p\_in  
 fixed velocity out  
 p\_out

### Parameters

crank_length	Crank length [m]
rod_length	Rod length [m]

## Library

Iconic Diagrams\Mechanical\Rotation\Gears

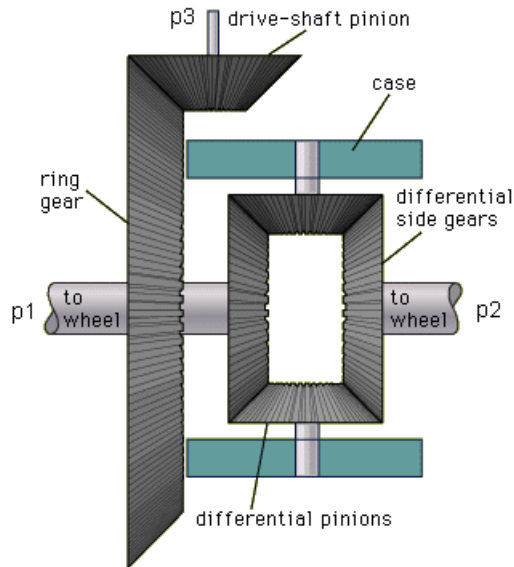
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description

A differential gear is well known for its use in automotive mechanics. It transfers power from the engine to the wheels, dividing the force equally between them but permitting them to follow paths of different lengths when turning a corner.





When  $p3$  is the drive-shaft and  $p1$  and  $p2$  the shafts connected to the wheels, the constitutive equations for this model are:

$$p3.\omega * 2 * i = p1.\omega + p2.\omega;$$

$$p1.T = p2.T = p3.T / (2 * i);$$

with  $i$  the gear ratio. The gear ratio is equal to the diameter of the drive shaft pinion divided by the diameter of the ring gear, which makes it equivalent to the angular velocity of the drive shaft divided by the average angular velocity of the wheel shafts:

$$i = p3.\omega / ((p1.\omega + p2.\omega) / 2);$$

## Interface

Ports	Description
$p1$	drive shaft port (Rotation)
$p2, p3$	driven shafts ports (Rotation)
Parameters	
$i$	gear ratio []

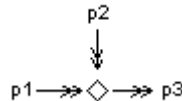
## Library

Iconic Diagrams\Mechanical\Rotation\Gears

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description

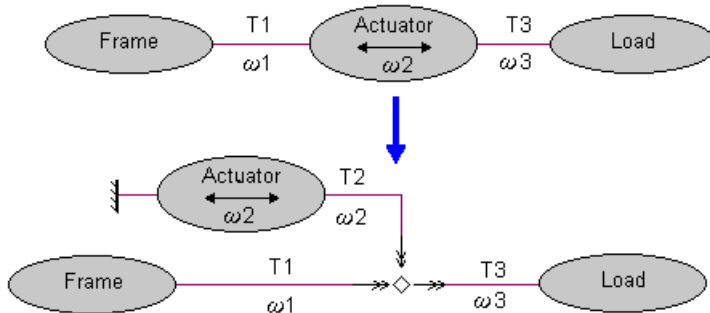


This model is equivalent to the fork model of the Translation library. It represents a special type of node where the torques are equal and the angular velocities are added:

$$p3.\omega = p1.\omega + p2.\omega;$$

$$p1.T = p2.T = p3.T;$$

This model can for example be used for actuators that generate a torque difference. With the differential model an equivalent model can be found with the actuator attached to the fixed world:



## Interface

Ports	Description
p1,p2,p3	Rotation ports.

## Library

Iconic Diagrams\Mechanical\Rotation\Gears

## Implementations

Ideal  
Lossy

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

**Description - Ideal**

This models represents any type of gearbox with two counter rotating shafts. The gear is ideal, i.e., it does not have inertia or friction. The gear has one fast moving shaft and one slow moving shaft. The gearbox has a reduction of  $i : 1$  and thus a transmission ratio of  $1/i$ .

The causality of this model is always mixed: one port has a torque out causality while the other has an angular velocity out causality:

$$\begin{aligned} p_{in}.T &= -1/i * p_{out}.T \\ p_{out}.omega &= -1/i * p_{in}.omega \end{aligned}$$

or:

$$\begin{aligned} p_{out}.T &= -i * p_{in}.T \\ p_{in}.omega &= -i * p_{out}.omega \end{aligned}$$

**Interface- Ideal**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p_in	Input port
p_out	Output port

**Causality**

p_in	not	equal
p_out		

**Parameters**

i	gearbox reduction, $i > 1$
---	----------------------------

**Description - Lossy**

This models represents any type of gearbox with two counter rotating shafts. The gearbox has a reduction of  $i : 1$  and thus a transmission ratio of  $1/i$ .

$$p_{in}.omega = -i * p_{out}.omega$$

Unlike the model of an ideal gearbox, this model includes rotational inertia and power loss. The inertia is defined at the input axis. If the gearbox manufacturer gives the inertia at the output axis you can calculate the inertia at input axis as:

$$J_{input} = J_{output}/i^2$$

The power loss is represented by the efficiency, where the efficiency is defined as the output power divided by the input power:

$$eff = P_{out} / P_{in}$$

The efficiency is a value between zero and one and given by the gearbox manufacturer. If you do not know the value, a good guess is a power loss of 2% per stage ( $eff = 0.98$ ). If your gearbox for example contains three stages, you can set the efficiency as:

$$eff = 0.98 * 0.98 * 0.98 = 0.94$$

### Interface - Lossy

#### Ports

Ports	Description
p_in	Input port
p_out	Output port

#### Causality

preferred angular  
velocity out p\_in  
preferred angular  
velocity out p\_out

#### Parameters

i	gearbox reduction [-], $i > 1$
J	moment of inertia [kgm <sup>2</sup> ]
eff	gearbox efficiency [-]

### Library

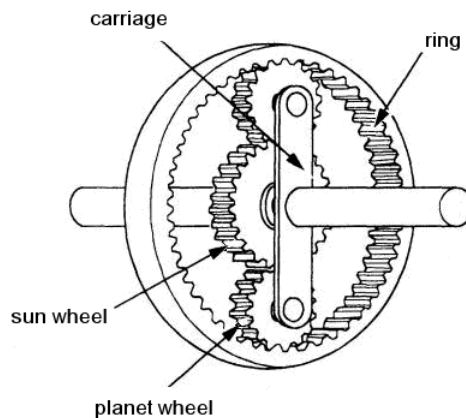
Iconic Diagrams\Mechanical\Rotation\Gears

#### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

#### Description

A planetary gear is well known for its use in automotive mechanics. It transfers power from a sun wheel to the planet wheels and the ring. In standard planetary gears, the planet wheels are connected by a carriage. I.e the gear has three rotation ports: the sun, the carriage and the ring.



The model that is used here is ideal. I.e. there is only power flow between the three axes. No internal dynamics or friction are incorporated. If the inertia cannot be neglected, you can easily add inertia models to the ports of the planetary gear model.

The number of teeth of the planet wheels are uniquely defined by the number of teeth of the sun wheel and the ring by:

$$z_p = (z_r - z_s)/2;$$

Therefore the ratio between the sun teeth and the ring teeth:

$$z = z_r / z_s;$$

determine the transmission ratio of the gearbox and therefore the dynamic equations of the gearbox:

$$\begin{aligned} carriage.\omega &= sun.\omega * (1/(1 + z)) + ring.\omega * (z/(1 + z)); \\ ring.T &= carriage.T * (z/(1 + z)); \\ sun.T &= carriage.T * (1/(1 + z)); \end{aligned}$$

## Interface

Ports	Description
sun	shaft attached to the sun wheel (Rotation)
carriage	shaft attached to the carriage (Rotation)
ring	shaft attached to the ring (Rotation)
<b>Parameters</b>	
z	number of ring teeth divided by the number of sun teeth []

## Library

Iconic Diagrams\Mechanical\Rotation\Gears  
Iconic Diagrams\Mechanical\Translation\Transmission

## Implementations

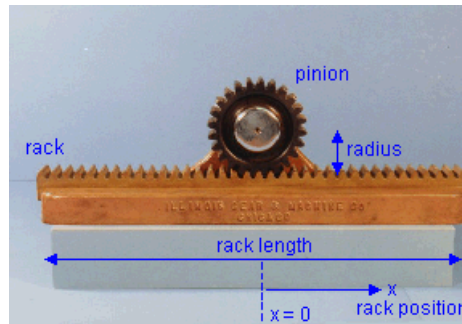
FixedPinion  
FixedRack

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation/Translation).

## Description - FixedPionion

This models represents a rack and pinion gear. The connection to the pinion gear is through the rotation port *p\_rot*. The connection to the rack is through the translation port *p\_trans*. The model is ideal, i.e. there is no compliance nor inertia nor backlash.



In this model the pinion bearing is connected to the fixed world and the rack is free to move. This is contrary to the model FixedRackPinionGear where the pinion bearing is free to move and the rack is connected to the fixed world.

The causality of this model is always mixed: torque out & velocity out or angular velocity out & force out:

$$p\_rot.T = radius * p\_trans.F$$

$$p\_trans.v = radius * p\_rot.\omega$$

or:

$$p\_trans.F = 1/radius * p\_rot.T$$

$$p\_rot.\omega = 1/radius * p\_trans.v$$

The rack position is determined by the internal variable  $x$ . For  $x = 0$ , the pinion gear is at the middle of the rack. When the pinion crosses the end of the rack, i.e.

$$abs(x) > rack\_length/2$$

a warning is given, *"WARNING: rack length has been exceeded at the rack and pinion gear!"*, and the simulation is stopped.

### Interface - FixedPionion

Ports	Description
p_rot	Rotation port.
p_trans	Translation port.

#### Causality

p_rot	notequal
p_trans	

#### Parameters

radius	pinion gear pitch radius [m]
rack_length	rack length [m]

#### Variables

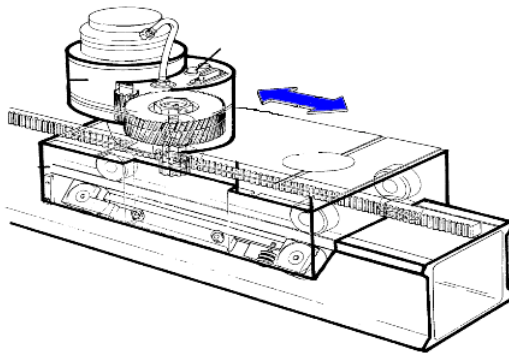
x Internal variable which denotes the rack position,  $\text{abs}(x) < \text{rack\_length}/2$   
else simulation halted.

### Initial values

x\_initial Initial rack position,  $\text{abs}(x\_initial) < \text{rack\_length}/2$

### Description - FixedRack

This models represents a fixed rack and pinion gear. The connection to the pinion gear is through the rotation port *p\_rot*. The connection to the rack is through the translation port *p\_trans*. The model is ideal, i.e. there is no compliance nor inertia nor backlash.



In this model the pinion bearing is free to move and the rack is connected to the fixed world. This is contrary to the model RackPinionGear where the pinion bearing is connected to the fixed world and the rack is free to move.

The causality of this model is always mixed: torque out & velocity out or angular velocity out & force out:

$$\begin{aligned} p\_rot.T &= radius * p\_trans.F \\ p\_trans.v &= radius * p\_rot.\omega \end{aligned}$$

or:

$$\begin{aligned} p\_trans.F &= 1/radius * p\_rot.T \\ p\_rot.\omega &= 1/radius * p\_trans.v \end{aligned}$$

The rack position is determined by the internal variable *x*. For  $x = 0$  the pinion gear is at the middle of the rack. When the pinion crosses the end of the rack, i.e.

$$\text{abs}(x) > \text{rack\_length}/2$$

a warning is given, *"WARNING: rack length has been exceeded at the rack and pinion gear!"*, and the simulation is stopped.

## Interface - FixedRack

### Ports

p_rot	Rotation port.
p_trans	Translation port.

### Causality

p_rot	notequal
p_trans	

### Parameters

radius	pinion gear pitch radius [m]
rack_length	rack length [m]

### Variables

x	Internal variable which denotes the rack position, $\text{abs}(x) < \text{rack\_length}/2$ else simulation halted.
---	--

### Initial values

x_initial	Initial rack position, $\text{abs}(x\_initial) < \text{rack\_length}/2$
-----------	---

## Library

Iconic Diagrams\Mechanical\Rotation\Gears  
Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Introduction

This models represents a spindle and nut. It transfers an angular motion of the spindle into a translational motion of the nut. The model is ideal, i.e., it does not have inertia or friction. The causality of this model is always mixed: one port has a torque out causality while the other has an angular velocity out causality:

$$\begin{aligned} p\_spindle.T &= i * p\_nut.F \\ p\_nut.v &= i * p\_spindle.omega \end{aligned}$$

or:

$$\begin{aligned} p\_nut.F &= 1/i * p\_spindle.T \\ p\_spindle.omega &= 1/i * p\_nut.v \end{aligned}$$

The model has two implementations which calculate the transform ratio  $i$  out of different parameters.

## Description - Pitch

In this implementation the transform ratio is calculated using the *pitch* (the advance of the nut during one revolution of the spindle):



$$i = \text{pitch} / (2 * \pi);$$

### Interface - Pitch

Ports	Description
p_spindle	Port at the spindle shaft (Rotation).
p_nut	Port at the wheel (Translation).

#### Causality

p\_spindle notequal  
p\_nut

#### Parameters

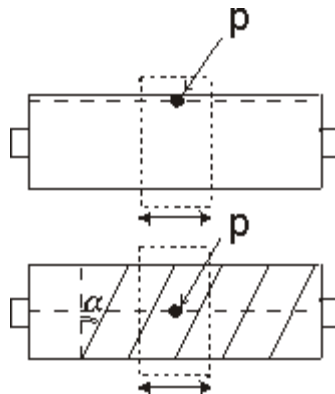
pitch translation of the nut during one revolution of the spindle [m]

### Description - LeadAngle

This implementation calculates the transform ratio out of the lead angle *alpha* and the radius *r\_spindle* of the spindle:

$$i = \tan(\alpha) * r_{\text{spindle}};$$

The pitch angle is shown in the figure below. *r\_spindle* is the effective radius of the spindle, i.e. the radius from the center of the spindle to the pitch point *p*.



### Interface -LeadAngle

Ports	Description
p_spindle	Port at the spindle shaft (Rotation).
p_nut	Port at the wheel (Translation).

#### Causality

p\_spindle notequal  
p\_nut

#### Parameters

r\_spindle                      effective radius of the spindle [m]  
 alpha                          lead angle of the spindle [rad]

## Library

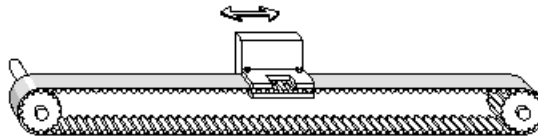
Iconic Diagrams\Mechanical\Rotation\Gears  
 Iconic Diagrams\Mechanical\Translation\Transmission

## Use

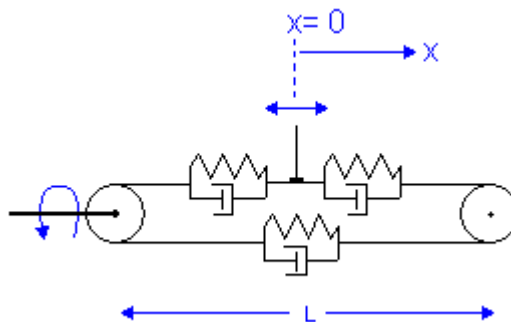
**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation/Translation).

## Introduction

This models represents a timing belt, used for linear positioning.



It has a rotating pulley which drives the the belt and clamp. The timing belt is modeled by a series of spring damper elements that convey the rotation of the pulley to a clamp translation. Because the output position is moving, stiffness and damping values are not constant.



The stiffness for a piece of belt can be expressed as:

$$k = E \cdot A / l$$

with

$E$  = Modulus of elasticity {N/m<sup>2</sup>}

$A$  = Belt area {m<sup>2</sup>}

$l$  = belt length {m}

If the belt is sufficiently pre-tensioned, the stiffness experienced at the clamp can be expressed as the combination of three individual belt parts:

$$k = E \cdot A / (0.5 \cdot l + x) + 1 / (1 / E \cdot A / (0.5 \cdot l - x) + 1 / E \cdot A / l)$$

which can be rewritten to:

$$k = E \cdot A \cdot (1 / (0.5 \cdot l + x) + 1 / (1.5 \cdot l - x))$$

The stiffness approaches infinity as the clamp moves to the driven pulley ( $x = -l/2$ ) and has a minimum value when the clamp moves to the other pulley ( $x = 0.5 \cdot l$ ). The minimum stiffness is equal to:

$$k = 2 \cdot E \cdot A / l$$

The belt position is determined by the internal variable  $x$ . For  $x = 0$  the clamp is in the middle. When the position crosses the driven pulley, i.e.

$$x < -\text{belt\_length}/2$$

the simulation is stopped: *"Error: clamp position larger than belt end!"*. When the position crosses the other pulley, i.e.

$$x > \text{belt\_length}/2$$

the simulation is also stopped, *"Error: clamp position smaller than belt start!"*.

### Description - Default

In this model the minimum stiffness is used, based on an output position at a length  $L$  of the driven pulley.

$$k = 2 \cdot E \cdot A / l$$

### Description - VariableStiffness

In this model a variable stiffness is used equal to:

$$k = E \cdot A \cdot (1 / (0.5 \cdot l + x) + 1 / (1.5 \cdot l - x))$$

Take care not to let the clamp get too close to the driven pulley, because the stiffness will then grow to infinity!

### Interface

Ports	Description
p_rot	Rotation port.
p_trans	Translation port.

### Causality

p_rot	notequal
p_trans	

### Parameters

radius	pinion gear pitch radius [m]
d	damping N.s/m]
E	Modulus of elasticity [N/m <sup>2</sup> ]

A                      A = Belt area [m2]

l                      belt length [m]

### Variables

x                      clamp position,  $\text{abs}(x) < \text{belt length}/2$

### Initial values

x\_initial              Initial clamp position,  $\text{abs}(x\_initial) < \text{belt length}/2$

## Library

Iconic Diagrams\Mechanical\Rotation\Gears

## Implementations

Ideal

Lossy

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description - Ideal

This models represents any type of gearbox with two shafts rotating in the same direction. The gear is ideal, i.e., it does not have inertia or friction. The gear has one fast moving shaft and one slow moving shaft. The gearbox has a reduction of  $i : 1$  and thus a transmission ratio of  $1/i$ .

The causality of this model is always mixed: one port has a torque out causality while the other has an angular velocity out causality:

$$\begin{aligned} p_{in}.T &= 1/i * p_{out}.T \\ p_{out}.omega &= 1/i * p_{in}.omega \end{aligned}$$

or:

$$\begin{aligned} p_{out}.T &= i * p_{in}.T \\ p_{in}.omega &= i * p_{out}.omega \end{aligned}$$

## Interface - Ideal

### Ports                      Description

p\_in                      Input port

p\_out                      Output port

### Causality

p\_in    not    equal

p\_out

### Parameters

i                      gearbox reduction,  $i > 1$

### Description - Lossy

This model represents any type of gearbox with two shafts rotating in the same direction. The gearbox has a reduction of  $i : 1$  and thus a transmission ratio of  $1/i$ .

$$p_{in}.omega = i * p_{out}.omega$$

Unlike the model of an ideal gearbox, this model includes rotational inertia and power loss. The inertia is defined at the input axis. If the gearbox manufacturer gives the inertia at the output axis you can calculate the inertia at input axis as:

$$J_{input} = J_{output}/i^2$$

The power loss is represented by the efficiency, where the efficiency is defined as the output power divided by the input power:

$$eff = P_{out} / P_{in}$$

The efficiency is a value between zero and one and given by the gearbox manufacturer. If you do not know the value, a good guess is a power loss of 2% per stage ( $eff = 0.98$ ). If your gearbox for example contains three stages, you can set the efficiency as:

$$eff = 0.98 * 0.98 * 0.98 = 0.94$$

### Interface - Lossy

Ports	Description
p_in	Input port
p_out	Output port

#### Causality

preferred angular  
velocity out p\_in  
preferred angular  
velocity out p\_out

#### Parameters

i	gearbox reduction [-], $i > 1$
J	moment of inertia [kgm <sup>2</sup> ]
eff	gearbox efficiency [-]

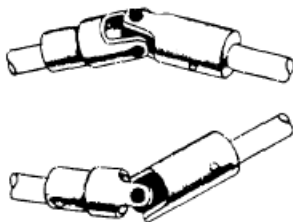
## Library

Iconic Diagrams\Mechanical\Rotation\Gears

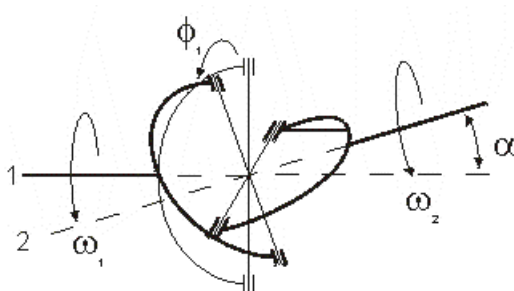
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description



Universal Joint couplings are used to couple axes which are not aligned. They can be used in single or double set-up. Consider the single Universal Joint coupling, shown in the picture below.



Due to the nature of the coupling, the output angular velocity  $\omega_1$  will show a sinusoidal ripple, compared to the input angular velocity  $\omega_2$ :

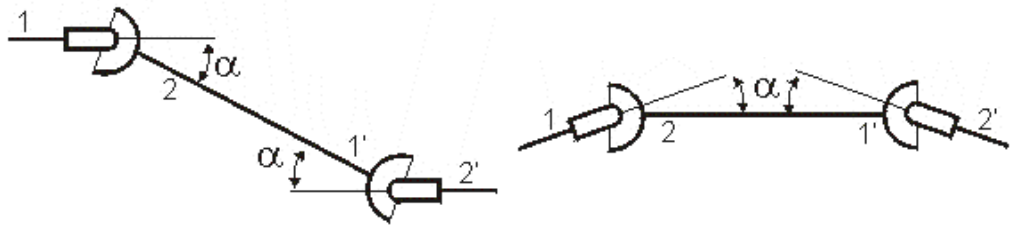
$$\omega_2 = \frac{\cos(\alpha)}{1 - \cos^2(\varphi_1) \sin^2(\alpha)} \cdot \omega_1$$

with  $\alpha$  the angle between the two axes and  $\varphi_1$  the initial rotation of the input axis. The initial rotation  $\varphi_1$  is defined with respect to a plane that is spanned by the axes (1 and 2).

When two Universal Joint couplings are combined, the angular velocity of the output axis will be equal to the angular velocity of the input axis (e.g. no ripple) when two conditions are met. When the output axis of the first coupling is connected to the input axis of the second coupling, these conditions are:

1. For both couplings the absolute value of the angle  $\alpha$  should be equal.
2. The difference in initial rotation of both couplings ( $\varphi_1 - \varphi_2$ ) should be equal to  $+\pi/2$  [rad] or  $-\pi/2$  [rad].

Two alignments are shown in the figure below.



$$\alpha = 0.35, \alpha' = -0.35, \varphi_1 = 0, \varphi_{1'} = \pi/2 \text{ [rad]} \quad \alpha = 0.35, \alpha' = 0.35, \varphi_1 = 0, \varphi_{1'} = \pi/2 \text{ [rad]}$$

## Interface

### Ports

p1, p2

### Description

The input and output axes (Rotation)

### Causality

### Input

p1 not equal p2

### Parameters

alpha The angle between the two axes ( $\alpha$ ).

### Initial Values

phi1\_initial The initial rotation of the input axis ( $\varphi_1$ ).

## Library

Iconic Diagrams\Mechanical\Rotation\Gears

## Implementations

Ideal

Backlash

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Description - Ideal



This model represents a worm gear with spindle (also referred to as worm) and wheel (also referred to as gear). The gear is ideal, i.e., it does not have inertia or friction. The causality of this model is always mixed: one port has a torque out causality while the other has an angular velocity out causality:

$$\begin{aligned} p\_spindle.T &= i * p\_wheel.T \\ p\_wheel.omega &= i * p\_spindle.omega \end{aligned}$$

or:

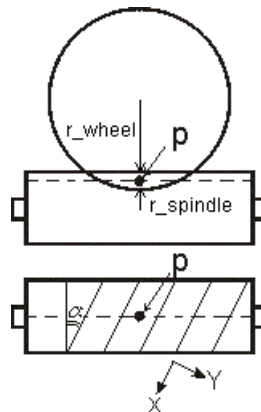
$$\begin{aligned} p\_wheel.T &= 1/i * p\_spindle.T \\ p\_spindle.omega &= 1/i * p\_wheel.omega \end{aligned}$$

with

$$i = \tan(\alpha) * r\_spindle / r\_wheel;$$

*Alpha* is the pitch angle as shown in the figure below. *r\_wheel* and *r\_spindle* are the effective radii of the wheel and spindle, i.e. the radii from the center of the wheel and spindle to the pitch point *p*.





### Interface - Ideal

Ports	Description
p_spindle	Port at the spindle shaft (Rotation).
p_wheel	Port at the wheel (Rotation).

#### Causality

p\_wheel notequal  
p\_spindle

#### Parameters

r_spindle	pitch radius spindle [m]
r_wheel	pitch radius wheel [m]
alpha	lead angle of the spindle [rad]

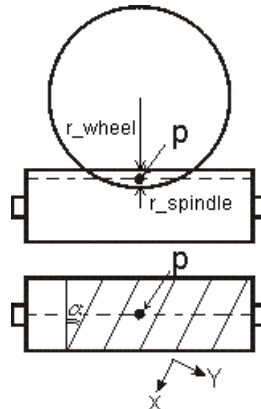
### Description - Backlash



This models represents a worm gear with spindle (also referred to as worm) and wheel (also referred to as gear). Between spindle and wheel, backlash and friction is modelled. The causality of this model is always fixed: both ports have a torque out causality.

## Analysis

The spindle and wheel have one or more pair of teeth contacting each other. The effective point of contact is called the pitch point **P**. At the pitch point a frame is defined, with an x- and y-direction. During rotation of the wheel and spindle, the teeth will experience a normal force **F<sub>n</sub>** in the x-direction and a friction force **F<sub>f</sub>** in the y-direction.



Between each pair of teeth, a clearance exists (y-direction), causing backlash. This effect is time-dependent, because of the tooth pairs coming in and out of contact. During normal operation this is a high frequency effect, which is filtered out by the damping of the construction. We therefore only use an **average backlash** at the pitch point. Using the same reasoning as backlash, an **average friction** is used at the pitch point.

To define both backlash and friction **a frame is used at the pitch point** (see picture above) to indicate velocities. The velocity in x-direction is the sliding velocity between the teeth and used to calculate the friction force. The position in y-direction is the position in the clearance and used to calculate the backlash force.

## Backlash

The backlash is described by the standard formula that is also used in the Backlash.emx model. The normal force is modelled by a spring-damper system. Inside the clearance a low damping and stiffness is used (**k1 and d1**), while a high stiffness and damping (**k2 and d2**) is used at both ends of the clearance. This yields a normal force **F<sub>n</sub>** of:

$$p.F = 0.5 \cdot k_2 \cdot \left( x - \sqrt{\left( -x - \frac{s}{2} \right)^2 + (ep \cdot s)^2} + x + \sqrt{\left( x - \frac{s}{2} \right)^2 + (ep \cdot s)^2} \right) + k_1 \cdot x + d_{1 \text{ or } 2} \cdot p.v$$

## Friction

Friction is described as static plus coulomb plus viscous plus Stribeck friction:

$$p.F = F_n * ((\mu_c + (\mu_{st} * \text{abs}(\tanh(\text{slope} * p.v))) - \mu_c) * \exp(-(p.v / v_{st})^2)) * \text{sign}(p.v) + \mu_v * p.v;$$

with:

$F_n$ : the normal force (given by the backlash formula)  
 $\mu_s$ : the static friction coefficient  
 $\mu_v$ : the viscous friction coefficient  
 $\mu_c$ : the coulomb friction coefficient  
 $slope$ : the steepness of the coulomb and static friction curve.  
 $v_{st}$ : the characteristic Stribeck velocity.

### Self-Locking

A worm gear is said to be self-locking, or irreversible when the wheel cannot drive the spindle. This condition is obtained, if the lead angle of the worm is small and the friction force between the teeth is high enough. Then the friction force becomes larger than the driving force on the teeth. Suppose we only consider static and Coulomb friction and both friction coefficients are equal. Then self locking is obtained when the following condition holds:

$$\begin{aligned}\mu_s &> \tan(\alpha) \\ \mu_c &> \tan(\alpha)\end{aligned}$$

### Interface - Backlash

#### Ports

	Description
p_spindle	Port at the spindle shaft (Rotation).
p_wheel	Port at the wheel (Rotation).

#### Causality

fixed torque out  
p\_spindle

#### Parameters

r_spindle	pitch radius spindle [m]
r_wheel	pitch radius wheel [m]
alpha	lead angle of the spindle [rad]
s	Interval of the play [m]
k1	Stiffness in the play [N/m]
k2	Stiffness outside the play [N/m]
d1	Damping inside the play [Ns/m]
d2	Damping outside the play [Ns/m]
ep	Relative round off (1e-6 -> sharp edges, 1e-2 -> smoother)
$\mu_s$	Static friction coefficient []
$\mu_v$	Viscous friction coefficient [s/m]
$\mu_{cv}$	Coulomb friction coefficient []
slope	Steepness of Coulomb friction curve [s/m]
$v_{st}$	Characteristic Stribeck velocity [m/s]

#### Interesting

#### Variables

$F_n$	Average normal force between teeth [N]
$F_f$	Average friction force between teeth [N]

$v_x$	Velocity in x-direction at the pitch frame [m/s] (used in friction formula)
$v_y$	Velocity in y-direction at the pitch frame [m/s] (used in backlash formula)
$x_x$	Position in x-direction at the pitch frame [m/s] (used in friction formula)
$x_y$	Position in y-direction at the pitch frame [m/s] (used in backlash formula)

## Library

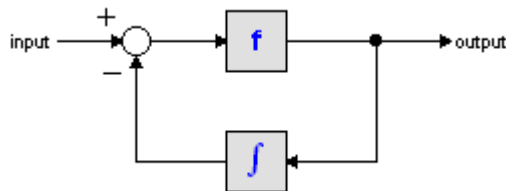
Iconic Diagrams\Mechanical\Rotation\Sensors

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

## Description

This model describes an acceleration sensor which derives an angular acceleration output out of a port angular velocity by differentiation. Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where  $f$  is the cut-off frequency. For very high values of  $f$ , the output becomes the pure derivative of the input. High values of  $f$ , however, increase simulations times. A good trade-off is a starting value of  $1e5$ .

The equations of this model are:

$$alpha = d(p.omega)/dt;$$

$$p.T = indifferent;$$

## Interface

Ports	Description
p	Rotation port p.
<b>Causality</b>	
fixed force out	

**Output**

alpha                      Absolute angular acceleration [rad/s<sup>2</sup>]

**Parameters**

f                              Cut-off frequency of the differentiation [Hz].  
 alpha\_initial              Initial angular acceleration [m/s].

**Library**

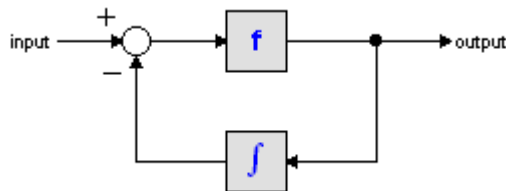
Iconic Diagrams\Mechanical\Rotation\Sensors

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

**Description**

This model describes an acceleration sensor which derives an angular acceleration output out of a angular velocity difference (between high and low terminals) by differentiation. Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where  $f$  is the cut-off frequency. For very high values of  $f$ , the output becomes the pure derivative of the input. High values of  $f$ , however, increase simulations times. A good trade-off is a starting value of 1e5.

The equations of this model are:

$$\begin{aligned} alpha &= d(p\_high.\omega - p\_low.\omega)/dt; \\ p\_low.T &= p\_high.T = indifferent; \end{aligned}$$

**Interface****Ports**

p\_high, p\_low

**Description**

Both terminals of the Mechanical port p.

**Causality**

fixed force out

**Output**

alpha                      Angular acceleration (measured as the difference between both terminals) [rad/s<sup>2</sup>]

**Parameters**

f                              Cut-off frequency of the differentiation [Hz].  
 alpha\_initial              Initial angular acceleration [m/s].

**Library**

Iconic Diagrams\Mechanical\Rotation\Sensors

**Implementations**

Ideal  
 Absolute  
 Incremental

**Use**

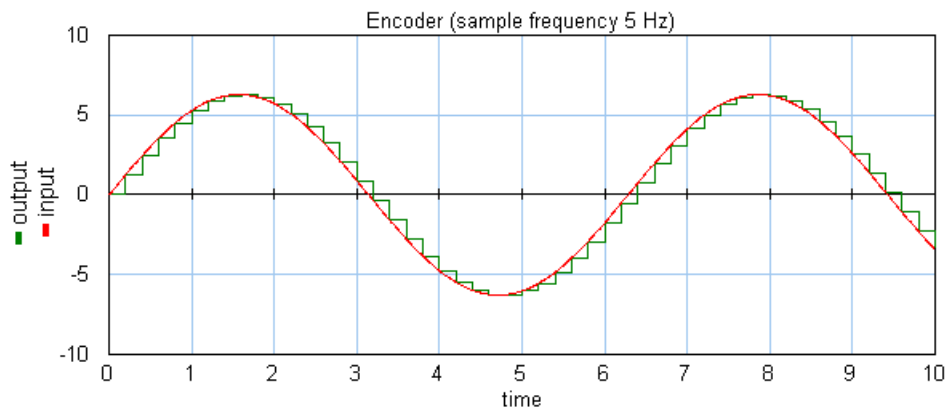
**Domains:** Continuous/Discrete. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation) / Block Diagrams.

**Description - Ideal**

This is a model of an optical encoder combined with sampling. The Encoder has no internal friction. The output signal is equal to the sampled shaft angle (in radians).

**Example**

The shaft angle is equal to a sine with amplitude 2\*pi (one revolution forward and one back), the sampling rate is 5 Hz.



**Interface - Ideal**

Ports	Description
p	Rotation port

**Causality**

fixed torque out     (The output torque is zero)

<b>Outputs</b>	<b>Description</b>
----------------	--------------------

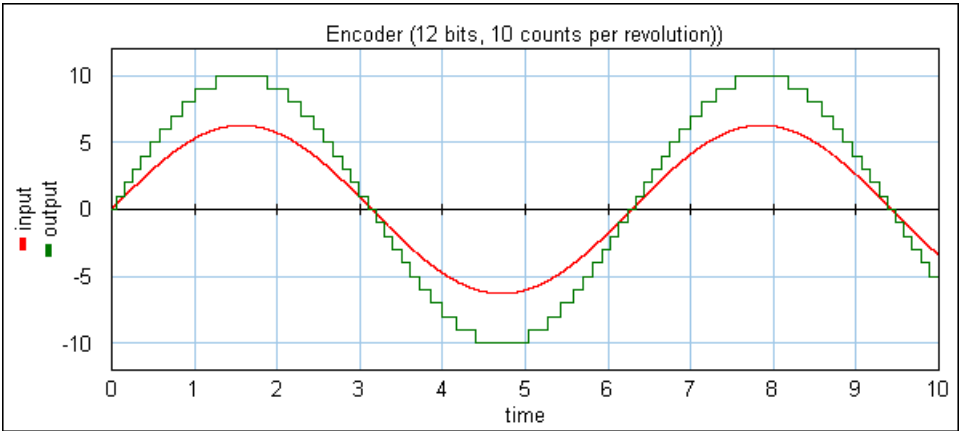
output	sampled shaft angle (rad)
--------	---------------------------

**Description - Absolute**

This is a model of an optical encoder combined with counting logic and analog to digital conversion. The encoder has no internal friction. Counting is absolute. The shaft angle is measured with an accuracy of a given number of counts per revolution.

**Example**

An encoder has an accuracy of 10 counts per revolution. This means an input signal with value 6.283185307 gives an output of 10. This is illustrated in the figure below. The input is a sine with amplitude  $2\pi$  (one revolution forward and one back).



**Overflow**

This model has no overflow.

**Interface - Absolute**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p	Rotation port
---	---------------

**Causality**

fixed torque out     (The output torque is zero)

<b>Outputs</b>	<b>Description</b>
----------------	--------------------

output	number of counts
--------	------------------

**Parameters**

counts	counts per revolution.
--------	------------------------

### Description - Incremental

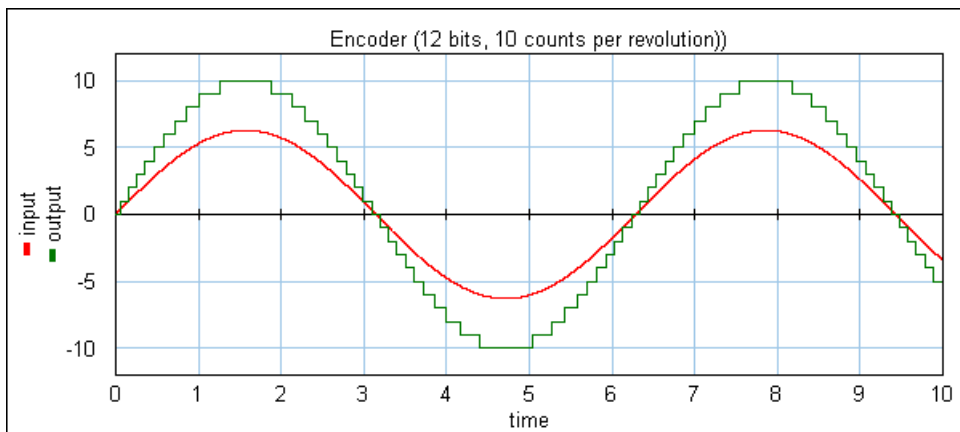
This is a model of an optical encoder combined with counting logic and analog to digital conversion. The encoder has no internal friction. Counting is incremental. The shaft angle is measured with an accuracy of a given number of counts per revolution and a window defined by the number of bits.

### Example

An encoder has an accuracy of 2000 counts per revolution. This means an input signal with value 6.283185307 gives an output of 2000.

### Example

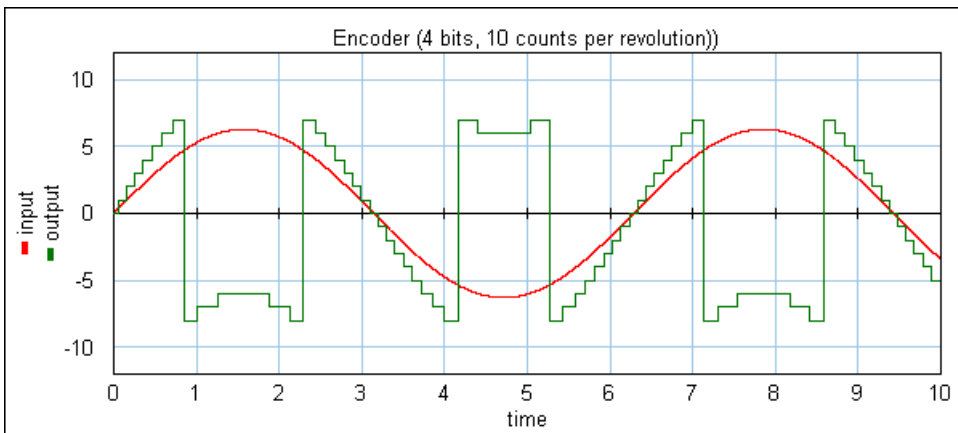
An encoder has an accuracy of 10 counts per revolution and a 5 bits counter. This means an input signal with value 6.283185307 gives an output of 10 and the output is clipping between +15 and -16. This is illustrated in the figure below. The input is a sine with amplitude  $2\pi$  (one revolution forward and one back).



*Encoder output without overflow.*

The next figure shows the same settings but only 4 bits are used. This means the output is clipping between +7 and -8.





Encoder output with overflow.

## Overflow

The maximum and minimum number of counts are equal to  $2^{(\text{bits}-1)} - 1$  and  $-2^{(\text{bits}-1)}$ . If the number of counts passes  $2^{(\text{bits}-1)} - 1$ , counting continues at  $-2^{(\text{bits}-1)}$  and vice versa.

## Interface - Incremental

Ports	Description
p	Rotation port
<b>Causality</b>	
fixed torque out	(The output torque is zero)
<b>Outputs</b>	
output	number of counts
<b>Parameters</b>	
counts	counts per revolution.
bits	maximum counting interval is between $2^{(\text{bits}-1)} - 1$ and $-2^{(\text{bits}-1)}$ .

## Limitations

The output of this model is a discrete signal. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

## Library

Iconic Diagrams\Mechanical\Rotation\Sensors

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (, Block Diagrams.), Block Diagrams.

## Description

This model translates a angular position to an output signal. It has a force out causality. The equations are:

$$\begin{aligned} p.T &= 0; \\ \phi &= \text{int}(p.\omega); \end{aligned}$$

## Interface

Ports	Description
p_high, p_low	Rotation port p.
<b>Causality</b>	
fixed force out	
<b>Output</b>	
phi	Absolute angular position [rad]
<b>Initial Values</b>	
phi_initial	Initial angular position [rad]

## Library

Iconic Diagrams\Mechanical\Rotation\Sensors

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

## Description

This model translates a angular position difference to an output signal. It has a force out causality. The port  $p$  of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.T &= p_{\text{high}}.T = p_{\text{low}}.T; \\ p.\omega &= p_{\text{high}}.\omega - p_{\text{low}}.\omega; \\ p.T &= 0; \\ \phi &= \text{int}(p.\omega); \end{aligned}$$

## Interface

Ports	Description
p_high, p_low	Both terminals of the Rotation port p.
<b>Causality</b>	
fixed force out	
<b>Output</b>	
phi	Relative angular position [rad]
<b>Initial Values</b>	

phi\_initial      Initial angular position [rad]

## Library

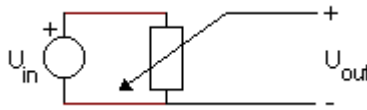
Iconic Diagrams\Mechanical\Rotation\Sensors

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation / Electric).

## Description

Potentiometers have a variable resistance according to a certain rotation. By establishing a voltage (see picture below) across the resistor it is possible to get a proportional relation between the angle and the output voltage.



with

$$U_{out} = U_{max} * angle / (turns * 2 * \pi)$$

Here  $U_{max}$  is the maximum voltage and turns is the maximum number of turns.

## Interface

Ports	Description
p1	Rotation port.
p2	Electric port.

## Causality

fixed   torque   out (The output torque is zero)

p1                      The output is equal to  $U_{out}$ .

fixed   voltage   out

p2

## Parameters

$U_{max}$	Maximum output voltage [V]
turns	maximum allowed number of turns []

## Library

Iconic Diagrams\Mechanical\Rotation\Sensors

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

## Description

This is an ideal sensor (no dissipation or other effects) that yields the power that flows through the model as output signal. The equations are:

$$\begin{aligned}p_{\_high}.T &= p_{\_low}.T \\p_{\_high}.\omega &= p_{\_low}.\omega \\P &= p_{\_high}.T * p_{\_high}.\omega;\end{aligned}$$

## Interface

Ports	Description
p_high, p_low	Both rotation ports.
<b>Causality</b>	
p_high not equal p_low	
<b>Output</b>	
P	Power [w].

## Library

Iconic Diagrams\Mechanical\Rotation\Sensors

## Use

**Domains:** Continuous/Discrete. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation) / Block Diagrams.

## Description

A tachometer is a transducer for measuring the rotation speed. It is normally mounted at the shaft of a motor and gives a voltage signal proportional to the rotation speed:

$$V = K_v \cdot v$$

with  $K_v$  the tachometer gradient [V / rad/s] and  $v$  the shaft velocity [rad/s]. This equation represents the ideal case. Due to the slots and commutator segments of the tachometer, a noise ripple will exist:

$$V_n = \frac{K_n}{100} \cdot K_v \cdot v \cdot \cos(N \cdot v \cdot t)$$

with  $N$  the ripple frequency [cycles per turn] and  $K_n$  the peak to peak noise Ripple [in % of the output voltage]. To convert the Voltage Gradient parameter from RPM units [V / RPM] to radian units [V / rad/s], use the conversion formula:

$$Kv_{rad/s} = Kv_{RPM} \cdot \frac{2 \cdot \pi}{60}$$

## Interface

Ports	Description
p	Rotation port.
<b>Causality</b>	
fixed torque out	(The output torque is zero)
<b>Outputs</b>	
output	Output voltage [V]
<b>Parameters</b>	
Kv	Voltage Gradient [ V / rad/s ].
Kn	Noise Ripple , relative to output voltage [%].
N	Ripple frequency in cycles per turn [.]

## Library

Iconic Diagrams\Mechanical\Rotation\Sensors

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

## Description

This model translates an applied torque to an output signal. It has an angular velocity out causality. The port  $p$  of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.T &= p\_high.T = p\_low.T; \\ p.\omega &= p\_high.\omega - p\_low.\omega; \\ p.\omega &= 0; \\ T &= p.T; \end{aligned}$$

## Interface

Ports	Description
p_high, p_low	Both terminals of the Rotation port p.
<b>Causality</b>	
fixed angular velocity out	
<b>Output</b>	
T	Applied torque [N/m]

## Library

Iconic Diagrams\Mechanical\Rotation\Sensors

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

### Description

This model translates an angular velocity to an output signal. It has a force out causality. The equations are:

$$\begin{aligned} p.T &= 0; \\ \omega &= p.\omega; \end{aligned}$$

### Interface

Ports	Description
p	Mechanical port p.
<b>Causality</b>	
fixed force out	
<b>Output</b>	
omega	Absolute angular velocity [rad/s]

## Library

Iconic Diagrams\Mechanical\Rotation\Sensors

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation), Block Diagrams.

### Description

This model translates a velocity difference to an output signal. It has a force out causality. The port p of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.T &= p_{\text{high}}.T = p_{\text{low}}.T; \\ p.\omega &= p_{\text{high}}.\omega - p_{\text{low}}.\omega; \\ p.T &= 0; \\ \omega &= p.\omega; \end{aligned}$$

### Interface

Ports	Description
p_high, p_low	Both terminals of the Rotation port p.
<b>Causality</b>	
fixed force out	

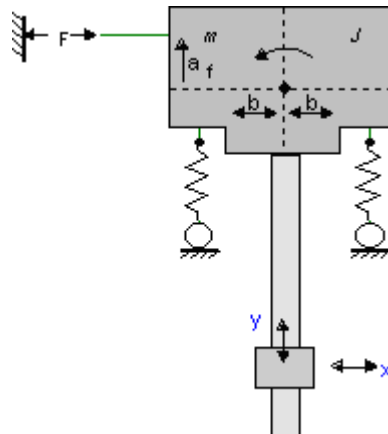
## Output

omega                      Relative angular velocity [rad/s]

## Introduction

The 2DSmallRotation library contains models that describe 2-D planar motion and are valid for small rotations. Due to these small rotations, the dynamic equations that describe the various models are simple and can be linearized symbolically. The library is therefore suited for modeling mechanical systems that experience small rotations and must be thoroughly analyzed in the frequency domain.

Consider the guidance system below. Due to the limited stiffness of the guidance wheels, the central body will experience a small rotation that results in a movement in the x-direction at the end-effector. To properly model the end-effector movement as a function of the driven force, this rotation has to be incorporated. To inspect the resulting resonance frequencies in a bode plot, the model must be linearized. If linearization is performed symbolically, the effect of parameter changes ( $af$ ,  $b$ ,  $J$ ) can be inspected directly in the bode plot, which is very useful when the system is still in the design phase.



To perform symbolic linearization, the example system should be modeled using the models of the 2DSmallAngles library.

## 2D

When we speak of **2D motion** we often mean all planar motion. However, to describe this motion, **three degrees of freedom** (displacement  $x$  and  $y$  and rotation  $\theta$ ) are used. In 20-sim we keep to the common naming standard of 2D for planar motion (3 degrees of freedom) and 3D for spatial motion (6 degrees of freedom). In 20-sim the three degrees of freedom for planar motion are combined in a vector notation:

d.o.f.	identity	forces	velocities
--------	----------	--------	------------

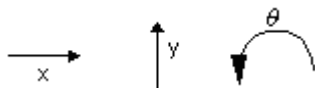
x	position	P.F[1] [N]	P.v[1] [m/s]
y	position	P.F[2] [N]	P.v[2] [m/s]
$\theta$	angle	P.F[3] [Nm]	P.v[3] [rad/s]

**Note**

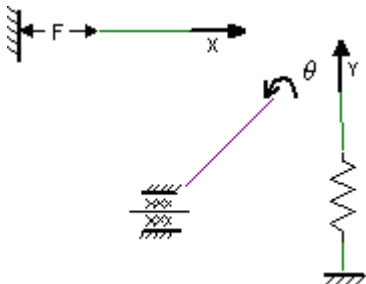
It is not possible in 20-sim to use vector elements with mixed units. Therefore element number 3 will be displayed with units [m/s] and [N] although it really is [rad/s] and [Nm]!

**1D**

The models in the 2DSmallRotation library have two types of connection ports: 1D and 2D. The 1D ports can represent movement and force (x- or y-direction) or an angular displacement and torque.



The models of the standard translation and rotation libraries can be used connect to these 1D ports as is shown in the picture below.



**2D**

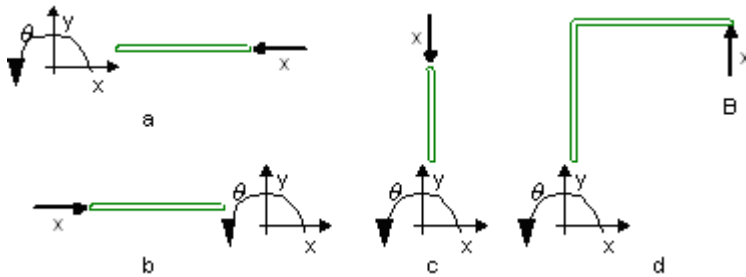
The 2D connection port is a vector that represents three degrees of freedom. The vector notation that is used in 20-sim is:

<b>d.o.f.</b>	<b>identity</b>	<b>forces</b>	<b>velocities</b>
x	position	P.F[1] [N]	P.v[1] [m/s]
y	position	P.F[2] [N]	P.v[2] [m/s]
$\theta$	angle	P.F[3] [Nm]	P.v[3] [rad/s]

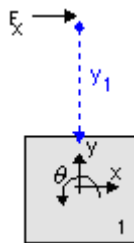
In 20-sim it is not possible to use vector ports with mixed units. This means that element number 3 will be always be displayed with the units [m/s] and [N] although it should be interpreted as [rad/s] and [Nm].

To connect 2D ports, only other models with 2D ports can be used. A double line indicates this vector connection.





Consider the body below:



Given a force  $F_x$  in  $x$ -direction acting upon the body at an offset  $y_1$  from the center, the resulting force at the center of the body is:

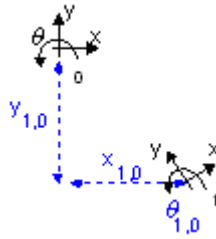
$$\begin{aligned} F1x &= F_x * \cos(q) \\ F1y &= F_x * \sin(q) \\ F1q &= F_x * -y_1 \end{aligned}$$

For small angles this can be simplified to:

$$\begin{aligned} F1x &= F_x \\ F1y &= 0 \\ F1q &= F_x * -y_1 \end{aligned}$$

A force acting upon a body at a certain offset is rewritten to a force at the center of the body. This is common in multibody dynamics and called a transformation. A force acting at a certain point can be transformed to see its effect at another point.

Consider two frames which have an arbitrary offset as shown in the picture below. We want to know how a force in frame 0 is transformed to a force in frame 1. We assume that frame 1 has an offset of  $x_1$  and  $y_1$  with respect to frame 0 and a rotation  $q_1$  with respect to frame 0. In order to make clear that the offsets are given with respect to frame 0 we will write the with extra indices ( $x_{1,0}$ ,  $y_{1,0}$  and  $\theta_{1,0}$ ).



Given an arbitrary force  $F_{1,0}$  at frame 0 the resulting force  $F_{1,1}$  at frame 1 is equal to:

$$F_{1,1} = R_0^1 \cdot F_{1,0} \quad \text{with} \quad R_0^1 = \begin{bmatrix} \cos(\theta_{1,0}) & \sin(\theta_{1,0}) & 0 \\ -\sin(\theta_{1,0}) & \cos(\theta_{1,0}) & 0 \\ -y_{1,0} & x_{1,0} & 1 \end{bmatrix}$$

For small angles this can be simplified to:

$$F_{1,1} = R_{01} \cdot F_{1,0} \quad \text{with} \quad R_{01} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ -y_{1,0} & x_{1,0} & 1 \end{bmatrix}$$

The accuracy of this simplification depends on the angle  $\theta$ . For an angle of 0.5 degrees (0.009 rad) this results in an almost 1% error in the calculation of  $F_{1,1}$ . Considering the cumulative effects of this error when multiple models are used, an angle of maximum 0.05 degrees (<1 mrad) is an upper bound for the models of the 2DSmallRotation library.

The simplification of the equations has two advantages. First because of the small rotations there is no frame rotation any more. Therefore all frames have the same direction (there is only an offset in x-direction and y-direction). Interpreting results is therefore much easier. But the biggest advantage is the simplification of equations which allows us to linearize models symbolically and thus perform tasks in the frequency like parameter sweeps!

## Degrees of Freedom

As described in the previous topic, the models in 2DSmallRotation library have two types of connection ports: 1D and 2D. The 1D port can represent movement in the x-direction, the y-direction or an angular displacement  $\theta$ .



The 2D port is a vector that contains all three degrees of freedom. The vector notation that is used in 20-sim is:

d.o.f.	identity	forces	velocities
x	position	P.F[1] [N]	P.v[1] [m/s]
y	position	P.F[2] [N]	P.v[2] [m/s]
$\theta$	angle	P.F[3] [Nm]	P.v[3] [rad/s]

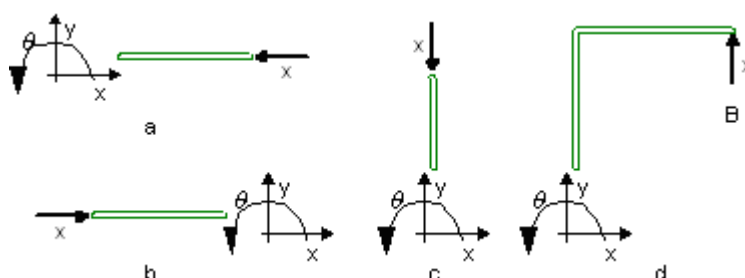
The vector element number (1, 2 or 3) denotes the identity of the degree of freedom (x, y and  $\theta$ ). To create meaningful models, we have to define the positive direction of each degree of freedom:

d.o.f.	positive direction
x	from left to right
y	from bottom to top
$\theta$	counter clockwise

This definition is arbitrary. We could as well define it any other way. In the 2DSmallRotation library we have chosen the definition above. It will help us define new models and interpret simulation results.

### Orientation Independent

The connections between models only indicate how variables (forces and velocities) are transferred from one model to the other and vice versa. The orientation of the models in the Graph Editor (how they are drawn) is therefore not important. **Flipping, rotating or moving** a model **does not change the model!** All four representations in the figure below are the same although their individual models are oriented differently.



The figure above shows a point model in x-direction connected to a 2D body. The point indicates a force in x-direction that is applied to the body. Since we defined that the positive x-direction is from the left to the right, intuitively figure b leads to the correct interpretation.

This indicates a problem. Although all models describe the same behavior, we would intuitively interpret them differently. It is therefore useful to impose some rules to prevent misinterpretation of a model by other users.

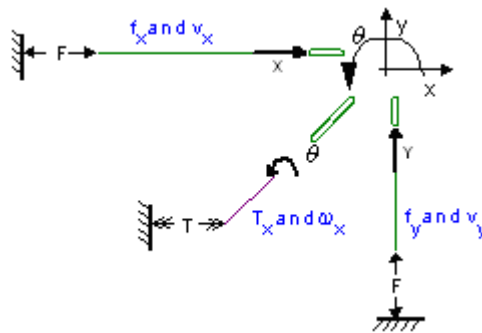
### Drawing Rules

1. Preferably leave the orientation of the models of the 2DSmallRotation library as they pop up on the screen.

2. If necessary, only flip or rotate models in a direction that does not lead to misinterpretations.
3. If possible, draw 1D connections in the following direction:

d.o.f.	positive direction
x	from left to right
y	from bottom to top
$\theta$	from left bottom to right top

An example is shown in the figure below:



TwoDBody

## Library

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Iconic Diagrams (2D Planar).

## Description

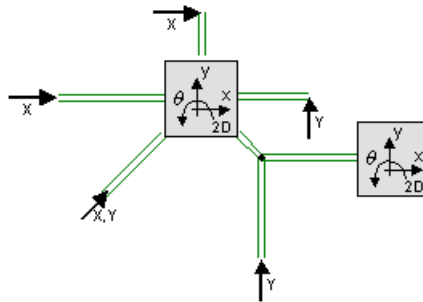
The central model in the 2DSmallRotation library is the TwoDBody model. It describes a body with three degrees of freedom: x, y and  $\theta$ . The TwoDBody is a point mass with rotational inertia. The constitutive equations are therefore very simple:

$$P.v = I .* \text{int}(P.F);$$

With

$$I = [1/M; 1/M; 1/J];$$

Any number of connections can be made to the TwoDBody model. All forces acting upon the body are added.



Because any number of connections can be made, successive ports are named  $P1$ ,  $P2$ ,  $P3$  etc. 20-sim will automatically create equations such that the resulting force  $P.F$  is equal to the sum of the forces of all connected ports  $P1 \dots Pn$ . The velocities of all connected ports are equal to  $P.v$ . The model has a preferred velocity out causality. The corresponding constitutive equations then contain an integration. The model can also have the non-preferred force out causality. The constitutive equations then contain a differentiation.

$$P.F = \text{sum}(P1.F, P2.F, \dots)$$

$$P.v = P1.v = P2.v = \dots$$

velocity out causality (preferred):

$$I = [1/M; 1/M; 1/J]$$

$$P.v = I * \text{int}(P.F);$$

force out causality:

$$I = [1/M; 1/M; 1/J]$$

$$P.F = I^{-1} * \text{ddt}(P.v);$$

## Interface

Ports	Description
P[3]	Port with three degrees of freedom (x, y, θ). Any number of connections can be made.

### Causality

preferred velocity  
out

### Parameters

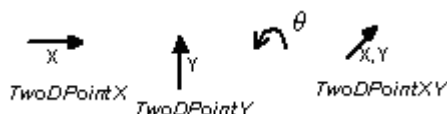
M	Mass [kg].
J	Moment of inertia [kgm <sup>2</sup> /rad]

### Note

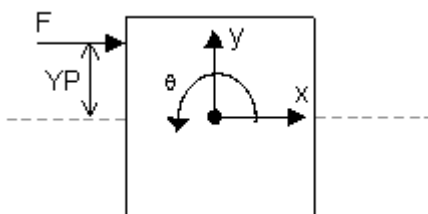
- A TwoDBody model can be connected to any other element of the 2D-library except other 2D-bodies. Two bodies can always be simplified to one TwoDBody model with the combined mass and inertia of both single bodies.

- TwoDBody models can be connected to 1D models using the TwoDPoint models as intermediate. If a TwoDPoint is connected to a body, it constrains the movement of the body in one direct

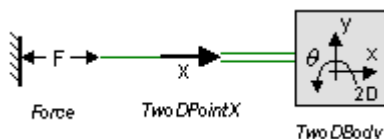
TwoDPoint models are used to connect 1D models to TwoDBodies. They indicate a 1D force or torque that is applied in a certain direction, onto a body.



A point model forms the connection between the single degree of freedom part of a system and the center of mass of a body. Consider the example below, where force  $F$  in  $x$ -direction (single degree of freedom) is pushing upon a body (three degrees of freedom) at an offset  $YP$  from the body center of mass.



To create such a construct, the TwoDPoint-X model is used:

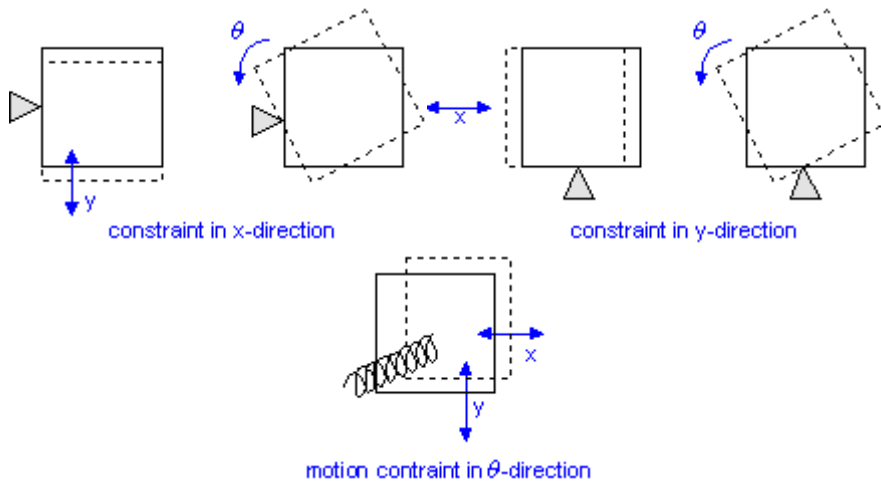


The TwoDPoint-X model describes the translation of a 1D force ( $x$ -direction) to a 2D-force ( $x$ -,  $y$ - and  $\theta$ -direction) and vice versa the translation of a 2D-velocity ( $x$ -,  $y$ - and  $\theta$ -direction) to a 1D velocity ( $x$ -direction).

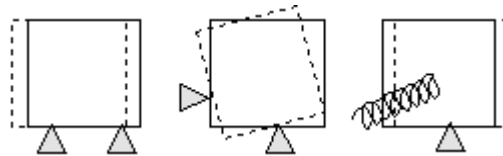
There are four point models. Three point models transform from  $x$ -direction,  $y$ -direction and  $\theta$ -direction to 2D. One point models transforms from direction with arbitrary orientation to 2D.

### Fixation of bodies

If a TwoDBody model is used in combination with TwoDPoint models, at least three non-coinciding, unequal (i.e. not having the same offsets) TwoDPoints must be connected to prevent the body from free motion. This is obvious when we interpret the point models physically. Point models can be interpreted as constraints on motion in one direction. The motion in the other two directions is free.



To show that two points are not sufficient to constrain all motions look at the figure below.



## Library

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

## Implementations

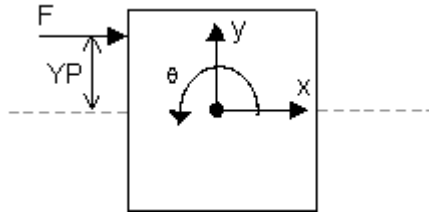
X  
Y  
theta  
XY

## Use

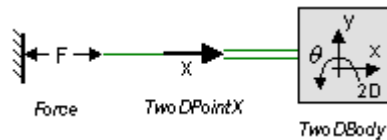
**Domains:** Continuous. **Size:** 1-D/2-D. **Kind:** Iconic Diagrams (1D Translation, 2D Planar).

## Description - X

[TwoDPoint models](#) are used to connect 1D models to TwoDBodies. They indicate a 1D force or torque that is applied in a certain direction, onto a body. The TwoDPoint-X model forms the connection between the single degree of freedom in x-direction and the center of mass of a body. Consider the example below, where force  $F$  in x-direction (single degree of freedom) is pushing upon a body (three degrees of freedom) at an offset  $YP$  from the body center of mass.



To create such a construct the TwoDPoint-X model is used:



The TwoDPoint-X model describes the transformation of force in x-direction to a force in three degrees of freedom. The single degree of freedom port  $p\_in$  describes the connection in x-direction and the three degree of freedom port  $P\_out$  describes connection with the 2D-body ( $x$ ,  $y$  and  $\theta$ ).

```
P_out.F[1] = p_in.F;           // x-direction
P_out.F[2] = 0;                // y-direction
P_out.F[3] = -p_in.F * YP;     // rotation
```

```
p_in.v = P_out.v[1] - YP * P_out.v // x-direction
[3];
```

## Interface - X

Ports	Description
$p\_in$	1D Translation port ( $x$ ).
$P\_out[3]$	2D Port with three degrees of freedom ( $x$ , $y$ , $\theta$ ).

### Causality

```
fixed force out
P_out
fixed velocity out
p_in
```

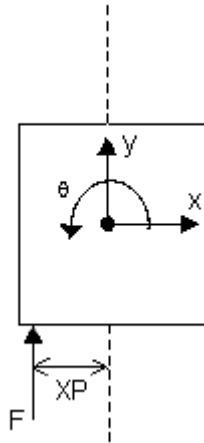
### Parameters

```
YP          Distance (y-direction) between connection and center of mass [m].
```

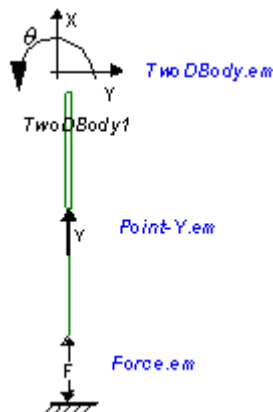


## Description - Y

**TwoDPoint models** are used to connect 1D models to TwoDBodies. They indicate a 1D force or torque that is applied in a certain direction, onto a body. The TwoDPoint-Y model forms the connection between the single degree of freedom in y-direction and the center of mass of a body. Consider the example below, where force  $F$  in y-direction (single degree of freedom) is pushing upon a body (three degrees of freedom) at an offset  $XP$  from the body center of mass.



To create such a construct the 2D-point-Y model is used:



The 2D-point-Y model describes the transformation of force in y-direction to a force in three degrees of freedom. The single degree of freedom port  $p\_in$  describes the connection in y-direction and the three three degree of freedom port  $P\_out$  describes connection with the 2D-body ( $x$ ,  $y$  and  $\theta$ ).

```

P_out.F[1] = 0;           // x-direction
P_out.F[2] = p_in.F;      // y-direction
P_out.F[3] = p_in.F * XP; // rotation

```

```
p_in.v = P_out.v[2] + XP * P_out.v // y-direction
[3];
```

## Interface - Y

Ports	Description
p_in	1D Translation port (y).
P_out[3]	2D Port with three degrees of freedom (x, y, $\theta$ ).

### Causality

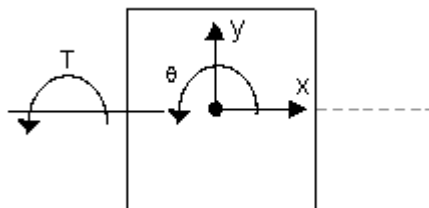
fixed force out  
P\_out  
fixed velocity out  
p\_in

### Parameters

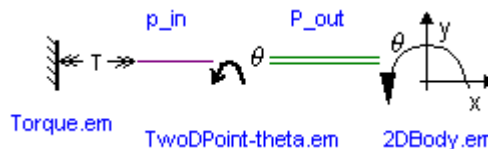
XP Distance (x-direction) between connection and center of mass [m].

## Description - theta

[TwoDPoint models](#) are used to connect 1D models to TwoDBodies. They indicate a 1D force or torque that is applied in a certain direction, onto a body. The TwoDPoint-Theta model forms the connection between the single degree of freedom rotation and the center of mass of a body. Consider the example below, where torque (single degree of freedom) is acting on a body (three degrees of freedom).



To create such a construct the TwoDPoint-Theta model is used:



The TwoDPoint-Theta model describes the transformation of a single rotation to a rotation of the 2D-body. The single degree of freedom port  $p\_in$  describes the connection to the single degree rotation the three three degree of freedom port  $P\_out$  describes connection with the 2D-body (x, y and  $\theta$ ).

```

P_out.F[1] = 0;           // x-direction
P_out.F[2] = 0;           // y-direction
P_out.F[3] = p_in.T;      // rotation

p_in.omega = P_out.v[3];  // rotation

```

## Interface - theta

Ports	Description
p_in	1D Rotation port ( $\theta$ ).
P_out[3]	2D Port with three degrees of freedom (x, y, $\theta$ ).

### Causality

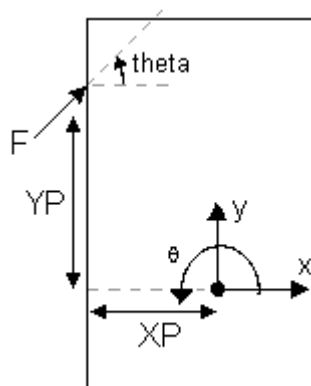
```

fixed force out
P_out
fixed velocity out
p_in

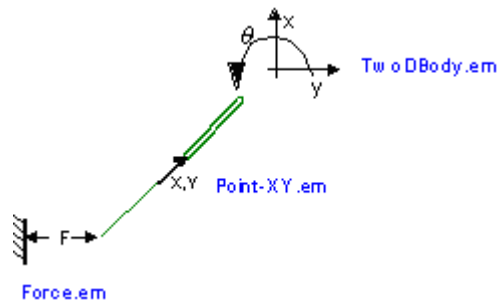
```

## Description - XY

[TwoDPoint models](#) are used to connect 1D models to TwoDBodies. They indicate a 1D force or torque that is applied in a certain direction, onto a body. The TwoDPoint-XY model forms the connection between a single degree of freedom in arbitrary direction and the center of mass of a body. Consider the example below, where force  $F$  (single degree of freedom) is pushing upon a body (three degrees of freedom) with an arbitrary angle  $\theta$  at an offset  $XP$  and  $YP$  from the body center of mass.



To create such a construct the TwoDPoint-XY model is used:



The TwoDPoint-XY model describes the transformation of a one degree of freedom force in an arbitrary direction to a force in three degrees of freedom. The single degree of freedom port  $p\_in$  describes the connection in the arbitrary direction and the three degree of freedom port  $P\_out$  describes connection with the 2D-body ( $x$ ,  $y$  and  $\theta$ ).

```

Fx = cos(theta)*p_in.F;           // arbitrary-direction
Fy = sin(theta)*p_in.F;           // arbitrary-direction

P_out.F[1] = Fx;                  // x-direction
P_out.F[2] = Fy;                  // y-direction
P_out.F[3] = Fy * XP - Fx * YP;   // rotation

p_in.v = cos(theta)*P_out.v[1] +  // arbitrary-direction
sin(theta)*P_out.v[2] +
XP * sin(theta)*P_out.v[3] -
YP * cos(theta) * P_out.v[3];

```

## Interface - XY

Ports	Description
$p\_in$	1D Translation port in arbitrary direction.
$P\_out[3]$	2D Port with three degrees of freedom ( $x$ , $y$ , $\theta$ ).

### Causality

fixed force out  
 $P\_out$   
 fixed velocity out  
 $p\_in$

### Parameters

$YP$	Distance (y-direction) between connection and center of mass [m].
$XP$	Distance (x-direction) between connection and center of mass [m].
$\theta$	Angle of impact of the single degree of freedom port [rad].

## Note

- A TwoDBody has to be connected to at least three unequal TwoDPoint models to prevent it from free motion (rotation & translation).
- Flipping or rotating the model does not change the direction of applied forces or measured directions. Preferably leave the orientation as it pops up on the screen.

## Library

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

### Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Iconic Diagrams (2D Planar).

### Description

The TwoDFixedWorld represents the fixed world in 3 degrees of freedom. It can be connected to other 2D models to freeze their motion. Models that can be connected to the fixed world are:

1. TwoDSprings
2. TwoDLinearSlides
3. TwoDLinearActuators

Although other models like the TwoDBody can also be connected to the TwoDFixedWorld model, it makes no sense because it completely fixates all equations of motion.

## Interface

Ports	Description
P	Port with three degrees of freedom ( $x$ , $y$ , $\theta$ ).

### Causality

fixed velocity out P

## Library

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

### Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Iconic Diagrams (2D Planar).

### Description

This model can be used to connect any open end of another 2D model that is not connected to the fixed world. It generates a three degree of freedom zero force while the velocity is free.

## Interface

Ports	Description
P	Port with three degrees of freedom (x, y, $\theta$ ).

### Causality

fixed force out P

To inspect the model behavior you can plot variables. Sometimes not all variables are available. Then sensor model can be used.

### 1D

To use the 1D sensor models from the standard library, connect them to the 2D models using the TwoDPoint models.

### 2D

To measure variables directly from the 2D models, three absolute sensors are available showing the absolute position, velocity and acceleration. Also two relative sensors are available showing the force and powerflow between two elements.

## Library

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

### Use

**Domains:** Continuous. **Size:** 1-D/2-D. **Kind:** Iconic Diagrams (1D Translation, 1D Rotation, 2D Planar).

### Description

This model is used to find the absolute position of a TwoDBody model. It has a port *P* which can be connected to the body and it has three output signals that denotes the x- and y-position and the angle of the body. The model has a force out causality. The equations are:

$$\begin{aligned} P.F &= 0; \\ x &= \text{int}(P.v[1]); \\ y &= \text{int}(P.v[2]); \\ \theta &= \text{int}(P.v[3]); \end{aligned}$$

## Interface

Ports	Description
P[3]	Port with three degrees of freedom (x, y, $\theta$ ).

### Causality

fixed force out P

### Output

x	Absolute position [m].
y	Absolute position [m].

theta Absolute angle [rad].

### Initial Values

x\_initial Initial position [m]

y\_initial Initial position [m]

theta\_initial Initial angle [m]

## Library

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

### Use

**Domains:** Continuous. **Size:** 1-D/2-D. **Kind:** Iconic Diagrams (1D Translation, 1D Rotation, 2D Planar).

### Description

This model is used to find the absolute velocity of a TwoDBody model. It has a port  $P$  which can be connected to the body and it has three output signals that denotes the  $x$ - and  $y$ -velocity and the angular velocity of the body. The model has a force out causality. The equations are:

$$\begin{aligned} P.F &= 0; \\ vx &= P.v[1]; \\ vy &= P.v[2]; \\ omega &= P.v[3]; \end{aligned}$$

### Interface

#### Ports

P[3] Port with three degrees of freedom ( $x$ ,  $y$ ,  $\theta$ ).

#### Causality

fixed force out P

#### Output

vx Absolute velocity [m].

vy Absolute velocity [m].

omega Absolute angular velocity [rad].

## Library

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

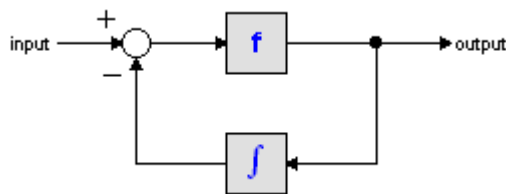
## Use

**Domains:** Continuous. **Size:** 1-D/2-D. **Kind:** Iconic Diagrams (1D Translation, 1D Rotation, 2D Planar).

## Description

This model is used to find the absolute acceleration of a TwoDBody model. It has a port *P* which can be connected to the body and it has three output signals that denotes the x- and y-acceleration and the angular acceleration of the body.

The acceleration output is calculated out of the velocity by differentiation. Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where *f* is the cut-off frequency. For very high values of *f*, the output becomes the pure derivative of the input. High values of *f*, however, increase simulations times. A good trade-off is a starting value of 1e5.

The equations of this model are:

```
P.F = 0;
ax = 2*pi*f*( P.v[1] - int(ax, 0));
ay = 2*pi*f*( P.v[2] - int(ay, 0));
alpha = 2*pi*f*( P.v[3] - int(alpha, 0));
```

## Interface

### Ports

P[3]

### Description

Port with three degrees of freedom (x, y,  $\theta$ ).

### Causality

fixed force out P

### Outputs

ax

Absolute acceleration [m].



ay	Absolute acceleration [m].
alpha	Absolute acceleration [rad].

**Initial Values**

ax_initial	Initial acceleration [m]
ay_initial	Initial acceleration [m]
alpha_initial	Initial angular acceleration [m]

**Library**

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

**Use**

**Domains:** Continuous. **Size:** 1-D/2-D. **Kind:** Iconic Diagrams (1D Translation, 1D Rotation, 2D Planar).

**Description**

This model can be used to measure the forces and torque between two components. It has a high and a low terminal to connect to both components. The equations are:

$$\begin{aligned}
 P.F &= P\_high.F = P\_low.F; \\
 P.v &= P\_high.v - P\_low.v; \\
 P.v &= 0; \\
 Fx &= P.F[1]; \\
 Fy &= P.F[2]; \\
 T &= P.F[3];
 \end{aligned}$$

**Interface**

Ports	Description
P[3]	Port with three degrees of freedom (x, y, $\theta$ ).

**Causality**

fixed velocity out  
P

**Outputs**

Fx	Force [N].
Fy	Force [N].
T	Torque [Nm].

## Library

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

### Use

**Domains:** Continuous. **Size:** 1-D/2-D. **Kind:** Iconic Diagrams (1D Translation, 1D Rotation, 2D Planar).

### Description

This model can be used to measure the powerflow between two models. It has two ports to to both models. The equations are:

$$\begin{aligned} P.F &= P_{high}.F = P_{low}.F; \\ P_{high}.F &= P_{low}.F; \\ P_{high}.v &= P_{low}.v; \\ P &= P_{high}.v \cdot P_{high}.F; \\ P_x &= P[1]; \\ P_y &= P[2]; \\ P_{theta} &= P[3]; \end{aligned}$$

### Interface

Ports	Description
-------	-------------

P[3]	Port with three degrees of freedom (x, y, $\theta$ ).
------	---

### Causality

fixed velocity out

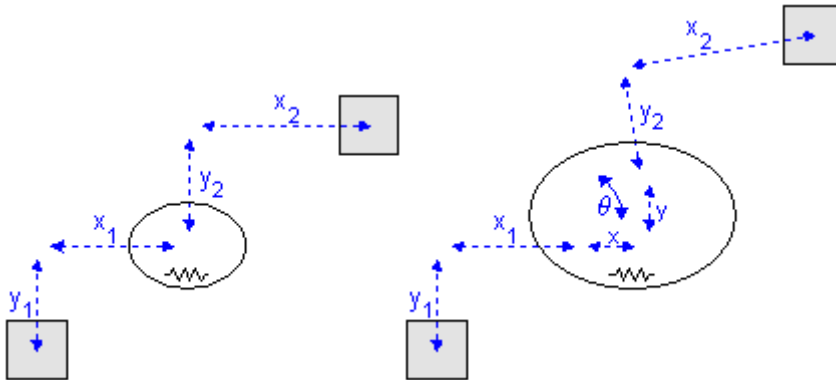
P

### Outputs

Px	Power [W].
Py	Power [W].
Ptheta	Power [W].

## 2D Springs

A TwoDSpring model represents a flexible spring between two bodies. The center of stiffness is located relative to the two bodies. The offsets from the bodies to the center of stiffness are indicated by  $x1$ ,  $y1$ ,  $x2$  and  $y2$  as shown in the picture below (left).



*A 2-D spring in rest (left) and stretched (right).*

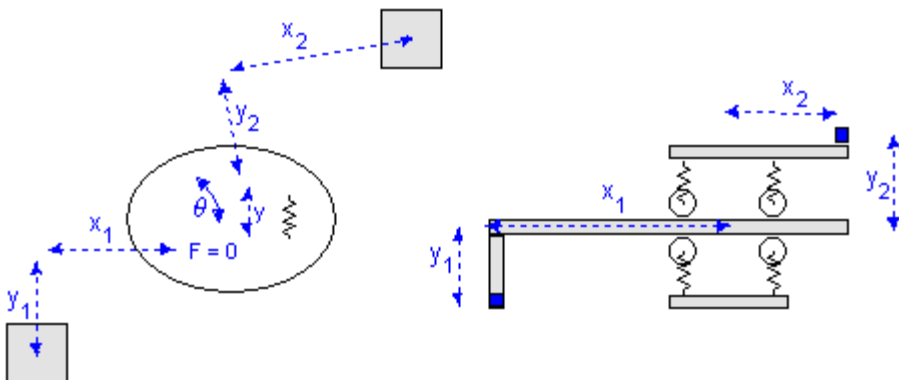
Note that  $x_1$ ,  $y_1$ ,  $x_2$  and  $y_2$  are defined with respect to the spring coordinate frame which is at the center of the spring. This means in the picture above  $x_1$  and  $y_1$  have a negative value and  $x_2$  and  $y_2$  have a positive value.

When the spring is stretched the offsets will change by the spring elongations  $x$ ,  $y$  and  $\theta$  as indicated in the picture (right). The center of stiffness is always located precisely in the middle of the spring elongations. Because all spring equations will be calculated from the center of stiffness this means that the offsets for a stretched spring are  $(x_1 - x/2)$ ,  $(y_1 - y/2)$ ,  $(x_2 + x/2)$  and  $(y_2 + y/2)$ .

For a realistic representation of vibration behavior, every 2D spring has a damper in parallel. If you want to turn off the effects of this damper, choose the damping parameters equal to zero. If you want to damp out unwanted vibrations, choose the damping parameters equal to 0.1% to 10% of the spring parameters.

### Linear Slides

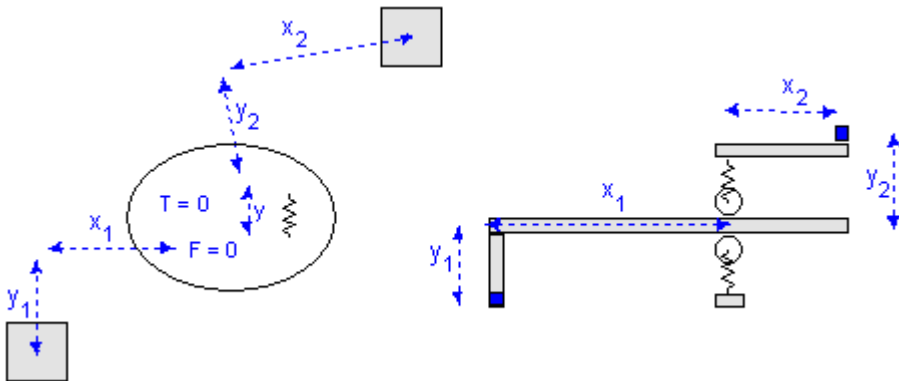
Take a look at the TwoDSpring model in the picture below. If we replace the spring in  $x$ -direction by a zero force we have created a linear slide.



*Linear slide:  $x = \text{free}$ ,  $y = \text{stiff}$ ,  $\theta = \text{stiff}$ .*

Consider a carriage that is clamped with four wheels to a slide. In the  $x$ -direction the carriage is free to move, which is equal to a zero force. The limited stiffness of the wheels is represented by springs. If there is a force with equal sign on both wheels, the carriage will slightly move in the  $y$ -direction. If there is a force with opposite sign on both wheels, the carriage will only rotate. This can be represented by two independent springs: one in the  $y$ -direction and  $\theta$ -direction.

If we repeat the same experiment and replace the spring in  $x$ -direction by a zero force and the spring in  $\theta$ -direction by a zero torque, we have created a linear slide with rotational freedom. In practice this can be found with carriages that are clamped with a limited set of wheels as shown below.



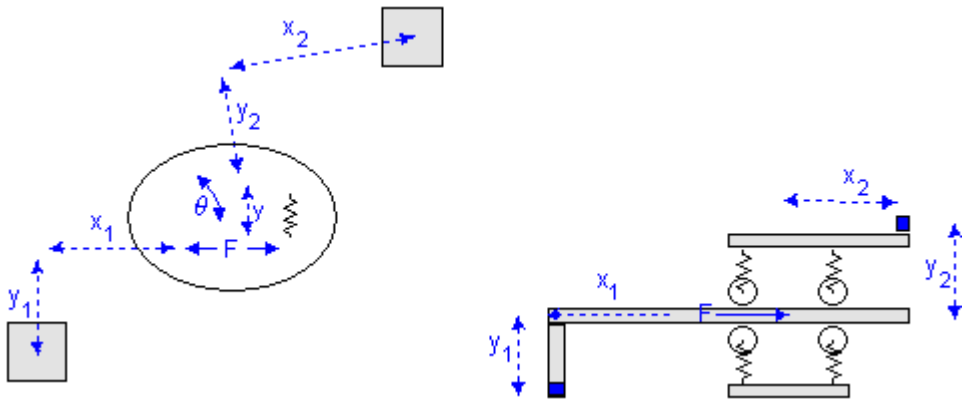
*Linear slide:  $x = \text{free}$ ,  $y = \text{stiff}$ ,  $\theta = \text{free}$ .*

The TwoDLibrary contains four Linear Slide models:

1	TwoDLinearSlide-X	$x = \text{free}$ , $y = \text{stiff}$ , $\theta = \text{stiff}$
2	TwoDLinearSlide-Y	$x = \text{stiff}$ , $y = \text{free}$ , $\theta = \text{stiff}$
3	TwoDLinearSlide-XTheta	$x = \text{free}$ , $y = \text{stiff}$ , $\theta = \text{free}$
4	TwoDLinearSlide-YTheta	$x = \text{free}$ , $y = \text{stiff}$ , $\theta = \text{free}$

### Linear Actuators

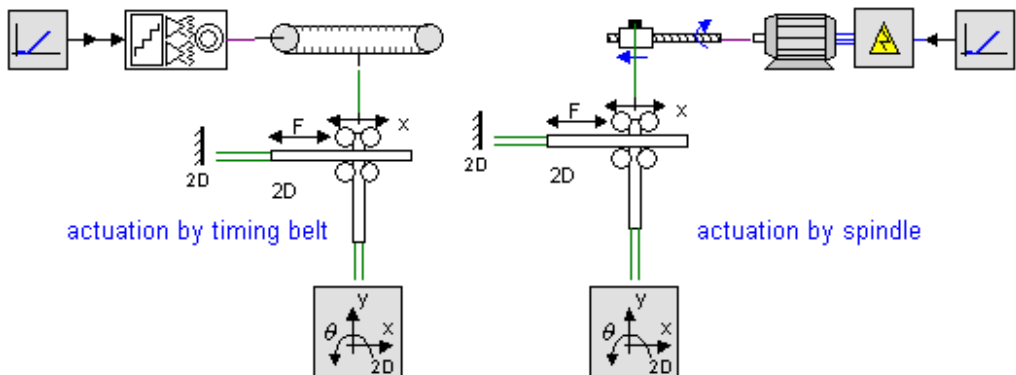
Instead of replacing the spring in  $x$ -direction with a zero force as with the linear slides, we can replace it by a 1D power port to allow all kind of connections with the models from the standard library. In this way we have created a linear actuator, that allows every kind of actuation.



Like the linear slides, for the linear actuators we can also replace the spring in  $\theta$ -direction by a zero torque, which makes the total number of linear actuator models equal to four:

- 1 TwoDLinearActuator-X  $F_x$  and  $v_x$  connected to a port
- 2 TwoDLinearActuator-Y  $F_y$  and  $v_y$  connected to a port
- 3 TwoDLinearActuator-XTheta  $F_x$  and  $v_x$  connected to a port,  $T = 0$ ,  $\omega = 0$
- 4 TwoDLinearActuator-YTheta  $F_y$  and  $v_y$  connected to a port,  $T = 0$ ,  $\omega = 0$

With the port connection ever possible form of actuation can be created. Two examples are shown below.



## Library

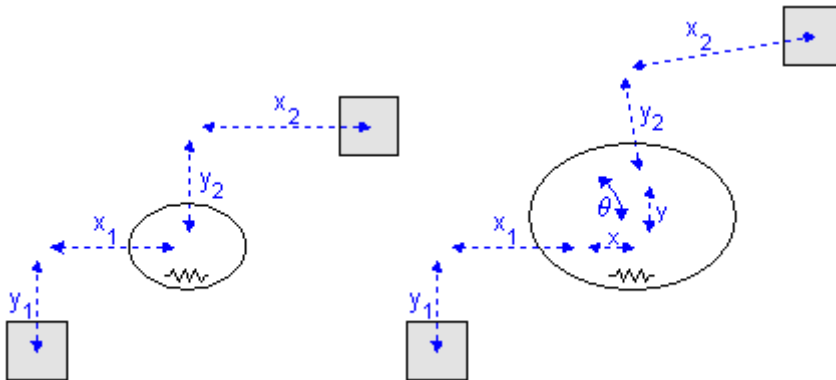
Iconic Diagrams\Mechanical\Translation\2DSmallAngles

## Use

**Domains:** Continuous. **Size:** 2-D. **Kind:** Iconic Diagrams (2D Planar).

## Description

A TwoDSpring model represents a flexible connection between two bodies. The bodies are located relative to the center of stiffness. The offsets from the bodies to the center of stiffness are indicated by  $x_1$ ,  $y_1$ ,  $x_2$  and  $y_2$  as shown in the picture below (left).



*A 2-D spring in rest (left) and stretched (right).*

Note that  $x_1$ ,  $y_1$ ,  $x_2$  and  $y_2$  are defined with respect to the spring coordinate frame which is at the center of the spring. This means in the picture above  $x_1$  and  $y_1$  have a negative value and  $x_2$  and  $y_2$  have a positive value.

When the spring is stretched the offsets will change by the spring elongations  $x$ ,  $y$  and  $\theta$  as indicated in the picture (right). The center of stiffness is always located precisely in the middle of the spring elongations. Because all spring equations will be calculated from the center of stiffness this means that the offsets for a stretched spring are  $(x_1 - x/2)$ ,  $(y_1 - y/2)$ ,  $(x_2 + x/2)$  and  $(y_2 + y/2)$ .

For a realistic representation of vibration behavior, every 2D spring has a damper in parallel. If you want to turn off the effects of this damper, choose the damping parameters equal to zero. If you want to damp out unwanted vibrations, choose the damping parameters equal to 0.1% to 10% of the spring parameters.

## Interface

### Ports

P[3]

### Description

Port with three degrees of freedom ( $x$ ,  $y$ ,  $\theta$ ).

### Causality

fixed force out P

### Parameters

x1	distance in x-direction from center of stiffness to port 1 [m]
y1	distance in y-direction from center of stiffness to port 1 [m]
x2	distance in x-direction from center of stiffness to port 2 [m]
y2	distance in y-direction from center of stiffness to port 2 [m]
kx	stiffness in x-direction [N/m]
ky	stiffness in y-direction [N/m]
kth	rotational stiffness [N.m/rad]
dx	damping in x-direction [N.s/m]
dy	damping in y-direction [N.s/m]
dth	rotational damping [N.m.s/rad]

**Initial Values**

x_initial	The initial extension of the spring [m].
y_initial	The initial extension of the spring [m].
theta_initial	The initial rotation of the spring [rad].

**Library**

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

**Implementations**

X  
Y  
XTheta  
YTheta

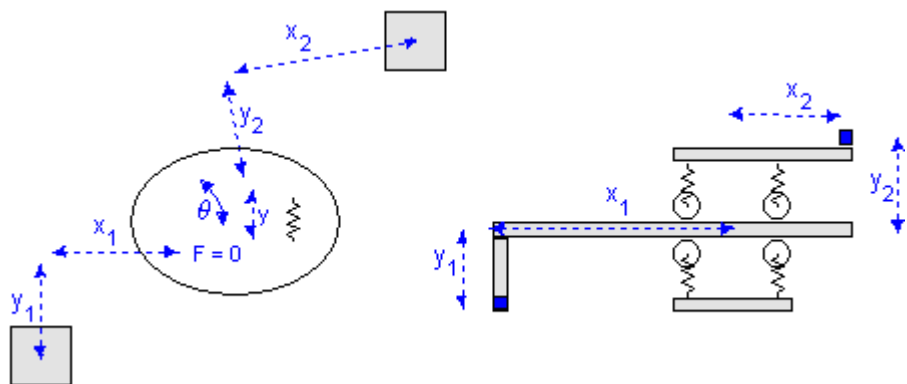
**Use**

**Domains:** Continuous. **Size:** 2-D. **Kind:** Iconic Diagrams (2D Planar).

**Description - X**

The TwoDLinearSlide-X model represents a flexible connection between two bodies in  $y$ - and  $\theta$ -direction. The bodies are located relative to the center of stiffness. The offsets from the bodies to the center of stiffness are indicated by the parameters  $x1$ ,  $y1$ ,  $x2$  and  $y2$  as shown in the picture below.

The TwoDLinearSlide-X model is based on the TwoDSpring model by replacing the spring and damper in  $x$ -direction by a zero force. Consider a carriage that is clamped with four wheels to a slide. In the  $x$ -direction the carriage is free to move, which is equal to a zero force. The limited stiffness of the wheels is represented by springs. If there is a force with equal sign on both wheels, the carriage will slightly move in the  $y$ -direction. If there is a force with opposite sign on both wheels, the carriage will only rotate. This can be represented by two independent springs: one in the  $y$ -direction and  $\theta$ -direction.



*Linear slide:  $x = \text{free}$ ,  $y = \text{stiff}$ ,  $\theta = \text{stiff}$ .*

For a realistic representation of vibration behavior, every spring has a damper in parallel. If you want to turn off the effects of this damper, choose the damping parameters equal to zero. If you want to damp out unwanted vibrations, choose the damping parameters equal to 0.1% to 10% of the spring parameters.

## Interface - X

### Ports

P[3]

### Description

Port with three degrees of freedom ( $x$ ,  $y$ ,  $\theta$ ).

### Causality

fixed force out P

### Parameters

$x_1$	distance in x-direction from center of stiffness to port 1 [m]
$y_1$	distance in y-direction from center of stiffness to port 1 [m]
$x_2$	distance in x-direction from center of stiffness to port 2 [m]
$y_2$	distance in y-direction from center of stiffness to port 2 [m]
$k_y$	stiffness in y-direction [N/m]
$k_{\theta}$	rotational stiffness [N.m/rad]
$d_y$	damping in y-direction [N.s/m]
$d_{\theta}$	rotational damping [N.m.s/rad]

### Initial Values

$y_{\text{initial}}$	The initial extension of the spring [m].
$\theta_{\text{initial}}$	The initial rotation of the spring [rad].

## Description - Y

The TwoDLinearSlide-Y model is equal to the TwoDLinearSlide-X model except that here the movement is free in the y-direction.



## Interface - Y

### Ports

P[3] Port with three degrees of freedom ( $x$ ,  $y$ ,  $\theta$ ).

### Causality

fixed force out P

### Parameters

x1	distance in x-direction from center of stiffness to port 1 [m]
y1	distance in y-direction from center of stiffness to port 1 [m]
x2	distance in x-direction from center of stiffness to port 2 [m]
y2	distance in y-direction from center of stiffness to port 2 [m]
kx	stiffness in x-direction [N/m]
kth	rotational stiffness [N.m/rad]
dx	damping in x-direction [N.s/m]
dth	rotational damping [N.m.s/rad]

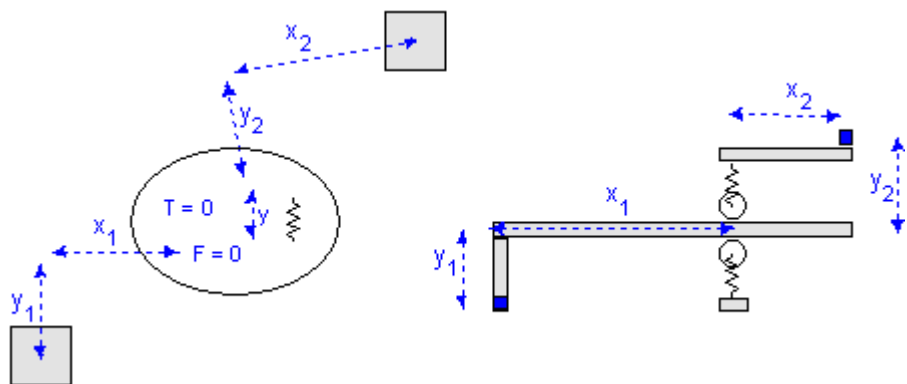
### Initial Values

x_initial	The initial extension of the spring [m].
theta_initial	The initial rotation of the spring [rad].

## Description - XTheta

The TwoDLinearSlide-XTheta model represents a flexible connection between two bodies in y-direction. The bodies are located relative to the center of stiffness. The offsets from the bodies to the center of stiffness are indicated by the parameters  $x1$ ,  $y1$ ,  $x2$  and  $y2$  as shown in the picture below.

The TwoDLinearSlide-X model is based on the TwoDSpring model by replacing the spring and damper in x- and  $\theta$ -direction by a zero force. Consider a carriage that is clamped with two wheels to a slide. In the x-direction the carriage is free to move, which is equal to a zero force. The carriage is also free to rotate, which is equal to a zero torque. The limited stiffness of the wheels is represented by springs. If there is a force on the wheels, the carriage will slightly move in the y-direction.



*Linear slide:  $x = \text{free}$ ,  $y = \text{stiff}$ ,  $\theta = \text{stiff}$ .*

For a realistic representation of vibration behavior, every spring has a damper in parallel. If you want to turn off the effects of this damper, choose the damping parameters equal to zero. If you want to damp out unwanted vibrations, choose the damping parameters equal to 0.1% to 10% of the spring parameters.

### Interface - XTheta

Ports	Description
P[3]	Port with three degrees of freedom ( $x$ , $y$ , $\theta$ ).

#### Causality

fixed force out P

#### Parameters

$x_1$	distance in x-direction from center of stiffness to port 1 [m]
$y_1$	distance in y-direction from center of stiffness to port 1 [m]
$x_2$	distance in x-direction from center of stiffness to port 2 [m]
$y_2$	distance in y-direction from center of stiffness to port 2 [m]
$k_y$	stiffness in y-direction [N/m]
$d_y$	damping in y-direction [N.s/m]

#### Initial Values

$y_{\text{initial}}$	The initial extension of the spring [m].
----------------------	--

### Description - YTheta

The TwoDLinearSlide-YTheta model is equal to the TwoDLinearSlide-XTheta model except that here the movement is free in the  $y$  and  $\theta$ -direction.

### Interface - YTheta

Ports	Description
P[3]	Port with three degrees of freedom ( $x$ , $y$ , $\theta$ ).

**Causality**

fixed force out P

**Parameters**

x1	distance in x-direction from center of stiffness to port 1 [m]
y1	distance in y-direction from center of stiffness to port 1 [m]
x2	distance in x-direction from center of stiffness to port 2 [m]
y2	distance in y-direction from center of stiffness to port 2 [m]
kx	stiffness in x-direction [N/m]
dx	damping in x-direction [N.s/m]

**Initial Values**

x_initial	The initial extension of the spring [m].
-----------	--

**Library**

Iconic Diagrams\Mechanical\Translation\2DSmallAngles

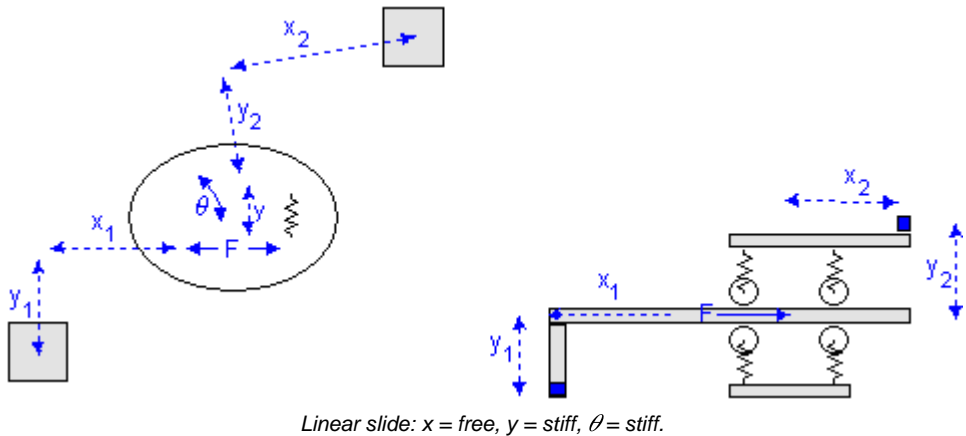
**Implementations**

X  
Y  
XTheta  
YTheta

**Use****Domains:** Continuous. **Size:** 1-D / 2-D. **Kind:** Iconic Diagrams (1D Translation, 2D Planar).**Description - X**

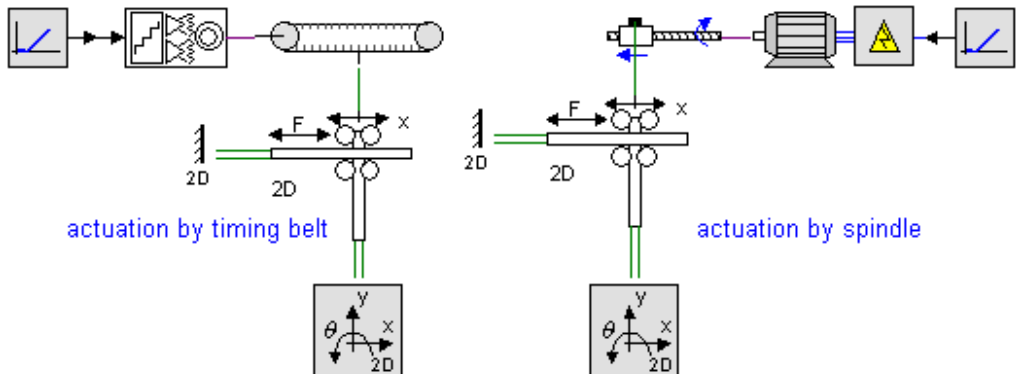
The TwoDLinearActuator-X model represents a flexible connection between two bodies in  $y$ - and  $\theta$ -direction. The TwoDLinearActuator-X model is based on the TwoDLinearSlide-X model. Instead of using a zero force in the  $x$ -direction, there is a coupling with a 1D translation port for the actuator force.

Consider a carriage that is clamped with four wheels to a slide. In the  $x$ -direction the carriage can be moved by a certain force. The limited stiffness of the wheels is represented by springs. If there is a force with equal sign on both wheels, the carriage will slightly move in the  $y$ -direction. If there is a force with opposite sign on both wheels, the carriage will only rotate. This can be represented by two independent springs: one in the  $y$ -direction and  $\theta$ -direction.



For a realistic representation of vibration behavior, every spring has a damper in parallel. If you want to turn off the effects of this damper, choose the damping parameters equal to zero. If you want to damp out unwanted vibrations, choose the damping parameters equal to 0.1% to 10% of the spring parameters.

With the 1D port connection every possible form of actuation can be created using the models from the standard library. Two examples are shown below.



## Interface - X

### Ports

P[3]

### Description

Port with three degrees of freedom ( $x$ ,  $y$ ,  $\theta$ ).

p

1D translation port

### Causality

fixed force out P

### Parameters

x1

distance in x-direction from center of stiffness to port 1 [m]

y1	distance in y-direction from center of stiffness to port 1 [m]
x2	distance in x-direction from center of stiffness to port 2 [m]
y2	distance in y-direction from center of stiffness to port 2 [m]
ky	stiffness in y-direction [N/m]
kth	rotational stiffness [N.m/rad]
dy	damping in y-direction [N.s/m]
dth	rotational damping [N.m.s/rad]

**Initial Values**

y_initial	The initial extension of the spring [m].
theta_initial	The initial rotation of the spring [rad].

**Description - Y**

The TwoDLinearActuator-Y model is equal to the TwoDLinearActuator-X model except that here the force acts in the y-direction.

**Interface - Y**

Ports	Description
P[3]	Port with three degrees of freedom (x, y, $\theta$ ).
p	1D translation port

**Causality**

fixed force out P

**Parameters**

x1	distance in x-direction from center of stiffness to port 1 [m]
y1	distance in y-direction from center of stiffness to port 1 [m]
x2	distance in x-direction from center of stiffness to port 2 [m]
y2	distance in y-direction from center of stiffness to port 2 [m]
kx	stiffness in x-direction [N/m]
kth	rotational stiffness [N.m/rad]
dx	damping in x-direction [N.s/m]
dth	rotational damping [N.m.s/rad]

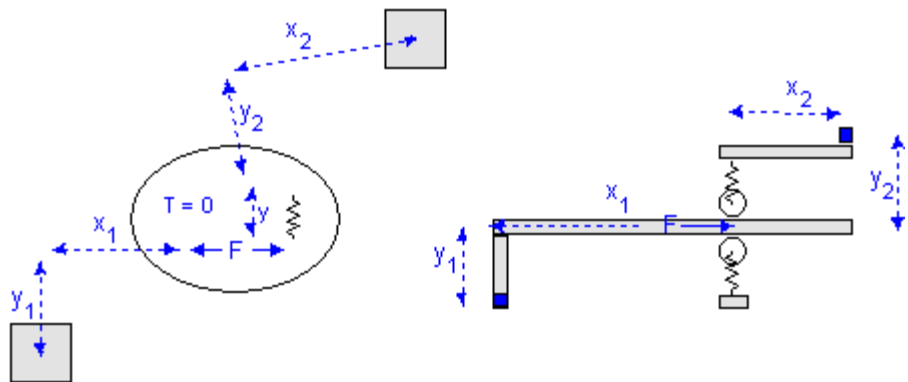
**Initial Values**

x_initial	The initial extension of the spring [m].
theta_initial	The initial rotation of the spring [rad].

**Description - XTheta**

The TwoDLinearActuator-XTheta model represents a flexible connection between two bodies in y-direction. The TwoDLinearActuator-XTheta model is based on the TwoDLinearSlide-XTheta model. Instead of using a zero force in the x-direction, there is a coupling with a 1D translation port for the actuator force.

Consider a carriage that is clamped with two wheels to a slide. In the x-direction the carriage can be moved by a certain force. The carriage is free to rotate, which is equal to a zero torque. The limited stiffness of the wheels is represented by springs. If there is a force acting on both wheels, the carriage will slightly move in the y-direction. If there is a force acting on the wheels, the carriage will slightly move in the y-direction.



Linear slide:  $x = \text{free}$ ,  $y = \text{stiff}$ ,  $\theta = \text{stiff}$ .

For a realistic representation of vibration behavior, the spring has a damper in parallel. If you want to turn off the effects of this damper, choose the damping parameters equal to zero. If you want to damp out unwanted vibrations, choose the damping parameter equal to 0.1% to 10% of the spring parameter.

With the 1D port connection every possible form of actuation can be created using the models from the standard library. For example see the TwoDLinearActuator-X model.

**Interface - XTheta**

Ports	Description
P[3]	Port with three degrees of freedom ( $x$ , $y$ , $\theta$ ).
p	1D translation port

**Causality**

fixed force out P

**Parameters**

x1	distance in x-direction from center of stiffness to port 1 [m]
y1	distance in y-direction from center of stiffness to port 1 [m]
x2	distance in x-direction from center of stiffness to port 2 [m]
y2	distance in y-direction from center of stiffness to port 2 [m]
ky	stiffness in y-direction [N/m]
dy	damping in y-direction [N.s/m]

**Initial Values**

y_initial	The initial extension of the spring [m].
-----------	--

## Description - YTheta

The TwoDLinearActuator-YTheta model is equal to the TwoDLinearActuator-XTheta model except that here the force acts in the y-direction.

## Interface - YTheta

Ports	Description
P[3]	Port with three degrees of freedom (x, y, $\theta$ ).
p	1D translation port
<b>Causality</b>	
fixed force out P	
<b>Parameters</b>	
x1	distance in x-direction from center of stiffness to port 1 [m]
y1	distance in y-direction from center of stiffness to port 1 [m]
x2	distance in x-direction from center of stiffness to port 2 [m]
y2	distance in y-direction from center of stiffness to port 2 [m]
kx	stiffness in x-direction [N/m]
kth	rotational stiffness [N.m/rad]
dx	damping in x-direction [N.s/m]
dth	rotational damping [N.m.s/rad]
<b>Initial Values</b>	
x_initial	The initial extension of the spring [m].
theta_initial	The initial rotation of the spring [rad].

When you are working with the 2D-Library for small angles, it is good to keep the following tips in mind:

- The 2DSmallRotations library is very well suited for frequency domain analysis through linearization.
- The 2DSmallRotations library is not suited for large rotations. Consider a rotation of 0.05 degrees or 1 mrad as an upper bound for every model part.
- It is not possible in 2D-sim to use vector elements with mixed units. Therefore element number 3 will be displayed with units [m/s] and [N] although it really is [rad/s] and [Nm]!
- The vector element number (1, 2 or 3) denotes the degree of freedom. Flipping or rotating of a model does not change this degree (e.g. a rotation does not change from x into y). Preferably leave the orientation of the models as they pop up on the screen.
- To create intuitive models, the positive direction of each degree of freedom is defined as: x from left to right, y from bottom to top,  $\theta$  counter clockwise.
- To prevent misinterpretation of a model by other users, stick to the drawing rules that are given.
- A TwoDBody model can be connected to any other element of the 2D-library except other 2D-bodies.

- A *TwoDBody* model can be connected to 1D models using the *TwoDPoint* models as intermediate.
- *TwoDPoint* models can only be connected to *TwoDBody* models.
- If a *TwoDBody* model is connected to *TwoDPoint* models only, it has to be connected to at least three non-coinciding, unequal (i.e. not having the same offsets) *TwoDPoints* to prevent it from free motion.

## Library

The *3DSmallRotation* library contains 3D models that are only suited for small rotations. The library is comparable to the *2DSmallRotation* library and suited for modeling systems that, due to limited stiffness, experience rotation that should be accounted for.

### Degrees of Freedom

All models in *3DSmallRotation* library contain one or more ports with 6 degrees of freedom. The first three degrees of freedom denote the x-, y- and z-position and the last three degrees of freedom denote the rotation around the x-, y- and z-axes. A vector notation is used to denote the forces and velocities for these degrees of freedom. For a model with a port *P* the notation is:

degree	identity	forces	velocities
x	position	P.F[1] [N]	P.v[1] [m/s]
y	position	P.F[2] [N]	P.v[2] [m/s]
z	position	P.F[3] [N]	P.v[3] [m/s]
$\theta_x$	angle	P.F[4] [Nm]	P.v[4] [rad/s]
$\theta_y$	angle	P.F[5] [Nm]	P.v[5] [rad/s]
$\theta_z$	angle	P.F[6] [Nm]	P.v[6] [rad/s]

### Note

- It is not possible in 20-sim to use vector elements with mixed units. Therefore element number 4 to 6 will be displayed with units [m/s] and [N] although it really is [rad/s] and [Nm]!
- The vector element number (1 to 6) denotes the identity of the degree of freedom. Flipping or rotating of a model does not change the this identity (e.g. a rotation does not change x into y). Preferably leave the orientation of the models as they pop up on the screen.



## 3D-body



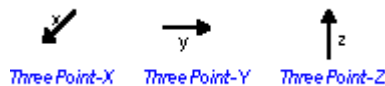
*TwoDBody*

The central model in the *3DSmallRotation* library is the 3D-body model which describes a body with 6 degrees of freedom.

### 3D-mass

The 3D-mass model is a body with only mass and zero rotational inertia.

### Points



The 3D-body model is nothing more than a center of mass. To connect a 3D-body with the outside (single degree of freedom) world, 3D-points are used. A 3D-point describes the offset between the center of mass and the connection point.

- A 3D-body has to be connected to 3D-points with at least three orthogonal nonzero offsets to prevent it from free rotation.
- A 3D-body has to be connected to at least three orthogonal 3D-point models to prevent it from free motion.

### Sensors

The velocities of bodies can be inspected directly in the body models. To find positions sensor models are available.

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

### Use

**Domains:** Continuous. **Size:** 6D. **Kind:** Iconic Diagrams (Translation,Rotation).

### Description

This is a model of a 6 degree of freedom body. It is the equivalent of the 2D-body model. The first three degrees of freedom in this model are represented by a single mass and the last three degrees of freedom by a rotational inertia. The 3D-body has to be connected to at least three orthogonal 3D-points, which define the reaction forces.

The model has a preferred velocity out causality. The corresponding constitutive equations then contain an integration. The model can also have the non-preferred force out causality. The constitutive equations then contain a differentiation. Because any number of connections can be made, successive ports are named  $P1$ ,  $P2$ ,  $P3$  etc. 20-sim will automatically create equations such that the resulting force  $P.F$  is equal to the sum of the forces of all connected ports  $P1 \dots Pn$ . The velocities of all connected ports are equal to  $P.v$

$$P.F = \text{sum}(P1.F, P2.F, \dots)$$

$$P.v = P1.v = P2.v = \dots$$

velocity out causality (preferred):

$$I = [1/M; 1/M; 1/M; 1/J[1]; 1/J[2]; 1/J[3]]; \\ P.v = I.*\text{int}(P.F);$$

force out causality:

$$I = [1/M; 1/M; 1/M; 1/J[1]; 1/J[2]; 1/J[3]]; \\ P.F = I-1.*\text{ddt}(P.v);$$

## Interface

Ports	Description
P[6]	Port with 6 degrees of freedom. Any number of connections can be made.
<b>Causality</b>	
preferred	velocity
out	
<b>Parameters</b>	
M	Mass [kg].
J[3]	Moment of inertia for three axes [kgm <sup>2</sup> ]

## Note

- A body has to be connected to 3D-points with at least three orthogonal nonzero offsets to prevent it from free rotation.
- A 3D-body has to be connected to at least three orthogonal 3D-point models to prevent it from free motion.
- Flipping or rotating the model does not change the direction of applied forces or measured directions. Preferably leave the orientation as it pops up on the screen.
- It is not possible in 20-sim to use vector elements with mixed units. Therefore element number 4 to 6 will be displayed with units [m/s] and [N] although it really is [rad/s] and [Nm]!

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

### Use

**Domains:** Continuous. **Size:** 6-D. **Kind:** Iconic Diagrams (Translation,Rotation).

### Description

This model represents the fixed world in 6 degrees of freedom. It can be connected to a 3D-body model to freeze its motion.

### Interface

Ports	Description
P	Port with 6 degrees of freedom.

### Causality

fixed velocity out P

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

### Use

**Domains:** Continuous. **Size:** 1-D/6-D. **Kind:** Iconic Diagrams (Translation,Rotation).

### Description

This model represents an ideal actuator. The actuator applies a force between its two terminals. This force can be set to a (fluctuating) value given by the input signal  $F$ , the velocity is indifferent.

This model is the equivalent of the 1 degree of freedom model ForceActuator-Relative.emx. It model represents an ideal actuator. The actuator applies a force between its two terminals. The force can be set to a (fluctuating) value given by a vector  $K$  multiplied by a signal  $F$ , the velocity is indifferent. By setting the elements of the vector  $K$  equal to zero or one, specific elements of the 6 degrees of freedom output force can set equal to the input signal  $F$ .

$$P_{high}.F[1:6] = P_{low}.F[1:6] = K * F;$$

### Interface

Ports	Description
P_high[6], P_low[6]	Both terminals of the port with 6 degrees of freedom.

### Causality

fixed force out P

### Parameters

$K[6]$  Vector with 6 elements to set the 6 force elements on or off.

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

## Use

**Domains:** Continuous. **Size:** 1-D/6-D. **Kind:** Iconic Diagrams (Translation,Rotation).

## Description

This model is the equivalent of the 1 degree of freedom model *ForceActuator.emx*. It model represents an ideal actuator. The actuator is mounted to the fixed world and applies a force. The force can be set to a (fluctuating) value given by a vector  $K$  multiplied by a signal  $F$ , the velocity is indifferent. By setting the elements of the vector  $K$  equal to zero or one, specific elements of the 6 degrees of freedom output force can set equal to the input signal  $F$ .

$$P.F[1:6] = K * F;$$

## Interface

### Ports

P

### Description

Port with 6 degrees of freedom.

### Causality

fixed force out P

### Parameters

$K[6]$  Vector with 6 elements to set the 6 force elements on or off.

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

## Use

**Domains:** Continuous. **Size:** 6D. **Kind:** Iconic Diagrams (Translation,Rotation).

## Description

This is a model of a 6 degree of freedom body without rotational inertia. The 3D-mass has to be connected to at least three orthogonal 3D-points, which define the reaction forces.

The model has a fixed velocity out causality. Because any number of connections can be made, successive ports are named  $P1$ ,  $P2$ ,  $P3$  etc. 20-sim will automatically create equations such that the resulting force  $P.F$  is equal to the sum of the forces of all connected ports  $P1 \dots Pn$ . The velocities of all connected ports are equal to  $P.v$

```

P.F = sum(P1.F, P2.F, ....)
P.v = P1.v = P2.v = ....
I = [1/M; 1/M; 1/M];
P.v[1..3] = I.*int(P.F);
P.v[4..6] = 0;

```

## Interface

### Ports

P[6] Port with 6 degrees of freedom. Any number of connections can be made.

### Causality

fixed velocity out

### Parameters

M Mass [kg].

## Note

- A 3D-body has to be connected to 3D-points with at least three orthogonal nonzero offsets to prevent it from free rotation.
- A 3D-body has to be connected to at least three orthogonal 3D-point models to prevent it from free motion.
- Flipping or rotating the model does not change the direction of applied forces or measured directions. Preferably leave the orientation as it pops up on the screen.
- It is not possible in 20-sim to use vector elements with mixed units. Therefore element number 4 to 6 will be displayed with units [m/s] and [N] although it really is [rad/s] and [Nm]!

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

## Implementations

X  
Y  
Z  
XYZ

## Use

**Domains:** Continuous. **Size:** 1-D/6-D. **Kind:** Iconic Diagrams (Translation,Rotation).

### Description - X

A point model forms the connection between the single degree of freedom part of a system and the center of mass of a 3D-body.

The 3D-point-X model is the equivalent of the 2D-point-X model. It describes the translation of force in x-direction to a force in 6 degrees of freedom. Because there are three rotational degrees of freedom, the 3D-point-X model has two offsets, *YP* and *ZP*.

The single degree of freedom port *p\_in* describes the connection in x-direction and the 6 degree of freedom port *P\_out* describes connection with the 3D-body.

```

P_out.F[1] = p_in.F;           // x-direction
P_out.F[2] = 0;               // y-direction
P_out.F[3] = 0;               // z-direction
P_out.F[4] = 0;               // x-rotation
P_out.F[5] = ZP*p_in.F;       // y-rotation
P_out.F[6] = -YP*p_in.F;      // z-rotation

p_in.v = P_out.v[1] - YP*P_out.v[6] // x-direction
+ ZP *P_out.v[5];

```

As can be seen from the equations, a nonzero offset *YP* or *ZP* (distance from center of mass) in a 3D-point will result in a momentum. Therefore a 3D-body has to be connected to 3D-points with at least three orthogonal nonzero offsets to prevent it from free rotation.

The equations also show that the y-direction and z-direction are not affected by the *3D-point-X* model. Therefore each 3D-body has to be connected to at least three orthogonal 3D-point models to prevent it from free motion.

## Interface - X

Ports	Description
p_in	Translation port with one degree of freedom (x [m]).
P_out[3]	Port with 6 degrees of freedom.

### Causality

```

fixed force out
P_out
fixed velocity out
p_in

```

### Parameters

YP	Distance (y-direction) between connection and center of mass [m].
ZP	Distance (z-direction) between connection and center of mass [m].

## Description - Y

A point model forms the connection between the single degree of freedom part of a system and the center of mass of a 3D-body.

The 3D-point-Y model is the equivalent of the 2D-point-Y model. It describes the translation of force in x-direction to a force in 6 degrees of freedom. Because there are three rotational degrees of freedom, the 3D-point-Y model has two offsets, *XP* and *ZP*.

The single degree of freedom port *p\_in* describes the connection in x-direction and the 6 degree of freedom port *P\_out* describes connection with the 3D-body.

```

P_out.F[1] = 0;           // x-direction
P_out.F[2] = p_in.F;       // y-direction

```

```

P_out.F[3] = 0; // z-direction
P_out.F[4] = -ZP*p_in.F; // x-rotation
P_out.F[5] = 0; // y-rotation
P_out.F[6] = XP*p_in.F; // z-rotation

p_in.v = P_out.v[2] + XP*P_out.v[6] // y-direction
- ZP *P_out.v[4];

```

As can be seen from the equations, a nonzero offset  $XP$  or  $ZP$  (distance from center of mass) in a 3D-point will result in a momentum. Therefore a 3D-body has to be connected to 3D-points with at least three orthogonal nonzero offsets to prevent it from free rotation.

The equations also show that the x-direction and z-direction are not affected by the 3D-point-Y model. Therefore each 3D-body has to be connected to at least three orthogonal 3D-point models to prevent it from free motion.

### Interface - Y

Ports	Description
p_in	Translation port with one degree of freedom (x [m]).
P_out[3]	Port with 6 degrees of freedom.

#### Causality

```

fixed force out
P_out
fixed velocity out
p_in

```

#### Parameters

XP	Distance (x-direction) between connection and center of mass [m].
ZP	Distance (z-direction) between connection and center of mass [m].

### Description - Z

A point model forms the connection between the single degree of freedom part of a system and the center of mass of a 3D-body.

The 3D-point-Z model is the equivalent of the 2D-point-X model. It describes the translation of force in z-direction to a force in 6 degrees of freedom. Because there are three rotational degrees of freedom, the 3D-point-Y model has two offsets,  $XP$  and  $YP$ .

The single degree of freedom port  $p\_in$  describes the connection in x-direction and the 6 degree of freedom port  $P\_out$  describes connection with the 3D-body.

```

P_out.F[1] = 0; // x-direction
P_out.F[2] = 0; // y-direction
P_out.F[3] = p_in.F; // z-direction
P_out.F[4] = YP*p_in.F; // x-rotation

```

```

P_out.F[5] = -XP*p_in.F;           // y-rotation
P_out.F[6] = 0;                     // z-rotation

p_in.v = P_out.v[3] - XP*P_out.v[5] // y-direction
+ YP *P_out.v[4];

```

As can be seen from the equations, a nonzero offset  $XP$  or  $YP$  (distance from center of mass) in a 3D-point will result in a momentum. Therefore a 3D-body has to be connected to 3D-points with at least three orthogonal nonzero offsets to prevent it from free rotation.

The equations also show that the x-direction and y-direction are not affected by the 3D-point-Z model. Therefore each 3D-body has to be connected to at least three orthogonal 3D-point models to prevent it from free motion.

## Interface - Z

Ports	Description
p_in	Translation port with one degree of freedom (x [m]).
P_out[3]	Port with 6 degrees of freedom.

### Causality

```

fixed force out
P_out
fixed velocity out
p_in

```

### Parameters

XP	Distance (x-direction) between connection and center of mass [m].
YP	Distance (y-direction) between connection and center of mass [m].

## Description - XYZ

A point model forms the connection between the single degree of freedom part of a system and the center of mass of a 3D-body.

The 3D-point-XYZ model is a combination of the 3D-point-X model, the 3D-point-Y model and the 3D-point-Z model. It describes the translation of force in x-direction, y-direction and z-direction to a force in 6 degrees of freedom. Because there are three rotational degrees of freedom, the model has three offsets,  $XP$ ,  $YP$  and  $ZP$ .

The single degree of freedom ports  $p_{inx}$ ,  $p_{iny}$  and  $p_{inz}$  describes the connection in x-direction, y-direction and z-direction and the 6 degree of freedom port  $P_{out}$  describes connection with the 3D-body.

```

P_out.F[1] = p_inx.F;           // x-direction
P_out.F[2] = p_iny.F;           // y-direction
P_out.F[3] = p_inz.F;           // z-direction
P_out.F[4] = YP*p_inz.F - ZP*p_iny.F; // x-rotation

```



```

P_out.F[5] = -XP*p_inz.F + ZP*p_inx.F;    // y-rotation
P_out.F[6] = XP*p_iny.F - YP*p_inx.F;    // z-rotation

p_inx.v = P_out.v[1] - YP*P_out.v[6] + ZP // x-direction
*p_out.v[5];                             // y-direction
p_iny.v = P_out.v[2] + XP*P_out.v[6] - ZP // z-direction
*p_out.v[4];
p_inz.v = P_out.v[3] - XP*P_out.v
[5] + YP *P_out.v[4];

```

As can be seen from the equations, a nonzero offset  $XP$ ,  $YP$  or  $ZP$  (distance from center of mass) in a 3D-point will result in a momentum. **Therefore a 3D-body has to be connected to 3D-points with at least three orthogonal nonzero offsets to prevent it from free rotation.**

## Interface - XYZ

Ports	Description
p_inx	Translation port with one degree of freedom [m].
p_iny	Translation port with one degree of freedom [m].
p_inz	Translation port with one degree of freedom [m].
P_out[3]	Port with 6 degrees of freedom.

### Causality

```

fixed   force   out
P_out
fixed   velocity out
p_in

```

### Parameters

YP	Distance (y-direction) between connection and center of mass [m].
XP	Distance (x-direction) between connection and center of mass [m].
theta	Angle of impact of the single degree of freedom port [rad].

## Note

- A body has to be connected to 3D-points with at least three orthogonal nonzero offsets to prevent it from free rotation.
- A 3D-body has to be connected to at least three orthogonal 3D-point models to prevent it from free motion.
- Flipping or rotating the model does not change the direction of applied forces or measured directions. Preferably leave the orientation as it pops up on the screen.

- It is not possible in 20-sim to use vector elements with mixed units. Therefore element number 4 to 6 will be displayed with units [m/s] and [N] although it really is [rad/s] and [Nm]!

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

### Use

**Domains:** Continuous. **Size:** 1-D/6D. **Kind:** Iconic Diagrams (Translation,Rotation).

### Description

This model is used to find the positions of a 3D-body model. It has a port  $P$  which can be connected to the body and an output signal pos that denotes the positions  $(x,y,z,\theta_x,\theta_y,\theta_z)$  of the body.

### Interface

Ports	Description
P[3]	Port with 6 degrees of freedom.

### Causality

fixed force out P

### Output

Pos(6) Absolute positions [m].

### Initial Values

Pos\_initial[6] Initial positions [m]

### Note

- The sensor model yields an absolute position starting at 0. Set the initial values to yield a position starting at other values.
- It is not possible in 20-sim to use vector elements with mixed units. Therefore element number 4 to 6 will be displayed with units [m] although it really is [rad]!

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

### Use

**Domains:** Continuous. **Size:** 1-D/6-D. **Kind:** Iconic Diagrams (Translation,Rotation).

### Description

This model is the equivalent of the 1 degree of freedom model SpringDamper.emx. It model represents an ideal spring-damper. The model has a preferred force out causality. The corresponding constitutive equations then contain integrations. The element can also have the non-preferred velocity out causality. The constitutive equations then contain derivatives. The spring-damper model has separate high and low ports. The equations are

$$P.F = P\_high.F = P\_low.F$$

$$P.v = P\_high.v - P\_low.v$$

Force out causality (preferred):

$$X = \text{int}(P.v);$$

$$P.F = S*X + D*P.v;$$

Velocity out causality:

$$P.v = \text{ddt}(X);$$

$$X = S^{-1}*(P.F - D*P.v);$$

## Interface

### Ports Description

P\_high[6], P\_low Both terminals of a port with 6 degrees of freedom.  
[6]

### Causality

preferred force out  
P

### Variables

X Vector with 6 spring extension values [m].

### Parameters

S[6] Stiffness vector [N/m]  
D[6] Damping vector [N.s/m]

### Initial Values

X\_initial[6] Vector with 6 initial extension values of the spring [m].

## Note

It is not possible in 20-sim to use vector elements with mixed units. Therefore element number 4 to 6 will be displayed with units [m/s] and [N] although it really is [rad/s] and [Nm] etc.!

## Library

Iconic Diagrams\Mechanical\Translation\3DSmallAngles

## Use

**Domains:** Continuous. **Size:** 6-D. **Kind:** Iconic Diagrams (Translation,Rotation).

## Description

This model can be used to connect any open end of another 3D model that is not connected to the fixed world. It generates a three degree of freedom zero force while the velocity is free.

## Interface

Ports	Description
P	Port with 6 degrees of freedom.

### Causality

fixed force out P

### Note

It is not possible in 20-sim to use vector elements with mixed units. Therefore element number 4 to 6 will be displayed with units [m/s] and [N] although it really is [rad/s] and [Nm] etc.!

## Library

Iconic Diagrams\Mechanical\Translation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model represents an ideal actuator. An acceleration input signal is integrated to a velocity difference between its two terminals:

$$\begin{aligned} p\_high.v &= p\_low.v + \text{int}(a, v\_initial); \\ p\_low.F &= p\_high.F = \text{indifferent}; \end{aligned}$$

## Interface

Ports	Description
p_high, p_low	Both terminals of the Translation port p.

### Causality

fixed velocity out

### Input

a	Acceleration [m/s <sup>2</sup> ].
---	-----------------------------------

### Parameters

v_initial	Initial velocity output of the integration [m/s].
-----------	---

## Library

Iconic Diagrams\Mechanical\Translation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model represents an ideal actuator. An acceleration input signal is integrated to a velocity at the translation port. The actuator is mounted to the fixed world:

$$p.v = \text{int}(a, v_{\text{initial}});$$

$$p.F = \text{indifferent};$$

### Interface

Ports	Description
p	Translation port.

### Causality

fixed velocity out

### Input

a	Acceleration [m/s <sup>2</sup> ].
---	-----------------------------------

### Parameters

v_initial	Initial velocity at the port [m/s].
-----------	-------------------------------------

## Library

Iconic Diagrams\Electric\Actuators

Iconic Diagrams\Mechanical\Translation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model represents a piezo actuator. The actuator translates a voltage difference at port *p1* to a mechanical position difference between the base at port *p2* and the end effector at port *p3*.

Although the underlying equations of this model are equal to the equations of the CMAStrecher.emx model, the default parameter values are typical for bending.

### Interface

Ports	Description
p	Translation port.

### Causality

fixed force out

**Input**

C	Capacitance [F]
KF	Voltage to force conversion factor [N/V]
m	Equivalent mass [kg]
k	Stiffness [N/m]
B	Relative damping ratio []
KB	Force to voltage conversion factor [V/N]

**Library**

Iconic Diagrams\Electric\Actuators

Iconic Diagrams\Mechanical\Translation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

**Description**

This model represents a piezo actuator. The actuator translates a voltage difference at port *p1* to a mechanical position difference between the base at port *p2* and the end effector at port *p3*.

Although the underlying equations of this model are equal to the equations of the CMABender.emx model, the default parameter values are typical for stretching.

**Interface****Ports**

p	Translation port.
---	-------------------

**Causality**

fixed force out

**Input**

C	Capacitance [F]
KF	Voltage to force conversion factor [N/V]
m	Equivalent mass [kg]
k	Stiffness [N/m]
B	Relative damping ratio []
KB	Force to voltage conversion factor [V/N]

## Library

Iconic Diagrams\Mechanical\Translation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model represents an ideal actuator. The actuator applies a force between its two terminals. This force can be set to a constant value  $F$ , the velocity is indifferent.

$$p_{high}.F = p_{low}.F = F$$

### Interface

Ports	Description
$p_{high}$ , $p_{low}$	Both terminals of the Translation port $p$ .
<b>Causality</b>	
fixed force out	
<b>Parameters</b>	
$F$	Force [N]

## Library

Iconic Diagrams\Mechanical\Translation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Description

This model represents an ideal actuator. The actuator is mounted to the fixed world and applies a force. The force can be set to a certain constant value, the velocity is indifferent.

$$p.F = F;$$

### Interface

Ports	Description
$p$	Translation port.
<b>Causality</b>	
fixed force out	
<b>Parameters</b>	
$F$	Force [N].

**Library**

Iconic Diagrams\Mechanical\Translation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

**Description**

This model represents an ideal actuator. The actuator applies a force between its two terminals. This force can be set to a (fluctuating) value given by the input signal  $F$ , the velocity is indifferent.

$$p_{high}.F = p_{low}.F = F$$

**Interface**

Ports	Description
$p_{high}$ , $p_{low}$	Both terminals of the Translation port p.
<b>Causality</b>	
fixed force out	
<b>Input</b>	
$F$	Force [N]

**Library**

Iconic Diagrams\Mechanical\Translation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

**Description**

This model represents an ideal actuator. The actuator is mounted to the fixed world and applies a force. The force can be set to a (fluctuating) value given by the input signal  $F$ , the velocity is indifferent.

$$p.F = F;$$

**Interface**

Ports	Description
p	Translation port.
<b>Causality</b>	
fixed force out	



**Input**

F Force [N].

**Library**

Iconic Diagrams\Mechanical\Translation\Actuators

**Use**

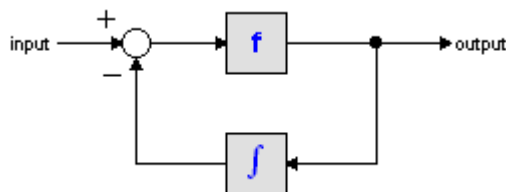
**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

**Description**

This model represents an ideal actuator. A position input signal is differentiated by a state variable filter to a velocity difference between its two terminals:

$$\begin{aligned} p_{high}.v &= p_{low}.v + dx/dt; \\ p_{low}.F &= p_{high}.F = \text{indifferent}; \end{aligned}$$

Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where  $f$  is the cut-off frequency. For very high values of  $f$ , the output becomes the pure derivative of the input. High values of  $f$ , however, increase simulations times. A good trade-off is a starting value of  $1e5$ .

**Interface****Ports**

p\_high, p\_low

**Description**

Both terminals of the Translation port p.

**Causality**

fixed velocity out

**Input**

x Position [m].

**Parameters**

f Cut-off frequency of the differentiation [Hz].

v\_initial Initial velocity output of the differentiation [m/s].

## Library

Iconic Diagrams\Mechanical\Translation\Actuators

## Use

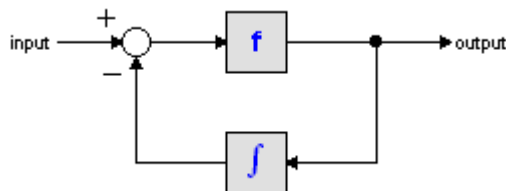
**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

## Description

This model represents an ideal actuator. A position input signal is differentiated by a state variable filter to a velocity at the translation port. The actuator is mounted to the fixed world:

$$\begin{aligned} p.v &= dx/dt; \\ p.F &= \text{indifferent}; \end{aligned}$$

Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where  $f$  is the cut-off frequency. For very high values of  $f$ , the output becomes the pure derivative of the input. High values of  $f$ , however, increase simulations times. A good trade-off is a starting value of  $1e5$ .

## Interface

Ports	Description
p	Translation port.
<b>Causality</b>	
fixed velocity out	
<b>Input</b>	
x	Position [m].

**Parameters**

f	Cut-off frequency of the differentiation [Hz].
v_initial	Initial velocity at the port [m/s].

**Library**

Iconic Diagrams\Mechanical\Rotation\Actuators  
 Iconic Diagrams\Mechanical\Translation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric).

**Description**

This is a masked model which opens the Servo Motor Editor when edited. The servo Motor Editor is a tool that can shows the torque speed plots numerous permanent magnet motors and can generate a dynamic model from any motor that you select. The following motor types are supported:

1. Brush DC
2. Brushless DC (trapezoidal EMC and square wave currents)
3. AC synchronous (sinusoidal EMC and sinusoidal currents)
4. AC synchronous linear (sinusoidal EMC and sinusoidal currents)

**Interface**

Depending on the type of motor that you have selected, the interface can vary:

**DC Brush**

Ports	Description
p	Rotation port.

**Causality**

fixed      rotational  
 velocity out

**Input**

i	The input current [A]
---	-----------------------

**DC Brushless**

Ports	Description
p	Rotation port.

**Causality**

fixed      rotational  
velocity out

**Input**

i                      The maximum input current [A]

**AC Synchronous**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p	Rotation port.
---	----------------

**Causality**

fixed      rotational  
velocity out

**Input**

i\_rms                      The rms phase current [A]

**AC Synchronous Linear**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p	Translation port.
---	-------------------

**Causality**

fixed velocity out

**Input**

i\_rms                      The rms phase current [A]

For more information on the parameters and variables of this model is referred to the Mechatronic Toolbox.

**Library**

Iconic Diagrams\Mechanical\Translation\Actuators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Description**

This model represents an ideal actuator. The actuator applies a velocity difference between its two terminals. This velocity can be set to a constant value  $v$ , the force is indifferent.

$$p\_low.v = p\_high.v + v$$

## Interface

Ports	Description
p_high, p_low	Both terminals of the Translation port p.
<b>Causality</b>	
fixed velocity out	
<b>Parameter</b>	
v	Velocity [m/s].

## Library

Iconic Diagrams\Mechanical\Translation\Actuators

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description

This model represents an ideal actuator. The actuator is mounted to the fixed world and applies a velocity. This velocity can be set to a certain constant value, the force is indifferent.

$$p.v = v;$$

## Interface

Ports	Description
p	Translation port
<b>Causality</b>	
fixed velocity out	
<b>Parameters</b>	
v	velocity [m/s]

## Library

Iconic Diagrams\Mechanical\Translation\Actuators

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

## Description

This model represents an ideal actuator. The actuator applies a velocity difference between its two terminals. This velocity can be set to a (fluctuating) value given by the input signal  $v$ , the force is indifferent.

$$p\_high.v = p\_low.v + v$$

## Interface

Ports	Description
p_high, p_low	Both terminals of the Translation port p.
<b>Causality</b>	
fixed velocity out	
<b>Input</b>	
v	Velocity [m/s].

## Library

Iconic Diagrams\Mechanical\Translation\Actuators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model represents an ideal actuator. The actuator is mounted to the fixed world and applies a velocity. This velocity can be set to a (fluctuating) value given by the input signal  $v$ , the force is indifferent.

$$p.v = v;$$

## Interface

Ports	Description
p	Translation port.
<b>Causality</b>	
fixed velocity out	
<b>Input</b>	
v	Velocity [m/s].

## Library

Iconic Diagrams\Mechanical\Translation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Description

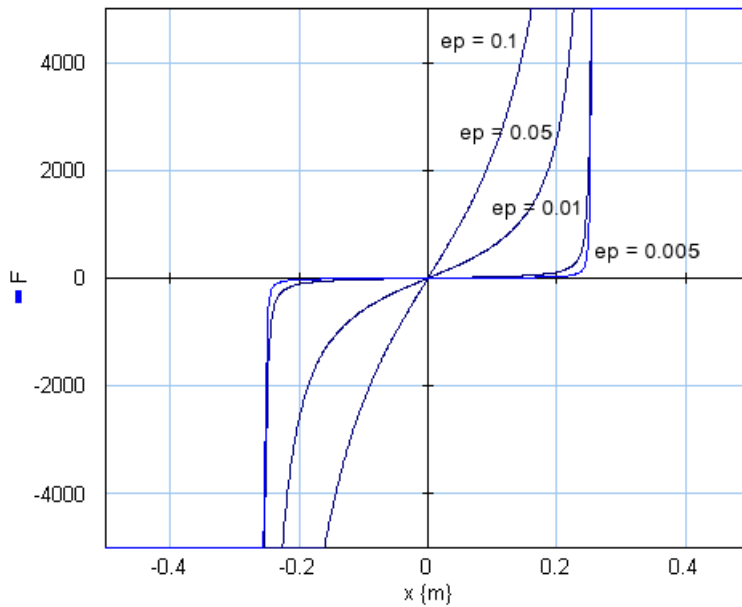
This model represents backlash by a spring damper system. Inside an outside the play, spring and damping can be set separately. Discontinuities are avoided by adding a round off. The model can has a force out causality. The port  $p$  of this model has separate high and low terminals. The equations are:

$$\begin{aligned} p.F &= p\_high.F = p\_low.F \\ p.v &= p\_high.v - p\_low.v \end{aligned}$$

$$p.F = 0.5 \cdot k_2 \cdot \left( x - \sqrt{\left(-x - \frac{s}{2}\right) + (ep \cdot s)^2} + x + \sqrt{\left(x - \frac{s}{2}\right) + (ep \cdot s)^2} \right) + k_1 \cdot x + d_{low2} \cdot p.v$$

with  $x$  the position within the play. Real backlash behavior is obtained by choosing low stiffness and damping values inside the play and choosing high stiffness and damping values outside the play.

The parameter  $ep$  determines the smoothness of the force curve that is obtained. A larger value ( $> 0.01$ ) makes the force change gradually when the position reaches the play boundaries. A smaller value ( $< 0.001$ ) makes the force change abruptly. This is shown in the figure below. A good starting value for  $ep$  is  $1e-4$ .



## Interface

### Ports

p\_high, p\_low

### Description

Both terminals of port p (Translation).

### Causality

fixed force out

### Parameters

s	Interval of the play [m]
c1	Stiffness in the play [N/m]
c2	Stiffness outside the play [N/m]
d1	Damping inside the play [Ns/m]
d2	Damping outside the play [Ns/m]
ep	Relative round off (1e-6 -> sharp edges, 1e-2 -> smoother)

### Initial Values

x_initial	Initial position in the play [m], $-s/2 < x_{\text{initial}} < s/2$
-----------	---

## Library

Iconic Diagrams\Mechanical\Translation\Components

## Implementations

Right  
Left

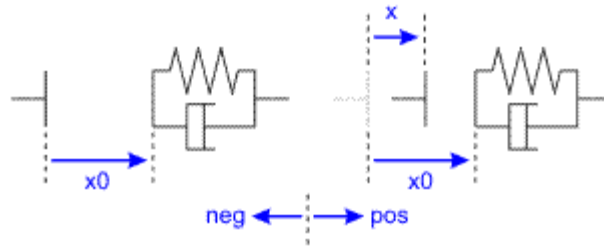


**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Description - Right**

This model represents an collision of an object with another object. It can be used to indicate a possible collision to the right of an object.



The collision force is modeled by a spring and damper:

$$p.F = \text{if } x > x0 \text{ then } k*(x-x0) + d*\text{limit}(p.v,0,1e20) \text{ else } 0 \text{ end;}$$

with a stiffness  $k$  and damping  $d$ . The *limit* function is used to prevent the damper force to become negative. The initial position of the spring is indicated by  $x0$  (see the figure above). Note that the positive direction is to the right. If  $x$  is larger than  $x0$ , the two sides have collided and are in contact. The collision model has separate high and low ports. The equations are

$$\begin{aligned} p.F &= p\_high.F = p\_low.F \\ p.v &= p\_high.v - p\_low.v \end{aligned}$$

**Interface - Right****Ports**

p\_high  
p\_low

**Description**

Two ports of the collision model.

**Causality**

fixed force out

**Variables**

$x$  extension of the spring [m]

**Parameters**

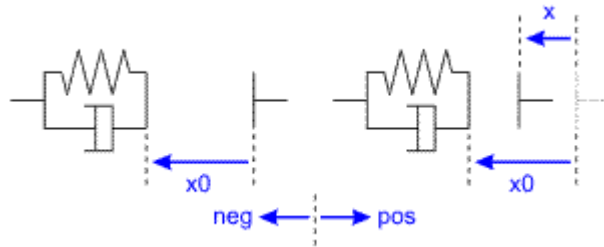
$x0$  unstretched spring position  
 $k$  stiffness [N/m]  
 $d$  damping [N.s/m]

**Initial Values**

$x\_initial$  The initial extension of the spring [m].

### Description - Left

This model represents an collision of an object with another object. It can be used to indicate a possible collision to the left of an object.



The collision force is modeled by a spring and damper. Note that the positive direction is to the right, so the initial position of the spring  $x_0$  has a negative value in the figure above. If  $x$  is smaller than  $x_0$ , the two sides have collided and are in contact.

### Interface - Left

#### Ports

p\_high  
p\_low

#### Description

Two ports of the collision model.

#### Causality

fixed force out

#### Variables

$x$  extension of the spring [m]

#### Parameters

$x_0$  unstretched spring position  
 $k$  stiffness [N/m]  
 $d$  damping [N.s/m]

#### Initial Values

$x_{\text{initial}}$  The initial extension of the spring [m].

### Library

Iconic Diagrams\Mechanical\Translation\Components

### Implementations

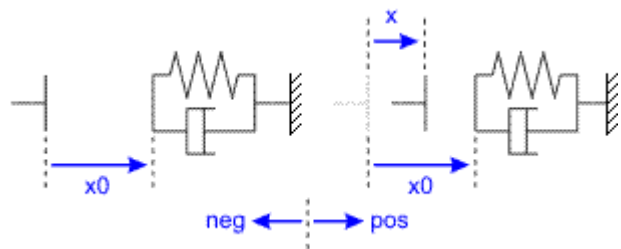
Right  
Left

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Description - Right

This model represents an collision of an object with the ground.



The collision force is modeled by a spring and damper:

$$p.F = \text{if } x > x_0 \text{ then } k*(x-x_0) + d*\text{limit}(p.v,0,1e20) \text{ else } 0 \text{ end;}$$

with a stiffness  $k$  and damping  $d$ . The *limit* function is used to prevent the damper force to become negative. The initial position of the spring is indicated by  $x_0$  (see the figure above). Note that the positive direction is to the right. If  $x$  is larger than  $x_0$ , the two sides have collided and are in contact. The collision model has separate high and low ports. The equations are

$$\begin{aligned} p.F &= p\_high.F = p\_low.F \\ p.v &= p\_high.v - p\_low.v \end{aligned}$$

### Interface - Right

#### Ports

p\_high  
p\_low

#### Description

Two ports of the collision model.

#### Causality

fixed force out

#### Variables

x extension of the spring [m]

#### Parameters

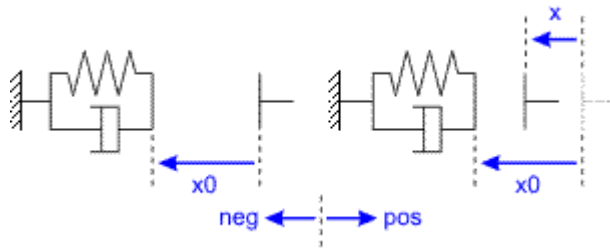
x0 unstretched spring position  
k stiffness [N/m]  
d damping [N.s/m]

#### Initial Values

x\_initial The initial extension of the spring [m].

### Description - Left

This model represents an collision of an object with the ground.



The collision force is modeled by a spring and damper. Note that the positive direction is to the right, so the initial position of the spring  $x_0$  has a negative value in the figure above. If  $x$  is smaller than  $x_0$ , the two sides have collided and are in contact.

### Interface - Left

#### Ports

$p\_high$   
 $p\_low$

#### Description

Two ports of the collision model.

#### Causality

fixed force out

#### Variables

$x$  extension of the spring [m]

#### Parameters

$x_0$  unstretched spring position  
 $k$  stiffness [N/m]  
 $d$  damping [N.s/m]

#### Initial Values

$x\_initial$  The initial extension of the spring [m].

### Library

Iconic Diagrams\Mechanical\Translation\Components

#### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

#### Description

This model represents a linear damper. It can have an force out as well as an velocity out causality. In the last case the constitutive equation, as shown below, is simply inverted. The port  $p$  of the damper model has separate high and low terminals. The equations are:

$$p.F = p\_high.F = p\_low.F$$

$$p.v = p\_high.v - p\_low.v$$

Force out causality:

$$p.F = d * p.v;$$

Velocity velocity out causality:

$$p.v = p.F / d;$$

## Interface

Ports	Description
p_high, p_low	Both terminals of the Translation port p.
<b>Causality</b>	
indifferent	
<b>Parameters</b>	
d	damping [Ns/m]

## Library

Iconic Diagrams\Mechanical\Translation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Description

This model represents the fixed world (velocity = 0). The model has only one initial port p defined. Because any number of connections can be made, successive ports are named p1, p2, p3 etc. which gives the constitutive equations:

$$\begin{aligned} p1.v &= p2.v = \dots = pn.v = 0; \\ p1.F &= free; p2.F = free; \dots; pn.F = free; \end{aligned}$$

## Interface

Ports	Description
p [any]	Any number of connections can be made (Translation).
<b>Causality</b>	
Fixed	angular All ports have a fixed velocity out causality.
velocity out	

## Library

Iconic Diagrams\Mechanical\Translation\Components

## Implementations

C

V

CV

SCVS

LuGre

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Introduction

These models represents friction relative to other objects. The amount of friction depends on the normal force that is applied and the friction function that is used. The normal force is given by the input signal  $F_n$ .



The port  $p$  of the friction models have separate high and low terminals. The equations are:

$$\begin{aligned} p.F &= p\_high.F = p\_low.F \\ p.v &= p\_high.v - p\_low.v \end{aligned}$$

Due to the use of normal force, the friction models all have a fixed torque out causality. The constitutive equations are therefore described as:

$$p.F = F_n * f(p.v);$$

with  $f$  the friction function.

## Description -C

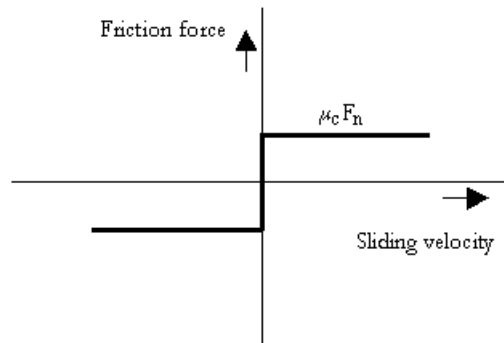
This model represents friction between two terminals described as coulomb friction:

$$p.F = F_n * \mu_c * \tanh(\text{slope} * p.v);$$

$F_n$ : normal force (given by the input signal  $F_n$ )

$\mu_c$ : the coulomb friction coefficient

$\text{slope}$ : the steepness of the coulomb friction curve.



## Interface - C

### Ports

p\_high, p\_low

### Description

Both terminals of port p (Translation).

### Causality

Fixed force out

### Input

$F_n$

Normal force [N]

### Parameters

$\mu_c$

Coulomb friction coefficient []

slope

Steepness of Coulomb friction curve [s/m]

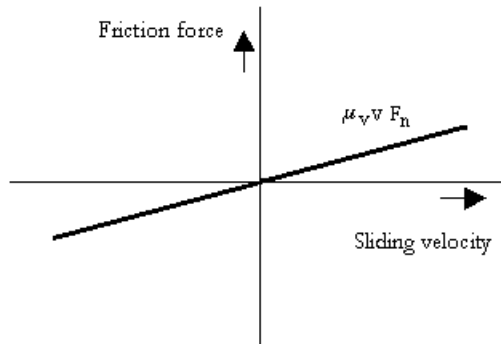
## Description - V

This model represents friction between two terminals described as viscous friction:

$$p.F = F_n * \mu_v * p.v;$$

$F_n$ : normal force (given by the input signal  $F_n$ )

$\mu_v$ : the viscous friction coefficient



### Interface -V

Ports	Description
-------	-------------

p_high, p_low	Both terminals of port p (Translation).
---------------	---

#### Causality

Fixed force out

#### Input

Fn	Normal force [N]
----	------------------

#### Parameters

mu_v	Viscous friction coefficient [s/m]
------	------------------------------------

### Description - CV

This model represents friction between two terminals described as coulomb plus viscous friction:

$$p.F = F_n * (\mu_c * \tanh(\text{slope} * p.v) + \mu_v * p.v);$$

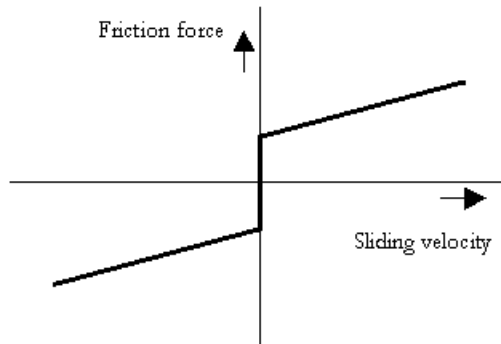
$F_n$ : normal force (given by the input signal  $F_n$ )

$\mu_v$ : the viscous friction coefficient

$\mu_c$ : the coulomb friction coefficient

$\text{slope}$ : the steepness of the coulomb friction curve.





### Interface - CV

#### Ports Description

p\_high, p\_low Both terminals of port p (Translation).

#### Causality

Fixed force out

#### Input

Fn Normal force [N]

#### Parameters

mu\_v Viscous friction coefficient [s/m]

mu\_cv Coulomb friction coefficient []

slope Steepness of Coulomb friction curve [s/m]

### Description - SCVS

This model represents friction between two terminals described as static plus coulomb plus viscous plus Stribeck friction:

$$p.F = F_n * ((mu_c + (mu_{st} * \tanh(slope * p.v)) - mu_c) * \exp(-(p.v / v_{st})^2)) * \text{sign}(p.v) + mu_v * p.v;$$

*F<sub>n</sub>*: normal force (given by the input signal Fn)

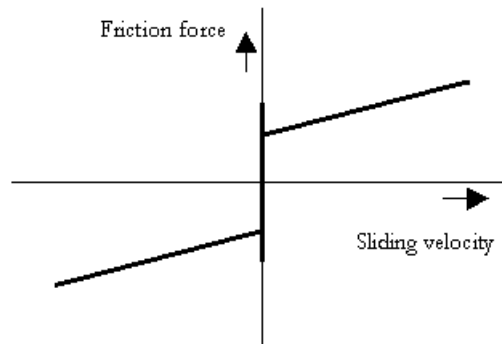
*mu<sub>s</sub>*: the static friction coefficient

*mu<sub>v</sub>*: the viscous friction coefficient

*mu<sub>c</sub>*: the coulomb friction coefficient

*slope*: the steepness of the coulomb and static friction curve.

*v<sub>st</sub>*: the characteristic Stribeck velocity.



### Interface - SCVS

Ports	Description
-------	-------------

p_high, p_low	Both terminals of port p (Translation).
---------------	---

#### Causality

Fixed force out

#### Input

Fn	Normal force [N]
----	------------------

#### Parameters

mu_s	Static friction coefficient []
mu_v	Viscous friction coefficient [s/m]
mu_cv	Coulomb friction coefficient []
slope	Steepness of Coulomb friction curve [s/m]
v_st	Characteristic Stribeck velocity [m/s]

### Description - LuGre

This model represents friction between two terminals described by the LuGre friction model:

$$p.F = FN * f_{lg}(p.v);$$

$FN$ : normal force (given by the input signal  $Fn$ )

$f_{lg}$ : the LuGre friction model

### Interface - LuGre

Ports	Description
-------	-------------

p_high, p_low	Both terminals of port p (Translation).
---------------	---

#### Causality

Fixed force out

**Input**

$F_n$  Normal force [N]

**Parameters**

$\mu_c$  Coulomb friction coefficient []  
 $\mu_s$  Static friction coefficient []  
 $\mu_v$  Viscous friction coefficient [s/m]  
 $v_{st}$  Characteristic Stribeck velocity [m/s]  
 $\mu_k$  Stiffness coefficient at zero speed []

**Library**

Iconic Diagrams\Mechanical\Translation\Components

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Implementations**

C  
V  
CV  
SCVS  
LuGre

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Introduction**

These models represents friction with the fixed world. The amount of friction depends on the normal force that is applied and the friction function that is used. The normal force is given by the input signal  $F_n$ .



The models have only one initial port  $p$  defined. Because any number of connections can be made, successive ports are named  $p_1$ ,  $p_2$ ,  $p_3$  etc. 20-sim will automatically create equations such that the resulting force  $p.F$  is equal to the sum of the forces of all connected ports  $p_1 \dots p_n$ . The velocities of all connected ports are equal to  $p.v$ .

$$p.F = \text{sum}(p_1.F, p_2.F, \dots)$$

$$p.v = p_1.v = p_2.v = \dots$$

Due to the use of normal force, the friction models all have a fixed force out causality. The constitutive equations are therefore described as:

$$p.F = F_n * f(p.v);$$

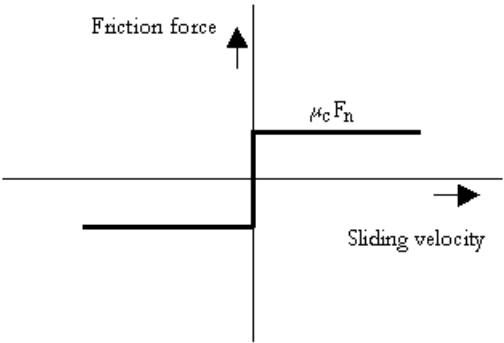
with  $f$  the friction function.

**Description - C**

This model represents friction with the fixed world described as coulomb friction:

$$p.F = F_n \cdot \mu_c \cdot \tanh(\text{slope} \cdot p.v);$$

*F<sub>n</sub>*: normal force (given by the input signal F<sub>n</sub>)  
*μ<sub>c</sub>*: the coulomb friction coefficient  
*slope*: the steepness of the coulomb friction curve.



**Interface - C**

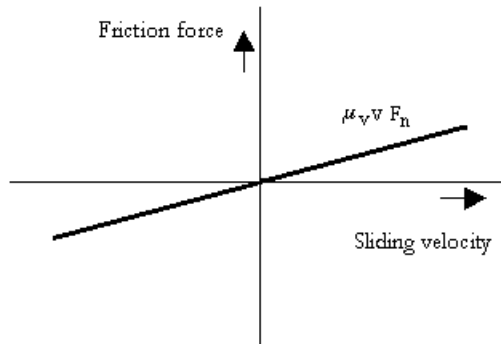
Ports	Description
p[any]	Any number of connections can be made (Translation).
<b>Causality</b>	
Fixed force out	
<b>Input</b>	
F <sub>n</sub>	Normal force [N]
<b>Parameters</b>	
μ <sub>c</sub>	Coulomb friction coefficient []
slope	Steepness of Coulomb friction curve [s/m]

**Description - V**

This model represents friction with the fixed world described as viscous friction:

$$p.F = F_n \cdot \mu_v \cdot p.v;$$

*F<sub>n</sub>*: normal force (given by the input signal F<sub>n</sub>)  
*μ<sub>v</sub>*: the viscous friction coefficient



### Interface - V

Ports	Description
p[any]	Any number of connections can be made (Translation).
<b>Causality</b>	
Fixed force out	
<b>Input</b>	
Fn	Normal force [N]
<b>Parameters</b>	
mu_v	Viscous friction coefficient [s/m]

### Description - CV

This model represents friction with the fixed world described as coulomb plus viscous friction:

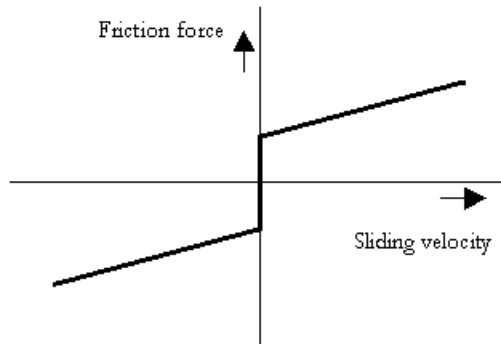
$$p.F = F_n * (\mu_c * \tanh(\text{slope} * p.v) + \mu_v * p.v);$$

$F_n$ : normal force (given by the input signal  $F_n$ )

$\mu_v$ : the viscous friction coefficient

$\mu_c$ : the coulomb friction coefficient

$\text{slope}$ : the steepness of the coulomb friction curve.



### Interface - CV

Ports	Description
p[any]	Any number of connections can be made (Translation)

#### Causality

Fixed force out

#### Input

Fn	Normal force [N]
----	------------------

#### Parameters

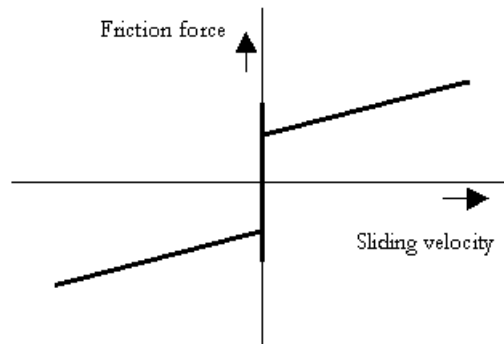
mu_v	Viscous friction coefficient [s/m]
mu_cv	Coulomb friction coefficient []
slope	Steepness of Coulomb friction curve [s/m]

### Description - SCVS

This model represents friction with the fixed world described as static plus coulomb plus viscous plus Stribeck friction:

$$p.F = F_n * ((\mu_c + (\mu_{st} * \text{abs}(\tanh(\text{slope} * p.v)) - \mu_c) * \exp(-(p.v / v_{st})^2)) * \text{sign}(p.v) + \mu_v * p.v);$$

*F<sub>n</sub>*: normal force (given by the input signal Fn)  
*μ<sub>s</sub>*: the static friction coefficient  
*μ<sub>v</sub>*: the viscous friction coefficient  
*μ<sub>c</sub>*: the coulomb friction coefficient  
*slope*: the steepness of the coulomb and static friction curve.  
*v<sub>st</sub>*: the characteristic Stribeck velocity.



### Interface - SCVS

Ports	Description
p[any]	Any number of connections can be made (Translation).
<b>Causality</b>	
Fixed force out	
<b>Input</b>	
Fn	Normal force [N]
<b>Parameters</b>	
mu_s	Static friction coefficient []
mu_v	Viscous friction coefficient [s/m]
mu_cv	Coulomb friction coefficient []
slope	Steepness of Coulomb friction curve [s/m]
v_st	Characteristic Stribeck velocity [m/s]

### Description - LuGre

This model represents friction with the fixed world described by the LuGre friction model:

$$p.F = FN * f_{lg}(p.v);$$

$FN$ : normal force (given by the input signal  $Fn$ )

$f_{lg}$ : the LuGre friction model

### Interface - LuGre

Ports	Description
p[any]	Any number of connections can be made (Translation).
<b>Causality</b>	
Fixed force out	
<b>Input</b>	
Fn	Normal force [N]

**Parameters**

mu_c	Coulomb friction coefficient []
mu_s	Static friction coefficient []
mu_v	Viscous friction coefficient [s/m]
v_st	Characteristic Stribeck velocity [m/s]
mu_k	Stiffness coefficient at zero speed []

**Library**

Iconic Diagrams\Mechanical\Translation\Components

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Description**

This model represents an ideal mass (no gravity). The element has a preferred velocity out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred force out causality. The constitutive equations then contain a derivation. Because any number of connections can be made, successive ports are named p1, p2, p3 etc. 20-sim will automatically create equations such that the resulting force p.F is equal to the sum of the forces of all connected ports p1 .. pn. The velocities of all connected ports are equal to p.v.

$$p.F = \text{sum}(p1.F, p2.F, \dots)$$

$$p.v = p1.v = p2.v = \dots$$

velocity out causality (preferred):

$$a = p.F/m;$$

$$p.v = \text{int}(a);$$

$$x = \text{int}(p.\text{omega});$$

force out causality:

$$a = \text{ddt}(p.v);$$

$$p.T = m*a;$$

$$x = \text{int}(p.v);$$

**Interface****Ports**

p[any]

**Description**

Any number of connections can be made (Translation).

**Causality**

preferred velocity out

An torque out causality results in a derivative constitutive equation.

**Variables**

x

position [m]



a	acceleration [m/s <sup>2</sup> ]
p	impulse [Ns]

**Parameters**

m	mass [kg]
---	-----------

**Initial Values**

p.v_initial	The initial velocity of the mass.
x_initial	The initial position of the mass.

**Library**

Iconic Diagrams\Mechanical\Translation\Components

**Implementations**

Stiffness  
Frequency

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Description - Stiffness**

This model represents a spring-damper-mass system that can be used for modal analysis. The springdamper is equivalent to the *SpringDamper-Stiffness.emx* model. The mass is equivalent to the *Mass.emx* model. The model has one output that can be connected to the *modal-summer.emx* model.

**Interface - Stiffness**

Ports	Description
p	Translation port.

**Causality**

preferred velocity out

**Parameters**

k	Stiffness [N/m]
b	Relative damping []
m	Equivalent mass [kg]

**Description - Frequency**

This model represents a spring-damper-mass system that can be used for modal analysis. The springdamper is equivalent to the *SpringDamper-Frequency* model. The mass is equivalent to the *Mass* model. The model has one output that can be connected to the *Modal-Summer* model.

## Interface - Frequency

### Ports

p

### Description

Translation port.

### Causality

preferred velocity out

### Parameters

b

Relative damping []

f

Resonance frequency [Hz]

m

Equivalent mass [kg]

## Library

Iconic Diagrams\Mechanical\Translation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Description

This model combines the results from all *modal.emx* models to one resulting output. The model has 8 input ports and one output port that shows the combined result. If more or less input ports are needed, you have to adapt the model (Choose *Go Down* and alter the internal description).

## Interface

### Ports

p1 .. p8

### Description

Input ports for *modal.emx* models (Translation).

p\_out

Port with the modal result (Translation)

### Causality

preferred force out p1..p8

preferred velocity out p\_out

### Parameters

A1 .. A8

Gains for each input port.

## Library

Iconic Diagrams\Mechanical\Translation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Description

This node model represents a structural connection between two or more parts, where the velocity of all connected parts is equal. The model has only one initial port  $p$  defined. Because any number of connections can be made, successive ports are named  $p_1$ ,  $p_2$ ,  $p_3$  etc.

### Interface

Ports	Description
$p$ [any]	Any number of connections can be made (Translation).

## Library

Iconic Diagrams\Mechanical\Translation\Components

### Implementations

Right

Left

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Introduction

This model represents a shock absorber with an open end. This type of shock absorbers is used to protect equipment from large impacts when reaching the end of a line.



The damper has an internal piston which can travel a certain length (i.e. the stroke  $l$ ) until it collides with the end cap. The shock absorber is modeled by a damper for the active damping part and a spring damper to model the impact with the end cap. The position of the damper is indicated by the parameter  $x0$ . Two implementations are available: one with the impact at the right and one with the impact at the left.

The damper is modeled by viscous damping, where the damping force is proportional with the velocity:

$$p.F = d * v;$$

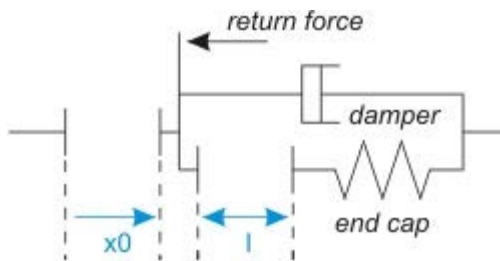
After a stroke of length  $l$ , the end caps are reached which are modeled by a spring damper:

$$p.F = k * x;$$

To get the damper back in its original position a return force is added.

### Description - Right

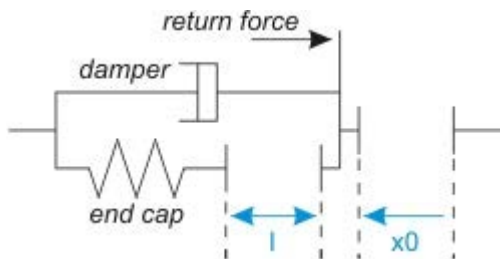
The *ShockAbsorber-Right* models a shock absorber with impact at the right of the system.



*Shock absorber model with impact at the right.*

### Description - Right

The *ShockAbsorber-Left* models a shock absorber with impact at the left of the system.



*Shock absorber model with impact at the left.*

## Interface

### Ports

p\_high  
p\_low

### Causality

fixed force out

### Description

Two ports of the shock absorber model.

### Parameters

k	stiffness at the end cap [N/m]
d	damping [N.s/m]
l	shock absorber stroke [m]
x0	position of the damper [m]
Fr	return force [N]

### Library

Iconic Diagrams\Mechanical\Translation\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Description

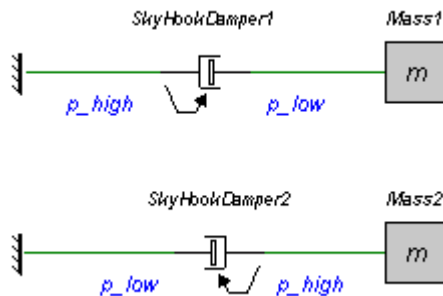
This model represents a skyhook damper. It can have an force out as well as an velocity out causality. In the last case the constitutive equation, as shown below, is simply inverted. The model has a fixed force out causality. The equations are:

**Force out causality:**

$$p\_high.F = d * p\_high.v;$$

$$p\_low.F = p\_high.F$$

As the equations point out, the force of the skyhook damper only depends on the velocity at the port *p\_high*. The position of *p\_high* is indicated by an arrow, as shown in the figure below.



In this figure two models are shown. In the top model, the damping force of the skyhook damper is zero because the velocity at *p\_high* is zero. Consequently the mass is free to move.

In the lower model, the damping force is proportional to the velocity of the mass. Here the skyhook damper acts as a normal damper.

## Interface

Ports	Description
p_high, p_low	Both Translation ports of the skyhook damper.
<b>Causality</b>	
fixed force out	
<b>Parameters</b>	
d	damping [Ns/m]

## Library

Iconic Diagrams\Mechanical\Translation\Components

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description

This model represents an ideal translational spring. The element has a preferred force out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred velocity out causality. The constitutive equations then contain a derivation. The spring model has separate high and low ports. The equations are

$$p.F = p\_high.F = p\_low.F$$

$$p.v = p\_high.v - p\_low.v$$

Force out causality (preferred):

$$x = \text{int}(p.v);$$

$$p.F = k * x;$$

Velocity out causality:

$$p.v = \text{ddt}(x);$$

$$x = p.F/k;$$

## Interface

Ports	Description
p_high	Two ports of the spring (Translation).
p_low	
Causality	
preferred force out	An velocity out causality results in a derivative constitutive equation.
Variables	
x	extension of the spring [m]

**Parameters**

k Stiffness [N/m]

**Initial Values**

x\_initial The initial extension of the spring [m].

**Library**

Iconic Diagrams\Mechanical\Translation\Components

**Implementations**

Default  
Stiffness  
Frequency

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Description - Default**

This model represents an ideal translational spring with damper. The element has a preferred force out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred velocity out causality. The constitutive equations then contain a derivation. The spring-damper model has separate high and low ports. The equations are

$$\begin{aligned} p.F &= p\_high.F = p\_low.F \\ p.v &= p\_high.v - p\_low.v \end{aligned}$$

Force out causality (preferred):

$$\begin{aligned} x &= \text{int}(p.v); \\ p.F &= k*x + d*p.v; \end{aligned}$$

Velocity out causality:

$$\begin{aligned} p.v &= \text{ddt}(x); \\ x &= (p.F - d*p.v)/k; \end{aligned}$$

**Interface - Default****Ports**

p\_high  
p\_low

**Description**

Two ports of the spring (Translation).

**Causality**

preferred force out

**Variables**

x extension of the spring [m]

**Parameters**

k Stiffness [N/m]  
d damping [N.s/m]

**Initial Values**

x\_initial The initial extension of the spring [m].

**Description - Stiffness**

This model represents another implementation of the ideal translational spring with damper. The damping value ( $d$ ) is calculated on the basis of a known stiffness ( $k$ ), relative damping ( $b$ ) and mass reference ( $m$ ). The mass is only used to compute the damping (no actual mass is used in this component).

The element has a preferred force out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred velocity out causality. The constitutive equations then contain a derivation. The spring-damper model has separate high and low ports. The equations are

$$\begin{aligned} p.F &= p\_high.F = p\_low.F \\ p.v &= p\_high.v - p\_low.v \end{aligned}$$

Force out causality (preferred):

$$\begin{aligned} x &= \text{int}(p.v); \\ p.F &= k * x + d * p.v; \\ d &= 2 * b * \text{sqrt}(k * m); \end{aligned}$$

Velocity out causality:

$$\begin{aligned} p.v &= \text{ddt}(x); \\ x &= (p.F - d * p.v) / k; \\ d &= 2 * b * \text{sqrt}(k * m); \end{aligned}$$

**Interface - Stiffness****Ports**

p\_high  
p\_low

**Description**

Two ports of the spring (Translation).

**Causality**

preferred force out

**Variables**

x extension of the spring [m]  
d damping [N.s/m]

**Parameters**



$k$	Stiffness [N/m]
$b$	Relative damping []
$m$	Reference mass [kg]

**Initial Values**

$x_{\text{initial}}$	The initial extension of the spring [m].
----------------------	--

**Description - Frequency**

This model represents another implementation of the ideal translational spring with damper. The stiffness ( $k$ ) is calculated on basis of a known resonance frequency. The damping value ( $d$ ) is calculated on the basis of the calculated stiffness ( $k$ ), relative damping ( $b$ ) and mass reference ( $m$ ). The mass is only used to compute the damping (no actual mass is used in this component).

The element has a preferred force out causality. The corresponding constitutive equations then contain an integration. The element can also have the non-preferred velocity out causality. The constitutive equations then contain a derivation. The spring-damper model has separate high and low ports. The equations are

$$\begin{aligned} p.F &= p_{\text{high}}.F = p_{\text{low}}.F \\ p.v &= p_{\text{high}}.v - p_{\text{low}}.v \end{aligned}$$

Force out causality (preferred):

$$\begin{aligned} x &= \text{int}(p.v); \\ p.F &= k * x + d * p.v; \\ k &= m * (2 * \pi * f)^2; \\ d &= 2 * b * \text{sqrt}(k * m); \end{aligned}$$

Velocity out causality:

$$\begin{aligned} p.v &= \text{ddt}(x); \\ x &= (p.F - d * p.v) / k; \\ k &= m * (2 * \pi * f)^2; \\ d &= 2 * b * \text{sqrt}(k * m); \end{aligned}$$

**Interface - Frequency****Ports**

$p_{\text{high}}$   
 $p_{\text{low}}$

**Description**

Two ports of the spring (Translation).

**Causality**

preferred force out

**Variables**

$x$	extension of the spring [m]
$k$	stiffness [N/m]
$d$	damping [N.s/m]

**Parameters**

b	Relative damping []
f	Resonance frequency [Hz]
m	Reference mass [kg]

**Initial Values**

x_initial	The initial extension of the spring [m].
-----------	--

**Library**

Iconic Diagrams\Mechanical\Translation\Components

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Description**

This model can be used to connect any open end of another model that is not connected to the fixed world. It generates a fixed force of 0 N while the velocity is free:

$$\begin{aligned} p.v &= \text{indifferent}; \\ p.F &= 0; \end{aligned}$$

**Interface**

Ports	Description
p	Translation port

**Causality**

Fixed force out

**Library**

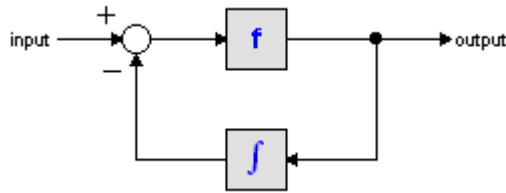
Iconic Diagrams\Mechanical\Translation\Sensors

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

**Description**

This model describes an acceleration sensor which derives an acceleration output out of a port velocity by differentiation. Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where  $f$  is the cut-off frequency. For very high values of  $f$ , the output becomes the pure derivative of the input. High values of  $f$ , however, increase simulations times. A good trade-off is a starting value of 1e5.

The equations of this model are:

$$a = d(p.v)/dt;$$

$$p.F = indifferent;$$

## Interface

### Ports

p

### Description

Translation port p.

### Causality

fixed force out

### Output

alpha

Acceleration [m/s<sup>2</sup>]

### Parameters

f

Cut-off frequency of the differentiation [Hz].

a\_initial

Initial acceleration [m/s].

## Library

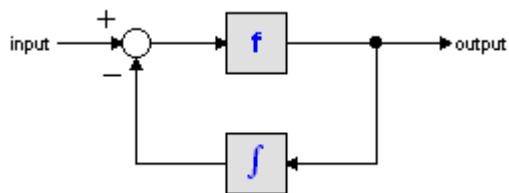
Iconic Diagrams\Mechanical\Translation\Sensors

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

## Description

This model describes an acceleration sensor which derives an acceleration output out of a velocity difference (between high and low terminals) by differentiation. Differentiation is performed by a state variable filter:



The S-domain function of this filter is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

where  $f$  is the cut-off frequency. For very high values of  $f$ , the output becomes the pure derivative of the input. High values of  $f$ , however, increase simulations times. A good trade-off is a starting value of 1e5.

The equations of this model are:

$$a = d(p\_high.v - p\_low.v)/dt;$$
$$p\_low.F = p\_high.F = indifferent;$$

**Interface**

Ports	Description
p_high, p_low	Both terminals of the Translational port p.
<b>Causality</b>	
fixed force out	
<b>Output</b>	
a	Acceleration (measured as the difference between both terminals) [m/s <sup>2</sup> ]
<b>Parameters</b>	
f	Cut-off frequency of the differentiation [Hz].
a_initial	Initial acceleration [m/s].

## Library

Iconic Diagrams\Mechanical\Translation\Sensors

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model translates an applied force to an output signal. It has a velocity out causality. The port  $p$  of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.F &= p\_high.F = p\_low.F; \\ p.v &= p\_high.v - p\_low.v; \\ F &= p.F; \\ p.v &= 0; \end{aligned}$$

### Interface

Ports	Description
p_high, p_low	Both terminals of the Translation port p.
<b>Causality</b>	
fixed velocity out	
<b>Output</b>	
F	Applied force [N].

## Library

Iconic Diagrams\Mechanical\Translation\Sensors

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model translates a position to an output signal. It has a force out causality. The equations are:

$$\begin{aligned} p.F &= 0; \\ x &= \text{int}(p.v); \end{aligned}$$

### Interface

Ports	Description
p_high, p_low	Translation port p.
<b>Causality</b>	
fixed force out	

**Output**

x Absolute position [m].

**Initial Values**

x\_initial Initial position [m]

**Library**

Iconic Diagrams\Mechanical\Translation\Sensors

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

**Description**

This model translates a position difference to an output signal. It has a force out causality. The port  $p$  of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.F &= p\_high.F = p\_low.F; \\ p.v &= p\_high.v - p\_low.v; \\ p.F &= 0; \\ x &= \text{int}(p.v); \end{aligned}$$

**Interface****Ports**                      **Description**

p\_high, p\_low Both terminals of the Translation port p.

**Causality**

fixed force out

**Output**

x Relative position [m].

**Initial Values**

x\_initial Initial position [m].

**Library**

Iconic Diagrams\Mechanical\Translation\Sensors

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

**Description**

This is an ideal sensor (no dissipation or other effects) that yields the power that flows through the model as output signal. The equations are:

$$\begin{aligned}
 p_{high}.F &= p_{low}.F \\
 p_{high}.v &= p_{low}.v \\
 P &= p_{high}.F * p_{high}.v;
 \end{aligned}$$

## Interface

Ports	Description
p_high, p_low	Both translation ports.
<b>Causality</b>	
p_high	not equal
p_low	
<b>Output</b>	
P	Power [w].

## Library

Iconic Diagrams\Mechanical\Translation\Sensors

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

## Description

This model translates a velocity to an output signal. It has a force out causality. The equations are:

$$\begin{aligned}
 p.F &= 0; \\
 v &= p.v;
 \end{aligned}$$

## Interface

Ports	Description
p	Translation port p.
<b>Causality</b>	
fixed force out	
<b>Output</b>	
v	Absolute velocity [m/s].

## Library

Iconic Diagrams\Mechanical\Translation\Sensors

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation), Block Diagrams.

### Description

This model translates a velocity difference to an output signal. It has a force out causality. The port  $p$  of the model has separate high and low terminals. The equations are:

$$\begin{aligned} p.F &= p\_high.F = p\_low.F; \\ p.v &= p\_high.v - p\_low.v; \\ p.F &= 0; \\ v &= p.v; \end{aligned}$$

### Interface

Ports	Description
$p\_high$ , $p\_low$	Both terminals of the Translation port $p$ .
<b>Causality</b>	
fixed force out	
<b>Output</b>	
$v$	Relative velocity [m/s].

## Library

Iconic Diagrams\Mechanical\Rotation\Gears

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation/Translation).

### Description

This models represents a belt and pulley. The connection to the pulley is through the rotation port  $p\_rot$ . The connection to the belt is through the translation port  $p\_trans$ . The model is ideal, i.e. there are no compliances or inertias. The causality of this model is always mixed: torque out & velocity out or angular velocity out & force out:

$$\begin{aligned} p\_rot.T &= radius * p\_trans.F \\ p\_trans.v &= radius * p\_rot.omega \end{aligned}$$

or:



$$p\_trans.F = 1/radius * p\_rot.T$$

$$p\_rot.omega = 1/radius * p\_trans.v$$

## Interface

Ports	Description
p_rot	Rotation port.
p_trans	Translation port.

### Causality

p_rot	notequal
p_trans	

### Parameters

radius	pulley radius [m]
--------	-------------------

## Library

Iconic Diagrams\Mechanical\Rotation\Gears  
 Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation/Translation).

## Description

This is a masked model which opens the Cam Wizard when edited. Depending on the selections entered, various cam motion profiles can be generated.

## Interface

Ports	Description
p_in	Driving axis (Rotation)
p_out	Output port with resulting motion (Rotation or Translation)

### Parameters

stroke	amplitude of resulting motion
start_angle	start angle motion
stop_angle	angle when the maximum is reached
return_angle	start angle of the return motion
end_angle	finish angle of the return motion

## Library

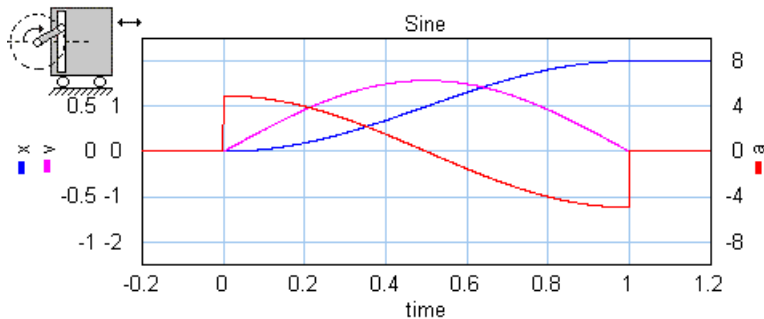
Iconic Diagrams\Mechanical\Rotation\Gears  
 Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description

This models represents a cam and rod mechanism. If the input shaft is rotating with a constant speed, the output motion is a pure sinusoidal.



The mechanism is ideal, i.e., it does not have inertia, friction or geometrical limitations. It has one rotation port ( $p_{in}$ ) and one translation port ( $p_{out}$ ). The causality of this model is always mixed: one port has a force out causality while the other has a velocity out causality:

$$p_{in}.T = i * p_{out}.F$$

$$p_{out}.v = i * p_{in}.omega$$

The transmission ratio ( $i$ ) is the ratio of the velocities of both ports (in fact a sinusoidal function of the shaft angle).

## Interface

Ports	Description
$p_{in}$	Driving axis (Rotation)
$p_{out}$	Output port with resulting motion (Translation)

### Causality

fixed	torque	out
$p_{in}$		
fixed	velocity	out
$p_{out}$		

### Parameters

stroke	Stroke of the translation port (is equal to half the length of the rod).
--------	--

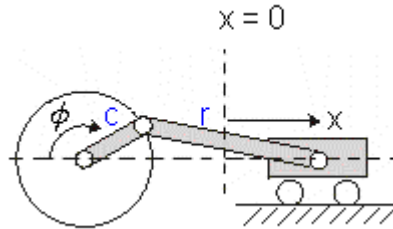
## Library

Iconic Diagrams\Mechanical\Rotation\Gears  
Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description



This model represents a crank and rod mechanism. The mechanism is ideal, i.e., it does not have inertia, friction or geometrical limitations. It has one rotation port (*p\_in*) and one translation port (*p\_out*). The causality of this model is always mixed: one port has a force out causality while the other has a velocity out causality:

$$p_{in}.T = i * p_{out}.F$$

$$p_{out}.v = i * p_{in}.omega$$

The transmission ratio (*i*) is the ratio of the velocities of both ports. It is a function of the shaft angle, the crank length and the rod length.

## Interface

Ports	Description
p_in	Driving axis (Rotation)
p_out	Output port with resulting motion (Translation)

### Causality

fixed torque out  
 p\_in  
 fixed velocity out  
 p\_out

### Parameters

crank_length	Crank length [m]
rod_length	Rod length [m]

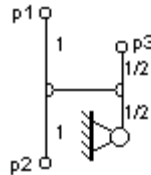
## Library

Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description

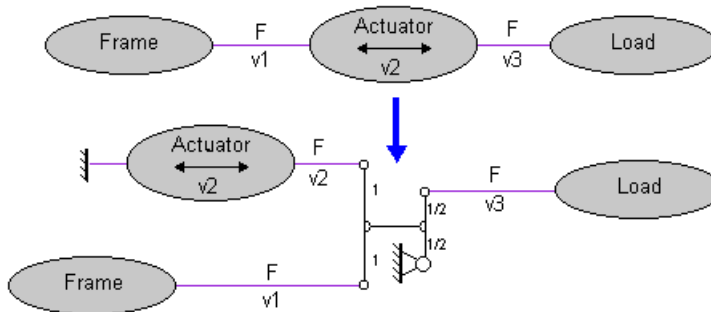


This model is equivalent to the differential model of the Rotation library. It represents a special type of node where the forces are equal and the velocities are added:

$$p3.v = p1.v + p2.v;$$

$$p1.F = p2.F = p3.F;$$

This model can for example be used for actuators that generate a force difference. With the fork model an equivalent model can be found with the actuator attached to the fixed world:



## Interface

### Ports

p1,p2,p3

### Description

Translation ports.

## Library

Iconic Diagrams\Mechanical\Translation\Transmission

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

### Description



This model represents any type of lever with two counter-moving ports. The lever is ideal, i.e., it does not have inertia, friction or geometrical limitations. The lever has one fast moving port and one slow moving port. The lever ratio is the (absolute) ratio of the velocities of both ports. The causality of this model is always mixed: one port has a force out causality while the other has a velocity out causality:

$$\begin{aligned} p_{fast}.F &= -i * p_{slow}.F \\ p_{slow}.v &= -i * p_{fast}.v \end{aligned}$$

or:

$$\begin{aligned} p_{slow}.F &= -1/i * p_{fast}.F \\ p_{fast}.v &= -1/i * p_{slow}.v \end{aligned}$$

### Interface

Ports	Description
p_fast	Fast moving translation port.
p_slow	Slow moving translation port.

### Causality

p_slow	notequal
p_fast	

### Parameters

i	lever ratio $p_{slow}.v / p_{fast}.v$ [], $0 < i < 1$
---	---

### Note

Keep the lever ratio  $i$  between 0 and 1. Confusion might otherwise exist:

- $i > 1$ : the fast moving port is slower than the slow moving port (you better interchange the connections of the lever model).
- $i < 0$ : the ports are not counter-moving (use the transmission model instead).

## Library

Iconic Diagrams\Mechanical\Rotation\Gears

Iconic Diagrams\Mechanical\Translation\Transmission

## Implementations

FixedPinion

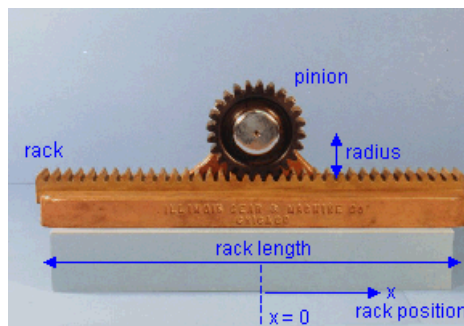
FixedRack

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation/Translation).

## Description - FixedPionion

This models represents a rack and pinion gear. The connection to the pinion gear is through the rotation port  $p\_rot$ . The connection to the rack is through the translation port  $p\_trans$ . The model is ideal, i.e. there is no compliance nor inertia nor backlash.



In this model the pinion bearing is connected to the fixed world and the rack is free to move. This is contrary to the model FixedRackPinionGear where the pinion bearing is free to move and the rack is connected to the fixed world.

The causality of this model is always mixed: torque out & velocity out or angular velocity out & force out:

$$\begin{aligned} p\_rot.T &= radius * p\_trans.F \\ p\_trans.v &= radius * p\_rot.\omega \end{aligned}$$

or:

$$\begin{aligned} p\_trans.F &= 1/radius * p\_rot.T \\ p\_rot.\omega &= 1/radius * p\_trans.v \end{aligned}$$

The rack position is determined by the internal variable  $x$ . For  $x = 0$ , the pinion gear is at the middle of the rack. When the pinion crosses the end of the rack, i.e.

$$abs(x) > rack\_length/2$$

a warning is given, "WARNING: rack length has been exceeded at the rack and pinion gear!", and the simulation is stopped.

## Interface - FixedPionion

Ports	Description
-------	-------------

p\_rot                      Rotation port.  
 p\_trans                   Translation port.

### Causality

p\_rot                      notequal  
 p\_trans

### Parameters

radius                      pinion gear pitch radius [m]  
 rack\_length               rack length [m]

### Variables

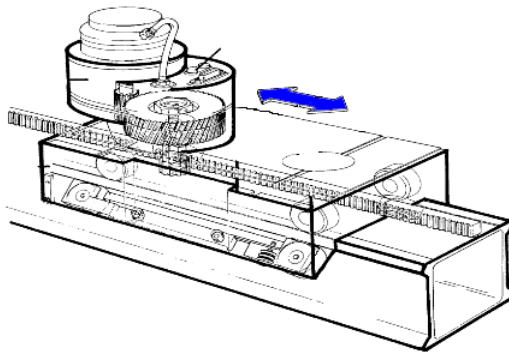
x                           Internal variable which denotes the rack position,  $\text{abs}(x) < \text{rack\_length}/2$   
 else simulation halted.

### Initial values

x\_initial                   Initial rack position,  $\text{abs}(x\_initial) < \text{rack\_length}/2$

### Description - FixedRack

This models represents a fixed rack and pinion gear. The connection to the pinion gear is through the rotation port *p\_rot*. The connection to the rack is through the translation port *p\_trans*. The model is ideal, i.e. there is no compliance nor inertia nor backlash.



In this model the pinion bearing is free to move and the rack is connected to the fixed world. This is contrary to the model RackPinionGear where the pinion bearing is connected to the fixed world and the rack is free to move.

The causality of this model is always mixed: torque out & velocity out or angular velocity out & force out:

$$\begin{aligned} p\_rot.T &= radius * p\_trans.F \\ p\_trans.v &= radius * p\_rot.\omega \end{aligned}$$

or:

$$p\_trans.F = 1/radius * p\_rot.T$$

$$p\_rot.omega = 1/radius * p\_trans.v$$

The rack position is determined by the internal variable x. For x = 0 the pinion gear is at the middle of the rack. When the pinion crosses the end of the rack, i.e.

$$abs(x) > rack\_length/2$$

a warning is given, *"WARNING: rack length has been exceeded at the rack and pinion gear!"*, and the simulation is stopped.

## Interface - FixedRack

Ports	Description
p_rot	Rotation port.
p_trans	Translation port.

### Causality

p_rot	notequal
p_trans	

### Parameters

radius	pinion gear pitch radius [m]
rack_length	rack length [m]

### Variables

x	Internal variable which denotes the rack position, $abs(x) < rack\_length/2$ else simulation halted.
---	--

### Initial values

x_initial	Initial rack position, $abs(x\_initial) < rack\_length/2$
-----------	---

## Library

Iconic Diagrams\Mechanical\Rotation\Gears  
Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation).

## Introduction

This models represents a spindle and nut. It transfers an angular motion of the spindle into a translational motion of the nut. The model is ideal, i.e., it does not have inertia or friction. The causality of this model is always mixed: one port has a torque out causality while the other has an angular velocity out causality:

$$p\_spindle.T = i * p\_nut.F$$

$$p\_nut.v = i * p\_spindle.omega$$

or:



$$p\_nut.F = 1/i * p\_spindle.T$$

$$p\_spindle.omega = 1/i * p\_nut.v$$

The model has two implementations which calculate the transform ratio  $i$  out of different parameters.

### Description - Pitch

In this implementation the transform ratio is calculated using the *pitch* (the advance of the nut during one revolution of the spindle):

$$i = pitch / (2 * pi);$$

### Interface - Pitch

#### Ports

Ports	Description
p_spindle	Port at the spindle shaft (Rotation).
p_nut	Port at the wheel (Translation).

#### Causality

p_spindle	notequal
p_nut	

#### Parameters

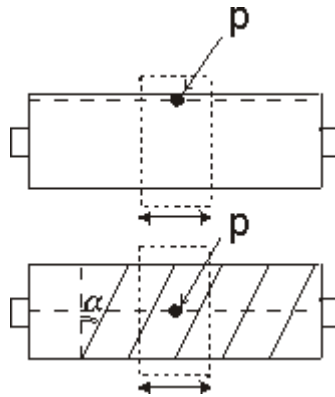
pitch	translation of the nut during one revolution of the spindle [m]
-------	---

### Description - LeadAngle

This implementation calculates the transform ratio out of the lead angle *alpha* and the radius *r\_spindle* of the spindle:

$$i = \tan(alpha) * r\_spindle;$$

The pitch angle is shown in the figure below. *r\_spindle* is the effective radius of the spindle, i.e. the radius from the center of the spindle to the pitch point *p*.



### Interface -LeadAngle

#### Ports

p_spindle	Port at the spindle shaft (Rotation).
p_nut	Port at the wheel (Translation).

#### Causality

p_spindle	notequal
p_nut	

#### Parameters

r_spindle	effective radius of the spindle [m]
alpha	lead angle of the spindle [rad]

### Library

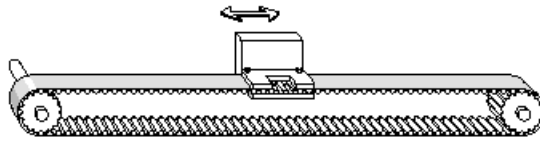
Iconic Diagrams\Mechanical\Rotation\Gears  
 Iconic Diagrams\Mechanical\Translation\Transmission

### Use

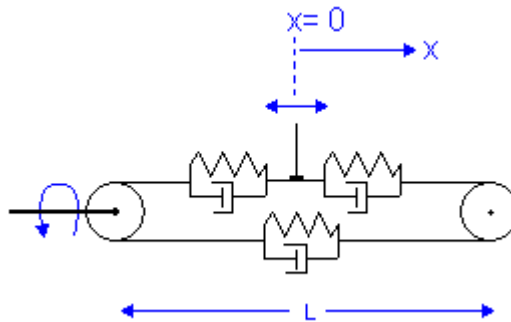
**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Rotation/Translation).

### Introduction

This models represents a timing belt, used for linear positioning.



It has a rotating pulley which drives the the belt and clamp. The timing belt is modeled by a series of spring damper elements that convey the rotation of the pulley to a clamp translation. Because the output position is moving, stiffness and damping values are not constant.



The stiffness for a piece of belt can be expressed as:

$$k = E \cdot A / l$$

with

$E$  = Modulus of elasticity {N/m<sup>2</sup>}

$A$  = Belt area {m<sup>2</sup>}

$l$  = belt length {m}

If the belt is sufficiently pre-tensioned, the stiffness experienced at the clamp can be expressed as the combination of three individual belt parts:

$$k = E \cdot A / (0.5 \cdot l + x) + 1 / ( 1 / E \cdot A / (0.5 \cdot l - x) + 1 / E \cdot A / l )$$

which can be rewritten to:

$$k = E \cdot A \cdot ( 1 / (0.5 \cdot l + x) + 1 / (1.5 \cdot l - x) )$$

The stiffness approaches infinity as the clamp moves to the driven pulley ( $x = -l/2$ ) and has a minimum value when the clamp moves to the other pulley ( $x = 0.5 \cdot l$ ). The minimum stiffness is equal to:

$$k = 2 \cdot E \cdot A / l$$

The belt position is determined by the internal variable  $x$ . For  $x = 0$  the clamp is in the middle. When the position crosses the driven pulley, i.e.

$$x < - \text{belt\_length} / 2$$

the simulation is stopped: *"Error: clamp position larger than belt end!"*. When the position crosses the other pulley, i.e.

$$x > \text{belt\_length}/2$$

the simulation is also stopped, *"Error: clamp position smaller than belt start!"*.

### Description - Default

In this model the minimum stiffness is used, based on an output position at a length L of the driven pulley.

$$k = 2 * E * A / l$$

### Description - VariableStiffness

In this model a variable stiffness is used equal to:

$$k = E * A * ( 1 / (0.5 * l + x) + 1 / (1.5 * l - x) )$$

Take care not to let the clamp get too close to the driven pulley, because the stiffness will then grow to infinity!

### Interface

Ports	Description
p_rot	Rotation port.
p_trans	Translation port.

### Causality

p_rot	notequal
p_trans	

### Parameters

radius	pinion gear pitch radius [m]
d	damping N.s/m]
E	Modulus of elasticity [N/m2]
A	A = Belt area [m2]
l	belt length [m]

### Variables

x	clamp position, $\text{abs}(x) < \text{belt length}/2$
---	--

### Initial values

x_initial	Initial clamp position, $\text{abs}(x\_initial) < \text{belt length}/2$
-----------	---

## Library

Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description



This model represents any type of lever with ports moving in the same direction. The lever is ideal, i.e., it does not have inertia, friction or geometrical limitations. The lever has one fast moving port and one slow moving port. The transmission ratio is the ratio of the velocities of both ports. The causality of this model is always mixed: one port has a force out causality while the other has a velocity out causality:

$$\begin{aligned} p\_fast.F &= i * p\_slow.F \\ p\_slow.v &= i * p\_fast.v \end{aligned}$$

or:

$$\begin{aligned} p\_slow.F &= 1/i * p\_fast.F \\ p\_fast.v &= 1/i * p\_slow.v \end{aligned}$$

## Interface

Ports	Description
p_fast	Fast moving rotation port.
p_slow	Slow moving rotation port.

## Causality

p_slow	notequal
p_fast	

## Parameters

i	transmission ratio $p\_slow.v / p\_fast.v$ [], $0 < i < 1$
---	--

## Note

Keep the transmission ratio  $i$  between 0 and 1. Confusion might otherwise exist:

- $i > 1$ : the fast moving port is slower than the slow moving port (you better interchange the connections of the transmission model).
- $i < 0$ : the ports are counter-moving (use the lever model instead).

## Library

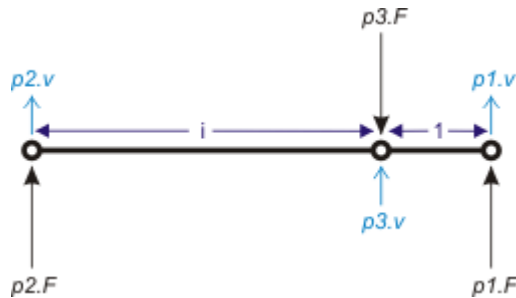
Iconic Diagrams\Mechanical\Translation\Transmission

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

## Description

This model represents an ideal transmission with a free pivot point. The relations are:



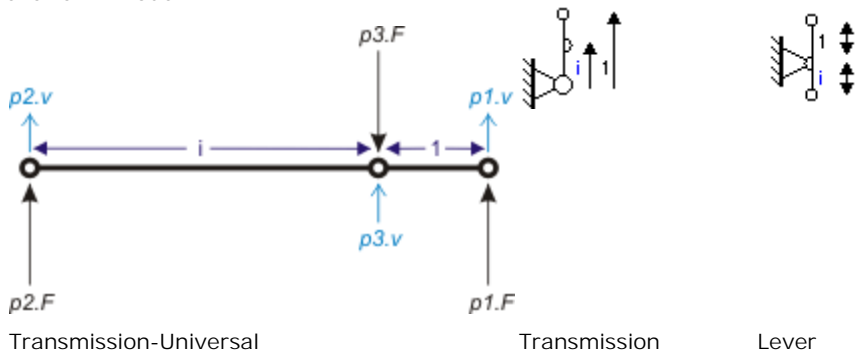
$$p3.v = (i/(1+i))*p1.v + (1/(1+i))*p2.v;$$

$$p2.F = (1/(1+i))*p3.F;$$

$$p1.F = (i/(1+i))*p3.F;$$

## Ground

Although each of the three ports may be connected to the ground, it is more efficient to use other models. When p1 or p2 is connected to the ground, this model is equal to the Transmission.emx model. When p3 is connected to the ground, this model is equal to the Lever.emx model.



## Interface

### Ports

p1,p2,p3

### Description

Translation ports.

### Parameters

i Transmission ratio []

## Thermal

The Thermal library contains components which are very useful for modeling thermal systems. The following libraries are available.

- Components
- Generators
- Sensors

### Note

- For domains that have port variables that do not multiply to power the name *pseudo* is used. This model has pseudothermal ports. The port variables of a pseudothermal port are the heat flow,  $p.dQ$  [W], and the temperature,  $p.T$  [K], which do not multiply to power.
- The base unit of temperature is degrees Kelvin. You can select degrees Celsius in the Parameters Editor or Variables Chooser desired. 20-sim will take care that internally always SI units (Kelvin) are used for calculations.

## Library

Iconic Diagrams\Mechanical\Thermal\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

### Description

This model describes linear heat convection between a material surface and gas or fluid flow. The basic equation is:

$$p.dQ = (p1.T - p2.T) * Gr;$$

where  $p1.T$  is the temperature of at the surface and  $p2.T$  the gas or fluid temperature.  $Gr$  is the thermal conductance which is function of the surface area  $A$  and the convection coefficient  $h$ :

$$Gr = A * h;$$

In most cases  $h$  is not constant but a non-analytical function of the gas or fluid speed and other properties. In most cases  $Gr$  is experimentally defined. Therefore  $G$  is given as an input signal.

## Interface

### Ports

p1

p2

### Description

Material port

Fluid port

### Causality

indifferent

### Input

G

thermal conductance [W/K]

## Library

Iconic Diagrams\Mechanical\Thermal\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

### Description

This is a general model for the heat storage that is so large that it can be considered constant (e.g. the environment). It is comparable to the ground in the electrical domain.

$$T0 = 25 \{degC\};$$

$$p.T = T0;$$

## Interface

### Ports

p[any]

### Description

Any number of connections can be made (pseudothermal).

### Causality

fixed temperature out

An torque out causality results in a derivative constitutive equation.

### Parameters

T0

temperature [degC]



# Library

Iconic Diagrams\Mechanical\Thermal\Components

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

## Description

This is a general model for the heat storage in a specific material. A constant temperature distribution in the material is assumed and a constant heat capacity:

$$E = \int (d.Q) + T0/C;$$
$$p.T = E/C;$$

*T0* is the initial temperature of the material, *E* the internal energy and *C* the thermal capacity. Because any number of connections can be made, successive ports are named p1, p2, p3 etc. 20-sim will automatically create equations such that the resulting heat flow *p.dQ* is equal to the sum of the heatflows of all connected ports p1 .. pn. The temperatures of all connected ports are equal to element temperature *p.T*.

$$p.dQ = \text{sum}(p1.dQ, p2.dQ, ....)$$
$$p.T = p1.T = p2.T = ....$$

The thermal capacity can be calculated with the specific heat capacity *cp* and material mass *m*:

$$C = cp*m;$$

Typical values for *cp* are:

water	4186
granite	790
glass	840
aluminium	900
concrete	840?
copper	387
silver	235
iron / steel	452
wood	1674
air (50 °C)	1046

## Interface

### Ports

p[any]

### Description

Any number of connections can be made (pseudothermal).

**Causality**

preferred temperature out      An torque out causality results in a derivative constitutive equation.

**Variables**

E      internal energy [J]

**Parameters**

C      thermal capacity [J/K]

## Library

Iconic Diagrams\Mechanical\Thermal\Components

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

**Description**

This model describes the heat transfer between to bodies through radiation:

$$p.dQ = Gr * \sigma * (p1.T^4 - p2.T^4);$$

where  $p1.T$  and  $p2.T$  are the temperatures of the body surfaces and  $\sigma$  is the Stefan-Boltzmann constant. For simple cases,  $Gr$  may be analytically computed. The analytical equations use  $\epsilon$ , the surface emissivity of a body which is in the range 0..1.  $\epsilon=1$ , if the body absorbs all radiation (= black body).  $\epsilon=0$ , if the body reflects all radiation and does not absorb any.

Typical values for  $\epsilon$  are:

aluminium, polished	0.04
copper, polished	0.04
gold, polished	0.02
paper	0.09
rubber	0.95
wood	0.85..0.9

**Analytical Equations for  $Gr$** 

Small convex object in large enclosure (e.g., a hot machine in a room):

$$Gr = \epsilon * A;$$

where

$e$ : Emission value of object (0..1)

$A$ : Surface area of object where radiation heat transfer takes place

Two parallel plates:

$$Gr = A/(1/e1 + 1/e2 - 1);$$

where

$e1$ : Emission value of plate1 (0..1)

$e2$ : Emission value of plate2 (0..1)

$A$  : Area of plate1 (= area of plate2)

## Interface

### Ports

p1	Material port
p2	Fluid port

### Causality

indifferent

### Input

G	thermal conductance [W/K]
---	---------------------------

## Library

Iconic Diagrams\Mechanical\Thermal\Components

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

### Description

When a temperature difference exists in a material, heat will flow from the high temperature part to the low temperature part. This model describes the transport of heat through a block of material with a temperature difference on both sides of the block. The heat conducting capacity of the material is indicated by the parameter  $G$  (thermal conductance):

$$p.dQ = p.T * G;$$

This model is the dual form of the thermal resistor where the insulation capacity of the block is indicated by the parameter  $R$  (thermal resistance):

$$p.dQ = p.T/R;$$

The heat flow through the material is ideal. I.e. there is no heat storage modeled. The thermal resistance model has separate high and low ports. The equations are

$$\begin{aligned} p.dQ &= p_{high}.dQ = p_{low}.dQ \\ p.T &= p_{high}.T - p_{low}.T \end{aligned}$$

### Block

The thermal conductance of a block can be calculated with the specific thermal conductivity  $k$ , the length  $L$  of the block, and the area  $A$  of both sides of the block:

$$G = k \cdot A / L$$

Typical values of the thermal conductivity [W.m-1.K-1] are:

water	0.6
granite	2,1
glass	1.0
aluminium	210
concrete	1.28
copper	390
silver	430
iron / steel	40-70
wood	0.13
air	0.026

**Interface**

**Ports**

p\_high, p\_low

**Description**

Both terminals of the pseudothermal port p

**Causality**

indifferent

**Parameters**

G thermal conductance [W/K]

**Library**

Iconic Diagrams\Mechanical\Thermal\Components

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

**Description**

When a temperature difference exists in a material, heat will flow from the high temperature part to the low temperature part. This model describes the transport of heat through a block of material with a temperature difference on both sides of the block. The insulation capacity of the block is indicated by the parameter *R* (thermal resistance):

$$p.dQ = p.T/R;$$

This model is the dual form of the thermal conductor where the heat conducting capacity of the material is indicated by the parameter *G* (thermal conductance):

$$p.dQ = p.T \cdot G;$$

The heat flow through the material is ideal. I.e. there is no heat storage modeled. The thermal resistance model has separate high and low ports. The equations are

$$\begin{aligned} p.dQ &= p_{high}.dQ = p_{low}.dQ \\ p.T &= p_{high}.T - p_{low}.T \end{aligned}$$

### Block

The thermal resistance of a block can be calculated with the specific thermal conductivity  $k$ , the length  $L$  of the block, and the area  $A$  of both sides of the block:

$$R = L/(k*A)$$

Typical values of the thermal conductivity [W.m-1.K-1] are:

water	0.6
granite	2,1
glass	1.0
aluminium	210
concrete	1.28
copper	390
silver	430
iron / steel	40-70
wood	0.13
air	0.026

### Interface

#### Ports

p\_high, p\_low

#### Description

Both terminals of the pseudothermal port p

#### Causality

indifferent

#### Parameters

R thermal resistance [K/W]

### Library

Iconic Diagrams\Mechanical\Thermal\Generators

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

**Description**

This model yields a heat flow that is set to a constant value. The temperature is indifferent. The model can represent any heat generating object with a constant heat flow.

**Interface**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p	
---	--

**Causality**

fixed heat flow out

**Parameters**

dQ	Heat flow [J/s]
----	-----------------

**Library**

Iconic Diagrams\Mechanical\Thermal\Generators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

**Description**

This model yields a heat flow that is equal to a (fluctuating) value given by the input signal  $dQ$ . The temperature is indifferent. The model can represent any heat generating object with a fluctuating heat flow.

**Interface**

<b>Ports</b>	<b>Description</b>
--------------	--------------------

p	
---	--

**Causality**

fixed heat flow out

**Parameters**

dQ	Heat flow [J/s]
----	-----------------

**Library**

Iconic Diagrams\Mechanical\Thermal\Generators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

## Description

This model has a temperature that is equal to a (fluctuating) value given by the input signal  $T$ . The heat flow is indifferent. This model can represent an object that has a heat capacity which is so much larger than the rest of the system, that its temperature can be seen as an independant variable.

## Interface

Ports	Description
p	
<b>Causality</b>	
fixed temperature out	
<b>Input</b>	
T	Variable temperature signal [K]

## Library

Iconic Diagrams\Thermal\Generators\Generators

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal, Electric).

## Description

This is a model of a resistor with a temperature coefficient. The resistance and voltage equation can be written as:

$$R = R_{ref} * (1 + \alpha * (p_{th}.T - T_{ref}));$$

$$p_{el}.u = p_{el}.i * R;$$

where  $R_{ref}$  is the reference resistance at reference temperature  $T_{ref}$  and alpha the temperature coefficient of resistance. The actual temperature of the resistor is given by the pseudothermal port of the model ,  $p_{el}.T$ . The heat generated by the resistor is equal to

$$p_{th}.dQ = p_{el}.u * p_{el}.i;$$

The electrical port  $p$  of the resistor model has separate high and low terminals. The equations are:

$$p_{el}.i = p_{high\_el}.i = p_{low\_el}.i;$$

$$p_{el}.u = p_{el\_high}.u - p_{el\_low}.u;$$

## Interface

Ports	Description
p_el_high	Both terminals of the Electric port.
p_el_low	
p_th	The pseudothermal port

**Causality**

indifferent p\_el  
 fixed heat flow out  
 p\_th

**Parameters**

R_ref	Reference resistance [Ohm].
T_ref	Reference temperature [K].
alpha	Temperature coefficient of the resistance []

## Library

Iconic Diagrams\Mechanical\Thermal\Generators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

**Description**

This model has a temperature that is set to a certain constant value. The heat flow is indifferent. The model can represent a piece of material which is so large that its temperature variation is neglectable (e.g. the environment) and thus can be seen as an ideal temperature source

**Interface**

Ports	Description
-------	-------------

p	
---	--

**Causality**

fixed temperature out
-----------------------

**Parameters**

T	Fixed temperature [K]
---	-----------------------

## Library

Iconic Diagrams\Thermal\Generators

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal, Electric).

**Description**

This is a model of a linear thermistor. Thermistors are thermally sensitive resistors and have, according to type, a negative (NTC), or positive (PTC) resistance/temperature coefficient. For linear thermistors the resistance and voltage equation can be written as:



$$R = R_{ref} * (1 + \alpha * (p_{th}.T - T_{ref}));$$

$$p_{el}.u = p_{el}.i * R;$$

where  $R_{ref}$  is the reference resistance at reference temperature  $T_{ref}$  and  $\alpha$  the temperature coefficient of resistance. The actual temperature of the thermistor is given by the pseudothermal port of the model,  $p_{el}.T$ . The heat generated by the thermistor is equal to

$$p_{th}.dQ = p_{el}.u * p_{el}.i;$$

The electrical port  $p$  of the thermistor model has separate high and low terminals. The equations are:

$$p_{el}.i = p_{high\_el}.i = p_{low\_el}.i;$$

$$p_{el}.u = p_{el\_high}.u - p_{el\_low}.u;$$

## Interface

Ports	Description
p_el_high	Both terminals of the Electric port.
p_el_low	
p_th	The pseudothermal port

### Causality

indifferent p\_el  
fixed heat flow out  
p\_th

### Parameters

R_ref	Reference resistance [Ohm].
T_ref	Reference temperature [K].
alpha	Temperature coefficient of the resistance []

## Library

Iconic Diagrams\Mechanical\Thermal

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

### Description

This is a model of an ideal heat flow sensor with an output signal  $dQ$  that is equal to the measured heat flow. The sensor is ideal which means that it does not store, lose or add heat.

## Interface

### Ports

p\_high, p\_low

### Description

Both ports of the sensor

### Causality

p\_high not equal p\_low

### Parameters

dQ

Measured heat flow [J/s]

## Library

Iconic Diagrams\Mechanical\Thermal

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Pseudothermal).

### Description

This is a model of an ideal temperature sensor with an output signal  $T$  that is equal to the measured temperature. The heat flow into the model is zero to assure zero power loss.

### Interface

### Ports

p

### Description

### Causality

fixed heat flow out

### Parameters

T

Measured temperature [K]

## 9.3 Signal

### Block Diagram

### Library

Signal\Block Diagram

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model divides an input signal by a constant value.

$$\text{output} = \text{input}/K$$

### Interface

Inputs	Description
input	
Outputs	
output	
Parameters	
K	Division parameter

### Library

Signal\Block Diagram

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This model delays the input signal by "T" seconds using a 4th order Pade approximation. The model is linear which means that it can be used in models that should be linearized.

### Interface

Inputs	Description
input	
Outputs	
output	
Parameters	
T	Delay time.

### Library

Signal\Block Diagram

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This model delays its input signal one simulation step.

$$\begin{aligned} \text{output} &= \text{initial}; (\text{time} = 0) \\ \text{output} &= \text{inp}(\text{time} - \text{hk}); (\text{time} > 0) \end{aligned}$$

where  $\text{hk}$  = simulation step size.

**Note**

To correctly use models with constant delays, simulation runs must be performed using integration algorithms with a constant time-step. Otherwise the model Delay-Time.emx should be used!

**Interface**

Inputs	Description
input	
Outputs	
output	
Parameters	
initial	The initial output value.

**Note**

- To correctly use models with constant delays, simulation runs must be performed using integration algorithms with a constant time-step. Otherwise the model Delay-Time.emx should be used!
- The delay-step.emx submodel is non-linear: i.e. models which include the *delay-step.emx* submodel cannot be linearized. Use the linear time delay Delay-Pade.emx if you want to perform linearization.

**Library**

Signal\Block Diagram

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This model stores the input signal and corresponding time in a buffer. After "delay" seconds the stored values are retrieved. When the simulation time step does not coincide with the delay time "delay", the output is calculated by first order interpolation.

$$\begin{aligned} \text{output} &= \text{initial}; (\text{time} < \text{delay}) \\ \text{output} &= \text{inp}(\text{time} - \text{delay}); (\text{time} \geq \text{delay}) \end{aligned}$$
**Interface**

Inputs	Description
input	
Outputs	
output	
Parameters	
initial	The initial output value.
delay	Delay time.

## Library

Signal\Block Diagram

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This model stores the input signal and corresponding time in a buffer. After "delay" seconds the stored values are retrieved. This delay is a variable input signal. When the simulation time step does not coincide with the delay time "delay", the output is calculated by first order interpolation.

```
output = initial; (time < delay)
output = input(time - delay); (time >= delay)
output = input(time); (delay < 0)
```

## Interface

Inputs	Description
input	
Outputs	
output	
Parameters	
initial	The initial output value.
delay	Delay time.

## Note

- The maximum storage capacity of the buffer is 58254 input values. When many input values are stored the simulation speed may slow down considerably!
- The delay-variabletime.emx submodel is non-linear: i.e. models which include the delay-variabletime.emx submodel cannot be linearized. Use the linear time delay Delay-Pade.emx if you want to perform linearization.

## Library

Signal\Block Diagram

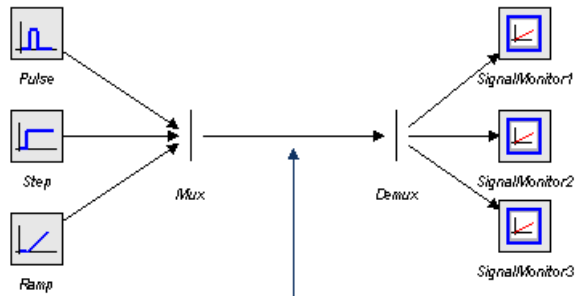
## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

You can use the Mux model to combine multiple input signals into one multi-dimensional signal.

This model can be used to split the multi-dimensional signal again into single signals.



## Interface

### Inputs

inputs

### Outputs

output[any]

### Description

Default 2 signals can be connected. Use the right mouse menu and choose *Edit Implementation* to change the number of signals.

The output signal size is equal to the number of inputs.

## Library

Signal\Block Diagram

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This model approximates the differentiation of an input signal by the equation:

$$y = \frac{2}{3} \cdot \frac{u(t) - u(t-h)}{h} + \frac{1}{3} \cdot y(t-h)$$

where  $h_k$  = simulation step size. The initial value of the output is equal to the parameter "initial". When the simulation step size is zero (time event, state event) the output value will be equal to the previous output value (the simulation step size part is not calculated to prevent a division by zero).

## Interface

### Inputs

input

### Outputs

output

### Parameters

initial

### Description

The initial value of the output.

Library

Signal\Block Diagram

Use

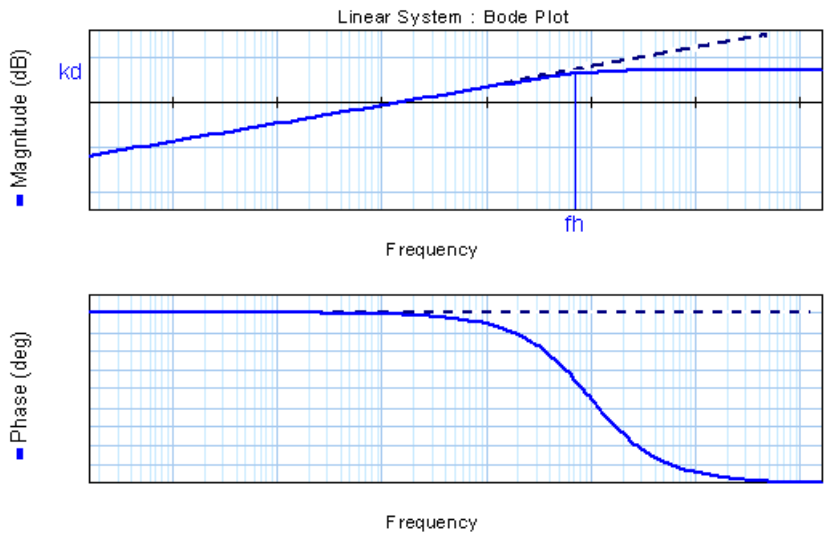
**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

Description

This model is a first order approximation of a differentiation. The transfer function is:

$$Y(s) = kd \cdot \frac{2 \cdot \pi \cdot fh \cdot s}{s + 2 \cdot \pi \cdot fh} \cdot U(s)$$

As shown in the figure below, the model behaves as a differentiator for frequencies below *fh*.



Interface

Inputs

input

Outputs

output

Parameters

kd

fh

Initial Values

output\_initial

Description

Differentiation gain []

Differentiation limit [Hz]

The initial value of the integral.

## Library

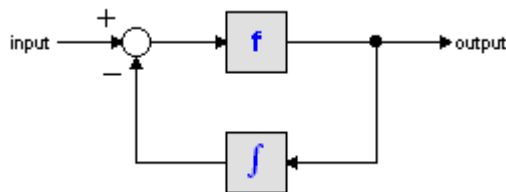
Signal\Block Diagram

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This model approximates the differentiation of an input with a state variable filter:



As can be seen, no differentiation is used in this model and consequently all integration algorithms can be used. In the S-domain the output of this model is equal to:

$$output = \frac{s}{\frac{s}{f} + 1} \cdot input$$

For very high values of N, the output becomes the pure derivative of the input. High values of N, however, increase simulations times. A good trade-off is a starting value of 10. If more accuracy is needed, this value can be increased.

## Interface

Inputs	Description
input	
Outputs	
output	
Parameters	
N	Derivative Gain Limitation.
initial	The initial value of the output.

## Library

Signal\Block Diagram

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This model differentiates an input signal. The initial value of the output is equal to the parameter "Initial".



```
output = ddt(input,initial);
```

Interface

Inputs

input

Outputs

output

Parameters

initial

Description

The initial value of the output.

Library

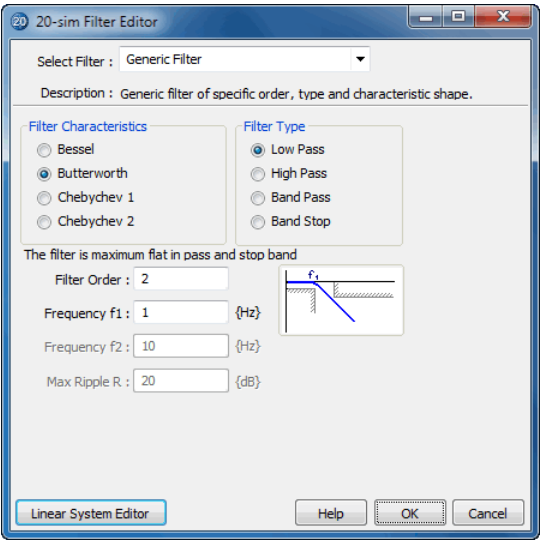
Signal\Block Diagram

Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

Description

When you select this model and click Go Down a special editor opens (Filter Editor), allowing you to choose a filter:



Interface

Inputs

input

Outputs

output

Description

**Initial Values**

The model has internal states that are not accessible.

**Parameters**

Parameters are entered by the Filter Editor.

**Library**

Signal\Block Diagram

**Use**

Domains: Continuous, Discrete. Size: 1-D. Allowed in: Block Diagrams.

**Description**

This model multiplies an input signal with a constant value.

$$output = K * input$$

**Interface**

Inputs	Description
input	
Outputs	
output	
Parameters	
K	Gain

**Library**

Signal\Block Diagram

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This model integrates an input signal over an exponential window with time constant  $T_0$  [s].

$$output(t) = \int_0^t input(\tau) \cdot e^{-(t-\tau)/T_0} d\tau$$

The model behaves as a signal averager, with an effective window of  $T_0$  [s].

**Interface**

Inputs	Description
input	
Outputs	
output	
Initial Values	
state(0)	The initial value of the integral.
Parameters	
T0	Window constant [s].

**Library**

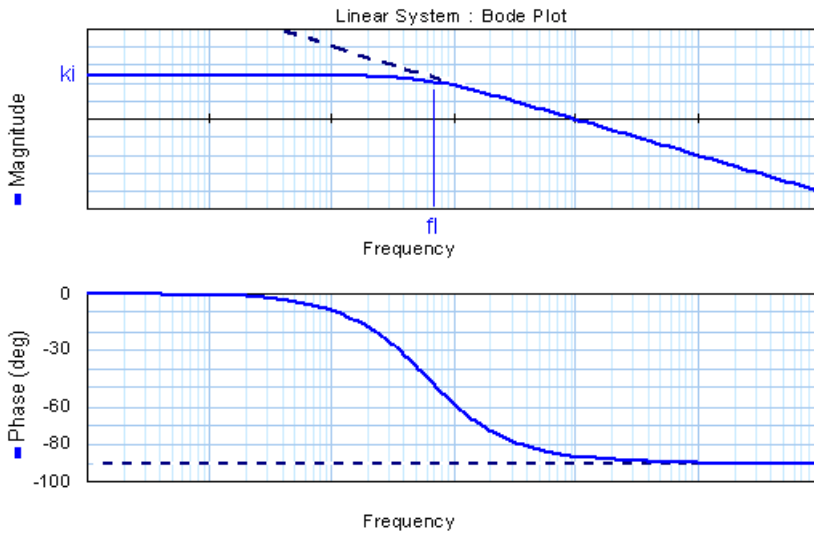
Signal\Block Diagram

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This model is a first order approximation of an integration. The transfer function is:

$$Y(s) = \frac{k_i}{2 \cdot \pi \cdot f_l + s} \cdot U(s)$$

As shown in the figure below, the model behaves as an integrator for frequencies above the  $f_l$



## Interface

### Inputs

input

### Outputs

output

### Parameters

ki

fl

output\_initial

### Description

Integration gain []  
 Integration limit [Hz]  
 Initial value.

## Library

Signal\Block Diagram

## Use

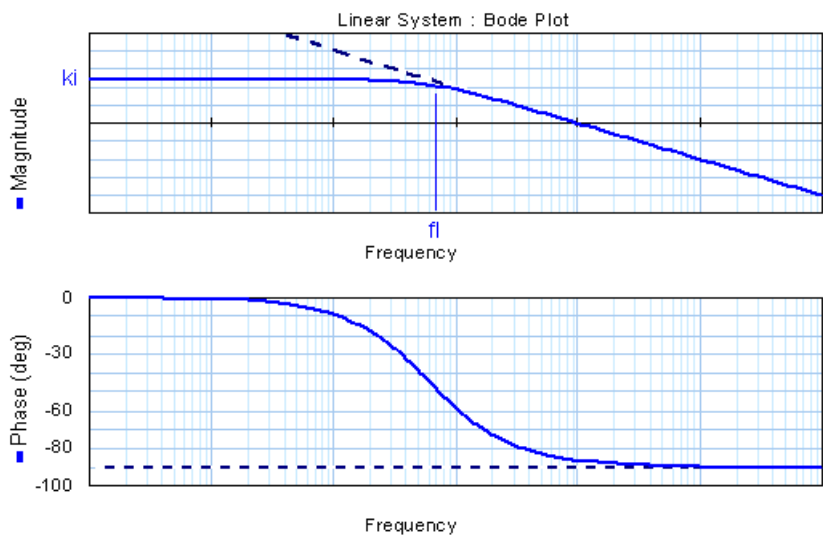
**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This model is a first order approximation of an integration with an output value limited to a minimum and maximum value. The model checks the output value to see if the maximum of minimum values have been crossed. If so the input value is set to zero to prevent the integral from winding-up. Between the bounds the transfer function is:

$$Y(s) = \frac{k_i}{2 \cdot \pi \cdot f_l + s} \cdot U(s)$$

As shown in the figure below, the model behaves as an integrator for frequencies above the  $f_l$



## Interface

Inputs	Description
input	
Outputs	
output	
Parameters	
ki	Integration gain []
fl	Integration limit [Hz]
output_initial	Initial value.
maximum	Maximum output value
minimum	Minimum output value

## Library

Signal\Block Diagram

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This model integrates an input signal. The output of this integral is limited between a maximum and minimum bound. If the integral is in saturated condition and the input changes sign, the output wanders away from the bounds immediately.

$$output = int(inp) + state(0); (minimum \leq output \leq maximum)$$

**Interface**

Inputs	Description
input	
Outputs	
output	
Initial Values	
state(0)	The initial value of the integral.
Parameters	
minimum	Minimum output value.
maximum	Maximum output value.

**Library**

Signal\Block Diagram

**Use**

**Domains: Continuous. Size: 1-D. Kind: Block Diagrams.**

**Description**

This model integrates an input signal over a limited time interval which is  $T_0$  [s] wide.

$$output = \int_{t-T_0}^t input \cdot dt$$

The model behaves as a signal averager, with a rectangular window of  $T_0$  [s].

**Interface**

Inputs	Description
input	
Outputs	
output	
Initial Values	
state(0)	The initial value of the integral.
Parameters	
$T_0$	Integration interval.

**Library**

Signal\Block Diagram

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This model integrates an input signal. The output of this integral may be reset to any desired value each time the reset signal is unequal to zero.

$$\text{output} = \text{int}(\text{inp}) + \text{state}(0); (\text{reset} = 0)$$

$$\text{output} = \text{reset to newoutput}; (\text{reset} \neq 0)$$
**Interface****Inputs**

input  
reset

newoutput

**Outputs**

output

**Initial Values**

state(0)

**Description**

Input signal

When reset  $\neq 0$ , the output changes to newoutput.

New output.

**Library**

Signal\Block Diagram

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This model integrates an input signal:

$$\text{output} = \text{int}(\text{input}) + \text{state}(0)$$
**Interface****Inputs**

input

**Outputs**

output

**Description**

**Initial Values**

state(0)

The initial value of the integral.

**Library**

Signal\Block Diagram

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model yields the inverse of the input signal.

$$output = 1 / input$$

**Interface**

Inputs

input

Outputs

output

Description

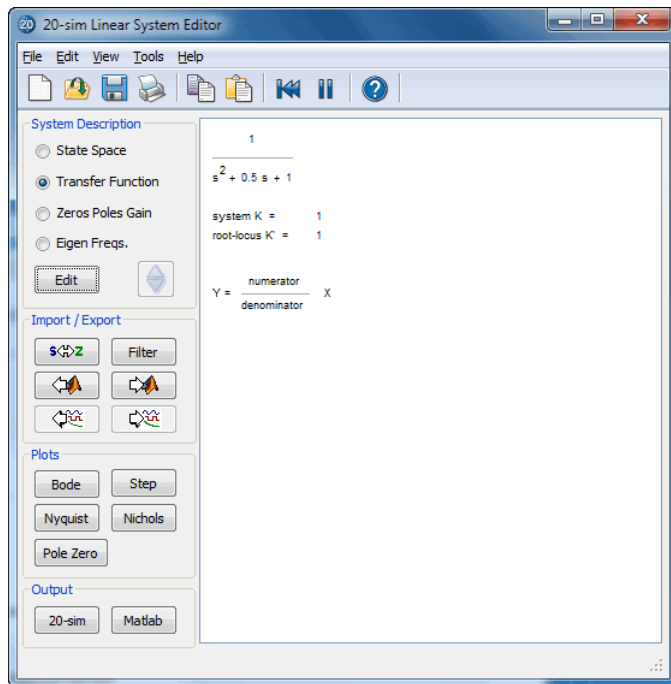
**Library**

Signal\Block Diagram

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

When you select this model and click Go Down a special editor opens (Linear System Editor), allowing you to enter a linear system in State Space form, as a Transfer Function or by adding poles and zeros:





## Interface

Inputs  
input  
Outputs  
output  
Initial Values

Parameters

Description

The model has internal states that are not accessible.

Parameters are entered by the Linear System Editor.

## Library

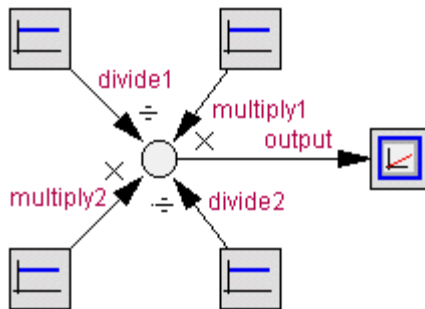
Signal\Block Diagram , System

## Use

**Domains:** Continuous, Discrete. **Size:** [n,m]. **Kind:** Block Diagrams.

## Description

This model yields a multiplication and/or division of one or more input signals. While connecting input signals, 20-sim will ask whether the signals should be multiplied or divided. The signals may have either size, but the size of all connected signals should be equal.



For example the MultiplyDivide model can have 2 signals connected that are multiplied and 2 signals that must be divided. 20-sim treats them as an array multiply and an array divide with:

$$\text{multiply} = [\text{multiply1}; \text{multiply2}];$$

and

$$\text{divide} = [\text{divide1}; \text{divide2}];$$

The output will then be equal to:

$$\text{output} = (\text{multiply1} * \text{multiply2}) / (\text{divide1} * \text{divide2});$$

## Interface

### Inputs

multiply[any]  
divide[any]

### Description

Any number of input signals (each of the same size) may be connected to be multiplied (multiply) or divided (divide).

### Outputs

output

### Limitations

The signals connected to this model should all have the same size.

## Library

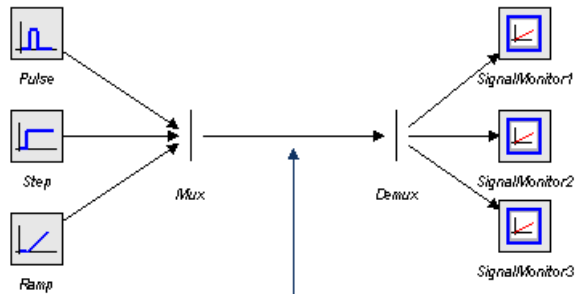
Signal\Block Diagram

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

You can use this model to combine multiple input signals into one multi-dimensional signal. The Demux model can be used to split the multi-dimensional signal again into single signals.



## Interface

### Inputs

inputs

### Description

Default 2 signals can be connected. Use the right mouse menu and choose *Edit Implementation* to change the number of signals.

### Outputs

output[any]

The output signal size is equal to the number of inputs.

## Library

Signal\Block Diagram

## Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

This model yields the negative of the input signal.

$$\text{output} = -\text{input}$$

## Interface

### Inputs

input

### Description

Outputs  
output

## Library

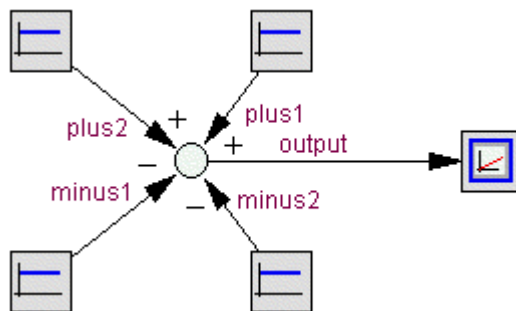
Signal\Block Diagram , System

## Use

**Domains:** Continuous, Discrete. **Size:** [n,m]. **Kind:** Block Diagrams.

## Description

This model yields a subtraction and/or summation of one or more input signals. While connecting input signals, 20-sim will ask whether the signals should be added or subtracted. The signals may have either size, but the size of all connected signals should be equal.



For example the PlusMinus model can have 2 signals connected that are added and 2 signals that must be subtracted. 20-sim treats them as an array plus and an array minus with:

$$plus = [plus1; plus2];$$

and

$$minus = [minus1; minus2];$$

The output will then be equal to:

$$output = plus1 + plus2 - minus1 - minus2;$$

## Interface

### Inputs

plus[any]  
minus[any]

### Description

Any number of input signals (each of the same size) may be connected to be added (plus) or subtracted (minus).

### Outputs

output

**Limitations**

The signals connected to this model should all have the same size.

**Library**

Signal\Block Diagram , Signal\Sources

**Use**

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

This model shows the value of its input in the Simulator. When you open the Simulator (select Properties and Plot) the input of this model is automatically selected as plotvariable. As label for this variable the local name of the SignalMonitor model is chosen. It is therefore advised to give each SignalMonitor model a useful name (select the model, click the right mouse button and select Attributes from the right mouse menu).

**Interface**

**Inputs**

input

**Description**

The value of the input is shown in the Simulator using the local name of the model as label.

**Library**

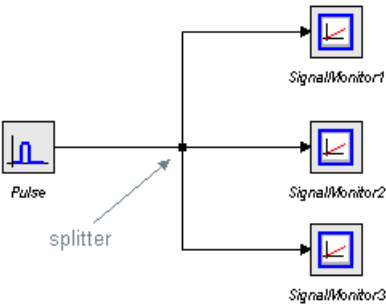
Signal\Block Diagram , System

**Use**

**Domains:** Continuous, Discrete. **Size:** [n,m]. **Kind:** Block Diagrams.

**Description**

This model can split one output signal into two or more output signals. The signals may have either size, but the size of all connected signals should be equal.



**Interface**

**Inputs**

**Description**

input

One input signal must be connected

Outputs

output[any]

Any number of input signals (each of the same size) may be connected.

**Limitations**

The signals connected to this model should all have the same size.

**Block Diagram Non-Linear****Library**

Signal\Block Diagram Non-Linear

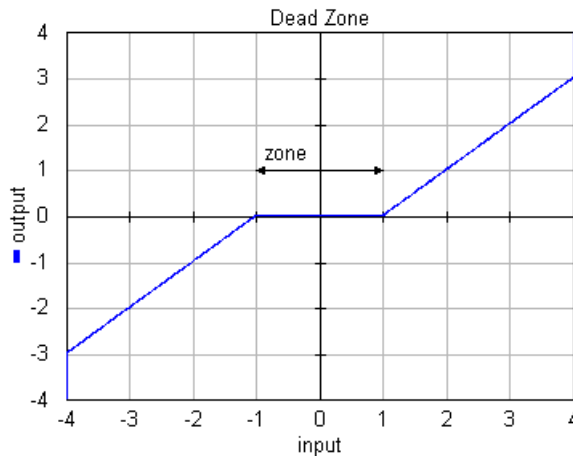
**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model generates zero output when the input is within a specified region, called the dead zone. Otherwise the output equals the input plus or minus half the zone.

$$\text{output} = \text{input} + \text{zone}/2; (\text{input} < -\text{zone}/2)$$

$$\text{output} = 0; (-\text{zone}/2 \leq \text{input} \leq \text{zone}/2)$$

$$\text{output} = \text{input} - \text{zone}/2; (\text{input} > \text{zone}/2)$$

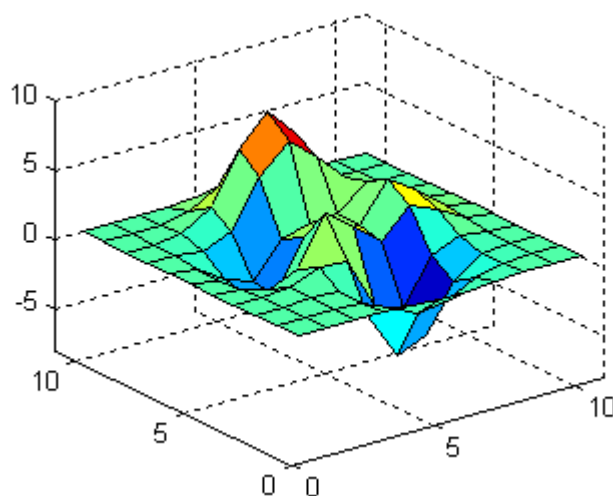
**Interface****Inputs**

input

**Description****Outputs**

output





This function can be put in a matrix form as:

0.0	-1.0	-0.8	-0.6	-0.4	-0.2	0.0	0.2	0.4	0.6	0.8	1.0
-1.0	1.9	2.4	2.4	1.8	0.7	-0.7	-1.8	-2.3	-2.0	-1.2	-0.3
-0.8	1.9	2.9	3.4	3.3	2.4	1.1	-0.1	-0.7	-0.5	0.1	0.9
-0.6	1.3	2.6	3.5	3.7	3.1	1.9	0.8	0.2	0.4	1.1	1.8
-0.4	0.3	1.7	2.9	3.3	2.9	1.9	0.9	0.4	0.7	1.6	2.5
-0.2	-0.8	0.6	1.9	2.5	2.3	1.5	0.6	0.3	0.8	1.8	2.8
0.0	-1.7	-0.3	1.0	1.7	1.7	1.0	0.3	0.2	0.8	1.9	2.9
0.2	-2.1	-0.9	0.4	1.1	1.1	0.6	0.1	0.0	0.7	1.8	2.8
0.4	-2.1	-1.1	0.0	0.7	0.8	0.4	0.0	0.0	0.7	1.6	2.5
0.6	-1.7	-0.8	0.1	0.8	0.9	0.7	0.4	0.4	0.9	1.6	2.2
0.8	-0.9	0.0	0.9	1.6	1.9	1.8	1.5	1.4	1.6	1.9	2.2
1.0	0.2	1.2	2.3	3.2	3.7	3.7	3.4	3.1	2.8	2.6	2.4

The first row and column denote the x-values and y-values and the other row-column pairs the corresponding peaks function values. This matrix can be entered in a text file:

2DTableLookup.txt - Notepad

0.0	-1.0	-0.8	-0.6	-0.4	-0.2	0.0	0.2	0.4	0.6	0.8	1.0
-1.0	1.9	2.4	2.4	1.8	0.7	-0.7	-1.8	-2.3	-2.0	-1.2	-0.3
-0.8	1.9	2.9	3.4	3.3	2.4	1.1	-0.1	-0.7	-0.5	0.1	0.9
-0.6	1.3	2.6	3.5	3.7	3.1	1.9	0.8	0.2	0.4	1.1	1.8
-0.4	0.3	1.7	2.9	3.3	2.9	1.9	0.9	0.4	0.7	1.6	2.5
-0.2	-0.8	0.6	1.9	2.5	2.3	1.5	0.6	0.3	0.8	1.8	2.8
0.0	-1.7	-0.3	1.0	1.7	1.7	1.0	0.3	0.2	0.8	1.9	2.9
0.2	-2.1	-0.9	0.4	1.1	1.1	0.6	0.1	0.0	0.7	1.8	2.8
0.4	-2.1	-1.1	0.0	0.7	0.8	0.4	0.0	0.0	0.7	1.6	2.5
0.6	-1.7	-0.8	0.1	0.8	0.9	0.7	0.4	0.4	0.9	1.6	2.2
0.8	-0.9	0.0	0.9	1.6	1.9	1.8	1.5	1.4	1.6	1.9	2.2
1.0	0.2	1.2	2.3	3.2	3.7	3.7	3.4	3.1	2.8	2.6	2.4



The model 2DTableLookup.emx (*Examples\Signal Processing*) shows how to use this text file as a 2-D table.

### Interface

Inputs	Description
input1	x-value
input2	y-value
Outputs	
output	z-value
Parameters	
filename	The filename of the table file.

### Library

Signal\Block Diagram Non-Linear

#### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

#### Description

This model yields the absolute value of an input signal.

$$outp = abs(inp);$$

### Interface

Inputs	Description
input	
Outputs	
output	

### Library

Signal\Block Diagram Non-Linear

#### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

#### Description

This model yields the cosine of an input signal.

$$output = cos(input);$$

### Interface

Inputs	Description
--------	-------------

input

### Outputs

output

## Library

Signal\Block Diagram Non-Linear

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model returns an output signal in decibel (dB):

$$output = 20 * \log_{10}(input);$$

### Interface

Inputs	Description
input	
Outputs	
output	

## Library

Signal\Block Diagram Non-Linear

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model returns the natural logarithm of the input.

$$output = \log(input);$$

### Interface

Inputs	Description
input	
Outputs	
output	

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model raises the values of an input signal to the power p.

$$output = input^p;$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Parameters**

p

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model returns the sign of the input. A zero input results in a zero output.

$$output = -1; (input < 0)$$

$$output = 0; (input = 0)$$

$$output = 1; (input > 0)$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model yields the sine of an input signal.

$$output = \sin(input);$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model returns the square of the input signal.

$$output = input^2;$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model yields the square root of an input signal.

$$outp = \text{sqrt}(inp);$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**This model yields the square root of an input signal with sign and multiplied by a parameter  $p$ .

$$output = \text{sign}(input) * \text{sqrt}(inp) / p;$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Parameters**

p

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model yields the square of an input signal with sign and multiplied by a parameter  $p$ .

$$output = p * sign(input) * input * input;$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Parameters**

p

**Library**

Signal\Block Diagram Non-Linear

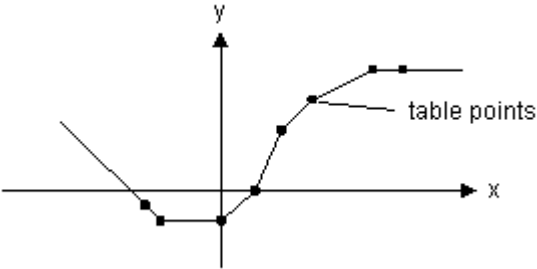
**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This model uses a one-dimensional table with data points to calculate the output  $y = f(x)$  as a function of the input  $x$ . The output  $y$  is calculated using linear interpolation between the table data points.

- The input data of the first column needs to be monotonically increasing.
- Discontinuities are allowed, by providing the same input point twice in the table.
- Values outside of the table range, are computed by linear extrapolation of the last two points.

table

-2.5	-0.5
-2	-1
0	-1
1	0
2	2
3	3.0
5	4
6	4.0



A table must be stored either as an ASCII (text) file or as a matrix inside the equation model. In both cases the table should consist two columns of data. The first column consists of the x-values and the second column of the corresponding y-values.

**Reading data from a file**

If the table is read from a file, each line of the file may only contain one x- and one corresponding y-value. The two values must be separated by a space or a tab. Each new set of x- and y-values must start on a new line. No comment or other text may be part of the table-file. The filename of the input file can be specified using the complete path (e.g. C:\data\data.tbl). When no path is given, the file is assumed to be in the experiment directory.

**Interface**

Inputs	Description
input	
Outputs	
output	
Parameters	
filename	The filename of the table file.

**Reading data from a matrix**

If the table is read from a matrix in an equation model, each row may only contain one x- and one corresponding y-value. The two values must be separated by a coma and each column must be separated by a semi-colon.

**Note**

Table interpolation can also be used directly in an equation model by using the function table.

**Library**

Signal\Block Diagram Non-Linear

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

This model yields the tangent of an input signal.

$$output = \tan(input);$$

Note that the tangent goes infinity for input signals that are a multiple of  $\pi$ .

**Interface****Inputs**

input

**Description****Outputs**

output

**Library**

Signal\Block Diagram Non-Linear

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

This model rounds the input towards zero (i.e. it removes the fraction of the input).

$$output = \text{trunc}(input);$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Parameters**

p



**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This model represents mechanical backlash between an input position and an output position.

*output = 0; (input is within the dead zone)*

*output = input - zone/2; (input is increasing and out of the dead zone)*

*output = input + zone/2; (input is decreasing and out of the dead zone)*

$$p.F = 0.5 \cdot k_2 \cdot \left( x - \sqrt{\left(-x - \frac{s}{2}\right) + (ep \cdot s)^2} + x + \sqrt{\left(x - \frac{s}{2}\right) + (ep \cdot s)^2} \right) + k_1 \cdot x + d_{1or 2} \cdot p.v$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Parameters**

zone

Size of the dead zone.

**zone** >= 0

initial

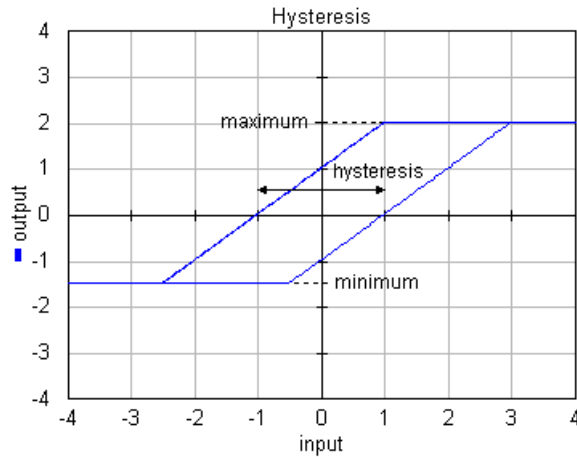
Value of the output at time = 0.

**initial** >= input(time = 0) - zone/2**initial** <= input(time = 0) + zone/2**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

The output signal of this submodel switches between *maximum* and *minimum*, depending on the sign of the input signal, with hysteresis applied. When traversing between *minimum* and *maximum* (dead zone), the rate of change is defined by the parameter *k*.



## Interface

### Inputs

input

### Outputs

output

### Parameters

minimum  
maximum  
hysteresis  
k

### Description

Minimum value of the output.  
Maximum value of the output.  
Magnitude of the hysteresis.  
Rate of change in the dead zone.

## Library

Signal\Block Diagram Non-Linear

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

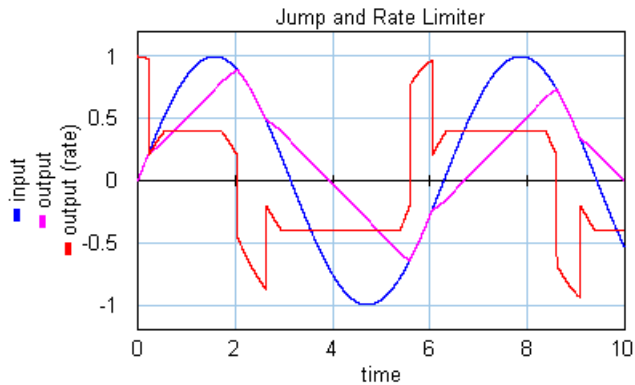
This model limits the input signal to a minimum and maximum jump and a minimum and maximum rate.

```

for minimum < input < maximum:
    output = input
else
    doutput/dt = dinput/dt; (minimumrate < dinput/dt < maximumrate)
    doutput/dt = minimum; (dinput/dt < minimumrate)
    output = maximum (dinput/dt > maximumrate)

```

An example is shown below where a sinusoidal input signal is limited to a minimum jump of -0.2, a maximum jump of 0.2, a maximum rate of 0.4 and a minimum rate of -0.4.



## Interface

### Inputs

input

Description

### Outputs

output

### Parameters

minimum  
maximum  
minimumrate  
maximumrate

Minimum jump of the output.  
Maximum jump of the output.  
Minimum rate of the output.  
Maximum rate of the output.

## Library

Signal\Block Diagram Non-Linear

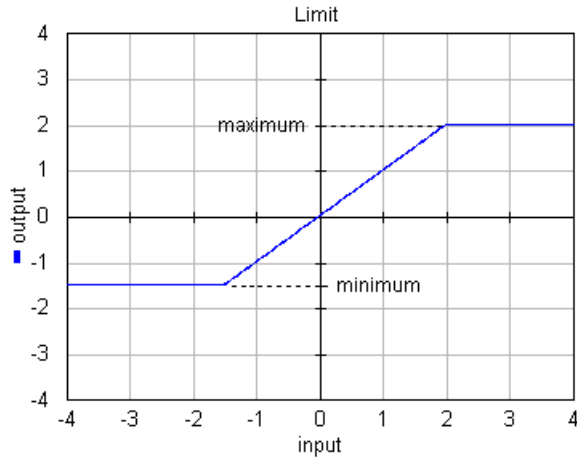
### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model limits the input signal to minimum and maximum bounds.

$output = minimum; (input < minimum)$   
 $output = input; (minimum \leq input \leq maximum)$   
 $output = maximum (input > maximum)$



## Interface

### Inputs

input

### Outputs

output

### Parameters

minimum  
 maximum

### Description

Minimum value of the output.  
 Maximum value of the output.

## Library

Signal\Block Diagram Non-Linear

### Use

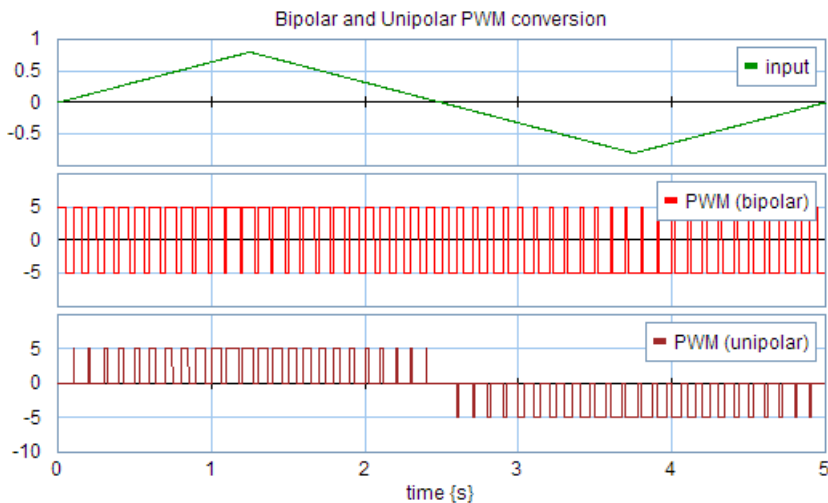
**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

Pulse width modulation (PWM) is a powerful technique for controlling analog circuits with a processor's digital outputs. PWM is employed in a wide variety of applications, ranging from measurement and communications to power control and conversion. The output of a PWM block is a pulse train. The duty cycle, (the time that a pulse is *on* divided by the time the pulse is *off*) is proportional to the value of the input signal if the input is within the range  $< -input\_amp, +input\_amp >$ . For Bipolar PWM the output signal switches between a positive and a negative value. For Unipolar PWM the output signal switches between zero and positive or negative value.

input	bipolar PWM	Unipolar PWM
$> input\_amp$	100% output_amp 0% -output_amp	100% output_amp 0% 0
input_amp	100% output_amp 0% -output_amp	100% output_amp 0% 0
$0.5 * input\_amp$	75% output_amp 25% -output_amp	50% output_amp 50% 0
0	50% output_amp 50% -output_amp	0
$-0.5 * input\_amp$	25% output_amp 75% -output_amp	50% 0 50% -output_amp
-input_amp	0% output_amp 100% -output_amp	0% 0 100% -output_amp
$< -input\_amp$	0% output_amp 100% -output_amp	0% 0 100% -output_amp

An example is shown in the graph below. The parameter *input\_amp* is equal to 1 and the parameter *max output* is equal to 5. The frequency of the PWM signal is 10 Hz.



Bipolar and Unipolar PWM conversion.

## Interface

### Inputs

input

### Description

### Outputs

output

### Parameters

f	The modulating frequency [Hz].
input_amp	Maximum value of the input signal.
output_amp	The output value will switch between output_amp, 0 and -output_amp.

## Library

Signal\Block Diagram Non-Linear

### Use

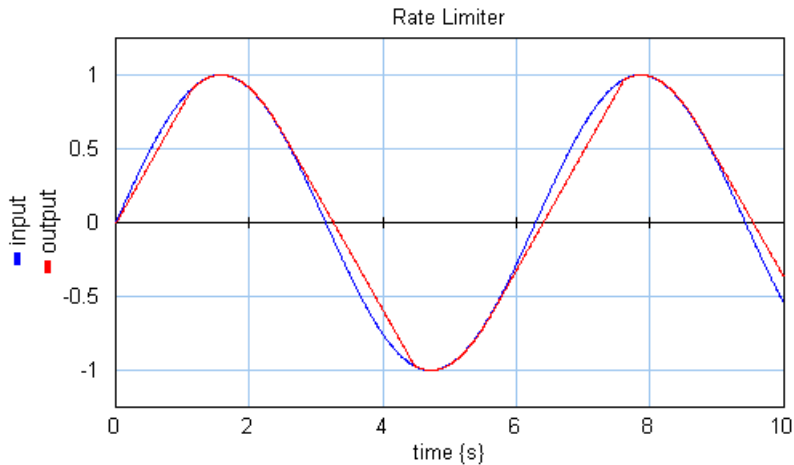
**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model limits the input signal to a minimum and maximum rate.

$$\begin{aligned}
 & \text{doutput/dt} = \text{dinput/dt}; \quad (\text{minimum} < \text{dinput/dt} < \text{maximum}) \\
 & \text{doutput/dt} = \text{minimum}; \quad (\text{dinput/dt} < \text{minimum}) \\
 & \text{output} = \text{maximum} \quad (\text{dinput/dt} > \text{maximum})
 \end{aligned}$$

An example is shown below where a sinusoidal input signal is limited to a maximum rate of 0.4 and a minimum rate of -0.8.



The rate limiter uses a first order filter to approximate the derivative of the input. Below the cut-off frequency  $f_l$  the approximation is accurate and the model behaves as a rate limiter. Above the cut-off frequency  $f_l$  the model output weakens to zero. For high values of the cut-off frequency  $f_l$ , the model will slow down simulation because it forces the integration method to take very small time-steps. A good trade-off for most models is a starting value of 100 [Hz].

## Interface

### Inputs

input

### Description

### Outputs

output

### Parameters

minimum  
maximum  
 $f_l$

Minimum rate of the output.  
Maximum rate of the output.  
Cut-off frequency [Hz]

## Library

Signal\Block Diagram Non-Linear

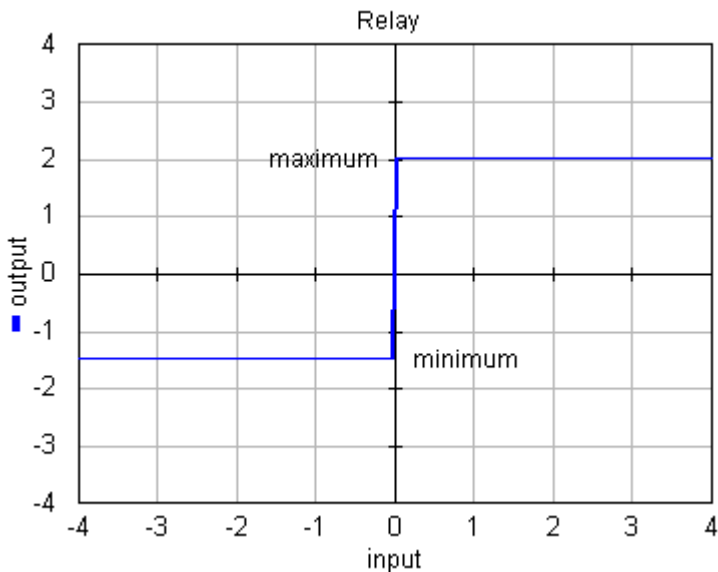
## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

The output signal of this submodel switches between a max and a min parameter using the sign of the input signal.

*output = minimum; (input < 0)*  
*output = maximum; (input >= 0)*



**Interface**

**Inputs**

input

**Description**

**Outputs**

output

**Parameters**

minimum	Minimum value of the output.
maximum	Maximum value of the output.

**Library**

Signal\Block Diagram Non-Linear

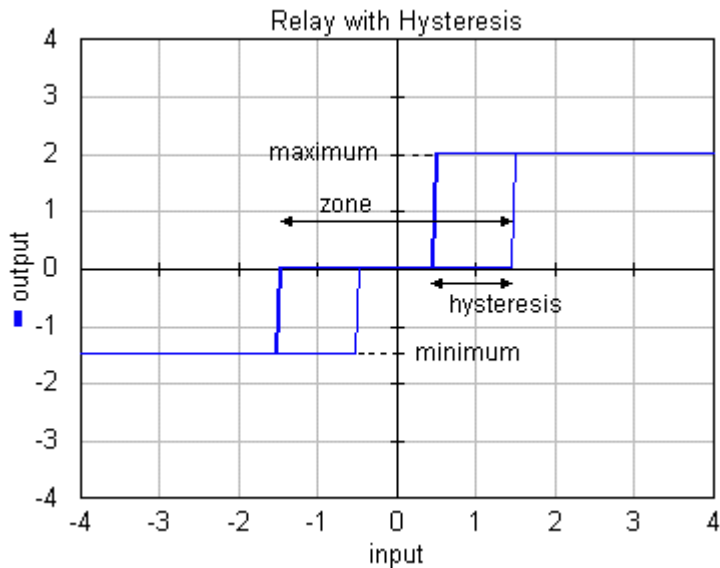
**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output signal of this submodel switches between max and min parameters, depending on the sign of the input signal, with hysteresis and dead zone applied.





Interface

Inputs

input

Outputs

output

Parameters

- minimum
- maximum
- zone
- hysteresis

Description

- Minimum value of the output.
- Maximum value of the output.
- Magnitude of the dead zone.
- Magnitude of the hysteresis.

Library

Signal\Block Diagram Non-Linear

Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

Description

This model switches between zero and the input signal, depending on the value of a condition input signal.

$$\begin{aligned} \text{output} &= 0; (\text{condition} > 0) \\ \text{output} &= \text{input}; (\text{condition} \leq 0) \end{aligned}$$

## Interface

Inputs	Description
input_high	
input_low	
condition	Switching condition

## Outputs

output

## Library

Signal\Block Diagram Non-Linear

## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

This model switches between two input signals, depending on the value of a third input signal.

$$\begin{aligned} \text{output} &= \text{input\_high}; (\text{condition} \geq 0) \\ \text{output} &= \text{inp\_low}; (\text{condition} < 0) \end{aligned}$$

## Interface

Inputs	Description
input_high	
input_low	
condition	Switching condition

## Outputs

output

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model switches between the input signal and zero, depending on the value of a condition input signal.

$$\begin{aligned} \text{output} &= \text{input}; (\text{condition} > 0) \\ \text{output} &= 0; (\text{condition} \leq 0) \end{aligned}$$
**Interface****Inputs**

input\_high  
input\_low  
condition

**Description**

Switching condition

**Outputs**

output

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model yields the maximum of two input signals.

$$\begin{aligned} \text{output} &= \text{input1}; (\text{input1} \geq \text{input2}) \\ \text{output} &= \text{input2}; (\text{input1} < \text{input2}) \end{aligned}$$
**Interface****Inputs**

input1  
input2

**Description****Outputs**

output

**Library**

Signal\Block Diagram Non-Linear

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model yields the minimum of two input signals.

$$\begin{aligned} \text{output} &= \text{input1}; (\text{input1} \leq \text{input2}) \\ \text{output} &= \text{input2}; (\text{input1} > \text{input2}) \end{aligned}$$
**Interface****Inputs****Description**

input1

input2

**Outputs**

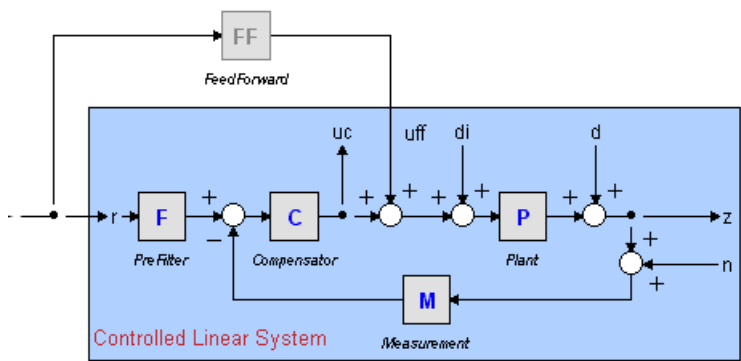
output

**Control****Library**

Signal\Control\Controlled Linear Systems

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a masked model which opens the Controller Design Editor when edited. Using this editor the settings for a controlled linear system can be entered.



Depending on the choices made, various inputs and outputs are available. In the picture above, the most complex model is shown. Read more about it in the Controller Design Editor topic.

Interface

Inputs

r	Controller setpoint
d	Output Disturbance
n	Measurement Disturbance
di	Input Disturbance
uff	Feedforward Input

Outputs

z	Plant output
uc	Feedforward Error Signal

Parameters

hidden	The parameters and initial values of this model are hidden for the user. Use the Controller Design Editor to edit this model (select the model and choose <b>Go Down</b> ).
--------	---

Library

Signal\Control\Controlled Linear Systems

Implementations

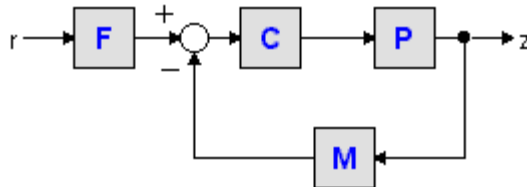
- rz
- rzff
- rzffn
- rzffnd
- rzffnddi
- rznd
- rznd
- rznddi

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Translation).

**Description - rz**

This model represents a controlled linear system described by graphically connected Linear systems:



These Linear Systems (F,C,P and M) can be edited using the Linear Systems Editor or replaced by drag and drop (any desired model) giving maximum flexibility.

**Interface - rz****Inputs**

r

**Description**

Controller setpoint

**Outputs**

z

**Description**

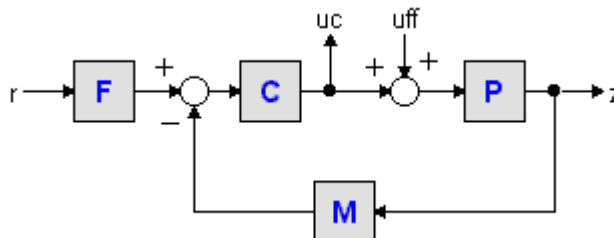
Plant output

**Parameters**

Depends on the implementation of the submodels.

**Description - rzff**

This model represents a controlled linear system described by graphically connected Linear systems:



These Linear Systems (F,C,P and M) can be edited using the Linear Systems Editor or replaced by drag and drop (any desired model) giving maximum flexibility.

**Interface - rzff****Inputs**

r

**Description**

Controller setpoint

uff

Feedforward Input

**Outputs****Description**

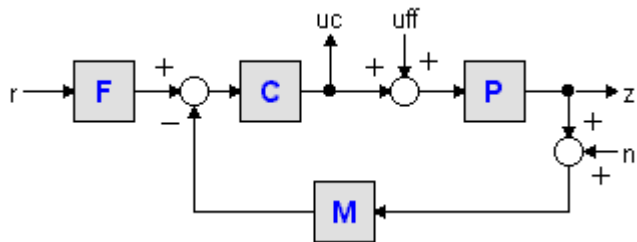
z	Plant output
uc	Feedforward Error Signal

**Parameters**

Depends on the implementation of the submodels.

**Description - rzffn**

This model represents a controlled linear system described by graphically connected Linear systems:



These Linear Systems (F,C,P and M) can be edited using the Linear Systems Editor or replaced by drag and drop (any desired model) giving maximum flexibility.

**Interface - rzffn**

**Inputs**

r	Controller setpoint
n	Measurement Disturbance
uff	Feedforward Input

**Outputs**

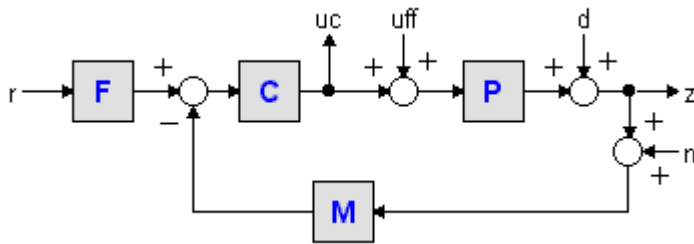
z	Plant output
uc	Feedforward Error Signal

**Parameters**

Depends on the implementation of the submodels.

**Description - rzffnd**

This model represents a controlled linear system described by graphically connected Linear systems:



These Linear Systems (F,C,P and M) can be edited using the Linear Systems Editor or replaced by drag and drop (any desired model) giving maximum flexibility.

### Interface - rzffnd

#### Inputs

r	Controller setpoint
d	Output Disturbance
n	Measurement Disturbance
uff	Feedforward Input

#### Outputs

z	Plant output
uc	Feedforward Error Signal

#### Description

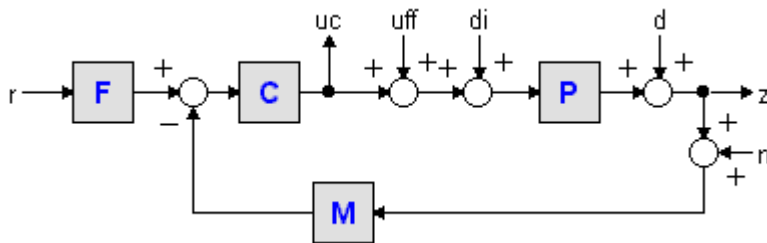
#### Description

#### Parameters

Depends on the implementation of the submodels.

### Description-rzffnddi

This model represents a controlled linear system described by graphically connected Linear systems:



These Linear Systems (F,C,P and M) can be edited using the Linear Systems Editor or replaced by drag and drop (any desired model) giving maximum flexibility.

### Interface-rzffnddi

#### Inputs

r	Controller setpoint
---	---------------------

#### Description



d	Output Disturbance
n	Measurement Disturbance
di	Input Disturbance
uff	Feedforward Input

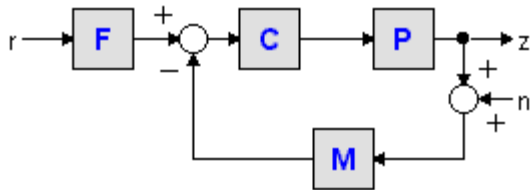
Outputs	Description
z	Plant output
uc	Feedforward Error Signal

**Parameters**

Depends on the implementation of the submodels.

**Description - rzn**

This model represents a controlled linear system described by graphically connected Linear systems:



These Linear Systems (F,C,P and M) can be edited using the Linear Systems Editor or replaced by drag and drop (any desired model) giving maximum flexibility.

**Interface - rzn**

Inputs	Description
r	Controller setpoint
n	Measurement Disturbance

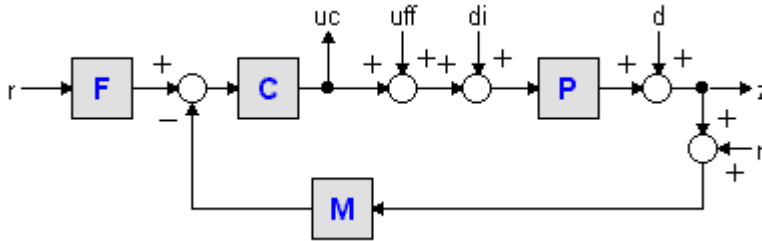
Outputs	Description
z	Plant output

**Parameters**

Depends on the implementation of the submodels.

**Description - rznd**

This model represents a controlled linear system described by graphically connected Linear systems:



These Linear Systems (F,C,P and M) can be edited using the Linear Systems Editor or replaced by drag and drop (any desired model) giving maximum flexibility.

### Interface - rznd

#### Inputs

r	Controller setpoint
d	Output Disturbance
n	Measurement Disturbance

#### Outputs

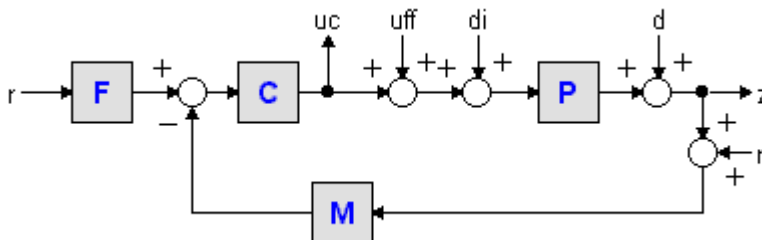
z	Plant output
---	--------------

#### Parameters

Depends on the implementation of the submodels.

### Description - rznddi

This model represents a controlled linear system described by graphically connected Linear systems:



These Linear Systems (F,C,P and M) can be edited using the Linear Systems Editor or replaced by drag and drop (any desired model) giving maximum flexibility.

### Interface - rznddi

#### Inputs

r	Controller setpoint
d	Output Disturbance
n	Measurement Disturbance

#### Description

di Input Disturbance

### Outputs **Description**

z Plant output

### Parameters

Depends on the implementation of the submodels.

## Library

Signal\Control\Neural Networks

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a masked model which opens the BSpline Editor when edited. Using this editor the settings for a B-Spline Network can be entered.

### Interface

#### Inputs

any

#### Description

The user can defined any input.

error

The error signal: the difference between the desired output and the network output.

#### Outputs

output

#### Description

The network output

#### Parameters

learning\_rate

The learning rate

network\_order

The order of the spline-interpolation.

online\_learning

A boolean: Learn at each sample (True) or Learn after Leaving Spline (False).

regularization

Not yet supported.

regularization\_width

Not yet supported.

load\_weights

A boolean: Load weights before simulation.

save\_weights

A boolean: Save weights after simulation.

## Library

Signal\Control\Neural Networks

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a masked model which opens the MLP Editor when edited. Using this editor the settings for a MLP Network can be entered.

### Interface

#### Inputs

any	The user can defined any network input.
error	The error signal: the difference between the desired output and the network output.

#### Outputs

any	The user can defined any network output.
-----	--

#### Description

#### Description

#### Parameters

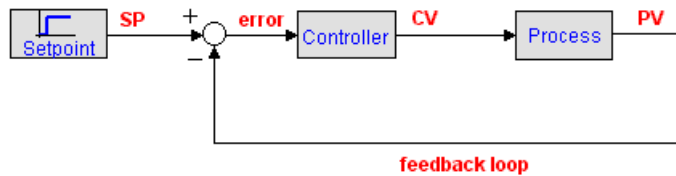
nr_hidden	Number of hidden neurons.
learning_rate	The learning rate.
readWeights	A boolean: Load weights before simulation.
writeWeights	A boolean: Save weights after simulation.

PID control stands for **P**roportional, **I**ntegral and **D**erivative control. PID controllers have been around since about 1940. Modern controllers perform the same functions as those, perhaps with a few embellishments and certainly more accurately, but the same functions nonetheless.

PID controllers are the best general purpose controllers to do the job. More sophisticated control algorithms will produce better performance when fitted to a specific process, but poorer performance results if the process changes. This sensitivity to process changes is called robustness, with more robust being less sensitive. The PID algorithm is an excellent trade-off between robustness and performance.

Although theory on PID-controllers is widespread and more or less uniform nowadays, in practice there are many algorithms and parameter settings. The 20-sim Control library, supports the most common algorithms.

A standard control loop is shown in the figure below. A controller tries to steer a process in a way that minimizes the difference between a given setpoint and the output of that process. In other words, the controller tries to get the process output as close as possible to the given setpoint.



## Setpoint

The **setpoint (SP)** is where the process output should match. It can be a static value (e.g. the desired temperature of a room) or a varying value (e.g. the desired position of a robot-tip).

The setpoint is where you would like the measurement to be. Error is defined as the difference between set-point and measurement.

## Process

The **process** is the system that should be controlled. It is sometimes referred to as **plant** or **system**. The process should have at least one input to control its behavior and at least one output that is a measure of its behavior. Consider for example a gas heated house as process. The heater feed could be the process input and the measured room temperature the process output.

The process input is connected to the **controller output** or **controller variable (CV)**. It is mostly the input for an actuator that can drive the process to a desired setpoint.

The **process output** is commonly known as **process variable (PV)**, or measured variable (MV). Other names of the process output are system output and measurement.

## Error

The **error** is defined as the setpoint minus the process output. It is a measure for how much the process deviates from the desired setpoint, and thus how much the controller should respond to get the process back to the desired setpoint.

## Setpoint Weighting

For many controllers the controller input is equal to the error signal. Some controllers, however use specialized inputs for their proportional, integral and derivative parts (setpoint weighting). They have two inputs, one for the setpoint and one for the measured variable and are therefore also described as 2-DOF controllers.

## Gain

When we talk about the proportional action of a controller, we generally refer to the **proportional gain**. The action means that the controller moves in proportion to the error between setpoint (SP) and process output (PV):

$$\text{controller output} = K \cdot \text{error} = K \cdot (SP - PV)$$

where the gain is denoted by the parameter K. Many terms have been used by different manufacturers to designate this action. It has been called proportional gain, **gain**, throttling band, sensitivity and **proportional band**.

### Proportional Band

In practice, the controller output is limited, either by its own limitations or by the limitations of the corresponding actuator. Let  $u_{\max}$  and  $u_{\min}$  denote the minimum and maximum output of the controller. The proportional band of the controller is then defined as:

$$PB = \frac{u_{\max} - u_{\min}}{K} \cdot 100\%$$

In the ideal case, a controller can have an unlimited output. The **proportional band (PB)** is then defined as:

$$PB = \frac{1}{K} \cdot 100\%$$

This definition of proportional band is often used instead of the controller gain. The value is expressed in percent (%).

### Direct Acting / Reverse Acting

Suppose a process with a controller output CV and a process output PV is in steady state and kept to a certain setpoint SP. For proportional control the following equations can be found:

$$\begin{aligned} PV &= P(CV) \\ CV &= K \cdot \text{error} = K \cdot (SP - PV) \end{aligned}$$

where P is the process function that yields a measured variable as a result of the controller output. If the controller output decreases as the measured variable increases the controller is said to be **direct acting**. If the controller output increases as the measured variable increases, then it is called **reverse acting**. In other words, the controller is direct acting if the **gain K is positive** and reverse acting if the **gain K is negative**.

This is not only valid for proportional control, but for all PID controllers in the 20-sim library. If you need a reverse acting controller, simply use a negative gain.

### Offset

If you look at the equation for the proportional gain:

$$CV = K \cdot \text{error} = K \cdot (SP - PV)$$

you will notice that there has to be an error to produce a controller output. This means that with proportional control only, there will always be a small offset between the setpoint and the measured variable. To remove this offset, integral control has to be used.

With **integral** action, the controller output is proportional to the amount of time the error is present. Integral action eliminates offset that remains when proportional control is used.

$$\text{controller output} = (1/T_i) \cdot \text{int}(\text{error})$$

where the parameter  $T_i$  is called the **integral time**. Integral action is also known as reset and the parameter  $T_i$  as reset time.

Integral action gives the controller a large gain at low frequencies that results in eliminating offset. Integrals give information concerning the past. That is why integrals are always late. Integrals provide stability but have a tendency to get stuck in the past. In most controllers the proportional and integral action are combined. The output of the combined proportional and integral action (in s-domain) is then:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} \right) \cdot E$$

with  $E$  equal to  $SP - PV$ .

With **derivative** action, the controller output is proportional to the rate of change of the measurement or error. Some manufacturers use the term rate or pre-act instead of derivative. Derivative, rate and pre-act are the same thing. The controller output is calculated by the rate of change of the error with time.

$$\text{controller output} = T_d \cdot d(\text{error})/dt = T_d \cdot d(SP - PV)/dt$$

where the parameter  $T_d$  is called **derivative time**. Derivative control is mathematically the opposite of integral action, but while we might have an integral-only controller, we would never have a derivative-only controller. The reason for this is that derivative control only knows the error is changing. It does not know what the setpoint actually is.

Derivative action has the potential to improve performance when sudden changes in measured variable occur, but it should be used with care. It is mostly a matter of using enough, not too much.

### Derivative Gain Limitation

In most commercial processes sudden changes in process output may appear. In most cases a sudden change in the slope of such a process output cannot be avoided at all times. Using such a process output in controllers with pure derivative action, would lead to unwanted steps in the controller output. Moreover, high frequency noise in the measured signals may lead to unwanted large outputs of the controller.

To prevent this unwanted effect, the derivative action can be filtered by a first-order system with time constant  $T_d/N$ .

$$s \cdot K \cdot T_d \rightarrow \frac{s \cdot K \cdot T_d}{1 + s \cdot \frac{T_d}{N}}$$

This approximation acts as a derivative for low-frequency signal components. The gain, however, is limited to  $K \cdot N$ . This means that high-frequency measurement noise is amplified at most by a factor  $KN$ . This is why the parameter  $N$  is called the **derivative gain limitation**. Typical values of  $N$  are 8 to 20. Sometimes the reciprocal value of  $N$  is used, mostly with the name beta ( $\beta = 1/N$ ).

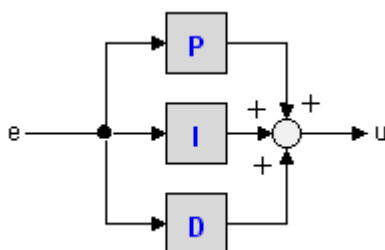
In literature various PID controller laws and types have been described. In industry two types prevail: the parallel form and the series form.

### Parallel Form

A PID controller in parallel form (also known as standard form, ISA form or non-interacting form), has the control equation:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} + s \cdot T_d \right) \cdot E$$

The controller actions (P, I and D) act independently as can be seen in the corresponding block diagram representation.

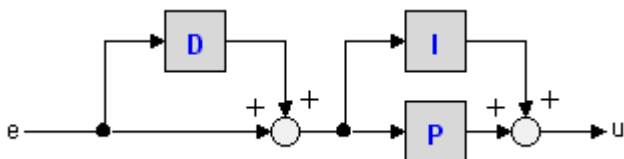


### Series Form

A PID controller in series form (also known as interacting form), has the control equation:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} \right) (1 + s \cdot T_d) \cdot E$$

The controller actions (P, I and D) act dependently as can be seen in the corresponding block diagram representation.



### Note

P and PI controllers are the same in series and parallel form.



Standard PID controller equations operate on the error signal (Error Based):

$$P - \text{action} : E_p = SP - PV$$

$$I - \text{action} : E_I = SP - PV$$

$$D - \text{action} : E_D = SP - PV$$

A more flexible structure is obtained by treating the setpoint (SP) and the process output (PV) separately (Setpoint Weighting):

$$P - \text{action} : E_p = b \cdot SP - PV$$

$$I - \text{action} : E_I = SP - PV$$

$$D - \text{action} : E_D = c \cdot SP - PV$$

The I-action always operates on the error to insure that the error between setpoint and process output will be minimized.

In most commercial controllers, the parameters b and c are chosen 1 or 0:

*b = 1 -> proportional control using the error: SP - PV (error feedback).*

*b = 0 -> only proportional control on the process output (PV).*

*c = 1 -> derivative control using the error: SP - PV (error feedback).*

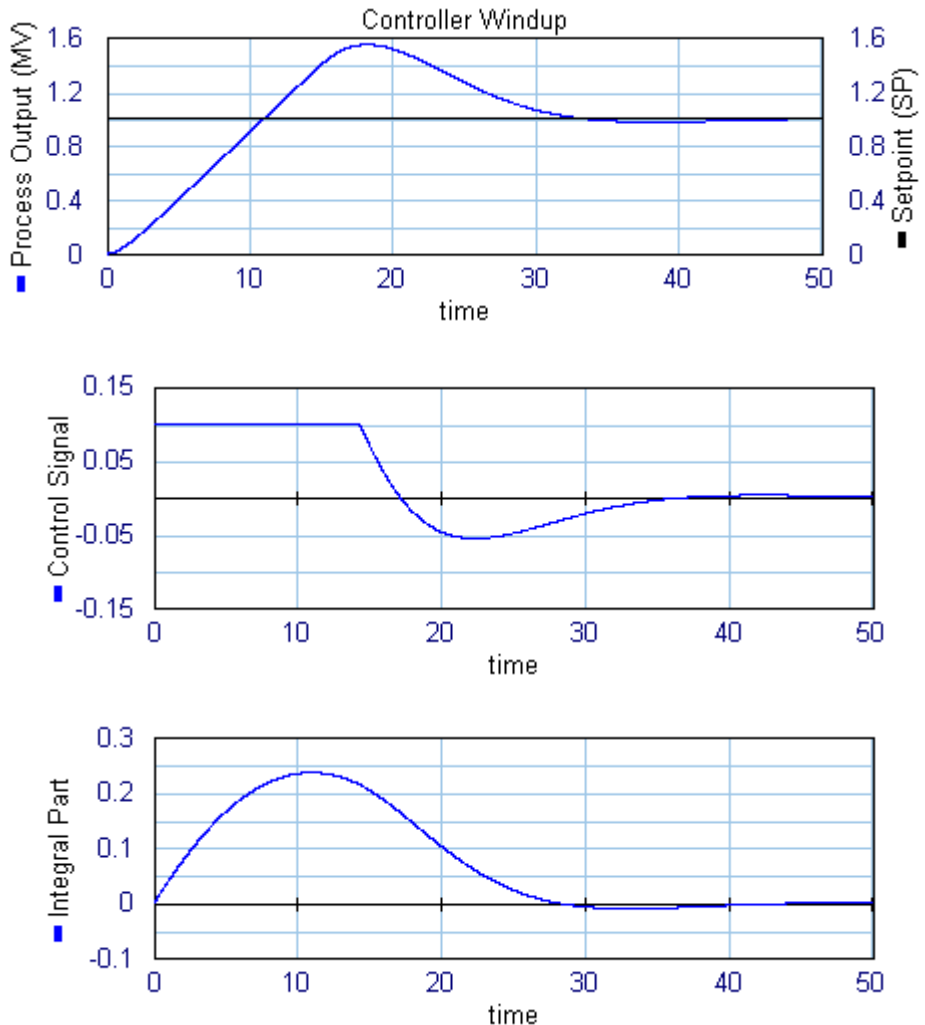
*c = 0 -> only derivative control on the process output (PV).*

All actuators have physical limitations, a control valve cannot be more than fully open or fully closed, a motor has limited velocity, etc. This has severe consequences for control. Integral action in a PID controller is an unstable mode. This does not cause any difficulties when the loop is closed. The feedback loop will, however, be broken when the actuator saturates because the output of the saturating element is then not influenced by its input. The unstable mode in the controller may then drift to very large values. When the actuator desaturates it may then take a long time for the system to recover. It may also happen that the actuator bounces several times between high and low values before the system recovers.

### Integrator windup

Integrator windup is illustrated in the figure below, which shows simulation of a system where the process dynamics is a saturation at a level of  $\pm 0.1$  followed by a linear system with the transfer function:

$$G(s) = \frac{1}{s(s+1)} \cdot x$$



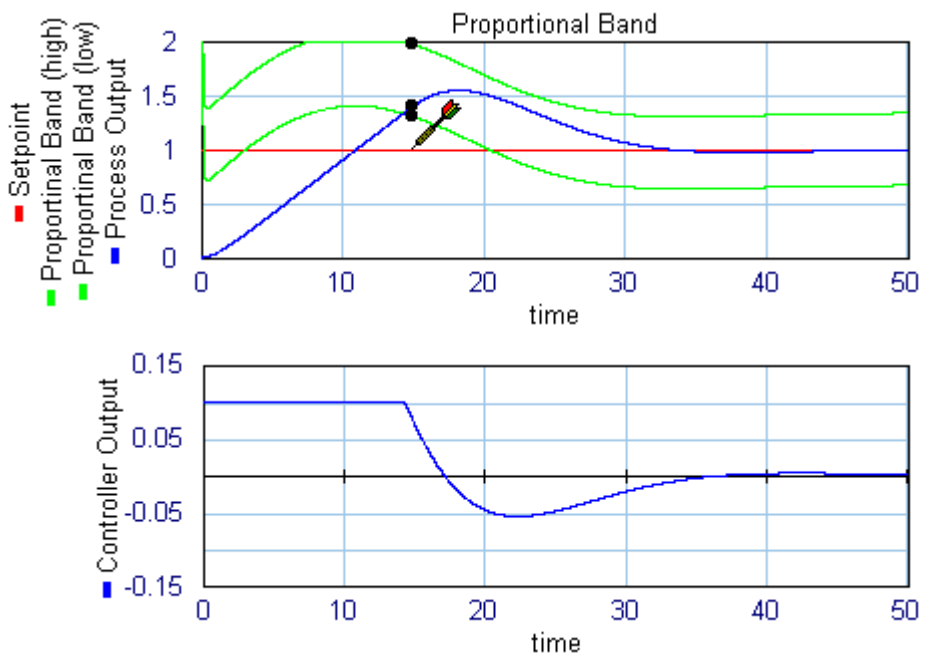
Because of the saturation in the actuator, the control signal saturates immediately when the step is applied. The control signal then remains in saturation level and the feedback is broken. The integral part continues to increase because the error ( $SP - PV$ ) is positive. The integral part starts to decrease when the process output (PV) has become larger than the setpoint (SP), but the process output remains saturated because of the large integral part. Slowly the process output decreases towards the setpoint.

The net effect is that there is a large overshoot. This phenomenon is called "integrator windup". A good insight in windup is found when looking at the proportional band.

## Proportional Band and Windup

The values of the process output that correspond to the minimum and maximum output are denoted as  $y_{\max}$  and  $y_{\min}$ . The controller operates linearly only if the process output is in the range  $(y_{\max}, y_{\min})$ . The controller output saturates when the process output is outside this band. A good insight into the windup problem is obtained by investigating the range  $(y_{\max}, y_{\min})$ . All 20-sim controller models in parallel form with anti-windup scheme, have the extra variables  $PB_{\text{high}}$  and  $PB_{\text{low}}$  which are equal to  $y_{\max}$  and  $y_{\min}$ .

An illustration of the proportional band is given below. The same linear system is used with the same controller. As can be seen, the actuator is saturated from  $t = 0$  until  $t = 14$ . At  $t = 14$  the process output enters the range  $(PB_{\text{high}}, PB_{\text{low}})$  and controller feedback is regained.

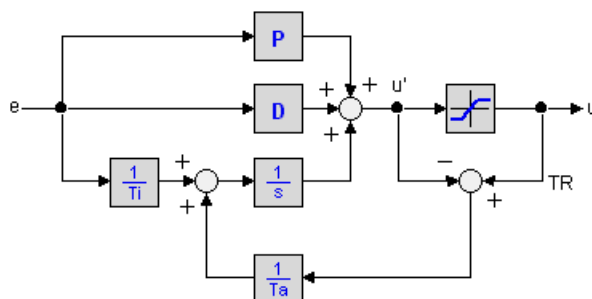


## Anti-Windup

Integrator windup can be avoided, by making sure that the integral is kept to a proper value when the actuator saturates, so that the controller is ready to resume action, as soon as the control error changes. This anti-windup scheme is known as tracking or back calculation.

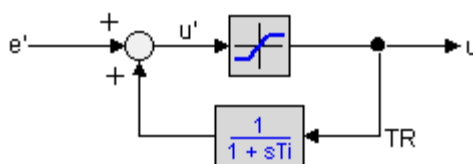
### parallel form

As well known form of tracking is linear feedback anti windup. It is shown in the figure below (parallel form). The actuator is represented by a signal limiter. The difference between actuator input and output (TR) is fed back to the integrator through the gain  $1/T_a$ . As soon as the limiter saturates, this signal becomes non-zero and prevents the integrator from winding up. The tracking time constant  $T_a$  can be used to tune then amount of anti windup.



### series form

The same scheme can also be used for controllers with a series form. A diagram is shown below.

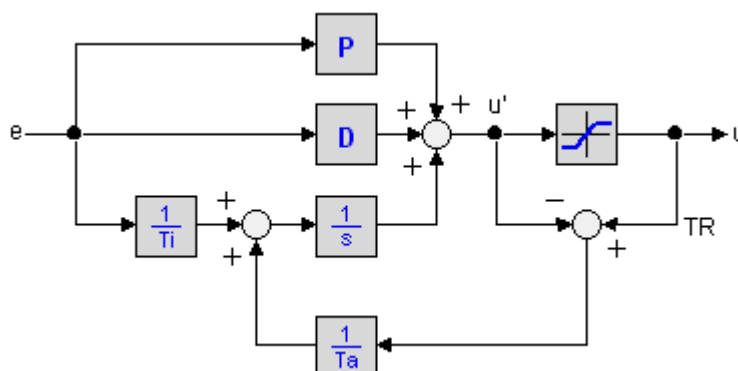


### Tracking Time constant

To prevent the integrator from saturating, the tracking time constant must be chosen small. Too small values, however decrease the controller performance. As a rule of thumb Åström suggested to choose the tracking time constant  $T_d \leq T_a \leq T_i$ . Some authors prefer a good controller performance and suggest to choose  $T_a = T_i$ .

### External Tracking

As long as the actuator output is equal to the controller output, anti-windup scheme will not be activated and the controller is in normal operation (*control mode*). When the actuator saturates, the anti-windup scheme will be activated and prevent the controller output from wandering away. In effect the anti-windup scheme matches the controller output and actuator output. This is why the actuator output is also known as the tracking signal (TR).

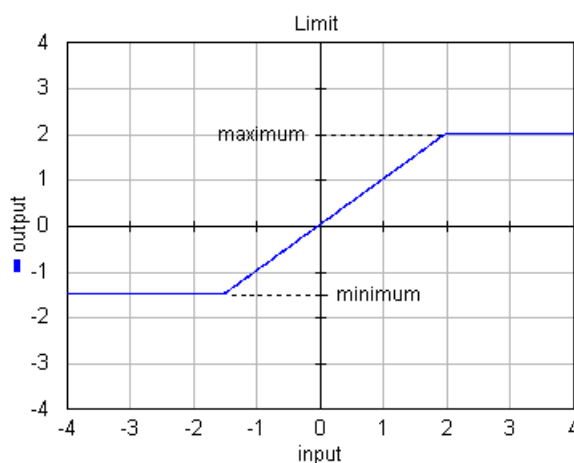


When an external actuator signal is used (external tracking signal) it is important to compensate for the actuator gain. Otherwise the tracking signal is not equal to the controller output, during normal operation and the anti-windup scheme is activated.

## Actuator Model

Anti-windup schemes are based on the difference between actuator input (controller output) and actuator output. These signals are not always available. Therefore an actuator model can be used inside the controller to yield this difference. In the library models, a signal limiter is used the actuator model:

*output = minimum; (input < minimum)*  
*output = input; (minimum ≤ input ≤ maximum)*  
*output = maximum (input > maximum)*



The output of PID controllers at time 0 depends on the given setpoint (SP), process output (PV) and control law. In general the process will not be at rest ( $PV \neq 0$ ) and the setpoint will not be equal to the process output ( $SP \neq PV$ ). This will result in an undesired step in the controller signal at startup. Even if the setpoint is equal to the process output ( $SP = PV$ ) at startup, the use of setpoint weighting may result in a step in the control signal:

$$P - \text{action} : E_p = b \cdot SP - PV$$

$$I - \text{action} : E_I = SP - PV$$

$$D - \text{action} : E_D = c \cdot SP - PV$$

Let PV be a non zero value and b or c equal to zero. The P or D -action will then lead to a step in the control signal.

To avoid such a step, the *initial output* of some PID-controllers can be set to any value. The slope of the the control output of these controllers at startup is equal to zero.

### Initial output for with delays

Controllers with manual output at start-up, use the process output at  $t = 0$ ,  $PV(0)$ , to calculate an internal offset that compensates for the initial controller output. Care should be taken when delays are available between the process output and the controller input. Due to these, the measured process output at  $t = 0$  in the controller ( $PV(0)'$ ) may not be the same as the real process output at  $t = 0$  ( $PV(0)$ ). As a result, a wrong offset will be calculated and the initial output will not have the desired value. To avoid this, all initial values of delay elements between the process and controller should be chosen properly (e.g. equal to the initial process output) !

According to b Åström the table below summarizes the properties of some commercial controllers.

Controller	Structure	Setpoint Weighting b	Setpoint Weighting c	Derivative Gain Limitation N	Sampling Periods
1. Allen Bradley PLC 5	P	1.0	1.0	None	Load dependent 0.25 0.1, 0.25 or 1.0 0.2 0.1 0.25 0.33, 0.5 or 1.0 0.1 0.2 0.25 0.2 0.036 – 1.56 0.1
2. Baliley Net 90	P	0.0 or 1.0	0.0 or	10	
3. Fisher Controls Provox	S	1.0	1.0	8	
4. Fisher Controls DPR	S	0.0	0.0	8	
900,910	S	1.0	0.0	none	
5. Fisher Porter Micro	S	1.0	0.0 or	10	
DCI	S	1.0	1.0	8	
6. Foxboro Model 761	S	1.0	0.0	1-30	
7. Honeywell TDC	S	0.0	1.0	8	
8. Moore Products Type	S	0.0 or 1.0	0.0	17 or 20	
352	S	1.0	0.0	3.3 – 10	
9. Alfa Laval ECA40,	S	1.0	0.0	none	
ECA 400	P	0.0 or 1.0	1.0	10	
10. Taylor Mod 30			1.0		
11. Toshiba TOSDIC 200			0.0 or		
12. Turnbull TCS 6000			1.0		
13. Yokogawa SLPC					

1. K.J. Astrom, T. Hagglund, Pid Controllers, Instrument Society of America; ISBN: 1556175167, (1995), (available at [www.amazon.com](http://www.amazon.com))
2. B.G. Liptak, Instrument Engineers' Handbook, Volume 1: Process Measurement, CRC Pr; ISBN: 0801981972, (2000), (available at [www.amazon.com](http://www.amazon.com)).
3. B.G. Liptak, Instrument Engineers' Handbook, Volume 2: Process Control, CRC Pr; ISBN: 0801982421, (2000), (available at [www.amazon.com](http://www.amazon.com)).
4. G.K. McMillan, D.M. Considine, Process/Industrial Instruments and Controls Handbook, McGraw Hill Text, ISBN: 0070125821, (1999), (available at [www.amazon.com](http://www.amazon.com)).
5. B. Wittenmark, K.J. Astrom, Computer-Controlled Systems: Theory and Design, Prentice Hall; ISBN: 0133148998, (1996), (available at [www.amazon.com](http://www.amazon.com)).

Expert information can also be found in the [sci.eng.control](http://sci.eng.control) newsgroup. An exelent frequently asked questions list can be found on the internet pages of Ron Graham (<http://www.tcnj.edu/~rgraham/PID-tuning.html>).

Two types of PID-controllers are available in this library. The first type of controllers use an **error** input and the second type of controllers use separate Setpoint (**SP**) and Measured Variable (**MV**) input.

### Error Input

PID-Controllers with the error as a direct input signal, are all in series form. The name simply denotes the type of controller: P, PI, PD or PID. Two versions of each controller exists: continuous time and discrete time. They can be found in the subdirectories Continuous and Discrete.

### Ports

All controllers have one input ports and one output port:

1. *error*: The error between setpoint and measured variable.
2. *output*: The controller output.

### Parameters

Depending on the type of controller, the following parameters can be used:

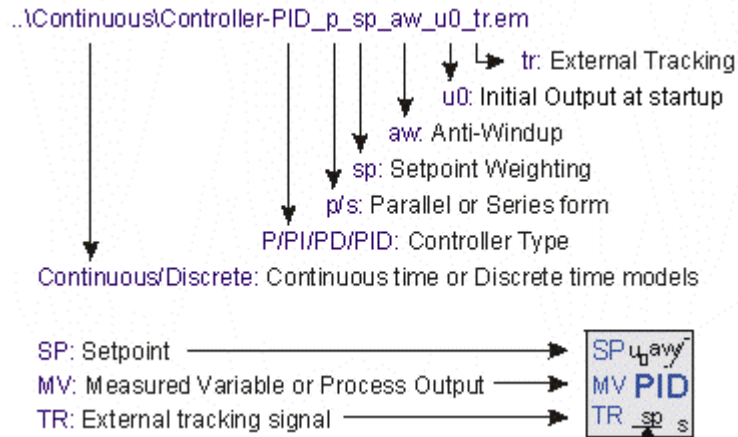
1. *kd*: The proportional gain of the controller.
2. *tauD*: The derivative time constant.
3. *beta*: The reciprocal derivative gain limitation.
4. *tauI*: The integral time constant.

### Controller Wizard

A special form of controllers with error input is generated by the ControllerWizard.emx submodel. When you select this model and click **Go Down** the Filter Editor is opened, allowing you to specify controllers with frequency oriented parameters.

## Separate Input

Controllers with separate inputs come in many forms. The naming denotes the type of controller and the options that are available. The type and options are also available in the model icons.



- Two versions of each controller exists: continuous time and discrete time. They can be found in the subdirectories *Continuous* and *Discrete*. Continuous-time controllers have icons with blue text and discrete-time controllers have icons with green text.
- The first characters denote the type of controller: *P*, *PD*, *PI* or *PID*.
- The character *p* or *s* denote the form: parallel (*p*) or series (*p*).
- If setpoint weighting is used, the term *sp* is added.
- If an anti-windup scheme is incorporated, the term *aw* is added.
- If the output at startup can be set manually, the term *u0* is added.
- If an external tracking signal is used, the term *tr* is added.

## Ports

All controllers have two inputs ports and one output port:

- SP*: The setpoint
- MV*: The measured variable (also called process variable).
- output*: The controller output.

## Parameters

Depending on the type of controllers, the following parameters can be used:

- K*: The proportional gain of the controller.
- Td*: The derivative time constant.



3. *N*: The derivative gain limitation.
4. *Ti*: The integral time constant.
5. *b*: The setpoint weighting constant for the proportional part of the controller.
6. *c*: The setpoint weighting constant for the derivative part of the controller.
7. *Ta*: The tracking time constant of the anti-windup scheme.
8. *minimum*: The minimum controller output representing actuator saturation.
9. *maximum*: The maximum controller output representing actuator saturation.
10. *output\_initial*: The controller output at start-up.

### Initial Values

Although most controllers have one or more internal states, the initial values of these states do not need to be set manually. You use the default values (0) at the start of a simulation. To get a desired output of the controller at startup, the parameter *output\_initial* should be used.

### Discrete Controllers

The discrete controllers that are available in the library are directly derived from their continuous counterparts, using approximation by backward differences. These discrete models have identical behavior, as long as the sample time is not chosen too low. Discrete loops in 20-sim are automatically detected and assigned a default sampletime. You can change the sample time in the Run Properties Editor (in the **Simulator** from the **Properties** menu select the **Simulation** command).

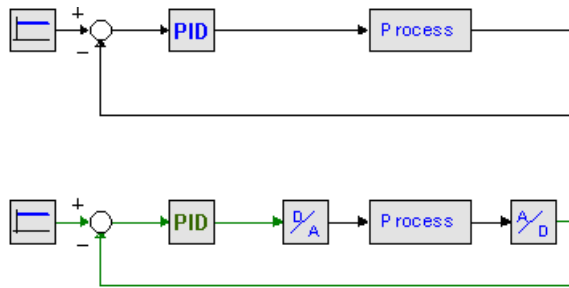
### Variables

Some PID controllers (parallel form with anti-windup) have two internal variables that are of interest. *PB\_high* and *PB\_low*. These parameters are the upper and lower bound of the proportional band.

All controllers must can be used as shown in the figure below. The upper part shows a continuous time controller and the bottom part shows a discrete time controller.

### Error Input

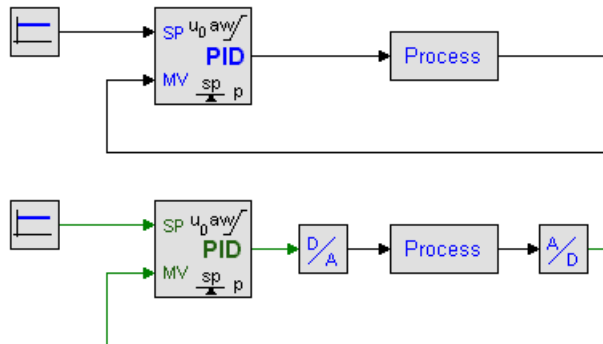
1. An error signal is generated with a plus minus element. Its serves as an input of the controller.
2. The controller output is connected with the process input.



As shown in the figure, analog to digital convertors and digital to analog convertors should be used, when connecting a discrete-time controller to a continuous-time process.

### Separate Input

1. A setpoint signal is connected with the **SP** port of the controller.
2. The process output is connected with the **PV** port of the controller.
3. The controller output is connected with the process input.



As shown in the figure, analog to digital convertors and digital to analog convertors should be used, when connecting a discrete-time controller to a continuous-time process.

### Library

Signal\Control\PID Control\Continuous

### Use

**Domains:** Continuous, Discrete **Size:** 1-D. **Kind:** Block Diagrams.

### Description

A special form of controllers with error input is generated by the ControllerWizard.emx submodel. When you select this model and click **Go Down** the Filter Editor is opened, allowing you to specify controllers with frequency oriented parameters.

## Interface

### Inputs

u

### Description

The error input signal: plant-output minus set point.

### Outputs

y

Output signal: input for the plant.

### Parameters

Look in the Filter Editor helpfile to find a detailed description of the possible controller types and their parameters.

## Library

Signal\Control\PID Control\Continuous

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a P controller. The output of this controller (in s-domain) is:

$$U = K \cdot E$$

with E equal to SP - PV.

## Interface

### Inputs

SP

### Description

Setpoint.

PV

Process output.

### Outputs

CV

Controller output: input for the process.

### Parameters

K

Proportional gain.

## Library

Signal\Control\PID Control\Continuous

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PD controller in parallel form. The output of this controller (in s-domain) is:

$$U = K \cdot \left( 1 + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \right) \cdot E$$

with E equal to SP - MV.

### Interface

#### Inputs

SP

MV

#### Description

Setpoint.

Measured variable or process output.

#### Outputs

output

Controller output: input for the process.

#### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

#### Initial Values

yes

Should be left default!

### Library

Signal\Control\PID Control\Continuous

#### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

#### Description

This is a PD controller in series form. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \right) \cdot E$$

with E equal to SP - MV.

### Interface

#### Inputs

SP

MV

#### Description

Setpoint.

Measured variable or process output.

**Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Library**

Signal\Control\PID Control\Continuous

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PI controller. The output of this controller (in s-domain) is:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} \right) \cdot E$$

with E equal to SP - MV.

**Interface****Inputs**

SP	Setpoint.
MV	Measured variable or process output.

**Description****Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Ti	Integral time constant ( $T_i > 0$ ).

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Library**

Signal\Control\PID Control\Continuous

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PI controller with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) \right)$$

**Interface****Inputs**

SP

**Description**

Setpoint.

MV

Measured variable or process output.

**Outputs**

output

Controller output: input for the process.

**Parameters**

K

Proportional gain.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

**Initial Values**

yes

Should be left default!

**Library**

Signal\Control\PID Control\Continuous

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PI controller with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) \right)$$

An anti-windup scheme has been added to this controller.

## Interface

### Inputs

SP

### Description

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

Ta

Tracking time constant.

minimum

Minimum controller output.

maximum

Maximum controller output.

### Initial Values

yes

Should be left default!

### Interesting Variables

PB\_high, PB\_low

Upper and lower bound of the proportional band.

## Library

Signal\Control\PID Control\Continuous

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PI controller with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up.

## Interface

### Inputs

SP

### Description

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

**Parameters**

K	Proportional gain.
Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.
Ta	Tracking time constant.
minimum	Minimum controller output.
maximum	Maximum controller output.
output_initial	The controller output at start-up.

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Interesting Variables**

PB_high, PB_low	Upper and lower bound of the proportional band.
-----------------	---

**Library**

Signal\Control\PID Control\Continuous

**Use**

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This is a PI controller with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up. An external tracking signal must be supplied to activate the anti-windup scheme.

**Interface****Inputs**

SP	Setpoint.
MV	Measured variable or process output.
TR	Tracking signal.

**Description****Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Ti	Integral time constant ( $T_i > 0$ ).



b	Proportional setpoint weighting parameter.
Ta	Tracking time constant.
output_initial	The controller output at start-up.

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Interesting Variables**

PB_high, PB_low	Upper and lower bound of the proportional band.
-----------------	---

**Library**

Signal\Control\PID Control\Continuous

**Use**

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This is a PID controller in parallel form. The output of this controller (in s-domain) is:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \right) \cdot E$$

with E equal to SP - MV.

**Interface****Inputs**

SP	Setpoint.
MV	Measured variable or process output.

**Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.
Ti	Integral time constant ( $T_i > 0$ ).

**Initial Values**

yes

Should be left default!

**Library**

Signal\Control\PID Control\Continuous

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PID controller in parallel form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot Ti} \cdot (SP - MV) + \frac{s \cdot Td}{1 + s \cdot \frac{Td}{N}} \cdot (c \cdot SP - MV) \right)$$

**Interface****Inputs**

SP

MV

**Description**

Setpoint.

Measured variable or process output.

**Outputs**

output

Controller output: input for the process.

**Parameters**

K

Td

N

Ti

b

c

Proportional gain.

Derivative time constant ( $T_d > 0$ ).

Derivative gain limitation.

Integral time constant ( $T_i > 0$ ).

Proportional setpoint weighting parameter.

Derivative setpoint weighting parameter.

**Initial Values**

yes

Should be left default!

**Interesting Variables**

PB\_high, PB\_low

Upper and lower bound of the proportional band.

## Library

Signal\Control\PID Control\Continuous

## Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PID controller in parallel form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot (c \cdot SP - MV) \right)$$

An anti-windup scheme has been added to this controller.

## Interface

### Inputs

SP

### Description

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

c

Derivative setpoint weighting parameter.

Ta

Tracking time constant.

minimum

Minimum controller output.

maximum

Maximum controller output.

### Initial Values

yes

Should be left default!

### Interesting Variables

PB\_high, PB\_low

Upper and lower bound of the proportional band.

## Library

Signal\Control\PID Control\Continuous

## Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PID controller in parallel form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot (c \cdot SP - MV) \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up.

## Interface

### Inputs

SP

### Description

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

c

Derivative setpoint weighting parameter.

Ta

Tracking time constant.

minimum

Minimum controller output.

maximum

Maximum controller output.

output\_initial

The controller output at start-up.

### Initial Values

yes

Should be left default!

### Interesting Variables

PB\_high, PB\_low

Upper and lower bound of the proportional band.

## Library

Signal\Control\PID Control\Continuous

## Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PID controller in parallel form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot (c \cdot SP - MV) \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up. An external tracking signal must be supplied to activate the anti-windup scheme.

## Interface

### Inputs

SP	Setpoint.
MV	Measured variable or process output.
TR	Tracking signal.

### Description

### Outputs

output	Controller output: input for the process.
--------	---

### Parameters

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.
Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.
c	Derivative setpoint weighting parameter.
Ta	Tracking time constant.
output_initial	The controller output at start-up.

### Initial Values

yes	Should be left default!
-----	-------------------------

### Interesting Variables

PB_high, PB_low	Upper and lower bound of the proportional band.
-----------------	---

**Library**

Signal\Control\PID Control\Continuous

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PID controller in series form. The output of this controller (in s-domain) is:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} \right) \left( \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \right) \cdot E$$

with E equal to SP - MV.

**Interface****Inputs**

SP

MV

**Description**

Setpoint.

Measured variable or process output.

**Outputs**

output

Controller output: input for the process.

**Parameters**

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).**Initial Values**

yes

Should be left default!

**Library**

Signal\Control\PID Control\Continuous

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PID controller in series form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \left( b + \frac{1}{s \cdot T_i} \right) \cdot \frac{1 + s \cdot c \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot SP - \left( 1 + \frac{1}{s \cdot T_i} \right) \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot MV \right)$$

## Interface

### Inputs

SP

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

c

Derivative setpoint weighting parameter.

### Initial Values

yes

Should be left default!

## Library

Signal\Control\PID Control\Continuous

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PID controller in series form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \left( b + \frac{1}{s \cdot T_i} \right) \cdot \frac{1 + s \cdot c \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot SP - \left( 1 + \frac{1}{s \cdot T_i} \right) \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot MV \right)$$

An anti-windup scheme has been added to this controller.

## Interface

### Inputs

SP

### Description

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

c

Derivative setpoint weighting parameter.

Ta

Tracking time constant.

minimum

Minimum controller output.

maximum

Maximum controller output.

### Initial Values

yes

Should be left default!

## Library

Signal\Control\PID Control\Continuous

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PID controller in series form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \left( b + \frac{1}{s \cdot T_i} \right) \cdot \frac{1 + s \cdot c \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot SP - \left( 1 + \frac{1}{s \cdot T_i} \right) \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot MV \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up.

## Interface

### Inputs

### Description



SP	Setpoint.
MV	Measured variable or process output.

**Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.
Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.
c	Derivative setpoint weighting parameter.
Ta	Tracking time constant.
minimum	Minimum controller output.
maximum	Maximum controller output.
output_initial	The controller output at start-up.

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Library**

Signal\Control\PID Control\Continuous

**Use**

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This is a PID controller in series form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \left( b + \frac{1}{s \cdot T_i} \right) \cdot \frac{1 + s \cdot c \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot SP - \left( 1 + \frac{1}{s \cdot T_i} \right) \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot MV \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up. An external tracking signal must be supplied to activate the anti-windup scheme.

**Interface****Inputs**

SP

**Description**

Setpoint.

MV	Measured variable or process output.
TR	Tracking signal.

### Outputs

output	Controller output: input for the process.
--------	---

### Parameters

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.
Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.
c	Derivative setpoint weighting parameter.
Ta	Tracking time constant.
output_initial	The controller output at start-up.

### Initial Values

yes	Should be left default!
-----	-------------------------

## Library

Signal\Control\PID Control\Continuous

### Use

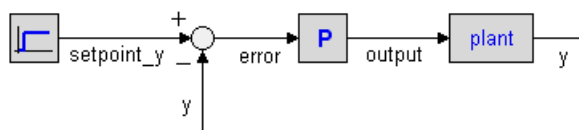
**Domains:** Continuous, Discrete **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a P controller. The output of this controller is:

$$\text{output} = k_p \cdot \text{error}$$

with the input of the controller equal to the error and the output of the controller used as the plant input:



## Interface

### Inputs

error

### Description

Input signal: plant-output minus set point.



## Library

Signal\Control\PID Control\Continuous

## Use

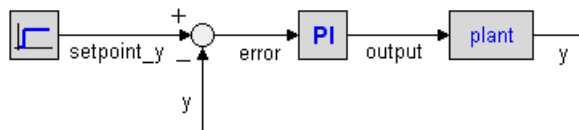
**Domains:** Continuous, Discrete **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PI controller. The transfer function of the controller is:

$$G(s) = k_p + \frac{k_p}{s \cdot \tau_{auI}}$$

with the input of the controller equal to the error and the output of the controller used as the plant input:



## Interface

### Inputs

error

### Description

Input signal: plant-output minus set point.

### Outputs

output

Output signal: input for the plant.

### Parameters

$k_p$

Proportional gain.

$\tau_{auI}$

Integral gain ( $\tau_{auI} < > 0$ ).

### Initial Values

$state(0)$

$output(0) = state(0) - k_p \cdot error(0)$

## Library

Signal\Control\PID Control\Continuous

## Use

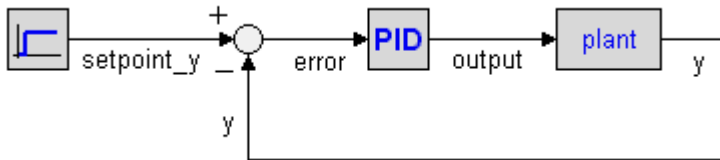
**Domains:** Continuous, Discrete **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PID controller in series form. The transfer function is:

$$G(s) = k_p \cdot \left( 1 + \frac{1}{s \cdot \tau_{auI}} \right) \left( \frac{1 + s \cdot \tau_{auD}}{1 + s \cdot \beta \cdot \tau_{auD}} \right)$$

with the input of the controller equal to the error and the output of the controller used as the plant input:



## Interface

### Inputs

error

### Description

Input signal: plant-output minus set point.

### Outputs

output

Output signal: input for the plant.

### Parameters

$k_p$

Proportional gain.

$\tau_{auD}$

Derivative gain ( $\tau_{auD} < > 0$ ).

$\tau_{auI}$

Integral gain ( $\tau_{auI} < > 0$ ).

$\beta$

Tameness constant ( $0 < \beta < 1$ ).

### Initial Values

$pdstate(0)$

$pdout(0) = pdstate(0) - k_p \cdot error(0) / \beta$

$pistate(0)$

$output(0) = pistate(0) - pdout(0)$

Two types of PID-controllers are available in this library. The first type used an error input and the second type of controller use separate setpoint and Measured Variable input. Both types use the same internal description, so the use is just a question of flavor.

## Error Input

PID-Controllers with the error as a direct input signal, are all in series form. The name simply denotes the type of controller: P, PI, PD or PID. Two versions of each controller exists: continuous time and discrete time. They can be found in the subdirectories Continuous and Discrete.

## Ports

All controllers have one input ports and one output port:

1. *error*: The error between setpoint and measured variable.

2. *output*: The controller output.

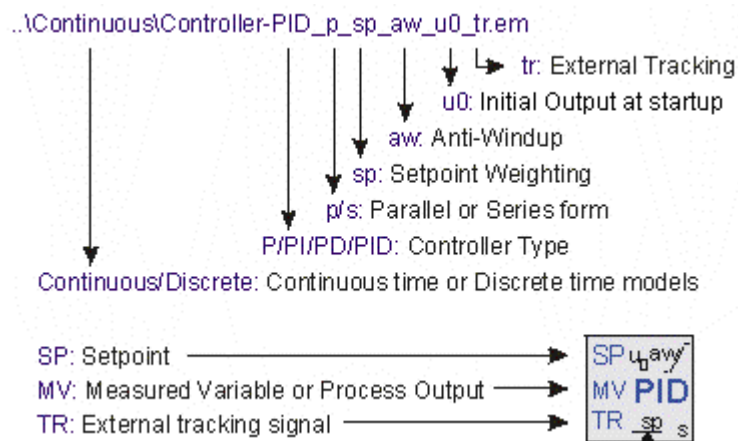
### Parameters

Depending on the type of controller, the following parameters can be used:

1. *kd*: The proportional gain of the controller.
2. *tauD*: The derivative time constant.
3. *beta*: The reciprocal derivative gain limitation.
4. *tauI*: The integral time constant.

### Separate Input

Controllers with separate inputs come in many forms. The naming denotes the type of controller and the options that are available. The type and options are also available in the model icons.



1. Two versions of each controller exists: continuous time and discrete time. They can be found in the subdirectories *Continuous* and *Discrete*. Continuous-time controllers have icons with blue text and discrete-time controllers have icons with green text.
2. The first characters denote the type of controller: *P*, *PD*, *PI* or *PID*.
3. The character *p* or *s* denote the form: parallel (*p*) or series (*p*).
4. If setpoint weighting is used, the term *sp* is added.
5. If an anti-windup scheme is incorporated, the term *aw* is added.
6. If the output at startup can be set manually, the term *u0* is added.
7. If an external tracking signal is used, the term *tr* is added.

### Ports

All controllers have two inputs ports and one output port:

1. *SP*: The setpoint
2. *MV*: The measured variable (also called process variable).
3. *output*: The controller output.

### Parameters

Depending on the type of controllers, the following parameters can be used:

1. *K*: The proportional gain of the controller.
2. *Td*: The derivative time constant.
3. *N*: The derivative gain limitation.
4. *Ti*: The integral time constant.
5. *b*: The setpoint weighting constant for the proportional part of the controller.
6. *c*: The setpoint weighting constant for the derivative part of the controller.
7. *Ta*: The tracking time constant of the anti-windup scheme.
8. *minimum*: The minimum controller output representing actuator saturation.
9. *maximum*: The maximum controller output representing actuator saturation.
10. *output\_initial*: The controller output at start-up.

### Initial Values

Although most controllers have one or more internal states, the initial values of these states do not need to be set manually. You use the default values (0) at the start of a simulation. To get a desired output of the controller at startup, the parameter *output\_initial* should be used.

### Discrete Controllers

The discrete controllers that are available in the library are directly derived from their continuous counterparts, using approximation by backward differences. These discrete models have identical behavior, as long as the sample time is not chosen too low. Discrete loops in 20-sim are automatically detected and assigned a default sampletime. You can change the sample time in the Run Properties Editor (in the **Simulator** from the **Properties** menu select the **Simulation** command).

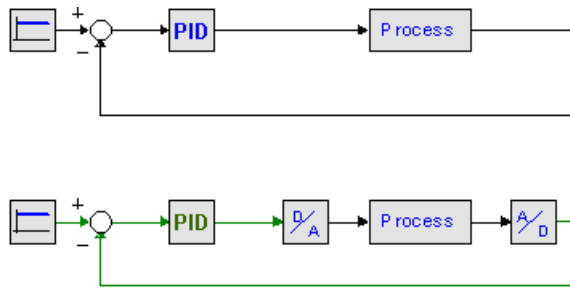
### Variables

Some PID controllers (parallel form with anti-windup) have two internal variables that are of interest. *PB\_high* and *PB\_low*. These parameters are the upper and lower bound of the proportional band.

All controllers must can be used as shown in the figure below. The upper part shows a continuous time controller and the bottom part shows a discrete time controller.

### Error Input

1. An error signal is generated with a plus minus element. Its serves as an input of the controller.
2. The controller output is connected with the process input.

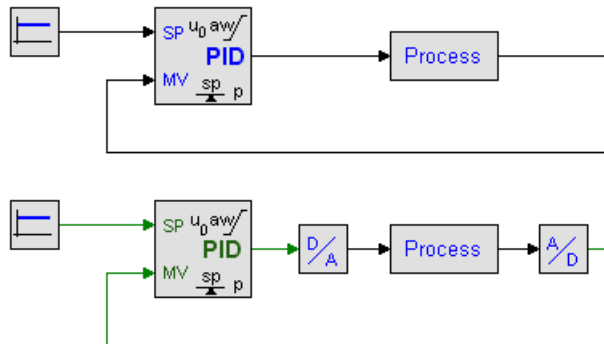


As shown in the figure, analog to digital convertors and digital to analog convertors should be used, when connecting a discrete-time controller to a continuous-time process.

### Separate Input

1. A setpoint signal is connected with the **SP** port of the controller.
2. The process output is connected with the **PV** port of the controller.

The controller output is connected with the process input.



As shown in the figure, analog to digital convertors and digital to analog convertors should be used, when connecting a discrete-time controller to a continuous-time process.

### Library

Signal\Control\PID Control\Discrete

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a P controller. The output of this controller (in s-domain) is:

$$U = K \cdot E$$

with E equal to SP - PV.



## Interface

### Inputs

SP

PV

### Description

Setpoint.

Process output.

### Outputs

CV

Controller output: input for the process.

### Parameters

K

Proportional gain.

## Library

Signal\Control\PID Control\Discrete

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PD controller in parallel form. The output of this controller (in s-domain) is:

$$U = K \cdot \left( 1 + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \right) \cdot E$$

with E equal to SP - MV.

## Interface

### Inputs

SP

MV

### Description

Setpoint.

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

### Initial Values

yes

Should be left default!

**Library**

Signal\Control\PID Control\Discrete

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PD controller in series form. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \right) \cdot E$$

with E equal to SP - MV.

**Interface****Inputs**

SP

MV

**Description**

Setpoint.

Measured variable or process output.

**Outputs**

output

Controller output: input for the process.

**Parameters**

K

Td

N

Proportional gain.

Derivative time constant ( $T_d > 0$ ).

Derivative gain limitation.

**Initial Values**

yes

Should be left default!

**Library**

Signal\Control\PID Control\Discrete

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PI controller. The output of this controller (in s-domain) is:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} \right) \cdot E$$

with E equal to SP - MV.

## Interface

### Inputs

SP

MV

### Description

Setpoint.

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Ti

Integral time constant ( $T_i > 0$ ).

### Initial Values

yes

Should be left default!

## Library

Signal\Control\PID Control\Discrete

## Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PI controller with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) \right)$$

## Interface

### Inputs

SP

MV

### Description

Setpoint.

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Library**

Signal\Control\PID Control\Discrete

**Use**

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This is a PI controller with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) \right)$$

An anti-windup scheme has been added to this controller.

**Interface****Inputs**

SP	Setpoint.
MV	Measured variable or process output.

**Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.
Ta	Tracking time constant.
minimum	Minimum controller output.
maximum	Maximum controller output.

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Interesting Variables**

PB_high, PB_low	Upper and lower bound of the proportional band.
-----------------	---

## Library

Signal\Control\PID Control\Discrete

## Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PI controller with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up.

## Interface

### Inputs

SP

### Description

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

Ta

Tracking time constant.

minimum

Minimum controller output.

maximum

Maximum controller output.

output\_initial

The controller output at start-up.

### Initial Values

yes

Should be left default!

### Interesting Variables

PB\_high, PB\_low

Upper and lower bound of the proportional band.

## Library

Signal\Control\PID Control\Discrete

## Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PI controller with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up. An external tracking signal must be supplied to activate the anti-windup scheme.

## Interface

### Inputs

SP	Setpoint.
MV	Measured variable or process output.
TR	Tracking signal.

### Description

### Outputs

output	Controller output: input for the process.
--------	---

### Parameters

K	Proportional gain.
Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.
Ta	Tracking time constant.
output_initial	The controller output at start-up.

### Initial Values

yes	Should be left default!
-----	-------------------------

### Interesting Variables

PB_high, PB_low	Upper and lower bound of the proportional band.
-----------------	---

**Library**

Signal\Control\PID Control\Discrete

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PID controller in parallel form. The output of this controller (in s-domain) is:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \right) \cdot E$$

with E equal to SP - MV.

**Interface****Inputs**

SP

MV

**Description**

Setpoint.

Measured variable or process output.

**Outputs**

output

Controller output: input for the process.

**Parameters**

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).**Initial Values**

yes

Should be left default!

**Library**

Signal\Control\PID Control\Discrete

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a PID controller in parallel form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot (c \cdot SP - MV) \right)$$

## Interface

### Inputs

SP

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

c

Derivative setpoint weighting parameter.

### Initial Values

yes

Should be left default!

### Interesting Variables

PB\_high, PB\_low

Upper and lower bound of the proportional band.

## Library

Signal\Control\PID Control\Discrete

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PID controller in parallel form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot (c \cdot SP - MV) \right)$$

An anti-windup scheme has been added to this controller.



## Interface

### Inputs

SP

### Description

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

c

Derivative setpoint weighting parameter.

Ta

Tracking time constant.

minimum

Minimum controller output.

maximum

Maximum controller output.

### Initial Values

yes

Should be left default!

### Interesting Variables

PB\_high, PB\_low

Upper and lower bound of the proportional band.

## Library

Signal\Control\PID Control\Discrete

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PID controller in parallel form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot (c \cdot SP - MV) \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up.

## Interface

### Inputs

SP

### Description

Setpoint.

MV

Measured variable or process output.

### Outputs

output

Controller output: input for the process.

### Parameters

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

c

Derivative setpoint weighting parameter.

Ta

Tracking time constant.

minimum

Minimum controller output.

maximum

Maximum controller output.

output\_initial

The controller output at start-up.

### Initial Values

yes

Should be left default!

### Interesting Variables

PB\_high, PB\_low

Upper and lower bound of the proportional band.

## Library

Signal\Control\PID Control\Discrete

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PID controller in parallel form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( (b \cdot SP - MV) + \frac{1}{s \cdot T_i} \cdot (SP - MV) + \frac{s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot (c \cdot SP - MV) \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up. An external tracking signal must be supplied to activate the anti-windup scheme.

## Interface

### Inputs

SP	Setpoint.
MV	Measured variable or process output.
TR	Tracking signal.

### Outputs

output	Controller output: input for the process.
--------	---

### Parameters

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.
Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.
c	Derivative setpoint weighting parameter.
Ta	Tracking time constant.
output_initial	The controller output at start-up.

### Initial Values

yes	Should be left default!
-----	-------------------------

### Interesting Variables

PB_high, PB_low	Upper and lower bound of the proportional band.
-----------------	---

## Library

Signal\Control\PID Control\Discrete

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PID controller in series form. The output of this controller (in s-domain) is:

$$U = K \cdot \left( 1 + \frac{1}{s \cdot T_i} \right) \left( \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \right) \cdot E$$

with E equal to SP - MV.

## Interface

### Inputs

### Description

SP	Setpoint.
MV	Measured variable or process output.

**Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.
Ti	Integral time constant ( $T_i > 0$ ).

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Library**

Signal\Control\PID Control\Discrete

**Use**

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This is a PID controller in series form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \left( b + \frac{1}{s \cdot T_i} \right) \cdot \frac{1 + s \cdot c \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot SP - \left( 1 + \frac{1}{s \cdot T_i} \right) \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot MV \right)$$

**Interface****Inputs**

SP	Setpoint.
MV	Measured variable or process output.

**Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.
Ti	Integral time constant ( $T_i > 0$ ).

b	Proportional setpoint weighting parameter.
c	Derivative setpoint weighting parameter.

**Initial Values**

yes	Should be left default!
-----	-------------------------

**Library**

Signal\Control\PID Control\Discrete

**Use**

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This is a PID controller in series form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \left( b + \frac{1}{s \cdot T_i} \right) \cdot \frac{1 + s \cdot c \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot SP - \left( 1 + \frac{1}{s \cdot T_i} \right) \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot MV \right)$$

An anti-windup scheme has been added to this controller.

**Interface**

**Inputs**

SP	Setpoint.
MV	Measured variable or process output.

**Description**

**Outputs**

output	Controller output: input for the process.
--------	---

**Parameters**

K	Proportional gain.
Td	Derivative time constant (Td > 0).
N	Derivative gain limitation.
Ti	Integral time constant (Ti > 0).
b	Proportional setpoint weighting parameter.
c	Derivative setpoint weighting parameter.
Ta	Tracking time constant.
minimum	Minimum controller output.
maximum	Maximum controller output.

**Initial Values**

yes Should be left default!

**Library**

Signal\Control\PID Control\Discrete

**Use**

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This is a PID controller in series form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \left( b + \frac{1}{s \cdot T_i} \right) \cdot \frac{1 + s \cdot c \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot SP - \left( 1 + \frac{1}{s \cdot T_i} \right) \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot MV \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up.

**Interface****Inputs**

SP

**Description**

Setpoint.

MV

Measured variable or process output.

**Outputs**

output

Controller output: input for the process.

**Parameters**

K

Proportional gain.

Td

Derivative time constant ( $T_d > 0$ ).

N

Derivative gain limitation.

Ti

Integral time constant ( $T_i > 0$ ).

b

Proportional setpoint weighting parameter.

c

Derivative setpoint weighting parameter.

Ta

Tracking time constant.

minimum

Minimum controller output.

maximum

Maximum controller output.

output\_initial

The controller output at start-up.

**Initial Values**

yes

Should be left default!

## Library

Signal\Control\PID Control\Discrete

## Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a PID controller in series form with setpoint weighting. The output of this controller (in s-domain) is:

$$U = K \cdot \left( \left( b + \frac{1}{s \cdot T_i} \right) \cdot \frac{1 + s \cdot c \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot SP - \left( 1 + \frac{1}{s \cdot T_i} \right) \frac{1 + s \cdot T_d}{1 + s \cdot \frac{T_d}{N}} \cdot MV \right)$$

An anti-windup scheme has been added to this controller as well as an offset for manual output at start-up. An external tracking signal must be supplied to activate the anti-windup scheme.

## Interface

### Inputs

SP	Setpoint.
MV	Measured variable or process output.
TR	Tracking signal.

### Description

### Outputs

output	Controller output: input for the process.
--------	---

### Parameters

K	Proportional gain.
Td	Derivative time constant ( $T_d > 0$ ).
N	Derivative gain limitation.
Ti	Integral time constant ( $T_i > 0$ ).
b	Proportional setpoint weighting parameter.
c	Derivative setpoint weighting parameter.
Ta	Tracking time constant.
output_initial	The controller output at start-up.

### Initial Values

yes	Should be left default!
-----	-------------------------

## Library

Signal\Control\PID Control\Discrete

## Use

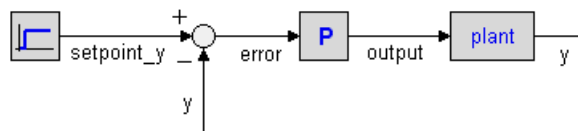
**Domains:** Continuous, Discrete **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a P controller. The output of this controller is:

$$\text{output} = k_p \cdot \text{error}$$

with the input of the controller equal to the error and the output of the controller used as the plant input:



## Interface

### Inputs

error

### Description

Input signal: plant-output minus set point.

### Outputs

output

Output signal: input for the plant.

### Parameters

$k_p$

Proportional gain.

## Library

Signal\Control\PID Control\Discrete

## Use

**Domains:** Continuous, Discrete **Size:** 1-D. **Kind:** Block Diagrams.

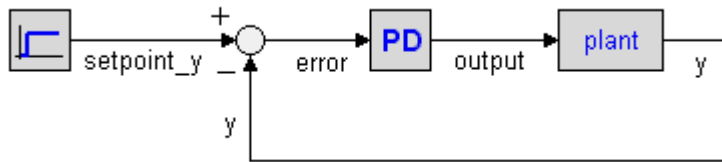
## Description

This is a PD controller in series form. The transfer function of an ideal PD-controller is:

$$G(s) = \frac{k_p (1 + s \cdot \tau_{auD})}{1 + s \cdot \beta \cdot \tau_{auD}}$$

with the input of the controller equal to the error and the output of the controller used as the plant input:





## Interface

### Inputs

error

### Description

Input signal: plant-output minus set point.

### Outputs

output

Output signal: input for the plant.

### Parameters

kp

Proportional gain.

tauD

Derivative gain (tauD <> 0).

beta

Tameness constant (0 < beta << 1).

### Initial Values

state\_initial

output(0) = state\_initial - kp\*error(0)/beta

## Library

Signal\Control\PID Control\Discrete

### Use

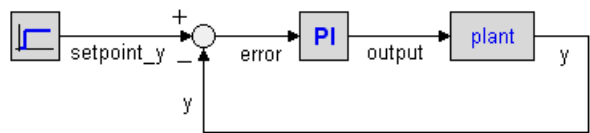
**Domains:** Continuous, Discrete **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a PI controller. The transfer function of the controller is:

$$G(s) = kp + \frac{kp}{s \cdot \tau_{auI}}$$

with the input of the controller equal to the error and the output of the controller used as the plant input:



**Interface**

**Inputs**

error

**Outputs**

output

**Parameters**

kp

taul

**Initial Values**

state(0)

**Description**

Input signal: plant-output minus set point.

Output signal: input for the plant.

Proportional gain.

Integral gain (taul <> 0).

output(0) = state(0) - kp\*error(0)

**Library**

Signal\Control\PID Control\Discrete

**Use**

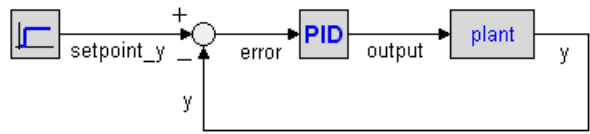
**Domains:** Continuous, Discrete **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This is a PID controller in series form. The transfer function is:

$$G(s) = k_p \cdot \left( 1 + \frac{1}{s \cdot \tau_{aI}} \right) \left( \frac{1 + s \cdot \tau_{aD}}{1 + s \cdot \beta \cdot \tau_{aD}} \right)$$

with the input of the controller equal to the error and the output of the controller used as the plant input:



**Interface**

**Inputs**

**Description**

error

Input signal: plant-output minus set point.

## Outputs

output

Output signal: input for the plant.

## Parameters

kp

Proportional gain.

tauD

Derivative gain ( $\tau_D \neq 0$ ).

taul

Integral gain ( $\tau_D \neq 0$ ).

beta

Tameness constant ( $0 < \beta \ll 1$ ).

## Initial Values

pdstate(0)

$$pdout(0) = pdstate(0) - kp * error(0) / beta$$

pistate(0)

```
output(0) = pistate(0) - pdout(0)
```

## Cost Functions

## Library

Signal\Cost Functions\Continuous

## Implementations

IE

ISE

IAE

ISTE

ITAE

ITSE

IAEWAI

ISEWSI

ITAEWAI

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric, Electric).

### Description - IE

This submodel yields the following cost function:

```
output = int(e);
```

### Description - ISE

This submodel yields the following cost function:

```
output = int(e2);
```

### Description

This submodel yields the following cost function:

*output = int(abs(e));*

**Description - ISTE**

This submodel yields the following cost function:

*output = int(time2\*e2);*

**Description - ITAE**

This submodel yields the following cost function:

*output = int(time\*abs(e));*

**Description - ITSE**

This submodel yields the following cost function:

*output = int(time\*e2);*

**I**

**Description - IAEWAI**

This submodel yields the following cost function:

*output = int(abs(e) + lambda\*abs(input));*

**Description - ISEWSI**

This submodel yields the following cost function:

*output = int(e2 + lambda\*input2);*

**Description**

This submodel yields the following cost function:

*output = int(time\*abs(e) + lambda\*abs(input));*

**Interface**

**Inputs**

e  
input

**Description**

Input signal  
Input signal

**Outputs**

output

**Parameters**

lambda

Weighting factor.

**Initial Values**

output\_initial

The initial value of the output.

**Library**

Signal\Cost Functions\Discrete

**Implementations**

IE  
 ISE  
 IAE  
 ISTE  
 ITAE  
 ITSE  
 IAEWAI  
 ISEWSI  
 ITAEWAI

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Iconic Diagrams (Electric, Electric).

**Description - IE**

This submodel yields the following cost function:

$$output = sum(e);$$

**Description - ISE**

This submodel yields the following cost function:

$$output = sum(e^2);$$

**Description - IAE**

This submodel yields the following cost function:

$$output = sum(abs(e));$$

**Description - ISTE**

This submodel yields the following cost function:

$$output = sum(time^2 * e^2);$$

**Description - ITAE**

This submodel yields the following cost function:

$$output = sum(time * abs(e));$$

**Description - ITSE**

This submodel yields the following cost function:

$$output = sum(time * e^2);$$

**I****Description - IAEWAI**

This submodel yields the following cost function:

$$\text{output} = \text{sum}(\text{abs}(e) + \text{lambda} * \text{abs}(\text{input}));$$

### Description - ISEWSI

This submodel yields the following cost function:

$$\text{output} = \text{sum}(e2 + \text{lambda} * \text{input2});$$

### Description

This submodel yields the following cost function:

$$\text{output} = \text{sum}(\text{time} * \text{abs}(e) + \text{lambda} * \text{abs}(\text{input}));$$

### Interface

#### Inputs

e	Input signal
input	Input signal

#### Outputs

output

#### Parameters

lambda	Weighting factor.
--------	-------------------

#### Initial Values

output_initial	The initial value of the output.
----------------	----------------------------------

### Discrete

### Library

Signal\Discrete

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model incorporates the basic functions of an analog to digital convertor: sample and hold, output window (i.e. restriction of the output between a minimum and maximum value) and quantization. The quantization is specified in bits. For example 8 bits quantization means the output has  $2^8 - 1 = 255$  possible values between the given minimum and maximum.

### Interface

#### Inputs

input	Description
-------	-------------

#### Outputs

output

#### Parameters

minimum	Minimum output value.
maximum	Maximum output value
bits	Quantization levels (bits).
initial	Initial output

Limitations

- The input of this model is a continuous signal. The output of this model is a discrete signal. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties, Simulation** and **Discrete System**).
- The initial output is bounded by the window given by the minimum and maximum and rounded by the number of bits used.

Library

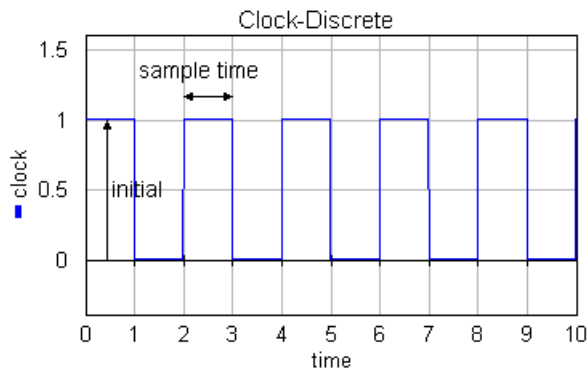
Signal\Discrete

Use

**Domains:** Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

Description

This models generates a logical discrete clock signal, i.e. a signal that changes from true (1) to false (0) and vice-versa, each sample time.



Interface

Outputs

output

Description

Parameters

initial

Initial value of the output.

### Limitations

The output of this model is a discrete signal. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

### Library

Signal\Discrete

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model incorporates the basic functions of a digital to analog convertor: zero order hold, output window (i.e. restriction of the output between a minimum and maximum value) and quantization. The quantisation is specified in bits. For example 8 bits quantisation means the output has  $2^8 - 1 = 255$  possible values between the given minimum and maximum.

The standard models of the discrete library assume that there is no time needed to perform the calculations the a discrete loop. In general these calculations do take time. To take this into account, the output of this model is delayed in time. This time delay can be set by the user and should correspond to the time needed to perform all calculations of the discrete loop in a real system.

### Interface

#### Inputs

input

#### Description

#### Outputs

output

#### Parameters

minimum	Minimum output value.
maximum	Maximum output value
bits	Quantisation levels (bits).
t_calc	Time needed to perform all calculations of the discrete loop.

### Limitations

The input of this model is a discrete signal. The output of this model is a continuous signal. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).



## Library

Signal\Discrete

## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

This model incorporates the basic functions of a digital to analog convertor: zero order hold, output window (i.e. restriction of the output between a minimum and maximum value) and quantization. The quantization is specified in bits. For example 8 bits quantization means the output has  $2^8 - 1 = 255$  possible values between the given minimum and maximum.

## Interface

### Inputs

input

### Description

### Outputs

output

### Parameters

minimum	Minimum output value.
maximum	Maximum output value
bits	Quantization levels (bits).

## Limitations

The input of this model is a discrete signal. The output of this model is a continuous signal. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

## Library

Signal\Discrete

## Use

**Domains:** Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is the the z-delay function with n samples delay.

$$\begin{aligned} \text{output}(k) &= \text{input}(k - n * T) \\ \text{with } k &= n * T, n = 1, 2, 3, \dots \end{aligned}$$

The sampletime T can be set in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

## Interface

### Inputs

input

### Description

### Outputs

output

### Initial Values

output\_initial                      The initial value of the block.

### Parameters

n                                      The number of sample delays ( $n = 1, 2, 3, \dots$ ).

### Limitations

- The parameter  $n$  can not be changed during simulation. If it is increased, recompiling of the model is necessary.
- The input and output of this model are discrete signals. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

## Library

Signal\Discrete

### Use

**Domains:** Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is the the z-delay function with one sample interval delay.

$$\begin{aligned} \text{output}(k) &= \text{input}(k - T) \\ \text{with } k &= n * T, n = 0, 1, 2, 3, \dots \end{aligned}$$

The sampletime  $T$  can be set in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

## Interface

### Inputs

input

### Description

### Outputs

output

**Initial Values**

output\_initial                      The initial value of the block.

**Limitations**

The input and output of this model are discrete signals. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

**Library**

Signal\Discrete

**Use**

**Domains:** Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This model represents the discrete equivalent of the continuous differentiation:

$$\begin{aligned} output(0) &= initial; \quad (k = 0) \\ output(1) &= (u(1) - initial)/sampletime; \quad (k = 1) \\ output(k) &= (u(k) - u(k-1))/sampletime; \quad (k = n * T, n = 2, 3, 4, \dots) \end{aligned}$$

The sampletime T can be set in the Simulator (choose **Properties**, **Simulation** and **Discrete System**). The discrete transfer function of this model is:

$$H(z) = (z - 1) / (z * sampletime)$$

which is the equivalent (using the backward difference transformation) of the continuous time transferential:

$$H(s) = s$$

**Interface****Inputs**

input

**Description****Outputs**

output

**Parameters**

initial                      Initial value of the output.

## Limitations

The input and output of this model are discrete signals. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

## Library

Signal\Discrete

## Use

**Domains:** Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This model represents the discrete equivalent of the continuous integration:

$$\begin{aligned} \text{output}(k) &= \text{initial}; (k = 0) \\ &\text{inp}(k-T)*T + \text{inp}(k-2T)*T + \text{inp}(k-3T)*T \\ &+ \dots + \text{inp}(0)*T + \text{initial}; (k = n * T, n = 1, 2, 3, \dots) \end{aligned}$$

The sampletime T can be set in the Simulator (choose **Properties**, **Simulation** and **Discrete System**). The discrete transfer function of this model is:

$$H(z) = \text{sampletime} / (z - 1)$$

which is the equivalent (using the forward difference transformation) of the continuous time transfer function:

$$H(s) = 1/s$$

## Interface

### Inputs

input

### Description

### Outputs

output

### Parameters

initial

Initial value of the output.

## Limitations

The input and output of this model are discrete signals. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

**Library**

Signal\Discrete

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model forms the interconnection between a discrete and continuous system: zero order hold.

**Interface****Inputs**

input

**Description**

discrete signal

**Outputs**

output

continuous signal

**Limitations**

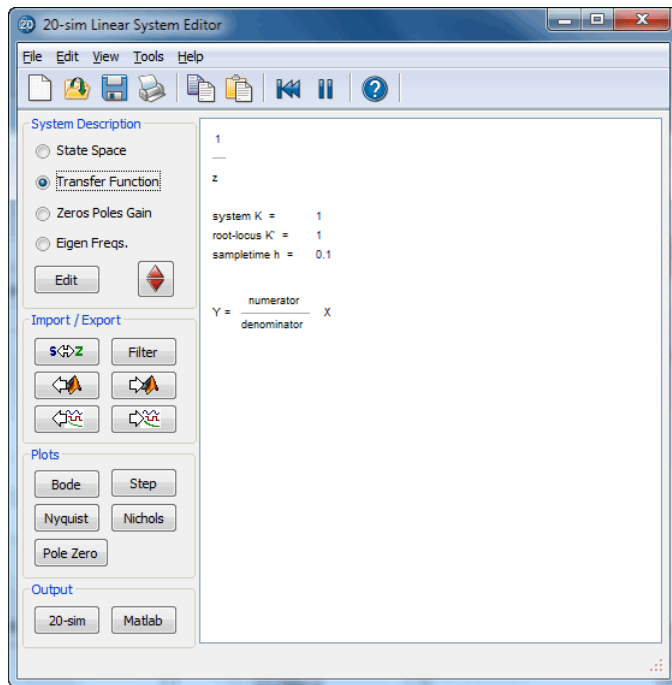
The input of this model is a discrete signal. The output of this model is a continuous signal. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

**Library**

Signal\Discrete

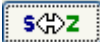

**Use****Domains:** Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

When you select this model and click *Go Down* a special editor opens (Linear System Editor), allowing you to enter a linear system in State Space form, as a Transfer Function or by adding poles and zeros:



### Note

This is a discrete linear system, using the transformation. The transformation is based on a sampletime (here 0.1 s). You can change the sampletime by going to a continuous-time

linear system (click the  button) and back (click again the  button).

### Interface

#### Inputs

input

#### Outputs

output

#### Initial Values

#### Parameters

#### Description

The model has internal states that are not accessible.

Parameters are entered by the Linear System Editor.

## Library

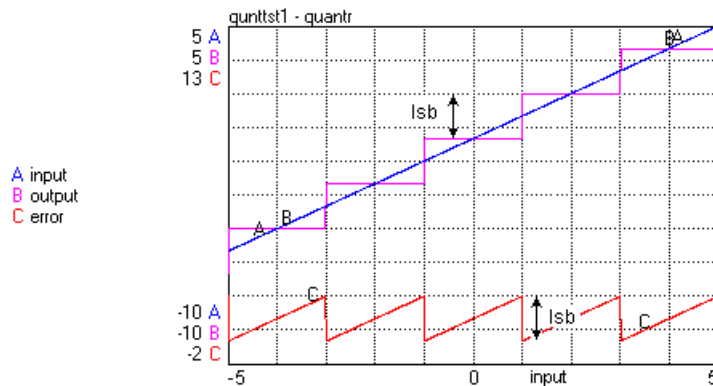
Signal\Discrete

## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

This model can be used to represent quantization of an input signal. It rounds the input as shown in the graph below. The quantization interval is specified by the least significant bit (lsb). The maximum output error is half a least significant bit.



## Note

Compare this model with the model Quantize-Truncate which represents quantization by truncation. Truncation results in a maximum error of a least significant bit.

## Interface

### Inputs

input

### Outputs

output

### Parameters

lsb

### Description

Least significant bit.

## Library

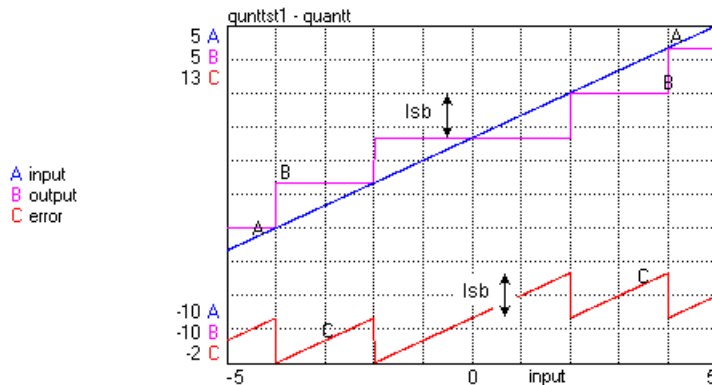
Signal\Discrete

## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

This model can be used to represent quantization of an input signal. It truncates the input as shown in the graph below. The quantization interval is specified by the least significant bit (lsb). The maximum output error is a least significant bit.



## Note

Compare this model with the model Quantize-Round which represents quantization by rounding. Rounding results in a maximum error of half a least significant bit.

## Interface

### Inputs

input

### Outputs

output

### Parameters

lsb

### Description

Least significant bit.



**Library**

Signal\Discrete

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model samples and holds the input every T [s].

$$\begin{aligned} \text{output} &= \text{input}; (t = k) \\ \text{where } k &= n * T, \text{ with } n = 0, 1, 2, 3, \dots \end{aligned}$$

The sampletime T can be set in the Simulator (choose **Properties**, **Run** and **Discrete System**).

**Interface****Inputs**

input

**Description****Outputs**

output

**Limitations**

The input of this model is a continuous signal. The output of this model is a discrete signal. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

**Library**

Signal\Discrete

**Use****Domains:** Discrete. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This model represents a discrete summation operator:

$$\begin{aligned} \text{output}(k) &= \text{initial}; \\ \text{with } k &= 0 \\ \text{outp}(k) &= \text{inp}(k-T) + \text{inp}(k-2T) + \text{inp}(k-3T) + \dots + \text{inp}(0) + \text{initial} \\ \text{with } k &= n * T, n = 1, 2, 3, \dots \end{aligned}$$

The sampletime T can be set in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

## Interface

### Inputs

input

### Description

### Outputs

output

### Parameters

initial

Initial value of the output.

### Limitations

The input and output of this model are discrete signals. 20-sim will automatically detect the existence of discrete models. Each chain of discrete models will be assigned a specific sampletime. You can set this sample time to any desired value in the Simulator (choose **Properties**, **Simulation** and **Discrete System**).

### Events

## Library

Signal\Events

### Implementations

CrossingBoth  
CrossingDown  
CrossingUp

### Use

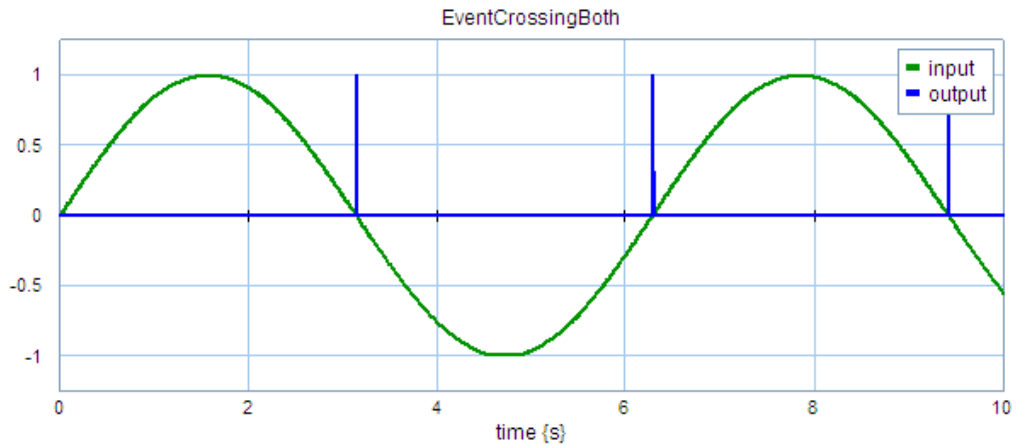
**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description - CrossingBoth

This is the block implementation of the event function. The output signal is a boolean which goes from false (0) to true (1) when the input signal crosses zero (offset = 0):

$$output = event(input - offset);$$

If desired, you can change the parameter *offset* to trigger the event on a non-zero input value.



The output of the event block for a sinusoidal input (parameter *offset* = 0).

## Interface - CrossingBoth

### Inputs

input

### Outputs

output

### Parameters

*offset*

### Description

### Description

event signal (boolean)

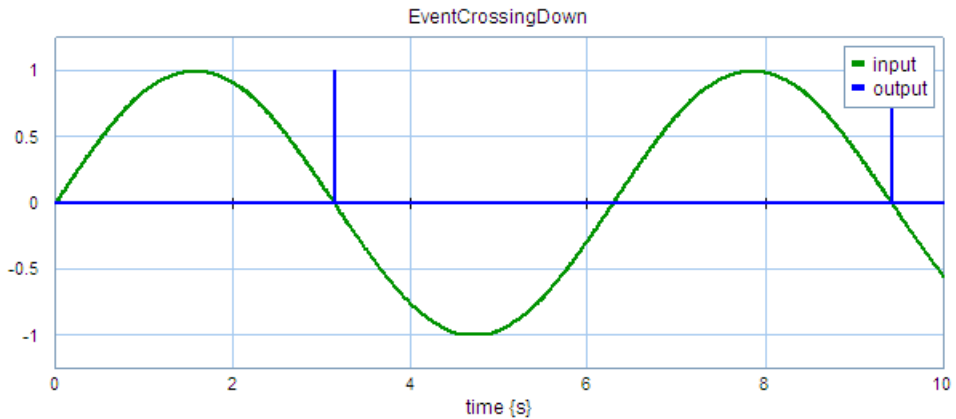
output is true (event) when the input signal crosses this value (default = 0)

## Description - CrossingDown

This is the block implementation of the `eventdown` function. The output signal is a boolean which goes from false (0) to true (1) when the input signal crosses zero with a negative slope (*offset* = 0):

$$\text{output} = \text{eventdown}(\text{input} - \text{offset});$$

If desired, you can change the parameter *offset* to trigger the event on a non-zero input value.



The output of the event block for a sinusoidal input (parameter offset = 0).

## Interface - CrossingDown

### Inputs

input

### Description

### Outputs

output

### Description

event signal (boolean)

### Parameters

offset

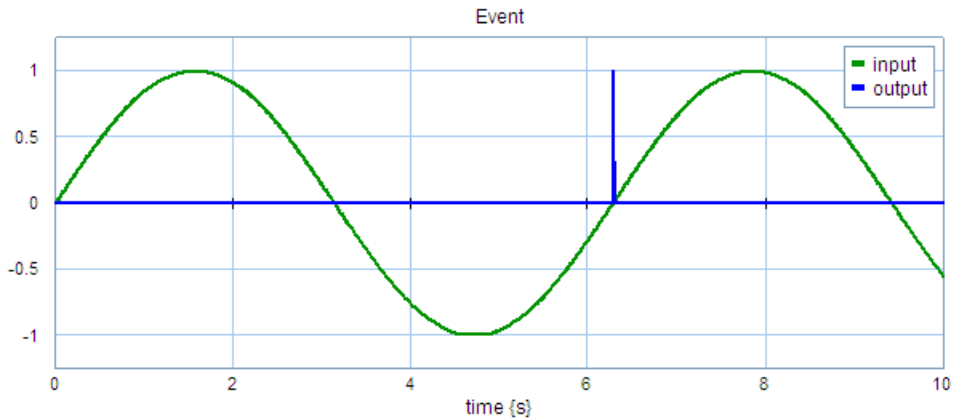
output is true (event) when the input signal crosses this value (default = 0).

## Description - CrossingUp

This is the block implementation of the eventup function. The output signal is a boolean which goes from false (0) to true (1) when the input signal crosses zero with a positive slope (offset = 0):

$$\text{output} = \text{eventup}(\text{input} - \text{offset});$$

If desired, you can change the parameter *offset* to trigger the event on a non-zero input value.



The output of the event block for a sinusoidal input (parameter offset = 0).

## Interface - CrossingUp

### Inputs

input

### Outputs

output

### Parameters

offset

### Description

### Description

event signal (boolean)

output is true (event) when the input signal crosses this value (default = 0).

## Library

Signal\Events

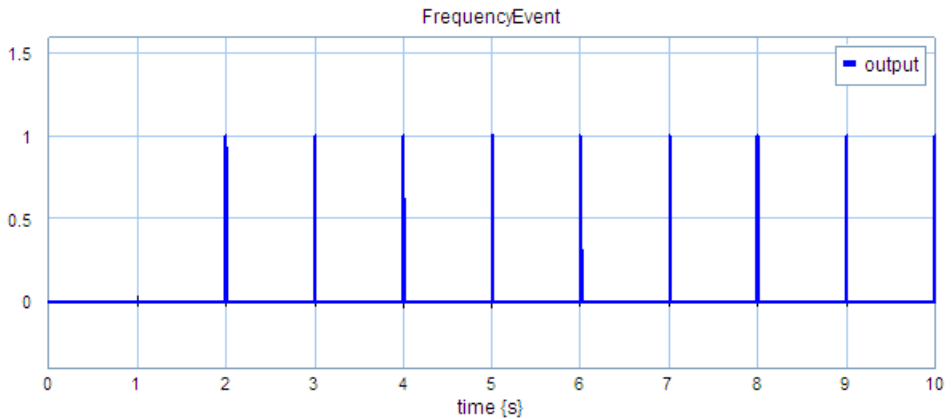
## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

This is the block implementation of the frequencyevent function. The output signal is a boolean which is true (1) every time when  $p$  [s] have passed. The function starts after an offset of  $o$  [s]. The offset parameter is optional.

$output = frequencyevent(p,o);$



*The output of the frequencyevent block with a period of 1 s and an offset of 2 s.*

## Interface

### Outputs

output

### Description

event signal (boolean)

### Parameters

period

period in [s]

offset

offset in [s]

## Library

Signal\Events

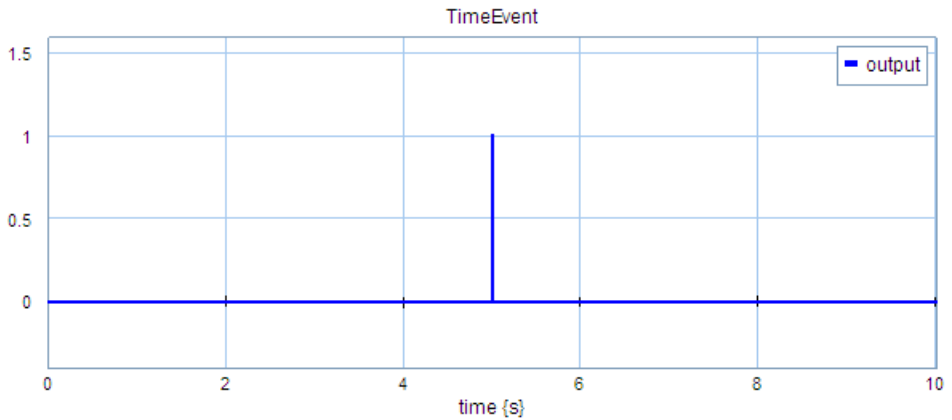
## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

This is the block implementation of the timeevent function. The output signal is a boolean which is true (1) at a specific time given by the parameter *triggerTime*:

```
output = timeevent(triggerTime);
```



The output of the timeevent block with a triggerTime of 5 s.

## Interface

### Outputs

output

### Description

event signal (boolean)

### Parameters

triggerTime

time in [s] when the output is true.

## Filters

## Library

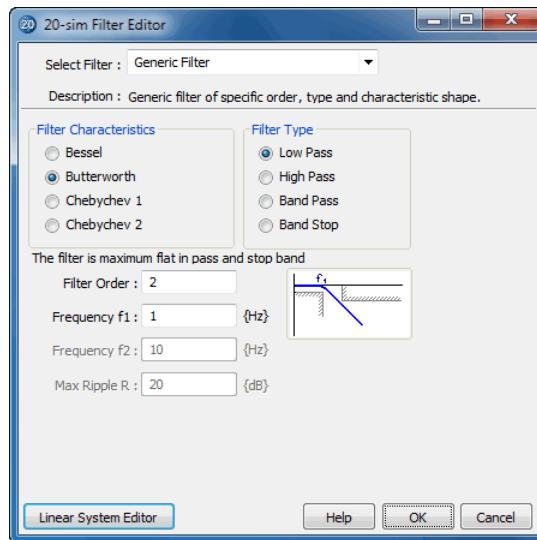
Signal\Block Diagram

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

When you select this model and click *Go Down* a special editor opens (Filter Editor), allowing you to choose a filter:



## Interface

### Inputs

input

### Outputs

output

### Initial Values

### Parameters

### Description

The model has internal states that are not accessible.

Parameters are entered by the Filter Editor.

## Library

Signal\Filters

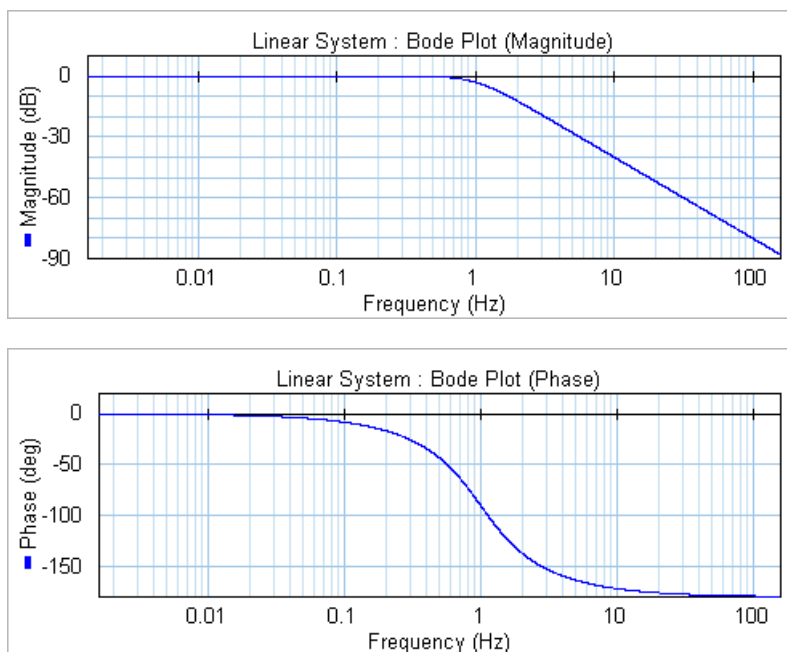
### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a second order Butterworth filter. The bandwidth is given in Hz. The phase and magnitude plot (bandwidth = 1 Hz) are shown in the figure below.





## Interface

### Outputs

input,output

### Parameters

BW

### Description

Bandwidth (Hz)

### Initial Values

y\_initial

Output value of the filter at  $t = 0$  s.

## Library

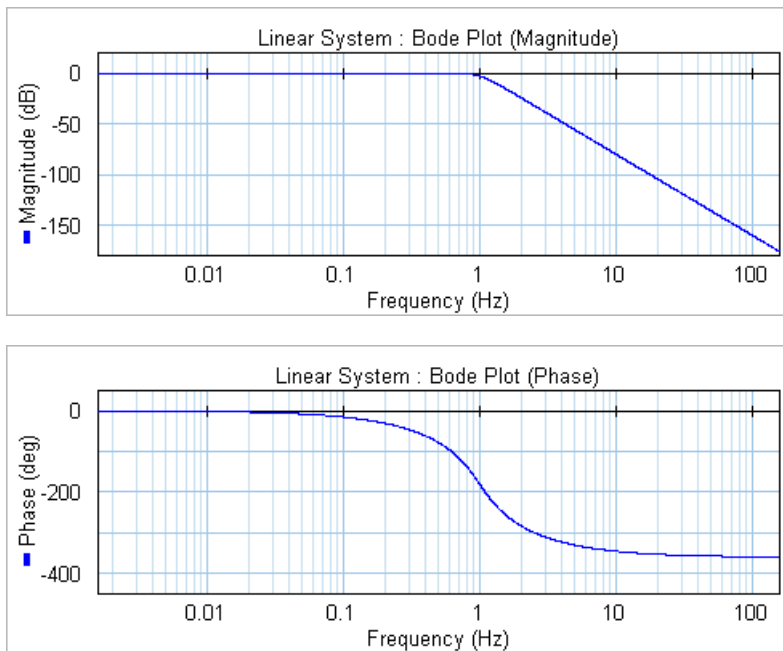
Signal\Filters

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a fourth order Butterworth filter. The bandwidth is given in Hz. The phase and magnitude plot (bandwidth = 1 Hz) are shown in the figure below.



## Interface

### Outputs

input,output

### Parameters

BW

### Description

Bandwidth (Hz)

### Initial Values

y\_initial

Output value of the filter at  $t = 0$  s.

**Library**

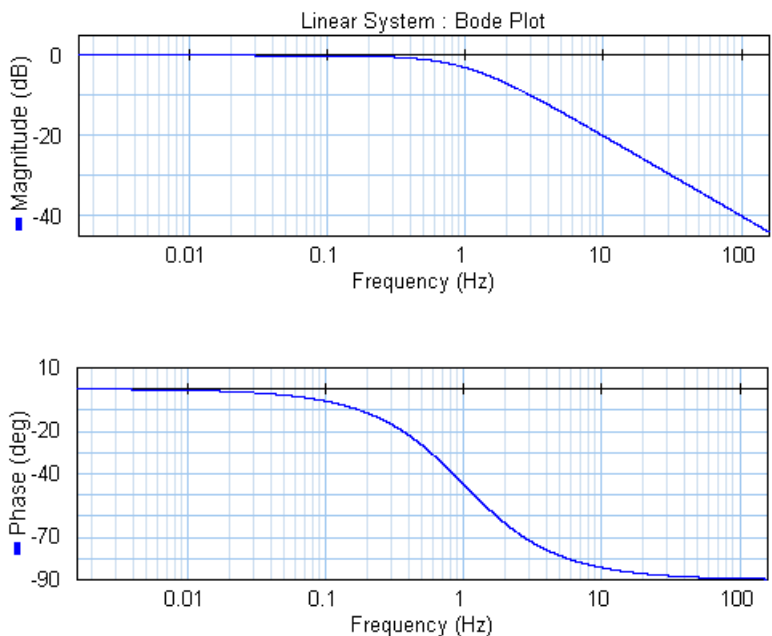
Signal\Filters

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a first order filter. with transfer function:

$$Y(s) = \frac{1}{\frac{s}{2 \cdot \pi \cdot BW} + 1} \cdot U(s)$$

The bandwidth is given in Hz. The phase and magnitude plot (bandwidth = 1 Hz) are shown in the figure below.

**Interface****Outputs**

input,output

**Description****Parameters**

BW

Bandwidth (Hz)

**Initial Values**

state\_initial

Output value of the filter at t = 0 s.

**Library**

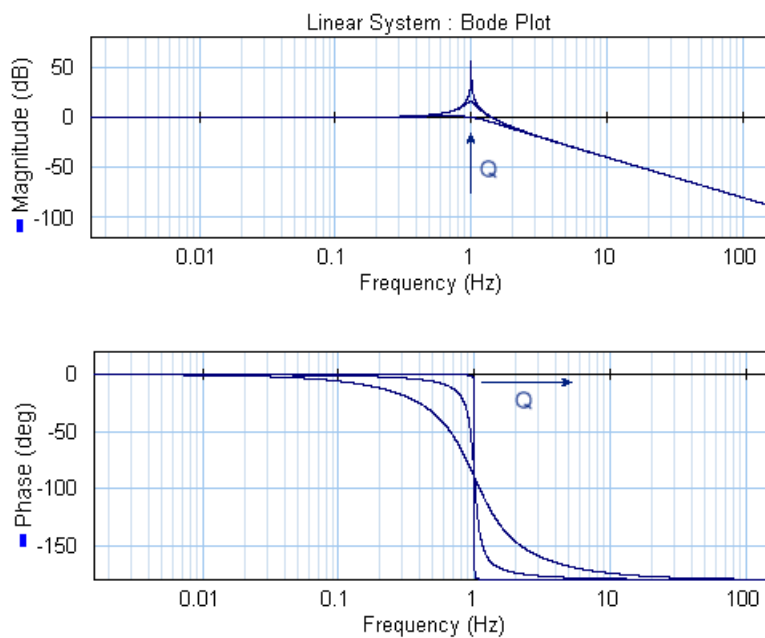
Signal\Filters

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This is a second order filter. with transfer function:

$$Y(s) = \frac{(2 \cdot \pi \cdot BW)^2}{s^2 + 2 \cdot \pi \cdot BW \frac{s}{Q} + (2 \cdot \pi \cdot BW)^2} \cdot U(s)$$

The bandwidth is given in Hz. The phase and magnitude plot (bandwidth = 1 Hz) are shown in the figure below.



## Interface

### Outputs

input,output

### Parameters

BW

Bandwidth (Hz)

Q

Quality ()

### Initial Values

state1\_initial

Output rate of the filter at  $t = 0$  s.

state2\_initial

Output value of the filter at  $t = 0$  s.

## Import Export

### Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel sends a command to the Matlab workspace during simulation, and gets the output signal from the Matlab workspace.

### Interface

#### Inputs

#### Description

#### Outputs

output

The variable from the Matlab workspace.

#### Parameters

command  
name

Command string in Matlab format

Name of the variable inside the Matlab workspace.

#### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

### Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel sends a command to the Matlab workspace at the end of the simulation.

### Interface

#### Inputs

#### Description

## Outputs

### Parameters

command

Command string in Matlab format

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

## Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel sends a command to the Matlab workspace at the start of the simulation.

### Interface

#### Inputs

#### Description

#### Outputs

### Parameters

command

Command string in Matlab format

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

## Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel sends a command to the Matlab workspace during simulation.

### Interface

#### Inputs

#### Description

## Outputs

### Parameters

command

Command string in Matlab format

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

## Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel gets an output from the Matlab workspace during simulation.

### Interface

#### Inputs

#### Description

### Outputs

output

The variable from the Matlab workspace.

### Parameters

name

Name of the variable inside the Matlab workspace

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

## Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel sends the input signal to the Matlab workspace, sends the command to the workspace, and gets the output variable back. This is done during the 20-sim simulation.



## Interface

### Inputs

input

### Description

The variable for the Matlab workspace.

### Outputs

output

The variable from the Matlab workspace

### Parameters

command

Command string in Matlab format

nameInput

Name of the input variable in the Matlab workspace.

nameOutput

Name of the output variable in the Matlab workspace.

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

## Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel sends the input signal and a command to the Matlab workspace during simulation.

## Interface

### Inputs

input

### Description

The variable for the Matlab workspace.

### Outputs

### Parameters

command

Command string in Matlab format

name

Name of the variable inside the Matlab workspace.

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

**Library**

Signal\Import Export\Matlab

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This submodel sends the input signal to the Matlab workspace, stores the input inside the Matlab workspace into a matrix, and plots the result in a graph. Each row of the matrix corresponds with a major simulation step, so the input is limited to a scalar or vector. Note: the name is set during the processing phase only

**Interface****Inputs**

input

**Description**

The variable to send to the Matlab workspace.

**Outputs****Parameters**

name

Name of the variable inside the Matlab workspace

**Tip**

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

**Library**

Signal\Import Export\Matlab

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This submodel sends the input signal to the Matlab workspace and stores the input inside the Matlab workspace into a matrix. Each row of the matrix corresponds with a major simulation step, so the input is limited to a scalar or vector. Note: the name is set during the processing phase only.

**Interface****Inputs**

input

**Description**

The variable to send to the Matlab workspace.

**Outputs****Parameters**

**name** Name of the variable inside the Matlab workspace

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

### Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel sends the time and input signal to the Matlab workspace. The input is limited to a scalar or vector. Note: the name is set during the processing phase only.  
Interface

### Inputs

input

### Description

The variable to send to the Matlab workspace.

### Outputs

### Parameters

**name** Name of the variable inside the Matlab workspace

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

### Library

Signal\Import Export\Matlab

### Use

**Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel sends the time and input signal to the Matlab workspace, stores the time and input inside the Matlab workspace into a matrix, and plots the result in a graph. Each row of the matrix corresponds with a major simulation step, so the input is limited to a scalar or column vector. Note: the name is set during the processing phase only

### Interface

### Inputs

### Description

input The variable to send to the Matlab workspace.

### Outputs

### Parameters

name Name of the variable inside the Matlab workspace

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

## Library

Signal\Import Export\Matlab

### Use

Domains: Continuous, Discrete. Size: 1-D. Allowed in: Block Diagrams.

### Description

This submodel sends the time and input signal to the Matlab workspace and stores the time and input inside the Matlab workspace into a matrix. Each row of the matrix corresponds with a major simulation step, so the input is limited to a scalar or column vector. Note: the name is set during the processing phase only

### Interface

#### Inputs

input

#### Description

The variable to send to the Matlab workspace.

#### Outputs

### Parameters

name Name of the variable inside the Matlab workspace

### Tip

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

## Library

Signal\Import Export\Matlab

### Use

Domains: Continuous, Discrete. Size: 1-D. Allowed in: Block Diagrams.

**Description**

This submodel sends a variable to the Matlab workspace during simulation.

**Interface**

**Inputs**

input

**Description**

The variable to send to the Matlab workspace.

**Outputs**

**Parameters**

name

Name of the variable inside the Matlab workspace

**Tip**

20-sim uses a single quote ' for strings. If you wish to include a single quote inside the command string for Matlab, use 2 single quotes '' in the command string instead.

**Logical**

**Library**

Signal\Logical\Continuous

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output signal of this model is according the truth table below:

	input2	false	true
input1			
false		false	false
true		false	true
with			
		false	true
inputs		<= 0.5	> 0.5
output		0.0	1.0

Interface

Inputs

input1  
input2

Outputs

output

Description

Library

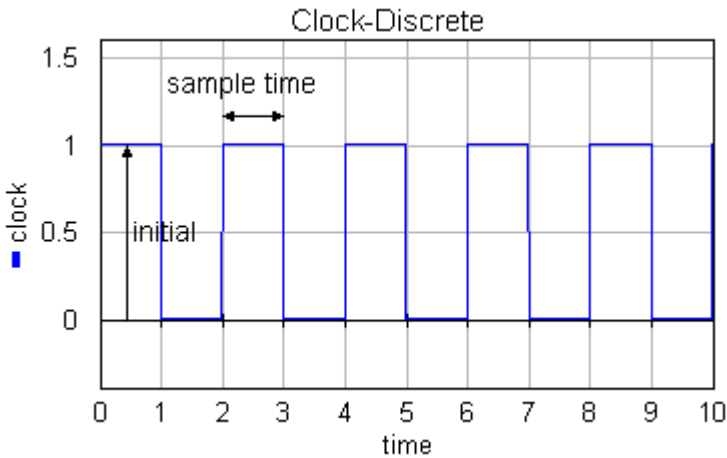
Signal\Logical\Continuous

Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

Description

This models generates a logical continuous clock signal, i.e. a signal that changes from true (1) to false (0) and back, each period T.



Interface

Outputs

output

Description

Parameters

initial  
T

Initial value of the output.  
Clock-period.

**Library**

Signal\Logical\Continuous

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

The initial output of this model is equal to the parameter *initial*. Otherwise the output signal is equal to the input signal each time the control input changes from false to true:

$$\begin{aligned} \text{output} &= \text{input}; (\text{oldcontrol} = \text{false and control} = \text{true}) \\ \text{output} &= \text{oldoutput}; (\text{otherwise}) \end{aligned}$$

with

	<b>false</b>	<b>true</b>
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

**Interface****Inputs**

input  
control

**Description****Outputs**

output

**Parameters**

initial Initial value of the output.

**Library**

Signal\Logical\Continuous

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

The output signal of this model is according the truth table below:

<b>input</b>	<b>output</b>
false	true
true	false

with

	false	true
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

Interface

Inputs	Description
input	
Outputs	
output	

Library

Signal\Logical\Continuous

Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

Description

The output signal of this model is according the truth table below:

	input2	false	true
input1			
false		false	true
true		true	false

with

	false	true
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

Interface

Inputs	Description
input1	
input2	
Outputs	
output	



**Library**

Signal\Logical\Continuous

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output signal of this model is according the truth table below:

	input2	false	true
input1			
false		true	true
true		true	false
with			
		false	true
inputs		<= 0.5	> 0.5
output		0.0	1.0

**Interface**

Inputs	Description
input1	
input2	
<b>Outputs</b>	
output	

**Library**

Signal\Logical\Continuous

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output signal of this model is according the truth table below:

	input2	false	true
input1			

<b>false</b>	true	false
<b>true</b>	false	false

with

	<b>false</b>	<b>true</b>
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

**Interface**

Inputs	Description
--------	-------------

input1  
input2

**Outputs**

output

**Library**

Signal\Logical\Continuous

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output signal of this model is according the truth table below:

	input2	<b>false</b>	<b>true</b>
input1			
<b>false</b>		false	true
<b>true</b>		true	true

with

	<b>false</b>	<b>true</b>
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

**Interface**

Inputs	Description
--------	-------------

input1  
input2

**Outputs**  
output

**Library**  
Signal\Logical\Continuous

**Use**  
**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**  
This is the continuous version of SetResetFlipFlop-Discrete.emx. The initial output of this model is equal to the parameter *initial*. Otherwise the output signal is according the truth table below:

input1	input2	output	
false	false	previous output	
true	false	true	<i>set condition</i>
false	true	false	<i>reset condition</i>
true	true	previous output	

with

	false	true
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

**Interface**

Inputs	Description
input1	
input2	

**Outputs**  
output

Parameters	
initial	Initial value of the output.

## Library

Signal\Logical\Continuous

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

Initially the output is equal to the parameter initial. Otherwise the output signal is changed each time the control input changes from false to true:

```
output = not oldoutput; (oldcontrol = false and control = true)
output = oldoutput; (otherwise)
```

with

	<b>false</b>	<b>true</b>
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

## Interface

Inputs	Description
input	
control	
Outputs	
output	
Parameters	
initial	Initial value of the output.

## Library

Signal\Logical\Discrete

## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

The output signal of this model is according the truth table below:

input2            **false**            **true**

input1		
<b>false</b>	false	false
<b>true</b>	false	true

with

	<b>false</b>	<b>true</b>
inputs	<= 0.5	> 0.5
output	0.0	1.0

**Interface**

Inputs	Description
input1	
input2	
<b>Outputs</b>	
output	

**Library**

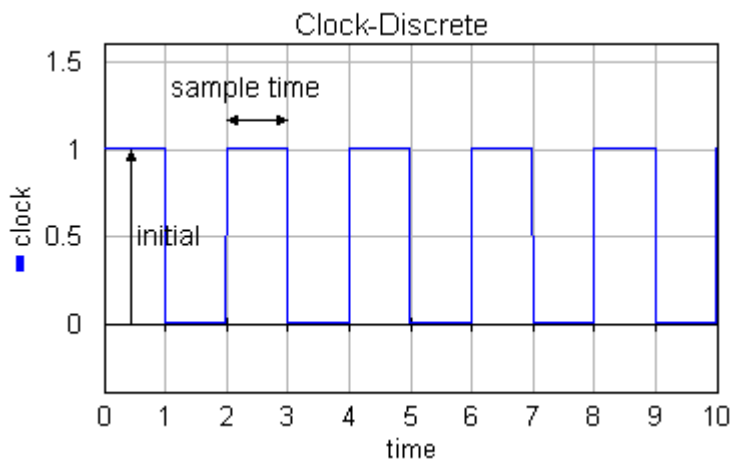
Signal\Logical\Discrete

**Use**

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

**Description**

This models generates a logical discrete clock signal, i.e. a signal that changes from true (1) to false (0) and vice-versa, each sample time.



Interface

Outputs

output

Description

Parameters

initial	Initial value of the output.
T	Clock-period.

Library

Signal\Logical\Discrete

Use

**Domains:** Discrete. **Size:** 1-D. **Kind:** Block Diagrams.  
The initial output of this model is equal to the initial value *oldoutput\_initial*. Otherwise the output signal is equal to the input signal each time the control input changes from false to true:

*output = input; (oldcontrol = false and control = true)*  
*output = oldoutput; (otherwise)*

with

	<b>false</b>	<b>true</b>
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

Interface

Inputs	Description
input	
control	
Outputs	
output	
Initial Values	
oldcontrol_initial	Initial value of the control signal.
oldoutput_initial	Initial value of the output.

Library

Signal\Logical\Discrete

Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

Description

The output signal of this model is according the truth table below:

input	output	
false	true	
true	false	
with		
	false	true
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

Interface

Inputs	Description
input	
Outputs	
output	

**Library**

Signal\Logical\Discrete

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output signal of this model is according the truth table below:

	input2	false	true
input1			
false		true	
true		true	
with			
		false	true
inputs		$\leq 0.5$	$> 0.5$
output		0.0	1.0

**Interface**

Inputs	Description
input1	
input2	
Outputs	
output	

**Library**

Signal\Logical\Discrete

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output signal of this model is according the truth table below:

	input2	false	true
input1			



<b>false</b>	true
<b>true</b>	false

with

	<b>false</b>	<b>true</b>
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

**Interface**

Inputs	Description
input1	
input2	
<b>Outputs</b>	
output	

**Library**

Signal\Logical\Discrete

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output signal of this model is according the truth table below:

	input2	<b>false</b>	<b>true</b>
input1			
<b>false</b>		false	
<b>true</b>		true	

with

	<b>false</b>	<b>true</b>
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

Interface

Inputs	Description
input1	
input2	
Outputs	
output	

Library

Signal\Logical\Discrete

Use

**Domains:** Discrete. **Size:** 1-D. **Kind:** Block Diagrams.

Description

The initial output of this model is equal to the initial\_value *oldoutput\_initial*. Otherwise the output signal is according the truth table below:

input1	input2	output	
false	false	previous output	
true	false	true	<i>set condition</i>
false	true	false	<i>reset condition</i>
true	true	previous output	

with

	false	true
inputs	$\leq 0.5$	$> 0.5$
output	0.0	1.0

Interface

Inputs	Description
input1	
input2	
Outputs	
output	

Initial Values

oldoutput_initial	Initial value of the output.
-------------------	------------------------------

**Library**

Signal\Logical\Discrete

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

Initially the output is equal to the initial value *oldoutput\_initial*. Otherwise the output signal is changed each time the control input changes from false to true:

$$\begin{aligned} \text{output} &= \text{not oldoutput}; (\text{oldcontrol} = \text{false and control} = \text{true}) \\ \text{output} &= \text{oldoutput}; (\text{otherwise}) \end{aligned}$$
**Interface****Inputs**

control

**Description****Outputs**

output

**Initial Values**

oldcontrol\_initial

Initial value of the control signal.

oldoutput\_initial

Initial value of the output.

**Library**

Signal\Logical\Discrete

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

The output signal of this model is according the truth table below:

	input2	<b>false</b>	<b>true</b>
input1			
<b>false</b>		false	
<b>true</b>		true	
with			
		<b>false</b>	<b>true</b>
inputs		<= 0.5	> 0.5

output                      0.0                      1.0

## Interface

### Inputs

input1

input2

### Outputs

output

### Description

## Signal Processing

### Library

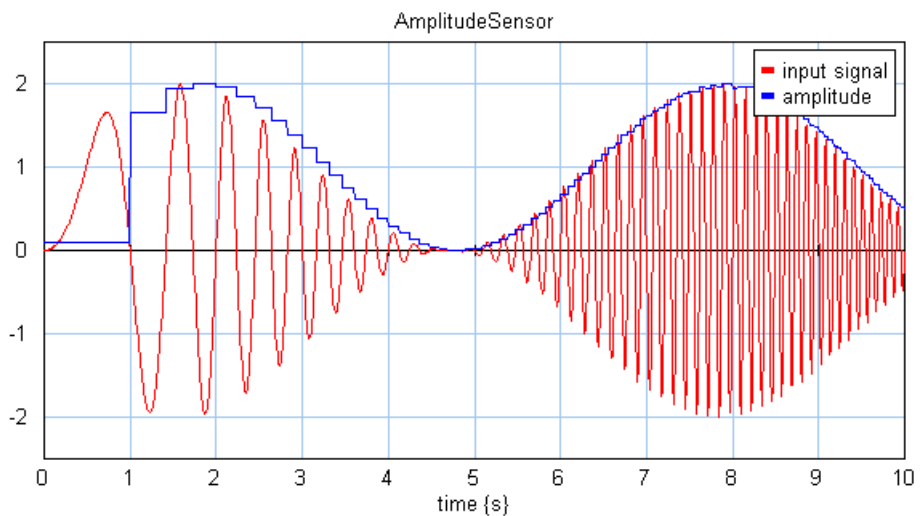
Signal\Signal Processing

### Use

**Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model measures the amplitude of harmonic signals, i.e. periodic signals, that go through zero twice every period. For half a period (between the passes through zero) the input signal is monitored. The largest value is stored and given as the absolute output signal, the next half period. That is why this sensor always has an output delay of half a period.



**Interface****Inputs**

input

**Description****Outputs**

output

**Parameters**

initial

Initial output value

**Library**

Signal\Signal Processing

**Use****Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This submodel yields the maximum value of an input signal.

**Interface****Inputs**

input

**Description**

Input signal

**Outputs**

output

Maximum value of the input signal

**Library**

Signal\Signal Processing

**Use****Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This submodel yields the mean of an input signal using the integral function:

$$\text{output} = \text{int}(\text{input})/\text{time}$$

### Interface

#### Inputs

input

#### Description

Input signal

#### Outputs

output

Mean value of the input signal

### Library

Signal\Signal Processing

### Use

**Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel yields the minimum value of an input signal.

### Interface

#### Inputs

input

#### Description

Input signal

#### Outputs

output

Minimum value of the input signal

### Library

Signal\Signal Processing

### Use

**Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel yields the average of an input signal over a window T0 (s) using an integral function:

$$\text{output} = \text{int}(\text{input}, 0)/T0$$

### Interface

#### Inputs

input

#### Description

Input signal

#### Outputs

output



**Library**

Signal\Signal Processing

**Use****Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This submodel yields the variance of an input signal using an integral function:

$$output = \text{int}((input - mean)^2 / time)$$

where mean is the mean of the input

**Interface****Inputs**

input

**Description**

Input signal

**Outputs**

output

Variance of the input signal

**Sources****Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**The output of this model is equal to the parameter  $C$ .

$$output = C;$$

**Interface****Outputs**

output

**Description****Parameters** $C$ The output is equal to  $C$ .



## Library

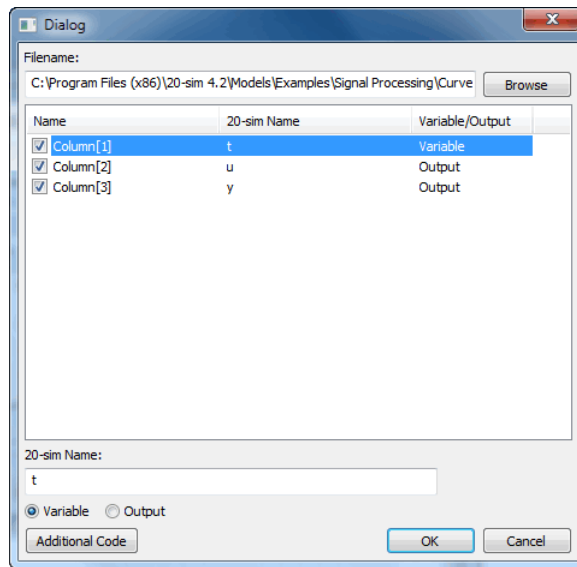
Signals\Sources

## Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

## Description

This is a masked model which opens the Data Input Wizard when edited. You can use this wizard to open a data file.



## Items

- **Filename:** Enter the filename of the datafile or use the *Browse* button.
- **Name:** The columns of data.
- **20-sim Name:** The 20-sim name that corresponds with the column data. You can enter any desired name.
- **Variable / Output:** The data may be a variable (useful for plotting in the simulator) or an output of the model (use as an input for other models).

## Interface

### Outputs

outputs

### Description

user defined outputs

## File format

20-sim supports data files in Comma Separated Values format (.csv). The first line is used as a header describing the column name. Without a proper header line, you have to define the 20-sim variable names for each column yourself.

Example CSV file format with header:

```
"time","x","y"
0.0, 1, 2
0.1, 5, 10
0.2, 6, 11
```

## Library

Signal\Sources

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model uses the joystick.dll function to get a joystick input.

### Interface

#### Outputs

outputs

#### Description

Various outputs

#### Parameters

Scale

Various scaling parameters

## Library

Signals\Sources

### Use

**Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.

### Description

This is a masked model which opens the Motion Profile Wizard when edited. Depending on the selections entered, various motion profiles can be generated.

### Interface

#### Outputs

x

v

a

#### Description

position

velocity

acceleration

#### Parameters

stroke

start\_time

amplitude of the profile

start time of the profile

stop_time	time when the maximum is reached
return_time	start time of the return motion
end_time	finish time of the return motion
period	period of the profile

**Library**

Signal\Sources

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output of this model is equal to one.

$$output = 1.0;$$

**Interface**

Outputs	Description
output	

**Library**

Signal\Sources

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

The output of this model is equal to pi.

$$output = \pi;$$

**Interface**

Outputs	Description
output	

**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model generates a cycloidal step signal:

$$tDelta = 2*pi*(time - start\_time)/(stop\_time - start\_time)$$

$$output = 0; (tDelta < 0)$$

$$output = amplitude*(tDelta - sin(tDelta))/2*pi; (0 \leq tDelta \leq 2*pi)$$

$$output = amplitude; (tDelta > 2*pi)$$

**Interface****Outputs**

output

**Description****Parameters**

start\_time

The start time of the step.

stop\_time

The stop time of the step.

amplitude

The amplitude of the step.

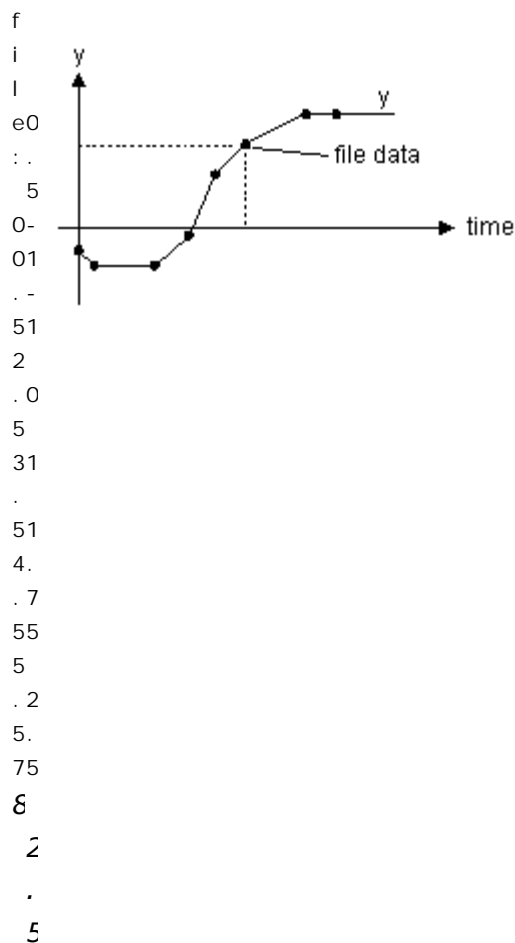
**Library**

Signal\Source

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This model generates an output by linear interpolation of data read from file. The data on file is stored in columns. The first column contains the time values ( $t$ ) and the second column contains the corresponding output values ( $y$ ).

- The time data of the first column needs to be monotonically increasing.
- Discontinuities are allowed, by providing the same time point twice in the table.
- Values outside of the range, are computed by linear extrapolation of the last two points.



*Example of an input file.*

The input file must be an ASCII (text) file and should consist at least two columns of data. The first column (number 0) should always contain the time values. The other columns (number 1, 2, 3, etc.) should contain the corresponding data values. The parameter *column* is used to specify which column is used for as output data.

The various values must be separated by a space or a tab. Each new set of time and data values must start on a new line. No comment or other text may be part of the file. The filename of the input file can be specified using the complete path (e.g. c:\data\data.tbl ). When no path is given, the file is assumed to be in the experiment directory.

**Interface**

**Outputs**

output

**Description**

**Parameters**

filename	Filename of the input file.
column	column number.

**Library**

Signal\Sources

**Implementations**

frequency\_limited\_FOH  
frequency\_limited\_ZOH  
unlimited

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description - frequency\_limited\_FOH**

This model generates a gaussian noise signal with gaussian distribution and variance 1 and random seed s. The noise is multiplied by the parameter amplitude.

$$output = amplitude * gauss(1, seed);$$

The noise signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two noise samples are interpolated (first order hold).

**Interface - frequency\_limited\_FOH**

<b>Outputs</b>	<b>Description</b>
----------------	--------------------

output

**Parameters**

seed	random seed
amplitude	-amplitude <= output <= +amplitude
frequency	frequency band of the noise

**Description - frequency\_limited\_ZOH**

This model generates a gaussian noise signal with gaussian distribution and variance 1 and random seed s. The noise is multiplied by the parameter amplitude.

$$output = amplitude * gauss(1, seed);$$

The noise signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two noise samples are interpolated (first order hold).

**Interface - frequency\_limited\_ZOH**

<b>Outputs</b>	<b>Description</b>
----------------	--------------------

output

### Parameters

seed	random seed
amplitude	-amplitude <= output <= +amplitude
frequency	frequency band of the noise

### Description - unlimited

This model generates a gaussian noise signal with gaussian distribution and variance 1 and random seed s. The noise is multiplied by the parameter amplitude.

*output = amplitude\*gauss(1,seed);*

The noise signal has no frequency limitation.

### Note

It is advised only to use this implementation with fixed step integration methods such as Euler and Runge Kutta 2/4. If you run this implementation with a variable step integration method, simulations may get very slow!

### Interface - unlimited

#### Outputs Description

output

### Parameters

seed	random seed
amplitude	-amplitude <= output <= +amplitude

### Limitations

seed must be a number in the region <0,65000>.

20-sim generates a sequence of random numbers for each simulation differently depending upon the value of the random seed parameter. The random noise function and gaussian noise function are affected by this. The default value of the random seed is 0. The maximum value is 65000.

### Default value (0)

When the random seed value is 0 (default value), 20-sim generates a new sequence of random numbers for each simulation and for each new random function. E.g. when two random functions with default random seed value (0) are used in one model, they will generate different sequences of random numbers during a simulation.

### Other values (>0)

When the random seed value is chosen larger than zero, 20-sim generates the same sequence of random numbers for each simulation. Moreover 20-sim will generate the same sequence of random numbers for each random function that uses the same random seed parameter (>0). E.g. when two random functions with random seed value 50, are used in one model, they will generate the same sequence of random numbers during a simulation.

**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This models yields a pulse signal:

$$\begin{aligned} \text{output} &= 0; \text{ (time < start\_time)} \\ \text{output} &= \text{amplitude}; \text{ (start\_time} \leq \text{time} \leq \text{stop\_time)} \\ \text{output} &= 0; \text{ (time} \geq \text{stop\_time)} \end{aligned}$$
**Interface****Outputs**

output

**Description****Parameters**

start_time	The start time of the pulse.
stop_time	The stop time of the pulse.
amplitude	The amplitude of the step.

**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This models yields a ramp signal:

$$\begin{aligned} \text{output} &= 0; \text{ (time < start\_time)} \\ \text{output} &= \text{slope} * \text{ramp}(\text{start\_time}); \text{ (time} \geq \text{start\_time)} \end{aligned}$$
**Interface****Outputs**

output

**Description****Parameters**

start_time	The start time of the ramp.
slope	The slope of the ramp.



**Library**

Signal\Sources

**Implementations**

frequency\_limited\_FOH  
frequency\_limited\_ZOH  
unlimited

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description - frequency\_limited\_FOH**

This model generates a random (noise) signal with values between -amplitude and +amplitude and random seed s. The

$$output = ran(ampl, seed);$$

The noise signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two noise samples are interpolated (first order hold).

**Interface - frequency\_limited\_FOH****Outputs**

output

**Description****Parameters**

seed	random seed
amplitude	-amplitude <= output <= +amplitude
frequency	frequency band of the noise

**Description - frequency\_limited\_ZOH**

This model generates a random (noise) signal with values between -amplitude and +amplitude and random seed s.

$$output = ran(ampl, seed);$$

The noise signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two noise samples are interpolated (first order hold).

**Interface - frequency\_limited\_ZOH****Outputs**

output

**Description****Parameters**

seed	random seed
amplitude	-amplitude <= output <= +amplitude

frequency

frequency band of the noise

**Description - unlimited**

This model generates a random (noise) signal with values between -amplitude and +amplitude and random seed s.

$$output = ran(ampl, seed);$$

The noise signal has no frequency limitation.

**Note**

It is advised only to use this implementation with fixed step integration methods such as Euler and Runge Kutta 2/4. If you run this implementation with a variable step integration method, simulations may get very slow!

**Interface - unlimited****Outputs**

output

**Description****Parameters**

seed

random seed

amplitude

-amplitude &lt;= output &lt;= +amplitude

**Limitations**

seed must be a number in the region <0,65000>.

**Library**

Signal\Sources

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

This models yields a step signal:

$$output = 0; (time < start\_time)$$

$$output = amplitude; (time \geq start\_time)$$
**Interface****Outputs**

output

**Description****Parameters**

start\_time

The start time of the step.

amplitude

The amplitude of the step.

**Library**

Signal\Sources

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

This model generates an output signal equal to the simulator time step.

**Interface****Outputs**

output

**Description**

Simulated time.

**Library**

Signal\Sources

**Implementations**

Default

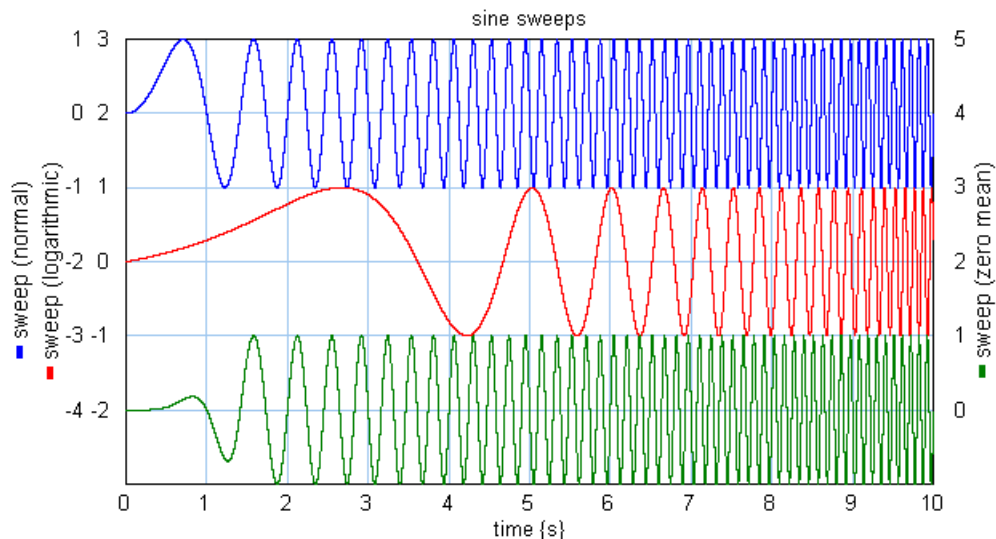
Logarithmic

ZeroMean

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description - Default**

The output of this model is a linear sine sweep. The signal starts with angular frequency "omega\_start" and ends at an angular frequency "omega\_stop".

In the picture below the three available sweep functions are shown. The curve on top shows the linear sine sweep. The middle curve shows the logarithmic sine sweep and the bottom curve shows the linear sine sweep with zero mean.



### Interface - Default

#### Outputs

output

#### Description

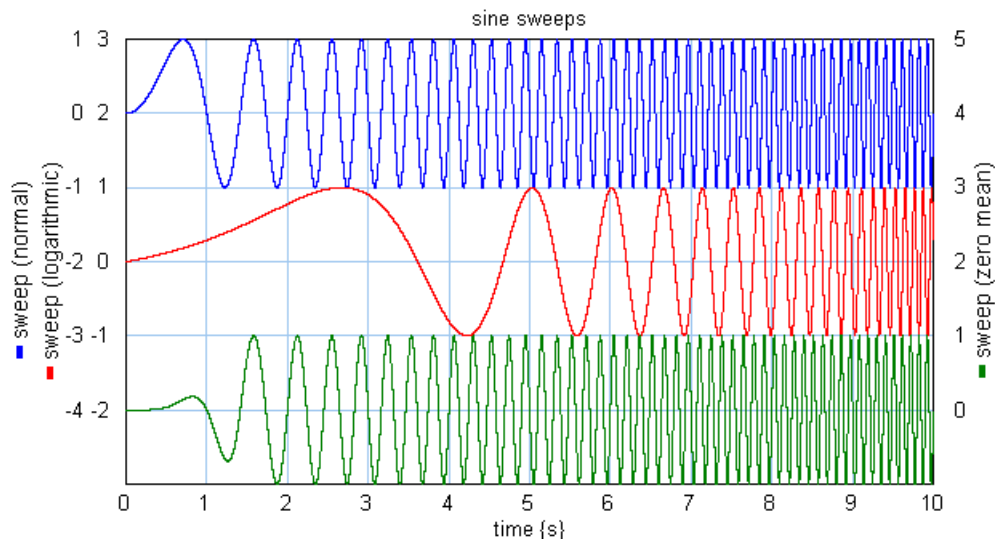
#### Parameters

start_time	The start time of the sweep.
stop_time	The stop time of the sweep.
amplitude	The amplitude of the sweep.
omega_start	The start frequency of the sweep.
omega_stop	The stop frequency of the sweep.

### Description - Logarithmic

The output of this model is a logarithmic sine sweep. Compared to the linear sine sweep the lower frequencies are stretched out and the higher frequencies are squeezed. The signal starts with angular frequency "omega\_start" and ends at an angular frequency "omega\_stop".

In the picture below the three available sweep functions are shown. The curve on top shows the linear sine sweep. The middle curve shows the logarithmic sine sweep and the bottom curve clearly uses more time for the lower frequencies and less time for the higher frequencies.



**Interface - Logarithmic**

**Outputs**

output

**Description**

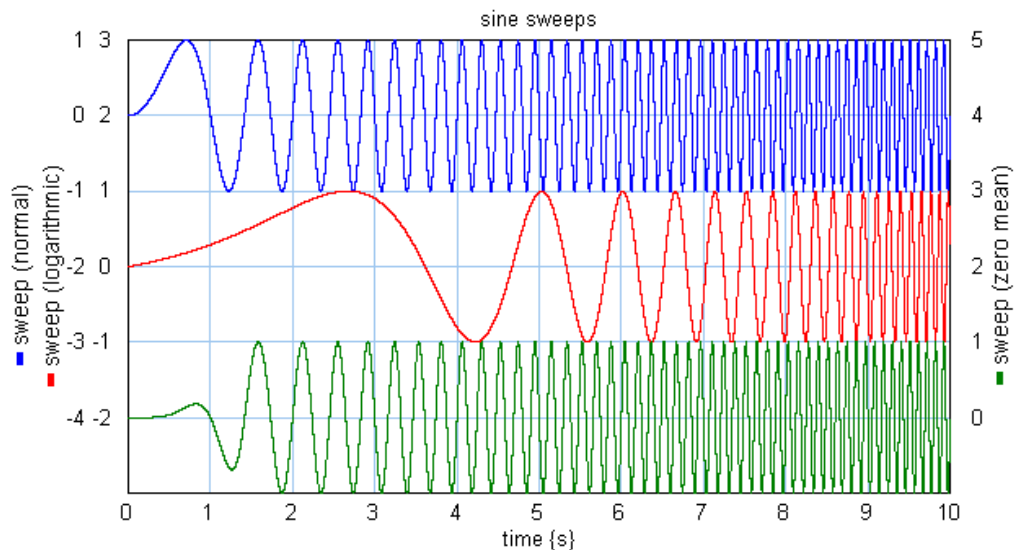
**Parameters**

start_time	The start time of the sweep.
stop_time	The stop time of the sweep.
amplitude	The amplitude of the sweep.
omega_start	The start frequency of the sweep.
omega_stop	The stop frequency of the sweep.

**Description - ZeroMean**

The output of this model is a linear sine sweep with compensation in the first period to get a zero mean output. A zero mean is important when the signal is integrated twice. To prevent drift the mean should be zero. Double integrals can occur in physical systems. For example when a force sweep is applied to a mechanical system and the position is measured, the mean force should be precisely zero to prevent the system from drifting away. The signal starts with angular frequency "omega\_start" and ends at an angular frequency "omega\_stop".

In the picture below the three available sweep functions are shown. The curve on top shows the linear sine sweep. The middle curve shows the logarithmic sine sweep and the bottom curve shows the linear sine sweep with zero mean. The bottom curve differs slightly from the top curve in the first period.



**Interface - ZeroMean**

**Outputs**

output

**Description**

**Parameters**

start_time	The start time of the sweep.
stop_time	The stop time of the sweep.
amplitude	The amplitude of the sweep.
omega_start	The start frequency of the sweep.
omega_stop	The stop frequency of the sweep.

**Library**

Signal\Sources

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description**

This model generates an output signal equal to the (simulated) time.

*output = time;*

**Interface**

**Outputs**

**Description**

output

Simulated time.

**Library**

Signal\Block Diagram , Signal\Sources

**Use****Domains:** Continuous, Discrete. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model shows the value of its input in the Simulator. When you open the Simulator (select Properties and Plot) the input of this model is automatically selected as plotvariable. As label for this variable the local name of the SignalMonitor model is chosen. It is therefore advised to give each SignalMonitor model a useful name (select the model, click the right mouse button and select Attributes from the right mouse menu).

**Interface****Inputs**

input

**Description**

The value of the input is shown in the Simulator using the local name of the model as label.

**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model generates a cosine wave.

$$output = amplitude * \cos(\omega * time);$$

**Interface****Outputs**

output

**Description****Parameters**

amplitude

The amplitude of the wave.

omega

The angular frequency of the wave.

**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model generates a sine wave with phase shift.

$$output = amplitude * \sin(\omega * time + phase);$$

**Interface****Outputs**

output

**Description****Parameters**

amplitude

The amplitude of the wave.

 $\omega$ 

The angular frequency of the wave.

phase

The phase shift of the wave.

**Library**

Signal\Source

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model generates a saw wave.

$$output = \text{upward ramp; (each cycle)}$$

**Interface****Outputs**

output

**Description****Parameters**

amplitude

The amplitude of the wave.

 $\omega$ 

The angular frequency of the wave.



**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model generates a sine wave.

$$output = amplitude * \sin(\omega * time);$$

**Interface****Outputs**

output

**Description****Parameters**

amplitude

The amplitude of the wave.

 $\omega$ 

The angular frequency of the wave.

**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model generates a block wave:

$$output = amplitude; \text{ (first wave half)}$$

$$output = 0; \text{ (second wave half)}$$

**Interface****Outputs**

output

**Description****Parameters**

amplitude

The amplitude of the wave.

 $\omega$ 

The angular frequency of the wave.

## Library

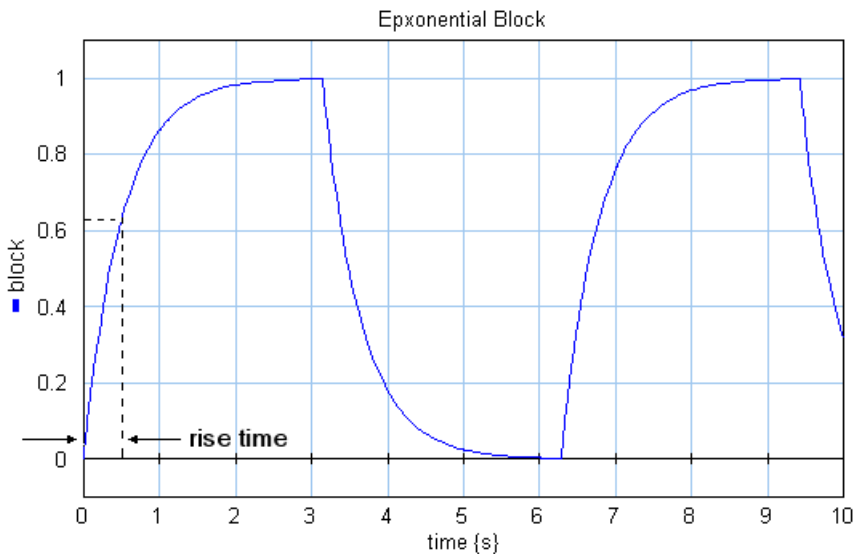
Signal\Sources

## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

## Description

This model generates a non-ideal block wave. The steepness of the edges are defined by the rise time. The rise time is defined as 63% of the amplitude being reached.



The output can be described as an exponential function:

$$\begin{aligned} \text{output} &= \text{amplitude} * (1 - \exp(-\text{time} / \text{rise\_time})); \text{ (first wave half)} \\ \text{output} &= \text{amplitude} * \exp(-\text{time} / \text{rise\_time}); \text{ (second wave half)} \end{aligned}$$

## Interface

### Outputs

output

### Parameters

amplitude  
omega  
rise\_time

### Description

The amplitude of the wave.  
The angular frequency of the wave.  
Rise time

**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This model generates a triangular wave.

*output = upward ramp; (first wave half)*  
*output = downward ramp; (second wave half)*

**Interface****Outputs**

output

**Description****Parameters**

amplitude

The amplitude of the wave.

omega

The angular frequency of the wave.

**Library**

Signal\Sources

**Use****Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

The output of this model is equal to zero.

*output = 0.0;*

**Interface****Outputs**

output

**Description**

## Stochastic

### Library

Signal\Signal Processing

### Use

**Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This submodel yields the mean of an input signal using the integral function:

$$output = \text{int}(input)/time$$

### Interface

#### Inputs

input

#### Description

Input signal

#### Outputs

output

Mean value of the input signal

### Library

Signal\Sources

### Implementations

frequency\_limited\_FOH

frequency\_limited\_ZOH

unlimited

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description - frequency\_limited\_FOH

This model generates a gaussian noise signal with gaussian distribution and variance 1 and random seed s. The noise is multiplied by the parameter amplitude.

$$output = amplitude * gauss(1, seed);$$

The noise signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two noise samples are interpolated (first order hold).

### Interface - frequency\_limited\_FOH

#### Outputs

output

#### Description

#### Parameters

seed

random seed

amplitude	-amplitude <= output <= +amplitude
frequency	frequency band of the noise

### Description - frequency\_limited\_ZOH

This model generates a gaussian noise signal with gaussian distribution and variance 1 and random seed s. The noise is multiplied by the parameter amplitude.

$$output = amplitude * gauss(1, seed);$$

The noise signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two noise samples are interpolated (first order hold).

### Interface - frequency\_limited\_ZOH

Outputs	Description
output	
Parameters	
seed	random seed
amplitude	-amplitude <= output <= +amplitude
frequency	frequency band of the noise

### Description - unlimited

This model generates a gaussian noise signal with gaussian distribution and variance 1 and random seed s. The noise is multiplied by the parameter amplitude.

$$output = amplitude * gauss(1, seed);$$

The noise signal has no frequency limitation.

### Note

It is advised only to use this implementation with fixed step integration methods such as Euler and Runge Kutta 2/4. If you run this implementation with a variable step integration method, simulations may get very slow!

### Interface - unlimited

Outputs	Description
output	
Parameters	
seed	random seed
amplitude	-amplitude <= output <= +amplitude

### Limitations

seed must be a number in the region <0,65000>.

**Library**

Signal\Sources

**Implementations**

frequency\_limited\_FOH  
frequency\_limited\_ZOH  
unlimited

**Use**

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description - frequency\_limited\_FOH**

This model generates a random (noise) signal with values between -amplitude and +amplitude and random seed  $s$ . The

$$output = ran(ampl, seed);$$

The noise signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two noise samples are interpolated (first order hold).

**Interface - frequency\_limited\_FOH****Outputs**

output

**Description****Parameters**

seed	random seed
amplitude	-amplitude <= output <= +amplitude
frequency	frequency band of the noise

**Description - frequency\_limited\_ZOH**

This model generates a random (noise) signal with values between -amplitude and +amplitude and random seed  $s$ .

$$output = ran(ampl, seed);$$

The noise signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two noise samples are interpolated (first order hold).

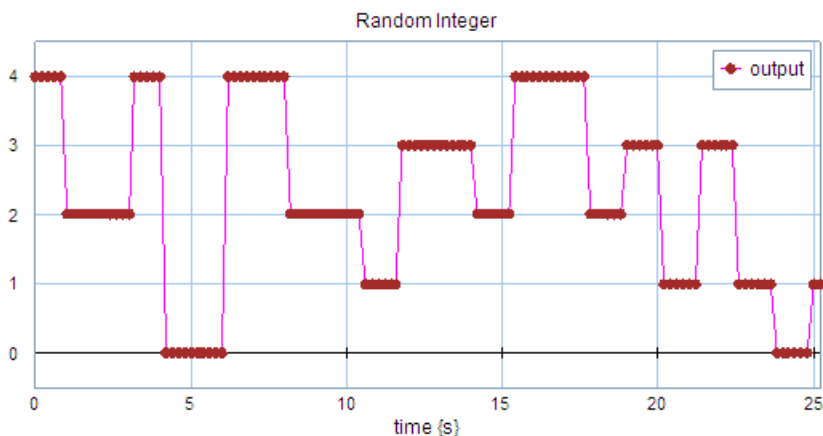
**Interface - frequency\_limited\_ZOH****Outputs**

output

**Description****Parameters**

seed	random seed
amplitude	-amplitude <= output <= +amplitude





*RandomInteger* output with a frequency of 1 Hz and  $m = 5$ .

The output signal is limited to a maximum frequency, which can be adjusted (parameter). Values in-between two samples are interpolated (first order hold).

## Interface

Outputs	Description
output	
<b>Parameters</b>	
seed	random seed
m	the output range [0, m-1]
frequency	frequency band of the output

## Limitations

seed must be a number in the region  $<0,65000>$ .

## Library

Signal\Stochastic

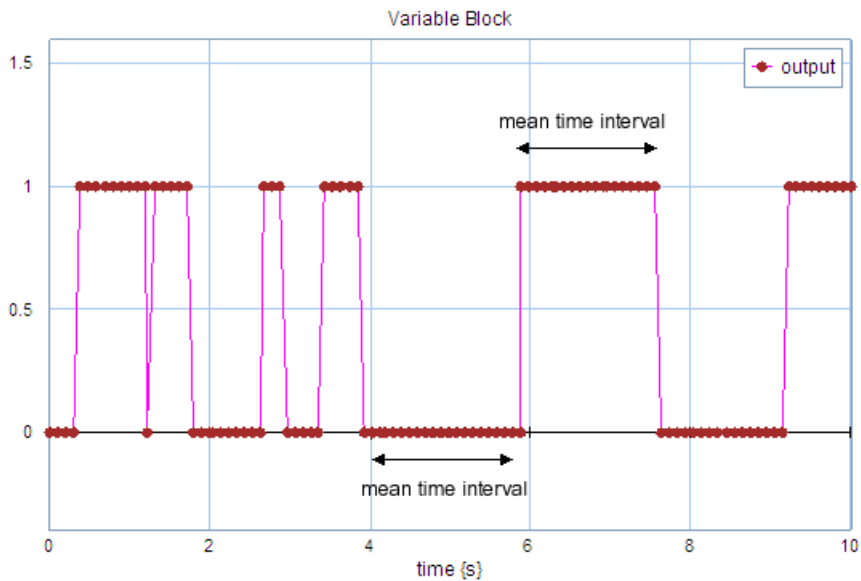
## Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description

This model generates a block signal that alternates between 0 and 1. The mean time interval of a section is given by the parameter *meanTimeInterval*. The distribution of the time interval is uniform between  $[0, 2 * \text{meanTimeInterval}]$ . With the parameter random seed you can choose to make the distribution variable or fixed for each simulation run.





*VariableBlock output with a mean time interval of 1 s.*

## Interface

### Outputs

output

### Description

### Parameters

meanTimeInterval

mean time {s} before the output signal changes

random seed

seed

### Limitations

seed must be a number in the region  $<0,65000>$ .

## Library

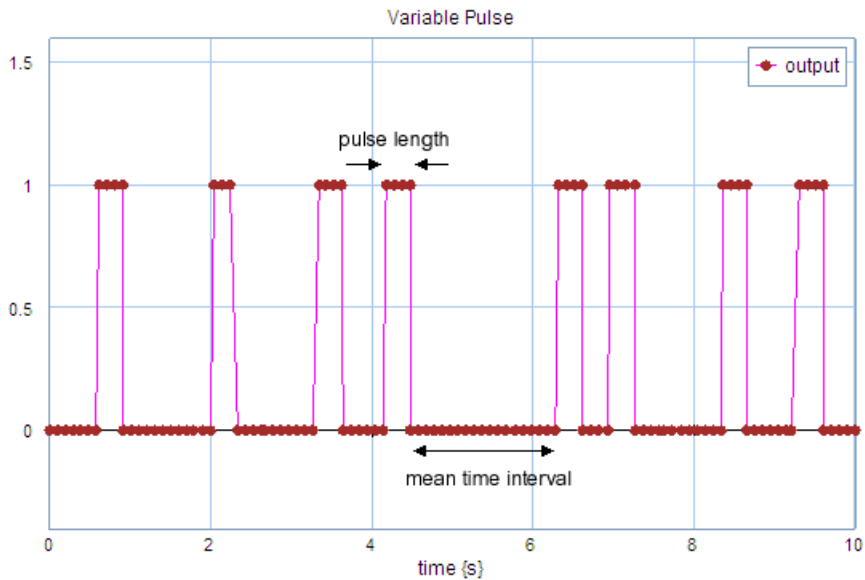
Signal\Stochastic

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

Description

This model generates a pulse train with a pulse value of 1. The pulse width is given by the parameter *pulseLength*. The mean time interval between two pulses is given by the parameter *meanTimeInterval*. The distribution of the time interval is uniform between [0, 2\**meanTimeInterval*]. With the parameter random seed you can choose to make the distribution variable or fixed for each simulation run.



*VariablePulse output with a pulse length of 0.3 s and a mean time interval of 1 s.*

Interface

Outputs

output

Parameters

meanTimeInterval

pulseLength

seed

Description

mean time {s} before the output signal changes

length of the pulse {s}

random seed

Limitations

seed must be a number in the region <0,65000>.

**Library**

Signal\Signal Processing

**Use****Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This submodel yields the standard deviation of an input signal using an integral function:

$$output = \sqrt{int( (input - mean)^2 / time) }$$

where mean is the mean of the input

**Interface****Inputs**

input

**Description**

Input signal

**Outputs**

output

Standard deviation of the input signal

**Library**

Signal\Signal Processing

**Use****Domains:** Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.**Description**

This submodel yields the variance of an input signal using an integral function:

$$output = int( (input - mean)^2 / time)$$

where mean is the mean of the input

**Interface****Inputs**

input

**Description**

Input signal

**Outputs**

output

Variance of the input signal

**Transfer Functions**

The Transfer Functions library contains a number of predefined transfer functions and a general transfer function model that opens the Linear System Editor.

**Without Dead Time**

<b>name</b>	<b>formula</b>	<b>description</b>
LinearSystem	-	Any Linear System without time delay
FO	$Y(s) = \frac{k}{\tau s + 1} \cdot U(s)$	First Order
FOL	$Y(s) = \frac{k(s\tau_L + 1)}{s\tau + 1} \cdot U(s)$	First Order with Lead Time
FOLA	$Y(s) = \frac{k(s\tau + 1)}{s\tau_L + 1} \cdot U(s)$	First Order with Lag
SOI	$Y(s) = \frac{k}{s(\tau s + 1)} \cdot U(s)$	Second Order with Integrator
SOO	$Y(s) = \frac{k}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot U(s)$	Second Order Overdamped
SOOL	$Y(s) = \frac{k(\tau_L s + 1)}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot U(s)$	Second Order Overdamped with Lead Time
SOU	$Y(s) = \frac{k}{\tau^2 s^2 + 2\zeta\tau s + 1} \cdot U(s)$	Second Order Underdamped
SOUO	$Y(s) = \frac{\omega^2 k}{s^2 + 2\zeta\omega s + \omega^2} \cdot U(s)$	Second Order Underdamped, Omega description

**With Dead Time**

<b>name</b>	<b>formula</b>	<b>description</b>
ZOD	$Y(s) = k e^{-\theta s} \cdot U(s)$	Zero Order plus Dead Time
FOD	$Y(s) = \frac{k e^{-\theta s}}{\tau s + 1} \cdot U(s)$	First Order plus Dead Time
SOID	$Y(s) = \frac{k e^{-\theta s}}{s(\tau s + 1)} \cdot U(s)$	Second Order with Integrator plus Dead Time

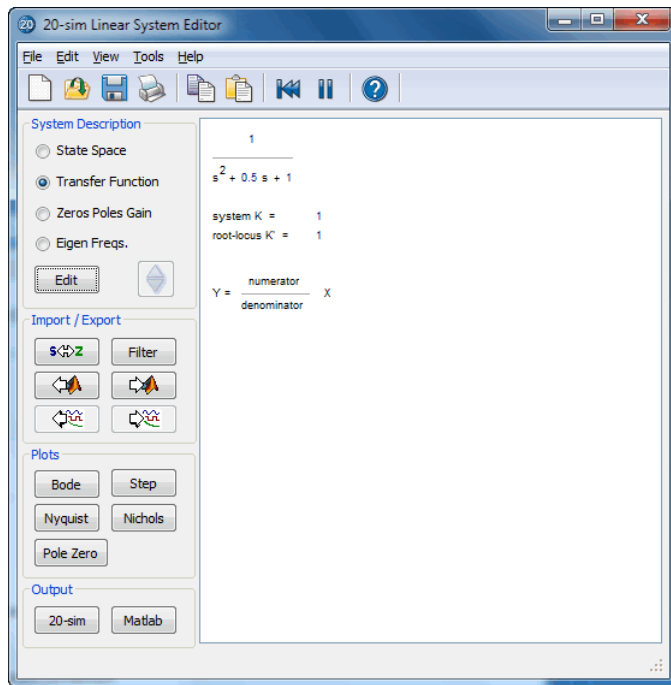
SOOD	$Y(s) = \frac{k e^{-\theta s}}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot U(s)$	Second Order Overdamped plus Dead Time
SOOLD	$Y(s) = \frac{k(\tau_L s + 1)e^{-\theta s}}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot U(s)$	Second Order Overdamped with Lead Time plus Dead Time
SOUD	$Y(s) = \frac{k e^{-\theta s}}{\tau^2 s^2 + 2\zeta\tau s + 1} \cdot U(s)$	Second Order Underdamped plus Dead Time
SOUDO	$Y(s) = \frac{\omega^2 k e^{-\theta s}}{s^2 + 2\zeta\omega s + \omega^2} \cdot U(s)$	Second Order Underdamped plus Dead Time, Omega description

**Library**

Signal\TransferFunctions

**Use****Domains:** Continuous. **Size:** 1-D. **Kind:** Block Diagrams.**Description**

When you select this model and click *Go Down* a special editor opens (Linear System Editor), allowing you to enter a linear system in State Space form, as a Transfer Function or by adding poles and zeros:



## Interface

### Inputs

input

### Outputs

output

### Initial Values

### Parameters

### Description

The model has internal states that are not accessible.

Parameters are entered by the Linear System Editor.

## Library

Signal\Transfer Functions

### Implementations

FO  
FOL  
FOLA  
SOI

SOO  
SOU  
SOUO  
SOOL

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

### Description - FO

This model describes a first order process determined by k and tau. The transfer function of this process is:

$$Y(s) = \frac{k}{\tau s + 1} \cdot U(s)$$

### Interface - FO

#### Inputs

input

#### Description

#### Outputs

output

#### Initial Values

state\_initial

The initial value of the output.

#### Parameters

k

Proportional gain [].

tau

Process time constant [s].

### Description - FOL

This model describes a first order process with lead time determined by the parameters k, tau and tauL. The transfer function of this process is:

$$Y(s) = \frac{k(s\tau_L + 1)}{s\tau + 1} \cdot U(s)$$

### Interface - FOL

#### Inputs

input

#### Description

#### Outputs

output

#### Initial Values

state_initial	Internal state.
---------------	-----------------

## Parameters

k	Proportional gain [].
tau	Process time constant [s].
tauL	Lead time constant [s].

### Description - FOLA

This model describes a first order process with lag determined by the parameters  $k$ ,  $\tau$  and  $\tau_L$ . The transfer function of this process is:

$$Y(s) = \frac{k(s\tau + 1)}{s\tau_L + 1} \cdot U(s)$$

## Interface - FOLA

Inputs	Description
input	
<b>Outputs</b>	
output	
<b>Initial Values</b>	
state_initial	Internal state.
<b>Parameters</b>	
k	Proportional gain [].
tau	Process time constant [s].
tauL	Lag time constant [s].

### Description - SOI

This model describes a second order process with integrator determined by the parameters  $k$  and  $\tau$ . The transfer function of this process is:

$$Y(s) = \frac{k}{s(\tau s + 1)} \cdot U(s)$$

## Interface - SOI

Inputs	Description
input	
Outputs	



output

**Initial Values**

state1_initial	Internal state.
state2_initial	The initial value of the output.

**Parameters**

k	Proportional gain [].
tau	Process time constant [s].

**Description - SOO**

This model describes an overdamped second order process determined by the parameters k, tau1 and tau2. The transfer function of this process is:

$$Y(s) = \frac{k}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot U(s)$$

**Interface - SOO**

**Inputs**

input

**Description**

**Outputs**

output

**Initial Values**

state1_initial	Internal state.
state2_initial	The initial value of the output.

**Parameters**

k	Proportional gain [].
tau1	First process time constant [s].
tau2	Second process time constant [s].

**Description - SOU**

This model describes an underdamped second order process, determined by the parameters k, tau and zeta. The transfer function of this process is:

$$Y(s) = \frac{k}{\tau^2 s^2 + 2\zeta\tau s + 1} \cdot U(s)$$

## Interface - SOU

## Inputs

input

## Outputs

output

### Initial Values

state1\_initial

Internal state.

state2\_initial

The initial value of the output after the dead time has passed.

## Parameters

k

Proportional gain [].

tau

Natural period of oscillation [s].

zeta

Damping factor [].

### Description - SOUO

This model describes an underdamped second order process, determined by the parameters  $k$ ,  $\omega$  and  $\zeta$ . The transfer function of this process is:

$$Y(s) = \frac{\omega^2 k}{s^2 + 2\zeta\omega s + \omega^2} \cdot U(s)$$

## Interface - SOUO

## Inputs

input

## Outputs

output

### Initial Values

state1\_initial

Internal state.

state2\_initial

The initial value of the output after the dead time has passed.

## Parameters

k

Proportional gain [].

omega	Natural frequency [rad/s].
zeta	Damping factor [].

### Description - SOOL

This model describes an overdamped second order process with lead time determined by the parameters k, tau1, tau2 and tauL. The transfer function of this process is:

$$Y(s) = \frac{k(\tau_L s + 1)}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot U(s)$$

### Interface - SOOL

#### Inputs

input

#### Description

#### Outputs

output

#### Initial Values

state1\_initial

Internal state.

state2\_initial

The initial value of the output.

#### Parameters

k

Proportional gain [].

tau1

First process time constant [s].

tau2

Second process time constant [s].

tauL

Lead time constant [s].

### Library

Signal\Transfer Functions

### Implementations

ZOD

FOD

SOD

SOOD

SOD

SOOLD

SOUDO

### Use

**Domains:** Discrete, Continuous. **Size:** 1-D. **Allowed in:** Block Diagrams.

**Description - ZOD**

This model describes a first zero process plus dead time determined by k and theta. The transfer function of this process is:

$$Y(s) = k e^{-\theta s} \cdot U(s)$$

**Interface - ZOD****Inputs**

input

**Description****Outputs**

output

**Parameters**

k

Proportional gain [].

theta

Dead time [s].

**Description - FOD**

This model describes a first order process plus dead time determined by k tau and theta. The transfer function of this process is:

$$Y(s) = \frac{k e^{-\theta s}}{\tau s + 1} \cdot U(s)$$

**Interface - FOD****Inputs**

input

**Description****Outputs**

output

**Initial Values**

state\_initial

The initial value of the output after the dead time has passed.

**Parameters**

k

Proportional gain [].

tau

Process time constant [s].

theta

Dead time [s].

**Description - SOID**

This model describes a second order process with integrator plus dead time determined by the parameters  $k$  and  $\tau$ . The transfer function of this process is:

$$Y(s) = \frac{k}{s(\tau s + 1)} \cdot U(s)$$

**Interface - SOID****Inputs**

input

**Description****Outputs**

output

**Initial Values**

state1\_initial

Internal state.

state2\_initial

The initial value of the output after the dead time has passed.

**Parameters** $k$ 

Proportional gain [].

 $\tau$ 

Process time constant [s].

 $\theta$ 

Dead Time [s].

**Description - SOOD**

This model describes an overdamped second order process plus dead time determined by the parameters  $k$ ,  $\tau_1$  and  $\tau_2$ . The transfer function of this process is:

$$Y(s) = \frac{k e^{-\theta s}}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot U(s)$$

**Interface - SOOD****Inputs**

input

**Description****Outputs**

output

**Initial Values**

state1\_initial

Internal state.

state2\_initial

The initial value of the output after the dead time has passed.

### Parameters

k	Proportional gain [].
tau1	First process time constant [s].
tau2	Second process time constant [s].
theta	Dead Time [s].

### Description - SOUD

This model describes an underdamped second order process plus Dead Time, determined by the parameters k, tau and zeta. The transfer function of this process is:

$$Y(s) = \frac{k e^{-\theta s}}{\tau^2 s^2 + 2\zeta \tau s + 1} \cdot U(s)$$

### Interface - SOUD

#### Inputs

input

#### Description

#### Outputs

output

#### Initial Values

state1_initial	Internal state.
state2_initial	The initial value of the output after the dead time has passed.

### Parameters

k	Proportional gain [].
tau	Natural period of oscillation [s].
zeta	Damping factor []
theta	Dead Time [s].

### Description - SOOLD

This model describes an overdamped second order process with lead time plus dead time determined by the parameters k, tau1, tau2 and tauL. The transfer function of this process is:

$$Y(s) = \frac{k(\tau_2 s + 1)e^{-\theta s}}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot U(s)$$

### Interface - SOOLD

#### Inputs

input

#### Outputs

output

#### Initial Values

state1\_initial

Internal state.

state2\_initial

The initial value of the output after the dead time has passed.

#### Parameters

k

Proportional gain [].

tau1

First process time constant [s].

tau2

Second process time constant [s].

tauL

Lead time constant [s].

theta

Dead Time [s].

### Description - SOUDO

This model describes an underdamped second order process plus Dead Time, determined by the parameters k, omega and zeta. The transfer function of this process is:

$$Y(s) = \frac{\omega^2 k e^{-\theta s}}{s^2 + 2\zeta\omega s + \omega^2} \cdot U(s)$$

### Interface - SOUDO

#### Inputs

input

#### Outputs

output

#### Initial Values

state1\_initial

Internal state.

state2\_initial

The initial value of the output after the dead time has passed.

**Parameters**

k

omega

zeta

theta

Proportional gain [].

Natural frequency [rad/s].

Damping factor []

Dead Time [s].



## 10 Modeling Tutorial

### 10.1 Friction

#### Introduction

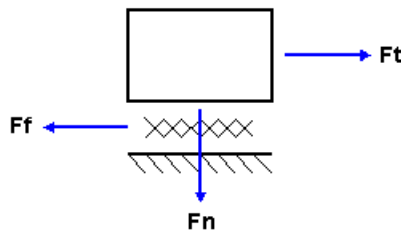
In all machines incorporating parts with relative motion, friction is present. Friction is a natural resistance to relative motion between two contacting bodies. At particular locations in machines, friction is an undesirable property. Friction can lead to bad performance of for example a servo system. At other locations, friction plays an important role and is desirable, as is the case for example in actions as walking and grasping and in a brake system.

In most systems, friction has a negative influence on the performance of the system. Under certain conditions, friction in a system can result in effects like a steady state error, tracking errors, especially nearby velocity reversals (reversal bump effect: getting stuck when moving through zero velocity), limit cycles (hunting) and/or stick-slip.

To overcome these negative effects, insight in friction phenomena, and proper models of these phenomena are useful. This chapter will give attention to these aspects of friction and describe the friction models that are available in the 20-sim library.

#### Normal Force

Assume a mass is dragged over a surface and experiences friction.



A tension force  $F_t$  has to be applied to overcome the amount of friction force  $F_f$ . The friction force will depend on the applied normal force as:

$$F_t = F_n * f(x, v, \dots);$$

where  $f$  is the friction function which depends on the displacement  $x$ , velocity  $v$  etc.

In most cases a normal force is available (disk breaks, surface friction, clutches etc.). Therefore all models in the 20-sim friction library are described with a normal force input. For those models that do not experience a normal force (bearings), a unity normal force  $F_n = 1$  [N] is applied.

## Friction Phenomena

There are different phenomena of friction. The following friction phenomena are described in the friction models in 20-sim:

- *static friction*: the torque or force necessary to initiate motion from rest (the so called break-away force); it is often larger than the Coulomb friction,
- *Coulomb friction (kinetic friction, dynamic friction)*: the friction component that is only dependent of the direction of velocity, not of the magnitude of the velocity,
- *viscous friction*: the friction component that is proportional to velocity and goes to zero at zero velocity,
- *Stribeck friction (Stribeck effect)*: the friction phenomenon that arises from the use of fluid lubrication and gives rise to decreasing friction with increasing velocity at low velocity,
- *pre-sliding displacement (Dahl effect)*: the spring-like behavior of friction that causes a displacement linear dependent on the applied force if this applied force is less than the break-away force,
- *varying break-away force (rising static friction)*: the dependence of the break-away force on the rate of increase of the applied force,
- *frictional lag*: the delay in the change of the friction force as a function of a change in the velocity.

Beside the friction phenomena mentioned above, some other effects with respect to friction are reported in the literature. These effects are not incorporated into the 20-sim library of friction models:

- *Time-dependent friction*: From experiments it is known that friction changes with time. These changes of friction with time are due to such things as loss of lubricant, deformation of the surface material, change in temperature due to generated heat and/or accumulation of wear debris.
- *Position-dependent friction*: A dependence of the friction on the position of a system is another effect that is experimentally observed and is well known by a lot of researchers. This position-dependency is caused by spatial inhomogeneities in the transmission of the system due to contact geometry and/or loading which varies as a function of position. As the load varies, the normal force between the sliding surfaces varies, causing a varying friction (friction is linear dependent on the normal force). By preloading the transmission elements and roller bearings this dependency of friction on the load can be decreased.
- *Direction-dependent friction*: A lot of researchers have found the friction to be dependent on the direction of the motion of a system. Different Coulomb and viscous friction levels in the left and right directions of a single, linear motion have been observed experimentally on many occasions. Theoretically, this may be due to anisotropies in material or geometry.

## Wet and Dry Friction

### Wet Friction

Most machines are lubricated in order to decrease the effects of friction. But in most cases, this is not sufficient and significant friction effects remain.

There are four regimes of lubrication in a system with grease or oil in which the phenomena act that are mentioned in the previous section: static friction, boundary lubrication, partial fluid lubrication and full lubrication. Each of these four regimes contribute to the dynamics of the system. In the figure below, these four regimes are given in the plot of the friction force as a function of the sliding velocity, sometimes referred to as the *Stribeck curve*.

A description of the four regimes is:

#### Regime 1: Static friction and pre-sliding displacement

Although in this regime of static friction there is no sliding, because of the fact that contacts between two surfaces are compliant, there are small motions when a force is applied. The contact between two surfaces can be seen as an elastic contact. The displacement is an approximately linear function of the applied force (a spring-like behavior), up to a critical force at which breakaway occurs and sliding begins. The transition from the elastic contact with pre-sliding displacement in static friction to sliding is not abrupt: first sliding starts at the boundary of a contact and then it propagates toward the center.

#### Regime 2: Boundary lubrication

In this regime the sliding velocity is very low and is not adequate to build a fluid film of the lubricant between the sliding surfaces. The boundary layer of the surfaces serves to provide lubrication. In most cases, the friction in this boundary lubrication regime is higher than in case of fluid lubrication, as is the situation in regimes three and four.

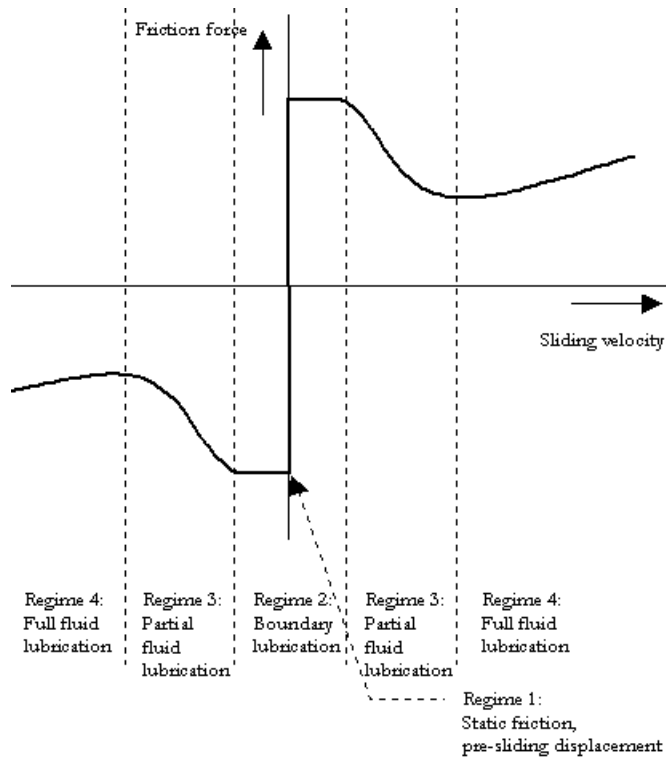
#### Regime 3: Partial fluid lubrication

Lubricant is brought into the load-bearing region between the sliding surfaces through motion. Some lubricant is expelled by pressure arising from the load, but as a result of the viscosity not all of the lubricant will escape and thus a thin film of lubricant is formed between the sliding surfaces. Not at all places of the contact of the surfaces this film will exist; at some places there is still solid-to-solid contact: there is partial fluid lubrication. As the velocity becomes larger, more lubricant will be brought between the surfaces and less solid-to-solid contacts will exist. This explains the descending friction force when the velocity increases, called the Stribeck effect.

There is a time lag between a change in the velocity or load conditions and the change in friction to a new steady state level: the phenomenon of frictional lag takes place. This effect is a consequence of the state in the frictional contact that does not come to its new equilibrium instantly: it takes time for the lubricant to be brought or removed between the load bearing region of the sliding surfaces.

#### Regime 4: Full fluid lubrication

In this regime the solid-to-solid contacts are all eliminated. The wear is reduced by orders of magnitude. The viscosity of the lubricant is determinative for the friction force and the friction phenomenon now at work is the well-behaved viscous friction, besides the Coulomb friction.



*The four dynamic regimes of friction in the plot of friction force as a function of sliding velocity.*

## Dry Friction

Dry friction is friction between two bodies in absence of contaminations of the contact surfaces. This is an ideal situation which is not possible to achieve in real systems, due to the fact that chemical reactions will occur at the surfaces. Therefore dry friction will show some of the effects described above. Some special effects due to the use of lubricants, such as the Stribeck effect and sometimes viscous friction will not be significant in dry friction.

## Static and Dynamic Phenomena

The friction phenomena can be grouped in static and dynamic phenomena:

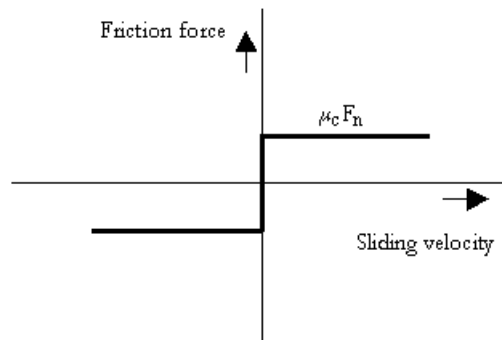
- static friction phenomena:
  - static friction
  - Coulomb friction (dynamic friction)
  - viscous friction
  - Stribeck friction (Stribeck effect)
- dynamic friction phenomena:
  - pre-sliding displacement (Dahl effect)
  - rising static friction (varying break-away force)
  - frictional lag

Static friction models only have a static dependency on velocity. Even when the applied force is very small, the result is a non-zero velocity. This means a significant displacement is found after some time. Therefore static friction models should only be used in systems where the applied forces are large ( $\gg$  static friction), or change sign often.

Dynamic friction models incorporate a spring like behavior for small forces. I.e. no significant displacement is found when the applied force is smaller than the static friction.

### Coulomb friction

Static friction phenomena only have a static dependency on velocity. The first static friction model was the classic model of friction of Leonardo Da Vinci: friction force is proportional to load, opposes the direction of motion and is independent of contact area. Coulomb (1785) further developed this model and the friction phenomena described by the model became known as *Coulomb friction*. The model is given in the figure below.



*The Coulomb friction model.*

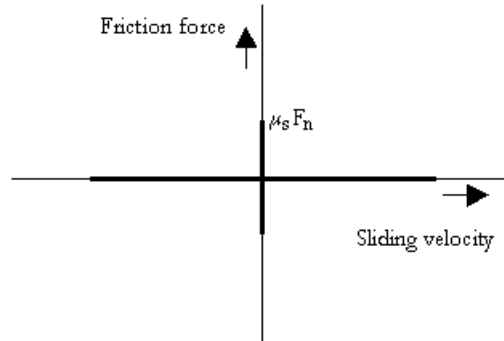
The friction force can be described as:

$$F_f = F_n * \mu_{c} * \text{sign}(v);$$

with  $\mu_c$  the *Coulomb friction coefficient*. The Coulomb friction model is, because of its simplicity, often used. In many textbooks it is also referred to as *dynamic friction* and  $\mu_s$  described as the *dynamic friction coefficient*.

## Static Friction

Morin (1833) introduced the idea of static friction: friction force opposes the direction of motion when the sliding velocity is zero.



The static friction force is equal to the tensile forces until a maximum or minimum is reached:

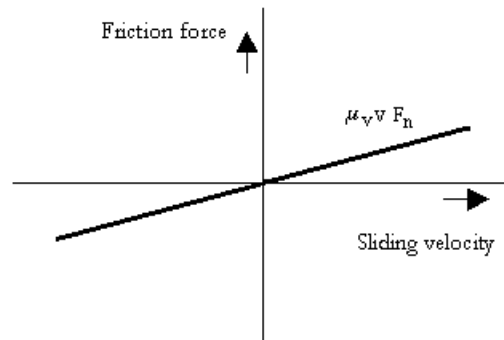
$$F_{f\_max} = F_n * \mu_{s\_};$$

$$F_{f\_min} = -F_n * \mu_{s\_};$$

with  $\mu_{s\_}$  the *static friction coefficient*.

## Viscous friction

Reynolds (1866) developed expressions for the friction force caused by the viscosity of lubricants. The term viscous friction is used for this friction phenomenon.



*The viscous friction model.*

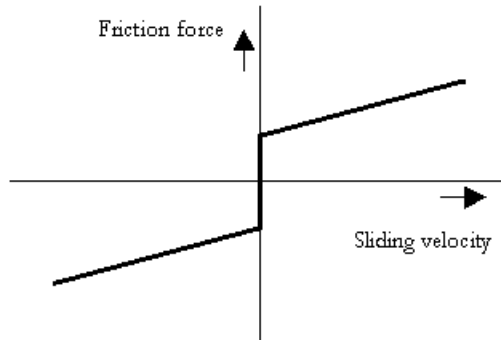
The friction force can be described as:

$$F_f = F_n * \mu_{v\_} * v;$$

with  $\mu_{v\_}$  the **viscous friction coefficient**.

### Coulomb plus Viscous friction

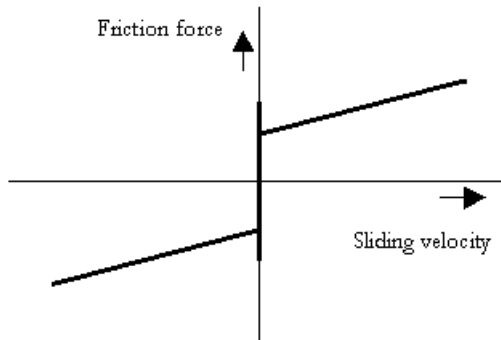
This viscous friction combined with the Coulomb friction gave the model given in the figure below.



*The Coulomb plus viscous friction model.*

### Static plus Coulomb plus Viscous friction

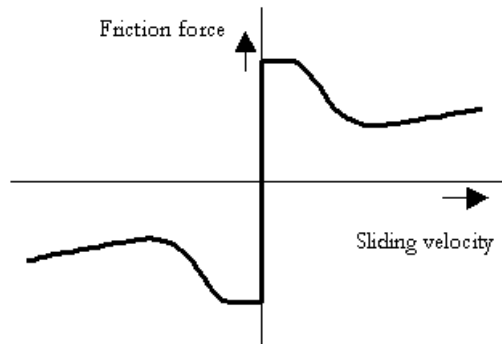
When static friction is added, a friction model appears that is commonly used in engineering: the *Static plus Coulomb plus Viscous friction model*. This model is depicted in the figure below.



*The static, Coulomb plus viscous friction model.*

### Static plus Coulomb plus Viscous plus Stribeck friction

Stribeck (1902) observed that for low velocities, the friction force is decreasing continuously with increasing velocities and not in a discontinuous manner as described above. This phenomenon of a decreasing friction at low, increasing velocities is called the Stribeck friction or effect. The model including *Static, Coulomb, Viscous and Stribeck friction* is given below.



*The static, Coulomb, viscous plus Stribeck friction model.*

The Stribeck effect is described by the parameter  $v_{st}$  which is the characteristic Stribeck velocity. It denotes the sliding velocity where only a 37% of the static friction is active. In other words, small values of  $v_{st}$  give a fast decreasing Stribeck effect and large values of  $v_{st}$  give a slow decreasing Stribeck effect.

### Continuous Functions

All these friction models above show a discontinuity at zero velocity. At zero velocity the friction force as a function of only velocity is not specified. What for example should the friction force be at zero velocity in the Coulomb friction model? The discontinuous behavior of this model near zero velocity is sometimes approximated with a continuous function, for example:

$$F = \tanh(\text{slope} * v);$$

and the inverse

$$v = \text{arctanh}(F)/\text{slope};$$

with *slope* a very large constant. The use of continuous functions results in straightforward models that are easy to simulate for large forces and velocities. For small forces and velocities, the the slope parameter has to be chosen sufficiently high, to avoid creep (the model starts to move, even when the applied force is smaller than the static or Coulomb friction force). This results in stiff models, which are hard to simulate.

### LuGre friction model

The LuGre model is inspired by the bristle interpretation of friction (surfaces are very irregular at the microscopic level and two surfaces make contact at a number of asperities, which can be thought of as elastic bristles), in combination with lubricant effects.

Friction is modeled as the average deflection force of elastic springs. When a tangential force is applied the bristles will deflect. If the deflection is sufficiently large, the bristles start to slip. The average deflection at steady state slip is determined by the velocity, so that for low velocities the steady state deflection, and therefore the friction force, decreases with increasing velocity. This corresponds to more lubricant being forced into the interface, and pushing the surfaces apart, as the velocity increases. This produces the Stribeck effect. The model also includes rate dependent friction phenomena such as varying break-away force and frictional lag. The model behaves like a well damped spring with a stiffness at zero speed for small motions.



## Comparison of Friction Models

In order to get insight in the friction phenomena, a friction model should incorporate as much friction phenomena and behave as much as real friction. In the table below an overview of the different models of the 20-sim library with respect to the friction phenomena is given.

	<b>Coulomb model</b>	<b>Coulomb, viscous model</b>	<b>static, Coulomb, viscous model</b>	<b>static, Coulomb, viscous, Stribeck model</b>	<b>LuGre model</b>
<b>static friction phenomena</b>					
Coulomb	<b>V</b>	<b>V</b>	<b>V</b>	<b>V</b>	<b>V</b>
viscous		<b>V</b>	<b>V</b>	<b>V</b>	<b>V</b>
static			<b>V</b>	<b>V</b>	<b>V</b>
Stribeck				<b>V</b>	<b>V</b>
<b>dynamic friction phenomena</b>					
pre-sliding displacement					<b>V</b>
varying break-away force					<b>V</b>
frictional lag					<b>V</b>

From this overview it can be seen that all friction phenomena are incorporated in the LuGre model. From the literature, it is known that the behavior of the LuGre model is much alike real friction.

For most engineering applications, a static friction model, for example a static, Coulomb, viscous friction model, is sufficient. If all friction effects should be modeled, the LuGre friction model seems best suited.

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## 10.2 Bond Graphs

### Dynamic Systems

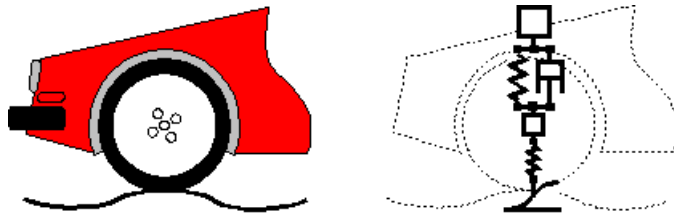
An important aspect in mechatronic systems is the dynamic behavior, i.e. the behavior of the system as function of time. Especially in systems that display swift changes or systems that should behave accurately, the dynamic behavior is important. It is therefore useful to predict the dynamic behavior of a system. Modeling and simulation is useful for making such predictions.

There are various methods of modeling and simulating dynamic systems. A well known one is the *Lumped Parameter Method*.

With the *Lumped Parameter Method*, the dynamic behavior of a system is concentrated in discrete points. The interaction of these points gives us insight in the behavior of the real system. The more discrete points are used the more accurate the model will be.

There are various ways to represent lumped parameter models. Well known representations are iconic diagrams, differential equations, block diagrams and bond graphs.

Let's consider the suspension of a car. A lumped parameter model starts with the identification of the various lumps (or parts or components) of this system. We start with the car body. It is supposed to be a rigid body and therefore this part is represented with the icon of a mass. The suspension of the car is represented by a spring damper combination. The wheel is considered to have a significant mass and to be elastic. This component is therefore represented by a mass and spring icon. Finally the road is modeled by path generator function. The resulting ideal physical model (IPM) is shown below.

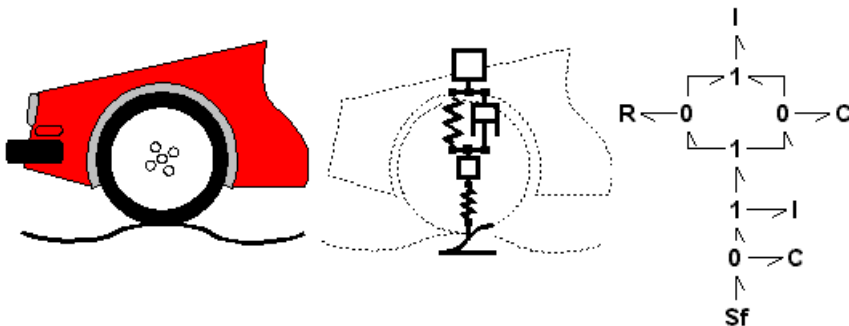


*Iconic diagram of a car suspension.*

## Bond Graphs

Bond graphs are a network-like description of physical systems in terms of ideal physical processes. With the bond graph method we split up the system characteristics into an (imaginary) set of separate elements. Each element describes an idealized physical process. To facilitate drawing of bond graphs, the common elements are denoted by special symbols.

Look again at the car suspension example. In the picture below at the right a bond graph is shown that has been entered in 20-sim. All elements of the ideal physical model have corresponding elements in the bond graph. The connections between the elements in the bond graph, which are known as bonds, represent ideal energy transfer between the elements, i.e. no energy is stored, generated or dissipated. Bonds are drawn with harpoons (the half arrows).



*The car suspension model (middle) and corresponding bond graph model (right).*

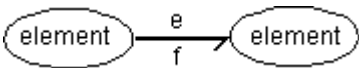
For the mechanical domain, ideal velocity sources are in bond graphs denoted by the symbol  $Sf$ . Dampers are denoted by an  $R$ , springs by a  $C$  and masses by a  $I$ . With a  $1$  a structural connection of elements is denoted and with a  $0$  a velocity difference is denoted.

A bond graph describes a physical system as a number of physical concepts (the elements) connected by energy flows (the bonds).

## Effort and Flow

A bond between two elements transfers power from one element to the other. This flow of energy can be described in many ways. For bond graphs a uniform approach is chosen:

The flow of energy between two elements (and thus a bond) is always characterized by two variables, of which the product is power. According to the bond graph notation, these variables are called *effort* (*e*) and *flow* (*f*).



*Effort and flow as variables of a bond.*

The effort and flow variables make up a combination that is typical for a physical domain. The product of effort and flow is always power. We call such a pair of variables *power conjugated variables*. For example voltage and current are used for electrical networks and force and velocity are used for mechanical (translation) systems. The table below shows the variables for the domains that are currently supported in 20-sim.

Domain	effort ( <i>e</i> )	flow ( <i>f</i> )
power	effort <i>e</i>	flow <i>f</i>
mechanical (translation)	force <i>F</i> [N]	velocity <i>v</i> [m/s]
mechanical (rotation)	torque <i>T</i> [Nm]	angular velocity <i>omega</i> [rad/s]
pneumatic	pressure <i>p</i> [Pa]	volume flow <i>phi</i> [m <sup>3</sup> /s]
thermal	temperature <i>T</i> [K]	entropy flow <i>dS</i> [J/Ks]
electric	voltage <i>u</i> [V]	current <i>i</i> [A]
hydraulic	pressure <i>p</i> [Pa]	volume flow <i>phi</i> [m <sup>3</sup> /s]
magnetic	current <i>i</i> [A]	voltage <i>u</i> [V]
pseudothermal	temperature <i>T</i> [K]	heat flow <i>dQ</i> [W]

*The effort and flow variables for several domains.*

To most general domain is power. Bonds of this domain can connected to elements of all domains. For the thermal domain there is one pair of effort and flow, *T* and *dS*, that multiplies to power. The pair *T* and *dQ* however, is more often used but does not multiply to power. Therefore the domain with these variables is called pseudothermal.

**Note**

- There is a direct relation between the across and through variables of an iconic diagram an the effort and flow variables of a bond graph:

Domain	Non-mechanical domains	Mechanical Domains
across variable	effort	flow
through variable	flow	effort

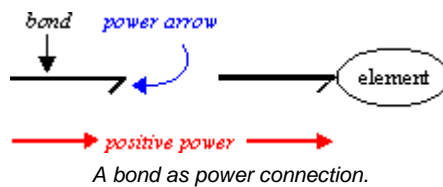
*The relation between across and through variables and effort and flow variables.*

- 20-sim propagates domains. If a bond of the general power domain is coupled with an element of the electrical domain, it automatically becomes an electrical bond. The other end of the bond can then only be connected to another element of the electrical domain.
- If you want to use a bond of a domain that is not supported or has variables other than across and through, use the general power domain. The across and through variables can then be used as an alias for your own variables.

## Bonds

The power of a bond is positive when both effort and flow have a positive value or both effort and flow have a negative value (power = effort  $\times$  flow).

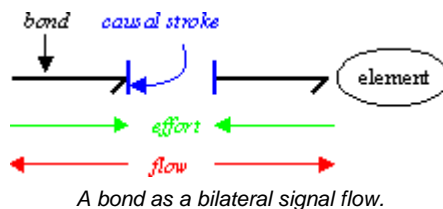
To denote the orientation, i.e. the direction of positive power, we use the harpoon at the end of a bond. An element with an inward bond connected, consumes power when the product of effort and flow is positive.



When two elements are connected by a bond, one element will always determine the effort, while the opposite element will always determine the flow. The element that determines the effort, gets an enforced flow from the other element.

We can therefore also see a bond as a bilateral signal connection (effort-signal and flow-signal), of which the directions are opposite to each other.

With *direction* we mean the direction of the flow of information, just like in a block diagram. In a block diagram the effort and flow variables, which together form the flow of power, are not shown as a couple. This breaks up the symmetry between the physical system and the structure of the model.



The interpretation of a bond as a bilateral signal flow, does not fix the individual direction of the effort and the flow. It only means the direction of the effort and flow are opposite. For the derivation of a simulation model out of a bond graph however, the individual directions are of importance.

*To indicate the individual direction of the effort and flow, we use a small stroke (causal stroke) perpendicular to the bond. This stroke indicates the direction of the effort. The direction of the flow is opposite.*

The choice of the direction of signals, also known as causality, depends on the element that is connected to the bond.

## Standard Elements

To facilitate drawing of bond graphs, the common elements are denoted by special mnemonic symbols. The elements can be divided in several classes:

- Junctions: (0 junction, 1 junction) elements that couple energy between various other elements.
- Buffers: (C,I) elements that store energy.
- Dissipators: (R) elements that dissipate energy.
- Sources: (Se,Sf) elements that generate energy.
- Modulated Sources: (MSe, MSf) elements that generate energy (driven by signals).
- Transformers and Gyrators: (TF, GY) elements that convert energy (ideally).
- Modulated Transformers and Gyrators: (MTF, MGY) elements that convert energy (driven by signals).
- Other elements: other elements and user defined elements.

## Orientation

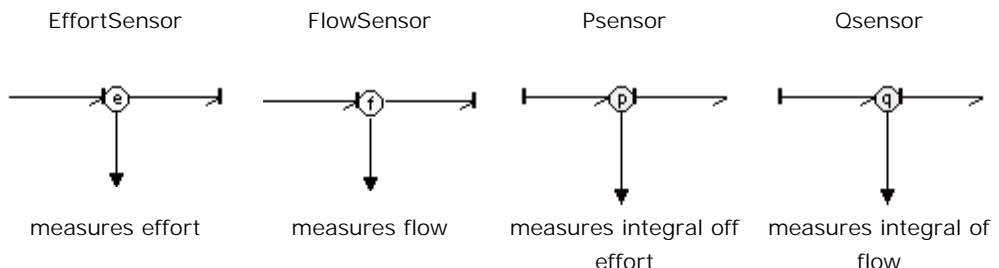
The orientation of a bond, i.e. the direction of the half arrow, denotes the direction of positive power. An element with an incoming bond consumes power when the product of effort and flow is positive. For R, C and I-elements an incoming bond is the standard orientation. For sources the standard orientation is outgoing, because a source supplies power to the rest of the system. For the TF and GY-element the standard orientation is one incoming bond and one outgoing bond, since this reflects the natural flow of power. For the other bonds in a model, as much as possible an orientation from source to load is applied.

## Bonds and Signals

Bonds Graph models are useful when describing systems with powerflow. In mechatronic systems these systems are usually coupled to systems that handle (powerless) signals. These systems are more conveniently described by block diagrams. Bond graphs can be combined with block diagrams. The coupling can be performed by special submodels.

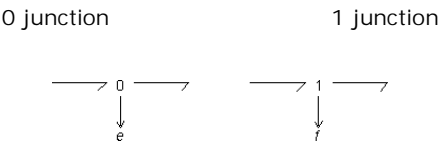
## Sensors

In general a sensor measures the flow, the effort, the integral of the flow or the integral of the effort. Sensors can be found in the 20-sim bond graph library.



Junctions

In 20-sim 1 junctions have a signal output which is equal to the flow. From a 1 junction a signal can be drawn which can be used as input for a block diagram. In a similar way an effort signal can be drawn from a 0 junction.

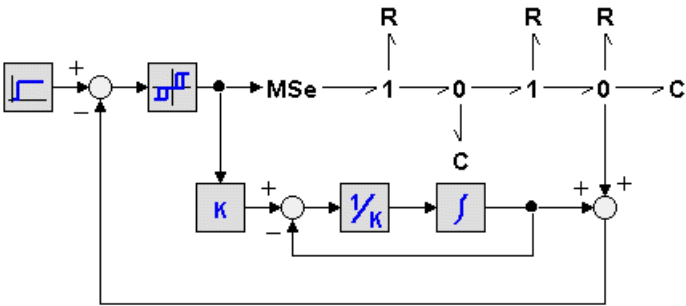


Modulated Elements

The result of a block diagram can be converted into power by means of a generator. In a bond graph model, this can be done by connecting a signal to modulated source elements. These elements convert input signals into efforts or flows. Other elements that use a signal input are modulated transformers and modulated gyrators.

Example

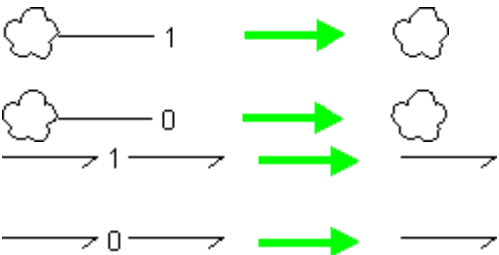
An example model where a bond graph and a block diagram are coupled is shown in the picture below. As can be seen an effort signal is measured at the 0 junction. In the block diagram part it is processed and fed back into the bond graph at the modulated effort source.



Simplification of Bond Graph Models

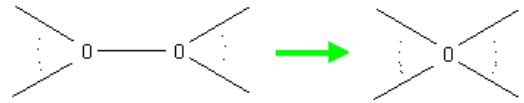
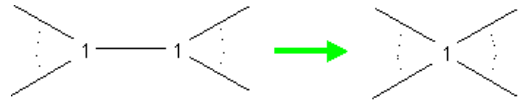
When a bond graph model has been created by converting all elements of the iconic diagram into bond graph elements and connecting the elements, simplifications can be performed. This can be easily done by applying the following set of rules (the bonds that have no half arrow, are allowed in both orientations).

- 1. Eliminate loose junctions.

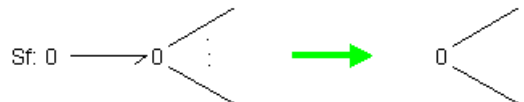
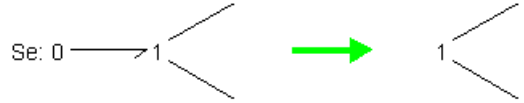


- 2. Eliminate junctions.

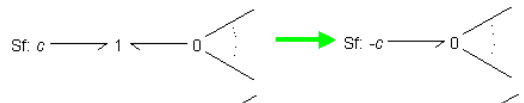
3. Melt equal junctions.



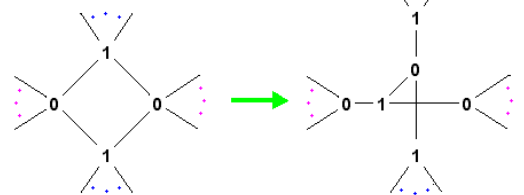
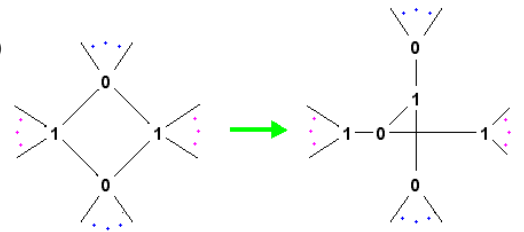
4. Eliminate sources with a zero output.



5. Eliminate junction in combination with a sign change on the source element.



6. Eliminate a double difference (two 0-junctions coupled with two 1-junctions)



### Note

Simplification rules 1, 2, 3 and 6 can be performed automatically in 20-sim using the Simplify Model command.



## Causality

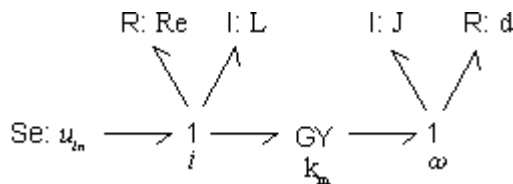
Causal analysis is the determination of the direction of the efforts and flows in a bond graph model. The result is a causal bond graph which can be considered as a compact block diagram. From causal bond graph we can directly derive an equivalent block diagram. In 20-sim causality is assigned automatically. To create a causal bond graph 20-sim will perform the following steps.

1. Apply causality for all elements with fixed causality (Se,Sf,Mse,MSf,user defined models), i.e. assign a causal stroke to all bonds connected to elements with fixed causality.
2. Apply,as much as possible, causality for elements that have a constraint causality (0 junction, 1 junction, TF,GY,MTF,MGY,user defined models).
3. Apply causality for an arbitrary element with preferred causality (C,I,user defined models). If possible, let this be the preferred causality. Now iterate step 2 and 3 as far as possible.
4. Apply causality for an arbitrary element with indifferent causality (R,user defined models). If this causality is not fixed, choose a causality arbitrarily. Now iterate step 2, 3 and 4 as far as possible.

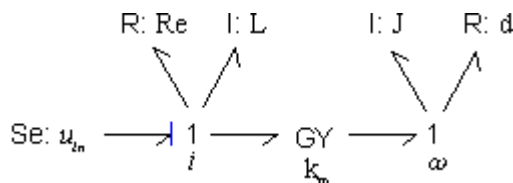
In many cases, the bond graph model is causal after step 2. However, sometimes a *causal conflict* occurs. This means the model is not correct arithmetically. Often this points out an ill-defined model. Redefinition of the ideal physical model will solve the problem. Sometimes the model is only causal after step 4. This means the model contains an *algebraic loop*. Models with algebraic loops are generally hard to simulate.

## Example

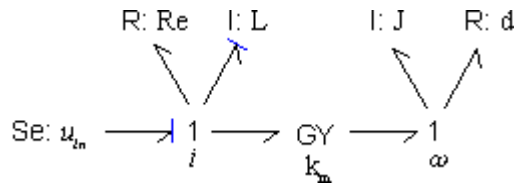
Causal assignment will be illustrated by an example. We will manually create a causal bond graph out of the following model:



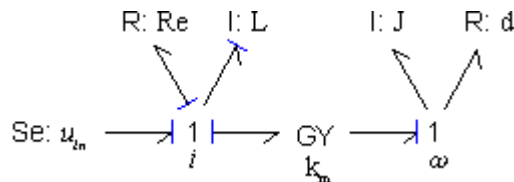
1. Apply fixed causality:



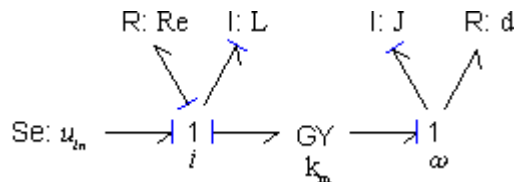
2. Apply constraint causality. This step is not yet applicable.
3. Apply preferred causality. We can choose between the two I-elements. Let's select the left one and assign causality in its preferred form:



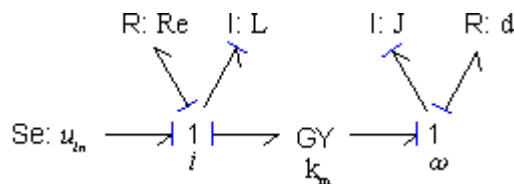
4. Apply constraint causality. The 1 junction on the left has one bond with effort-out causality (seen from the 1 junction). The other bonds connected must therefore have effort-in causality (seen from the 1 junction). In a same way we can now assign causality for the GY-element:



5. Apply preferred causality. Only the right I-element is left. We can assign causality in its preferred form:



6. Apply constraint causality. The 1 junction on the right has one bond with effort-out causality (seen from the 1 junction). The other bonds connected must therefore have effort-in causality. Therefore we can assign causality for the R-element:



## Creating a Bond Graph model

There are various methods described in literature to convert a ideal physical model into a bond graph. The simplest method is a direct conversion of the parts of the ideal physical model into bond graph elements. It is based on the fact that for every physical domain, junctions have a special interpretation. This allows us to make tables of ideal physical model parts and their direct representation as bond graph elements. The drawback of the method is that it is not generally applicable: for physical domains that are not described here, the user is referred to other methods.

1. Create an ideal physical model.
2. Replace each part of the ideal physical model with corresponding bond graph elements. Standard replacements are shown in the tables of this tutorial.
3. Select the bond graph elements in the 20-sim library and drag and drop them to the 20-sim editor.
4. Connect the elements according to the ideal physical model.
5. Simplify the bond graph according to the given rules.
6. Compile the bond graph model and run a simulation.

## From Iconic Diagram to Bond Graph

There are various methods described in literature to convert a iconic diagrams into bond graph models. The simplest method is a direct conversion of iconic diagrams into bond graph elements. It is based on the fact that for every physical domain, junctions have a special interpretation. This allows us to make tables of iconic diagrams and their direct representation as bond graph elements. The drawback of the method is that it is not generally applicable: for physical domains that are not described here, the user is referred to other methods.

- Mechanical Domain
- Electrical Domain

## Iconic Diagrams to Bond Graphs (Electrical Domain)

In the electrical domain, terminals and knots can be replaced by 0 junctions. With this knowledge and the description of various icons a table can be created that shows icons of electrical elements and their equivalent bond graph elements. The method of creating a bond graph model is:

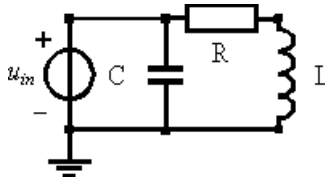
1. Create an iconic diagram of the electrical system.
2. Reference points or grounds are split up as much as possible.
3. Replace every element of the diagram by its bond graph equivalent using the conversion table.
4. Replace every knot that has been left by a 0 junction.
5. Connect all elements and junctions with bonds according to the layout of the electrical system.

- Simplify the resulting bond graph model, using the given set of simplification rules.

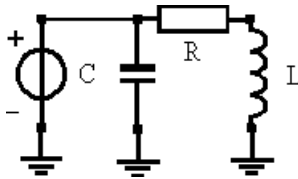
### Example

The method will be illustrated by an example. We will convert an electrical circuit into a bond graph model.

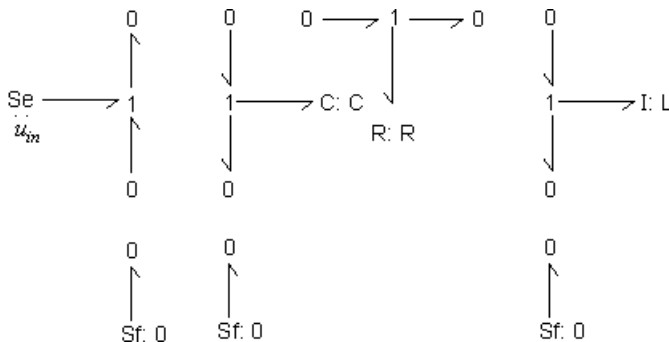
- Create an iconic diagram



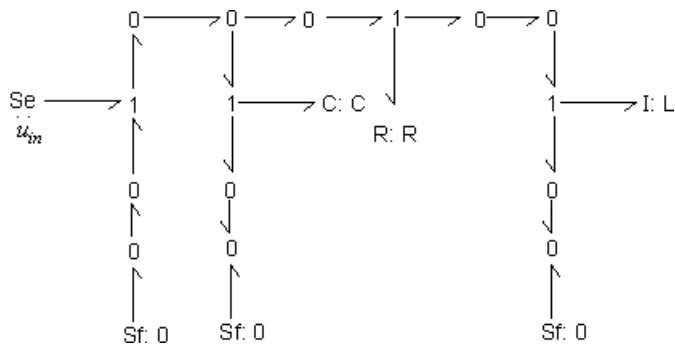
- Split up reference points.



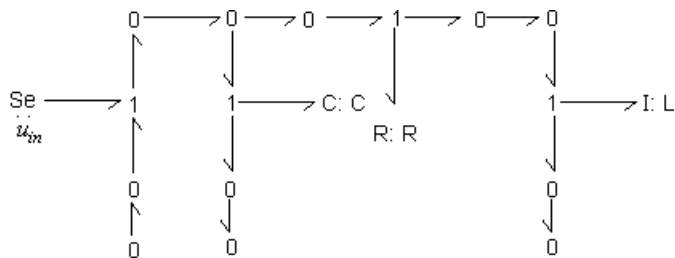
- Replace elements by bond graph equivalents. Note that we have arranged the orientation of the bonds (the direction of the half arrow) as much as possible in the direction of the power flow from the source to the load elements.



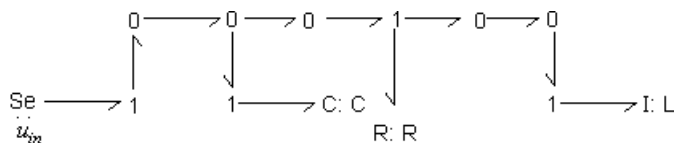
- Replace every knot that has been left by a 0 junction. In this model no knots have been left. Step 4 is therefore not applicable.
- Connect all elements and junctions with bonds, according to the layout of the electrical system. A comparison between the iconic diagram and the bond graph model clearly shows the symmetry between both representations. It is obvious that any change or addition in the iconic diagram, can be easily implemented in the bond graph model.



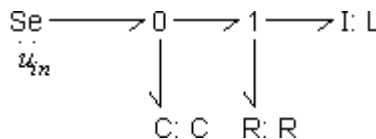
7. Simplify the resulting bond graph model. First we eliminate the Sources (Se elements) with zero output.



8. Eliminate loose junctions.



9. Eliminate junctions.



The simplified model does not show a direct symmetry with the iconic diagram. It does give a clear insight in the flows of power from the voltage source to the other elements.

### Iconic Diagrams to Bond Graphs (Mechanical Domain)

In the mechanical domain, both translational and rotational, terminals and knots can be replaced by  $1$  junctions. With this knowledge and the description of various icons a table can be created that shows icons of mechanical elements and their equivalent bond graph elements. The method of creating a bond graph model is:

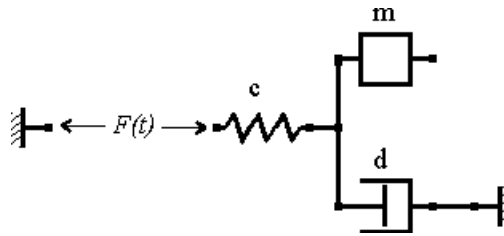
1. Create an iconic diagram of the mechanical system.
2. Reference points or grounds are split up as much as possible.

3. Replace every element of the diagram by its bond graph equivalent using the conversion table.
4. Replace every knot that has been left by a 1 junction.
5. Connect all elements and junctions with bonds, according to the layout of the mechanical system.
6. Simplify the resulting bond graph model, using the given set of simplification rules.

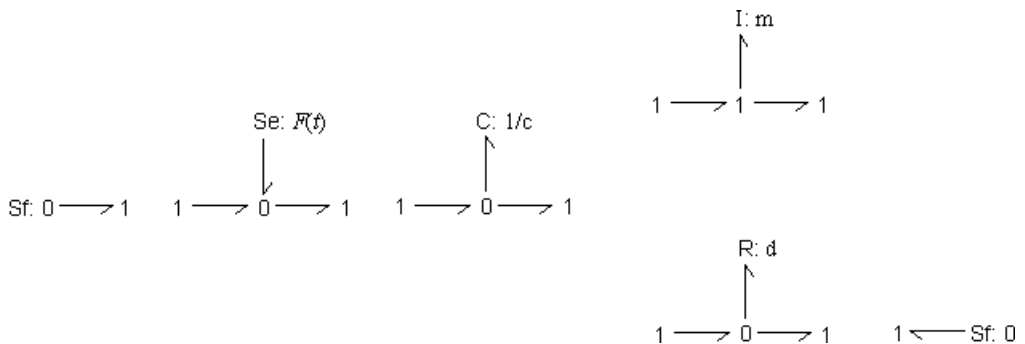
### Example

The method will be illustrated by an example. We will convert an mechanical structure (translational) into a bond graph model.

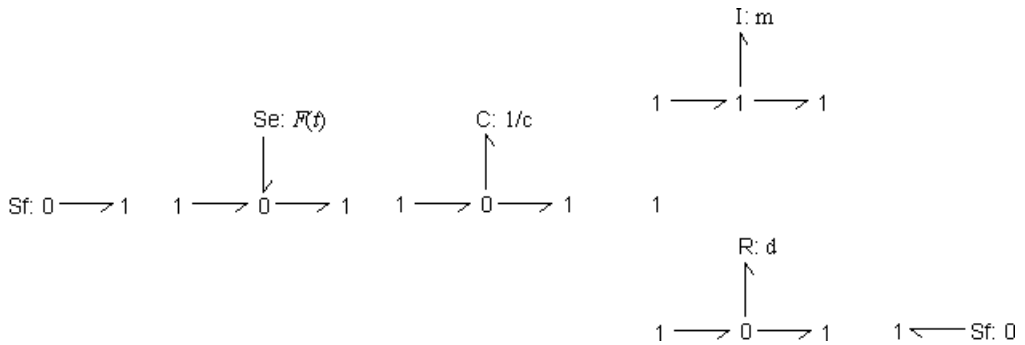
1. Create an iconic diagram



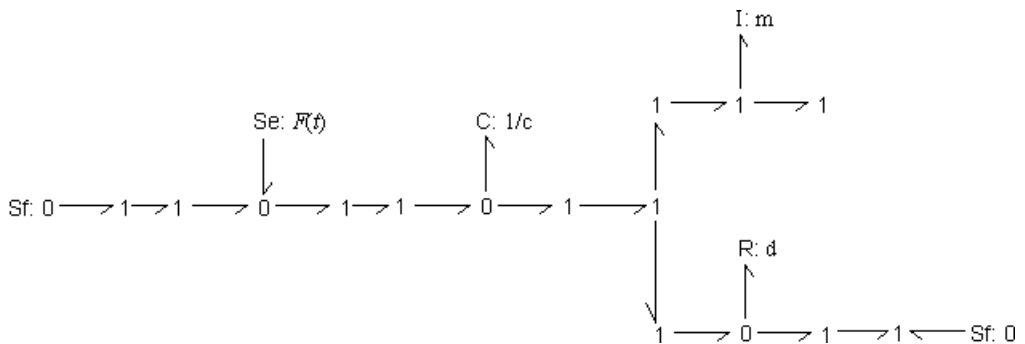
2. Split up reference points. In this diagram this is not possible.
3. Replace elements by bond graph equivalents. Note that we have arranged the orientation of the bonds (the direction of the harpoon) as much as possible in the direction of the power flow from the source to the load elements.



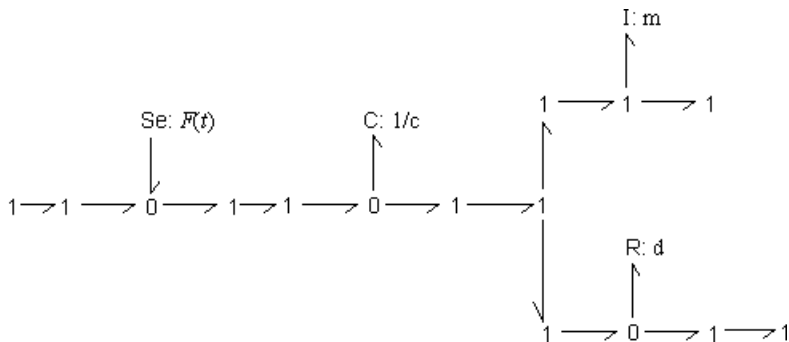
4. Replace every knot that has been left by a 1 junction.



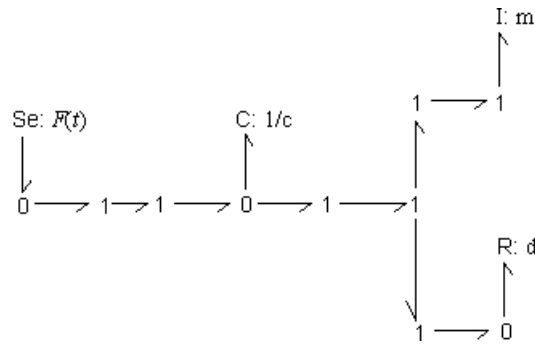
5. Connect all elements and junctions with bonds, according to the layout of the mechanical system. A comparison between the iconic diagram and the bond graph model clearly shows the symmetry between both representations. It is obvious that any change or addition in the iconic diagram, can be easily implemented in the bond graph model.



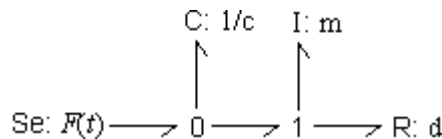
6. Simplify the resulting bond graph model. First we eliminate the Sources ( $Se$  elements) with zero output.



7. Eliminate loose junctions.



8. Eliminate junctions.



The simplified model does not show a direct symmetry with the iconic diagram. It does give a clear insight in the flows of power from the force source to the other elements.

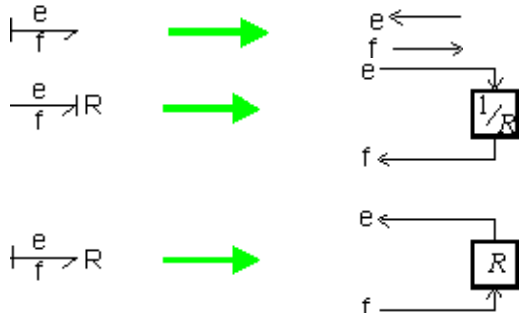
### From Bond Graph to Block Diagram

With a causal bond graph model, equivalent block diagram models can easily be derived. To create a block diagram, the following steps have to be performed.

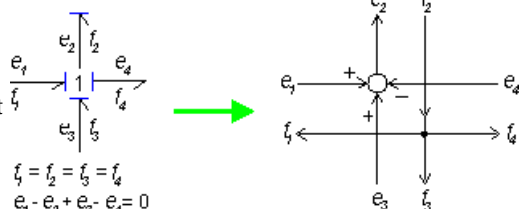
- Change bonds by equivalent bilateral signals.



- Replace elements by corresponding block diagram symbols. Use the correct effort and flow description which can be found in the element tables. As an example both descriptions for the R-element are given.



- Replace the junctions by signal summation points and signal splitters. If correct, the bonds have already been replaced by effort and flow signals. Out of these signals and the junction description you can derive the effort

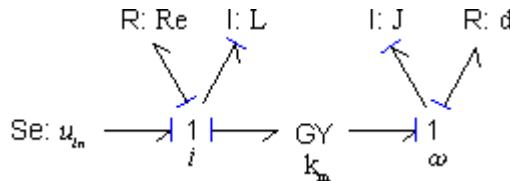




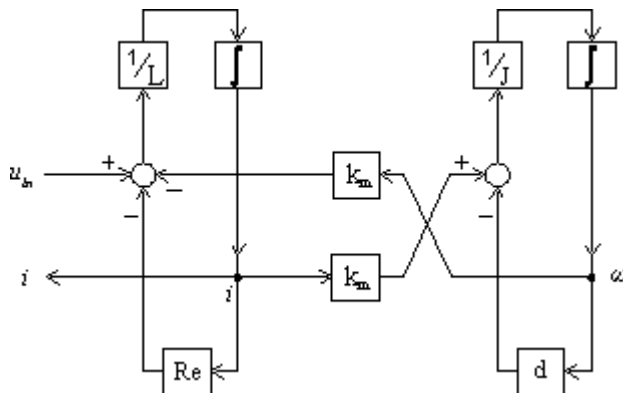
and flow equations for the junction. As an example the conversion for a 1 junction is shown.

### Example

As an example in the figure below a causal bond graph model is shown.



Using the given set of rules and the element descriptions an equivalent block diagram model is found, which is shown below.



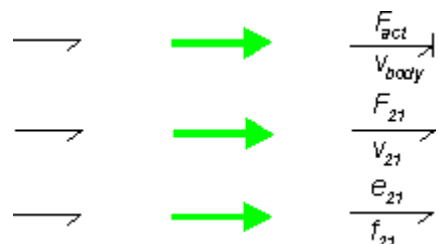
The resulting block diagram model can be simplified by combining blocks and elimination of loops. Out of the block diagram, easily a set of dynamic equations can be deduced.

### From Bond Graph to Equations

With a causal bond graph model, equivalent dynamic equations can easily be derived. To create the dynamic equations, the following steps have to be performed.

- Denote for every bond its effort and flow pair.

You can use names that are obvious or methodically use numbers. Some examples are shown at the right.



- Replace elements by corresponding dynamic equations. Use the correct effort and flow description which can be found in the element tables. As an example descriptions for the R-element are given.

$$\begin{array}{lcl} \frac{F_{act}}{V_{body}} \rightarrow R & \longrightarrow & V_{body} = (1/R) F_{act} \\ \frac{e_{21}}{f_{21}} \rightarrow R & \longrightarrow & e_{21} = R f_{21} \end{array}$$

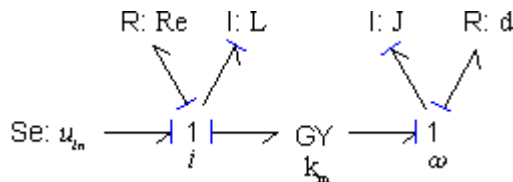
- Replace the junctions by the correct equations. For 0 junctions the efforts are equal. All flows of the bonds pointing towards the 0 junction should be added and all flows of the bonds pointing from the 0 junction should be subtracted. For 1 junctions the flows are equal. All efforts of the bonds pointing towards the 0 junction should be added and all efforts of the bonds pointing from the 0 junction should be subtracted. Some examples are shown at the right.

$$\begin{array}{lcl} \begin{array}{c} e_2 \uparrow f_2 \\ e_1 \rightarrow 1 \leftarrow e_4 \\ f_1 \leftarrow f_4 \\ e_3 \downarrow f_3 \end{array} & \longrightarrow & \begin{array}{l} f_1 = f_2 = f_3 = f_4 \\ e_1 - e_2 + e_3 - e_4 = 0 \end{array} \\ \begin{array}{c} e_2 \uparrow f_2 \\ e_1 \rightarrow 0 \leftarrow e_4 \\ f_1 \leftarrow f_4 \\ e_3 \downarrow f_3 \end{array} & \longrightarrow & \begin{array}{l} e_1 = e_2 = e_3 = e_4 \\ f_1 - f_2 + f_3 - f_4 = 0 \end{array} \end{array}$$

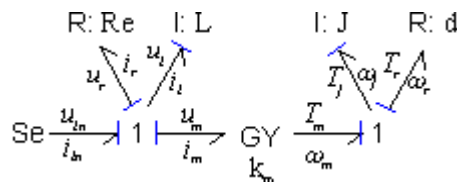
- Rearrange the equations by removing redundant variables.

### Example

As an example in the figure below a causal bond graph model is shown. We will derive the set of dynamic equations out of this model.



- Denote all efforts and flows. This is shown below:



- Write the dynamic equations of the elements and junctions:

#### elements

#### equations

Se	$u_{in} = \text{constant}, i_{in} = \text{free}$
R	$u_r = R i_r$
I	$i_l = (1/L) \int u_l dt$
1 junction	$i_{in} = i_r = i_l = i_m$ $u_{in} - u_r - u_l - u_m = 0$
GY	$u_m = k_m \omega_m$ $T_m = k_m i_m$
I	$T_j = (1/J) \int \omega_j dt$
R	$T_r = d \omega_r$
1 junction	$\omega_m = \omega_j = \omega_r$ $T_m - T_l - T_r = 0$

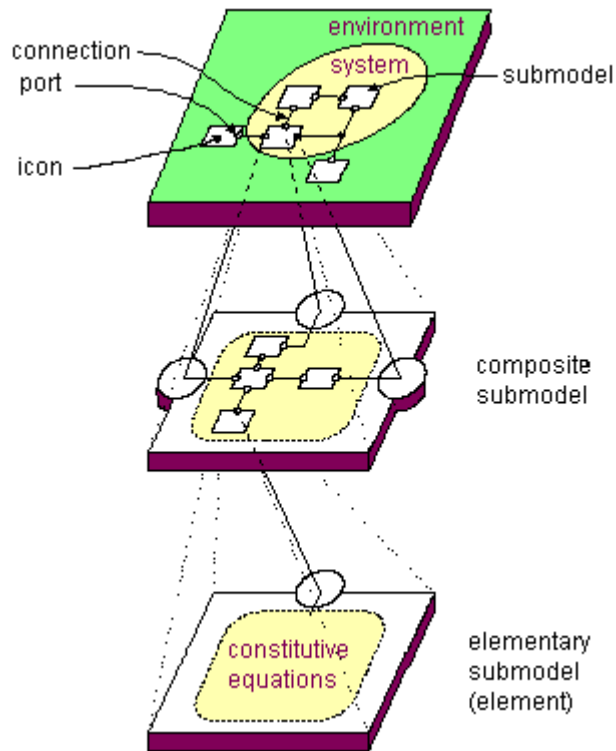
3. Reduce the amount of equations. We replace the equalities of the 1 junctions:  
 $i_{in} = i_r = i_l = i_m = i$  and  $\omega_m = \omega_j = \omega_r = \omega$ .

<b>elements</b>	<b>equations</b>
Se	$u_{in} = \text{constant}$
R	$u_r = R i$
I	$i = (1/L) \int u_l dt$
1 junction	$u_{in} - u_r - u_l - u_m = 0$
GY	$u_m = k_m \omega$ $T_m = k_m i$
I	$T_j = (1/J) \int \omega dt$
R	$T_r = d \omega$
1 junction	$T_m - T_l - T_r = 0$

The resulting dynamic equations can be used for simulation. 20-sim can automatically extract the dynamic equations out of a bond graph model. The equations can be shown using the Show Equations command or used in the Simulator for simulation.

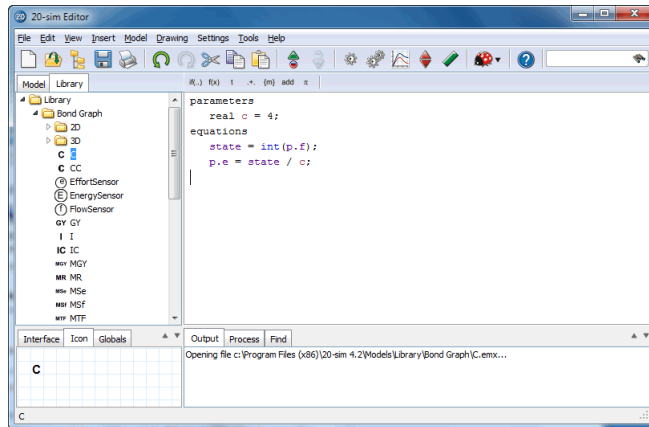
## Ports

A port is a location where an element can exchange information (in case of a signal port) or power (in case of a power port) with its environment. So, it is the model port that defines the connection with the element. A port is an important concept, as it allows you to describe the properties of the bonds that can be connected to the element, i.e., its direction, size, domain, etc. Ports can be defined in 20-sim using the *Interface Editor*.



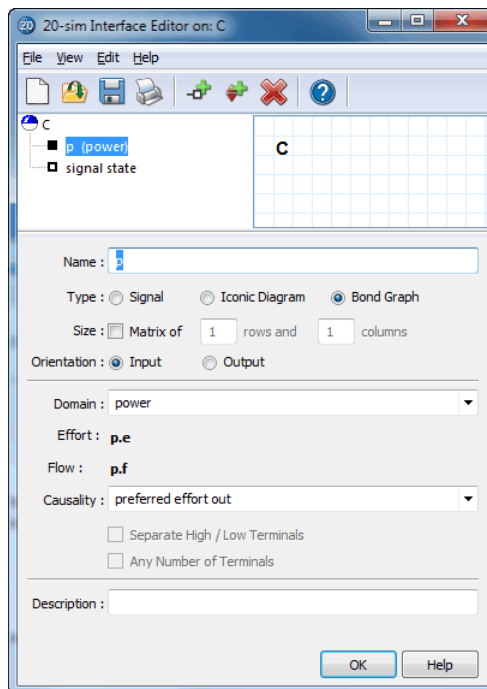
## Port Variables

All ports of a submodel are shown in the Interface tab. In the figure below a standard *C-element* is shown with one power port  $p$ . Each port has an effort and a flow variable. In 20-sim these variables are denoted with the extensions  $.e$  and  $.f$ . You can see an example in the figure below where equations are defined using the variables  $p.e$  and  $p.f$ .



## Port Properties

Ports can be added and defined in the 20-sim Interface Editor. The *Interface Editor* of the *C-element* is shown below.



Bond graph ports have several properties:

- **Name:** The name of the port.
- **Type:** Next to bond graph ports, 20-sim also knows iconic diagram ports and signal ports
- **Orientation:** The orientation of a connected bond (indicated by the half arrow).

- *fixed in orientation*: The bond will point towards the element.
- *fixed out orientation*: The bond will point from the element to another element.
- *Rows/Columns*: The standard size of a port and corresponding bond is 1 but you can also define ports with larger sizes.
- *Domain*: The domain of the port.
- *Causality*: The preferred causality of the port variable (effort and flow). You have to defined here what should be the input variable (effort or flow) and what should be the output variable (effort or flow).

## Creating your own Elements

In 20-sim you can easily create your own bond graph elements. The process of creation consists of three parts:

1. For any bond connected to your submodel an internal port has to be defined. For each port you have to specify some data:
  - The physical domain.
  - The size.
  - The orientation.
  - The causality.
2. Create the icon for the component. This can be done with a specialized drawing editor.
3. Create the element description. This can be done by (differential) equations or by a bond graph.

## Bond Graph Literature

A vast number of publications and books on bond graph modeling have been issued. Here is only referred to some well known books. A comprehensive collection of bond graph literature can be found on the Internet pages of prof. F. Cellier (<http://www.ece.arizona.edu/~cellier/bg.html>) and the mirror site at the Glasgow University (<http://www.eng.gla.ac.uk/bg/>).

Alan J. Blundell (1982)

Bond Graphs for Modelling Engineering Systems

Ellis Horwood Publishers, Chichester, United Kingdom, and Halsted Press, New York, 151p.

Peter C. Breedveld, Geneviève Dauphin-Tanguy (1992)

Bond Graphs for Engineers

Elsevier Science Publishers, Amsterdam.

François Edouard Cellier (1991)

Continuous System Modeling

Springer-Verlag, New York, ISBN 0-387-97502-0, 755p.

Dean C. Karnopp, Ronald C. Rosenberg (1968)

Analysis and Simulation of Multiport Systems - The Bond Graph Approach to Physical Systems Dynamics

M.I.T. Press.

Dean C. Karnopp, Ronald C. Rosenberg (1974)

System Dynamics: A Unified Approach  
John Wiley, New York.

Dean C. Karnopp, Donald L. Margolis, Ronald C. Rosenberg (1990)  
System Dynamics: A Unified Approach - 2nd Edition  
John Wiley, New York.

Lennart Ljung, Torkel Glad (1994)  
Modeling of Dynamic Systems  
Prentice Hall, Englewood Cliffs, N.J.

Henry M. Paynter (1961)  
Analysis and Design of Engineering Systems  
M.I.T. Press, Cambridge, Mass.

Ronald C. Rosenberg, Dean C. Karnopp (1983)  
Introduction to Physical System Dynamics  
McGraw-Hill, New York.

Nobuhide Suda (1988)  
System Dynamics  
Koronasha, Tokyo. (in Japanese)

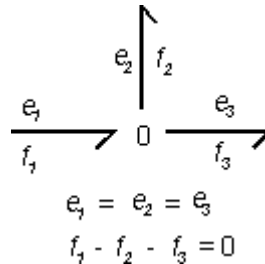
Jean U. Thoma (1982)  
Grundlagen und Anwendungen der Bonddiagramme  
Girardet Taschenbuch GT20, Essen, Germany.

Jean U. Thoma (1989)  
Simulation by bond graphs - Introduction to a Graphical Method  
Springer-Verlag, New York.

## Standard Elements

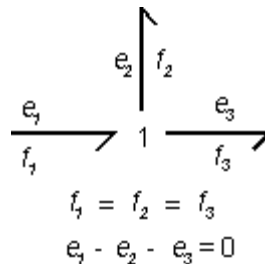
Junctions couple one or more elements of a model in a power continuous mode: no energy is stored or dissipated. Examples are a series junction or parallel junction in an electrical network, a fixed connection between two mechanical parts etc. Two types of junctions exist: 0 junctions and 1 junctions.

## 0 junction



The 0 junction represents a coupling where all efforts of the connected bonds are equal. As a consequence of the property of power continuity the sum of the flows must be equal to zero. The orientation of the bonds determines the sign of the flow summation: all flows of the bonds pointing towards the 0 junction should be added and all flows of the bonds pointing from the 0 junction should be subtracted. This summation corresponds to the *Kirchhoff current law* for electrical networks. The equality of the efforts, limits the causality. Only one bond may have an "effort-in" causality (the stroke pointed towards the 0 junction). All other bonds must have (seen from the 0 junction) an "effort-out" causality (stroke pointing from the 0 junction). In other words: the 1 junction has a *constraint causality*.

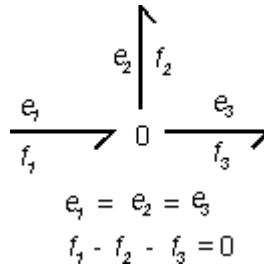
## 1 junction



The 1 junction is the dual form of the 0 junction (effort and flow are opposite). The 1 junction represents coupling where all flows of the connected bonds are equal. As a consequence of the property of power continuity the sum of the efforts must be equal to zero. The orientation of the bonds determines the sign of the flow summation: all efforts of the bonds pointing towards the 1 junction should be added and all efforts of the bonds pointing from the 1 junction should be subtracted. This summation corresponds to the *Kirchhoff voltage law* for electrical networks. The equality of the flows, limits the causality. Only one bond may have an "effort-out" causality (the stroke pointing from the 1 junction). All other bonds must have (seen from the 1 junction) an "effort-in" causality (stroke pointing to the 1 junction). In other words: the 1 junction has a *constrained causality*.



Suppose we have the following 0 junction with one bond (1) pointing towards the junction and two bonds (2 and 3) pointing from the junction.



1. For a 0 junction the efforts are always equal! This means:

$$e_1 = e_2 = e_3$$

2. The junction is power continuous. For the figure above this means:

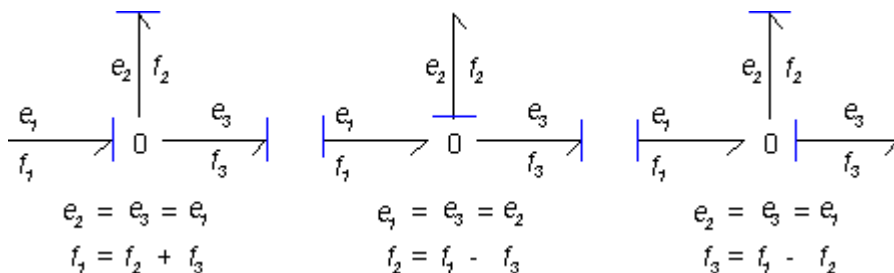
$$e_1 \times f_1 = e_2 \times f_2 + e_3 \times f_3$$

3. Combining 1 and 2 yields:

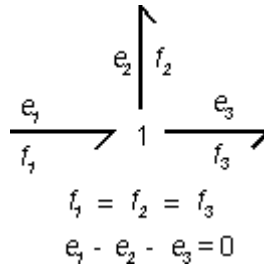
$$f_1 - f_2 - f_3 = 0$$

The last equation can also be derived with a rule of thumb: All flows of the bonds pointing *towards* the 0 junction should be added and all flows of the bonds pointing *from* the 0 junction should be subtracted.

The first equation, limits the causality. Only one bond may have an *effort-in* causality (the stroke pointed towards the 0 junction). All other bonds must have (seen from the 0 junction) an *effort-out* causality (strokes pointing from the 0 junction). For the example junction this means three possible causal forms can exist:



Suppose we have the following 1 junction with one bond (1) pointing towards the junction and two bonds (2 and 3) pointing from the junction.



1. For a 1 junction the flows are always equal! This means:

$$f_1 = f_2 = f_3$$

2. The junction is power continuous. For the figure above this means:

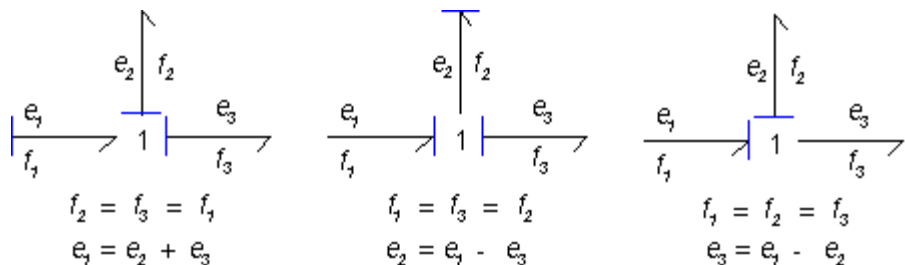
$$e_1 \times f_1 = e_2 \times f_2 + e_3 \times f_3$$

3. Combining 1 and 2 yields:

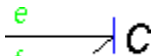
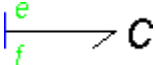
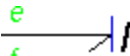
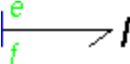
$$e_1 - e_2 - e_3 = 0$$

The last equation can also be derived with the rule of thumb: All effort of the bonds pointing *towards* a 1 junction should be added and all efforts of the bonds pointing *from* the 1 junction should be subtracted.

The first equation, limits the causality. Only one bond may have an *flow-in* causality (the stroke pointed from the 1 junction). All other bonds must have (seen from the 1 junction) a *flow-out* causality (strokes pointed towards the 1 junction). For the example junction this means three possible causal forms can exist:

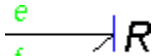
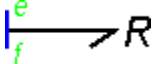


Buffers are bond graph elements that can store energy. There are two types of buffers: **C-elements** and **I-elements**. The table below shows the effort and flow descriptions that belong to these elements. The parameters "C" and "I" are the *buffer constants*, which determine a linear buffer behavior. Examples of C-elements are a mechanical spring and an electrical capacitor. Examples of an I-element are a mechanical inertia and an electrical inductance.

C-element	bond graph element	equation
effort-in causality		$f = C \, de/dt$
effort-out causality		$e = (1/C) \, \text{int}(f)$
I-element	bond graph element	equation
effort-in causality		$f = (1/I) \, \text{int}(e)$
effort-out causality		$e = I \, df/dt$

Buffer elements do not fix the direction of the effort and flow. Both effort-in as well as effort-out causality is allowed. With simulation however, we prefer to avoid differentiation. In other words, with the C-element the effort-out causality is *preferred* and with the I-element the effort-in causality is *preferred*.

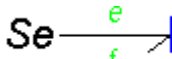
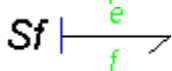
A resistance, R, dissipates free energy. This energy of any arbitrary domain is transported **irreversibly** to the thermal domain. This means the power towards a resistance is always positive. In the table below the effort and flow description of the resistance is shown. Examples of a resistance are a mechanical damper and an electrical resistor.

R-element	bond graph element	equation
effort-in causality		$f = (1/R) \, e$
effort-out causality		$e = R \, f$

The direction of effort and flow is not restricted for a resistance and there is no preferred form for the equation. In other words: the R-element has a *indifferent causality*.



Sources represent the interaction of a systems with its environment. There are two types of source elements: effort sources (Se) and flow sources (Sf).

In the table below the effort and flow description of the source elements is shown. Examples of a flow source are an electrical current source and a hydraulic pump that generates a constant flow of liquid. Examples of an effort source are an electrical voltage source and a constant mechanical force.

element	bond graph element	equation
effort source		$e = c, f = \text{free}$
flow source		$f = c, e = \text{free}$

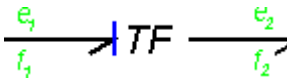
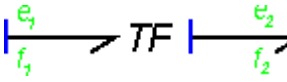
The direction of effort and flow for sources are restricted. In other words: the Se-element (effort-out) and Sf-element (effort-in) have a *fixed causality*.


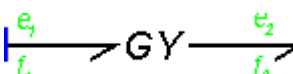
Next to the standard effort and flow sources, that generate a constant effort and flow, bond graph modeling also allows the use of so called **modulated sources**. In these sources the resulting effort or flow are equal to a (fluctuating) value provided by an input signal. Two types of modulated sources are known: the modulated effort source **MSe** and the modulated flow source **MSf**. In the table below the effort and flow description of the source elements is shown.

element	bond graph element	equation
modulated effort source		$e = u, f = \text{free}$
modulated flow source		$f = u, e = \text{free}$

The direction of effort and flow for sources are restricted. In other words: the MSe-element (effort-out) and MSf-element (effort-in) have a *fixed causality*.

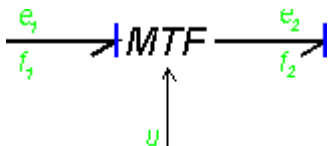
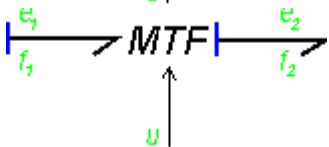
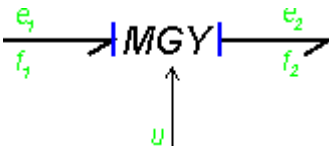
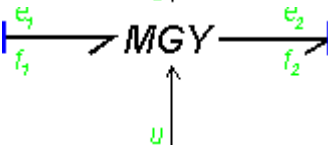
Transformers and gyrators are bond graph elements that can convert energy ideally, as well in one physical domain as well as between one physical domain and another. A transformer is denoted by the mnemonic code **TF** and a gyrator by the code **GY**. In the table below the effort and flow equations are shown. The parameters  $r$  and  $n$  are the *transformation ratio* and *gyration ratio*. An example of a transformer is a mechanical gear. An example of a gyrator is a DC-motor.

TF-element	bond graph element	equation
effort-in causality		$f_1 = (1/n) f_2$ $e_2 = (1/n) e_1$
effort-out causality		$f_2 = n f_1$ $e_1 = n e_2$

<i>GY-element</i>	<i>bond graph element</i>	<i>equation</i>
effort-in causality		$f_1 = (1/r) e_2$ $f_2 = (1/r) e_1$
effort-in causality		$e_1 = r f_2$ $e_2 = r f_1$

The directions of the flow and effort are partly fixed for a transformer. Like the 1 junction and the 0 junction, the causality is *constraint*. For a transformer, an effort-in causality on the incoming bond results in an effort-out causality on the outgoing bond and vice-versa. For a gyrator, an effort-in causality on the incoming bond results in an effort-in causality on the outgoing bond and vice-versa.

Next to transformers and gyrators with a fixed transformation ratio and gyration ratio, in bond graphs also modulated transformers (**MTF**) and modulated gyrators (**MGY**) are supported. In these models the transformation ratio or gyration ratio are equal to a (fluctuating) value provided by an input signal. In the table below the effort and flow equations are shown.

<i>MTF-element</i>	<i>bond graph element</i>	<i>equation</i>
effort-in causality		$f_1 = (1/u) f_2$ $e_2 = (1/u) e_1$
effort-out causality		$f_2 = u f_1$ $e_1 = u e_2$
<i>MGY-element</i>	<i>bond graph element</i>	<i>equation</i>
effort-in causality		$f_1 = (1/u) e_2$ $f_2 = (1/u) e_1$
effort-in causality		$e_1 = u f_2$ $e_2 = u f_1$

The directions of the flow and effort are partly fixed for a modulated transformer. Like the 1 junction and the 0 junction, the causality is *constraint*. For a transformer, an effort-in causality on the incoming bond results in an effort-out causality on the outgoing bond and vice-versa. For a gyrator, an effort-in causality on the incoming bond results in an effort-in causality on the outgoing bond and vice-versa.

### 10.3 Iconic Diagrams

#### Dynamic Systems

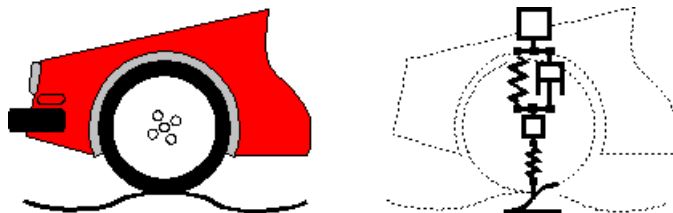
An important aspect in mechatronic systems is the dynamic behavior, i.e. the behavior of the system as function of time. Especially in systems that display swift changes or systems that should behave accurately, the dynamic behavior is important. It is therefore useful to predict the dynamic behavior of a system. Modeling and simulation is useful for making such predictions.

There are various methods of modeling and simulating dynamic systems. A well known one is the *Lumped Parameter Method*.

With the *Lumped Parameter Method*, the dynamic behavior of a system is concentrated in discrete points. The interaction of these points gives us insight in the behavior of the real system. The more discrete points are used the more accurate the model will be.

There are various ways to represent lumped parameter models. Well known representations are iconic diagrams, differential equations, block diagrams and bond graphs.

Let's consider the suspension of a car. A lumped parameter model starts with the identification of the various lumps (or parts or components) of this system. We start with the car body. It is supposed to be a rigid body and therefore this part is represented with the icon of a mass. The suspension of the car is represented by a spring damper combination. The wheel is considered to have a significant mass and to be elastic. This component is therefore represented by a mass and spring icon. Finally the road is modeled by path generator function. The resulting ideal physical model (IPM) is shown below.



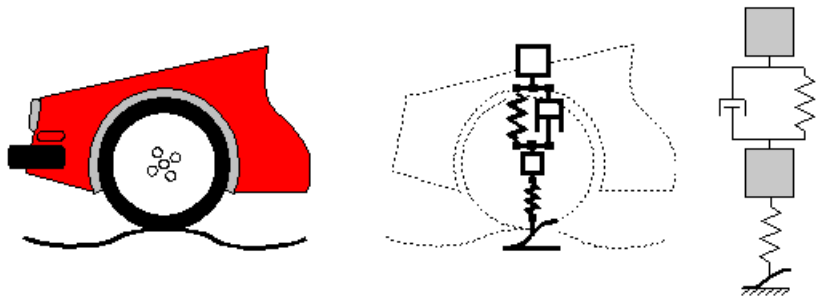
*Iconic diagram of a car suspension.*

#### Iconic Diagrams

If we can represent the various parts of an ideal physical model by predefined models or components modeling is easy. In 20-sim a large library of components is available allowing you to create a model just by selecting the proper components and connect them according to the ideal physical model. To make modeling even more easy, the components are displayed in the editor by icons which look like the corresponding parts of the ideal physical model. In 20-sim these kind of models are called iconic diagrams (sometimes other simulation tools refer to this kind of modeling as component based modeling). 20-sim can

automatically compute simulation code out of an iconic diagram and start a simulation.

Look again at the car suspension example. In the picture below at the right an iconic diagram is shown that has been entered in 20-sim. As you can see, the iconic diagram is similar to the ideal physical model. Each component of the iconic diagram represents a physical process. For example the mass component represents the law of motion ( $F = m \cdot a$ ) and the spring represents the linear spring equation ( $F = k \cdot x$ ). The connections between the components in the iconic diagram represent ideal energy transfer between those components, i.e. no energy is stored, generated or dissipated.



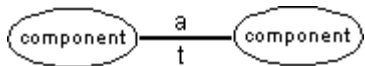
*A iconic diagram model of a car suspension.*

An iconic diagram describes a physical system as a number of physical concepts (the components) connected by energy flows (the connections).

**Across and through**

A connection between two components transfers energy from one component to the other. This flow of energy can be described in many ways. In 20-sim a uniform approach is chosen:

The flow of energy between two components of an iconic diagram can be characterized by two variables, of which the product is power. These variables are called *across* (*a*) and *through* (*t*).



*Across and through as variables of a connection.*

The across and through variables make up a combination that is typical for a physical domain. For example voltage and current are used for electrical networks and force and velocity are used for mechanical (translation) systems. The table below shows the variables for the domains that are currently supported in 20-sim.

Domain	across ( <i>a</i> )	through ( <i>t</i> )
power	across <i>a</i>	through <i>t</i>
mechanical (translation)	velocity <i>v</i> [m/s]	force <i>F</i> [N]
mechanical (rotation)	angular velocity <i>omega</i> [rad/s]	torque <i>T</i> [Nm]
pneumatic	pressure <i>p</i> [Pa]	volume flow <i>phi</i> [m <sup>3</sup> /s]

thermal	temperature $T$ [K]	entropy flow $dS$ [J/Ks]
electric	voltage $u$ [V]	current $i$ [A]
hydraulic	pressure $p$ [Pa]	volume flow $\phi$ [m <sup>3</sup> /s]
magnetic	magnetomotive force $i$ [A]	flux change $d\phi/dt$ [V]
pseudothermal	temperature $T$ [K]	heat flow $dQ$ [W]

*The across and through variables for several domains.*

To most general domain is power. Connections of this domain can be used for all domains. For the thermal domain there is one pair of across and through,  $T$  and  $dS$ , that multiplies to power. The pair  $T$  and  $dQ$  however is more often used but does not multiply to power. Therefore the domain with these variables is called pseudothermal.

There is a direct relation between the across and through variables of an iconic diagram and the effort and flow variables of a bond graph:

Domain	Non-mechanical domains	Mechanical Domains
across variable	effort	flow
through variable	flow	effort

*The relation between across and through variables and effort and flow variables.*

### Note

- 20-sim propagates domains. If a connection of the general power domain is tied to a component of the electrical domain, it automatically becomes an electrical connection. The other end of the connection can then only be tied to another component of the electrical domain. In this way it is prevented to connect components of different physical domains.
- If you want to use a connection of a domain that is not supported or has variables other than across and through, use the general power domain. The across and through variables can then be used as an alias of your own variables.

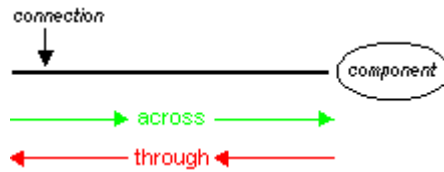
### Connections

When two components in an Iconic Diagram are connected, one component will always compute the across variable, while the opposite component will always determine the through variable.

We can therefore also interpret a connection as a bilateral signal connection (across-signal and through-signal), of which the directions are opposite to each other.



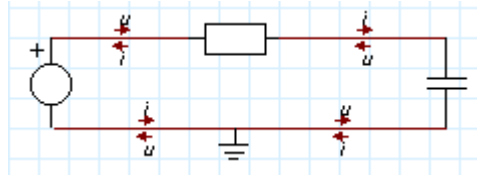
With "direction" we mean the computational direction, just like signals in a block diagram. In a block diagram the across and through variables, which together form the flow of power, are not shown as a couple. This breaks up the symmetry between the physical system and the structure of the model.



*A connection as a bilateral signal flow.*

The interpretation of a connection as a bilateral signal flow, does not fix the individual direction of the across variable and the through variable. It only means the direction of the across variable and through variable are opposite.

The specific computational direction of across and through variables is called causality. In 20-sim an advanced algorithm detects the possible causalities of each submodel and tries to combine these in such a way, that optimal simulation code will be generated. The result can be inspected using the *Causality Info* command from the *View* menu. The result of this command is shown in the example below. The computational direction of forces and velocities is clearly shown for all the connections.

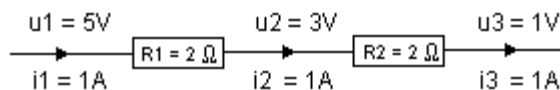


## Orientation (Across)

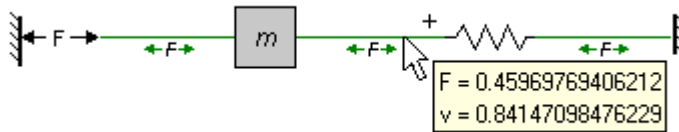
When simulating, you have to know how across and through variables are oriented to make a correct interpretation of what is happening. 20-sim can show the orientation when you select the *Orientation Info* option of the *View* menu.

### Across variables in the Top Level

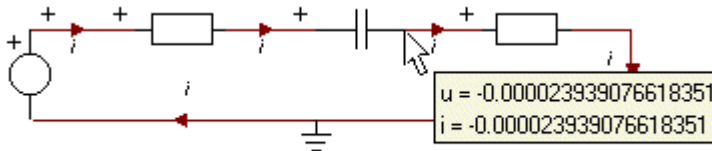
Across variables in the top level of a model are always defined with respect to a single global reference. In the picture below an electrical iconic diagram is shown with three voltages ( $u_1 = 5\text{ V}$ ,  $u_2 = 3\text{ V}$  and  $u_3 = 1\text{ V}$ ). This means these voltages are all defined with respect to the same reference, e.g., the ground  $u = 0\text{ V}$ .



All variables values of a connection can be easily inspected during simulation by placing the mouse pointer on top of that connection as shown below. The connection between the mass and the spring (see picture below) shows an across value  $v = 0.84\text{ m/s}$ . This means the point where the mass and spring are connected has a global velocity of  $v = 0.84\text{ m/s}$ .



In the figure below the connection between the capacitor and the resistor shows a negative voltage of  $u = -2e-5$  V.

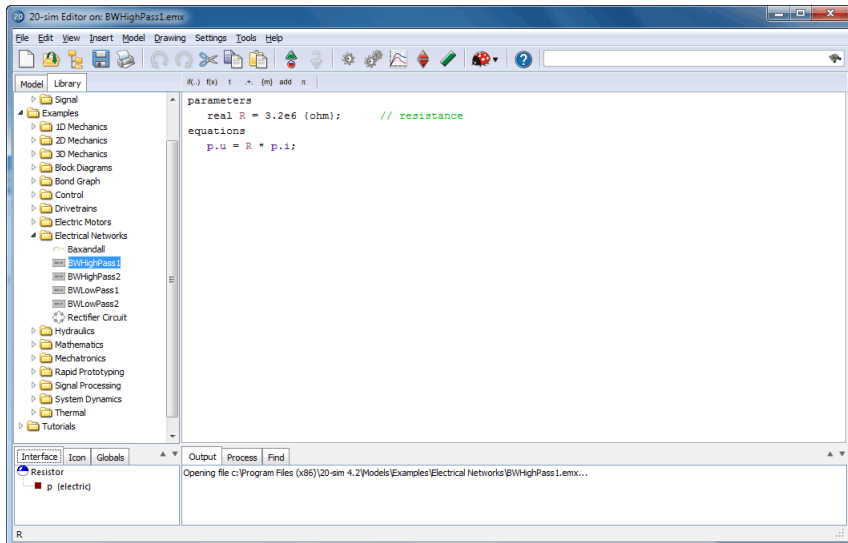


### Across variables in Submodels

In submodels you have to inspect how across variables are defined. For example an ideal electrical resistor (see figure below) uses separate high and low terminals. The internal equations are:

$$\begin{aligned} p.u &= p\_high.u - p\_low.u; \\ p\_high.i &= p\_low.i = p.i; \\ p.u &= R * p.i; \end{aligned}$$

where p.high and p\_low are the ports to the connections at both sides of the resistor. p\_high.u and p\_low.u are voltages defined with respect to the global reference, but p.u is the voltage difference between the high and low port and therefore not defined with respect to the global reference.



The definition of across variables depends on the definition of number of terminals of a port, which is shown in the Type Editor. To inspect the ports, put the mouse pointer on top of the Type section and select **edit type** from the right mouse menu.

### Note

- The geometrical layout of the iconic diagram does not have a meaning. If a resistor is drawn upside down, its current is still defined with respect to the resistor (flowing towards or from). If a mass is drawn upside down, its force is still defined with respect to that mass (pulling or pushing).
- To show or hide the orientation of an Iconic Diagram select or deselect the *Orientation Info* option of the *View* menu.

### Orientation (Through)

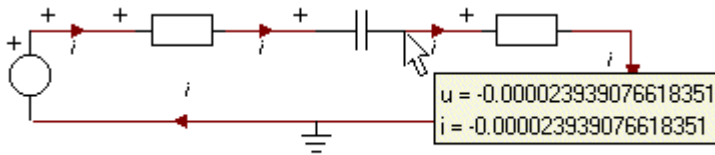
When simulating, you have to know how across and through variables are oriented to make a correct interpretation of what is happening. 20-sim can show the orientation when you select the *Orientation Info* option of the **View** menu.

### Through variables in connections

Through variables in connections are always defined with respect to the components they are connected with. 20-sim automatically assigns an orientation for these through variables. This orientation can be made visible by selecting the *Orientation Info* command of the *View* Menu.

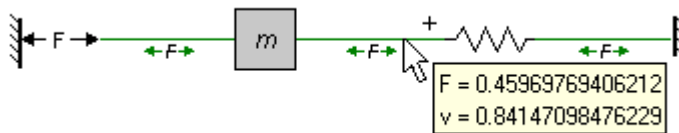
### Non-mechanical

Through variables that are not of the mechanical domain are always shown with an arrow in the connection. The arrow indicates the direction of the positive flow. The figure below shows a negative current:  $i = -2e-5$  A. This means the current flows in the opposite direction of the arrow.



## Mechanical

Through variables of the mechanical domain are always shown with two arrows. The arrows indicate the direction of the positive force. The figure below shows a positive force:  $F = 0.45$  N. This means the spring pushes with a force of  $F = 0.45$  [N] upon the mass and the mass pushes with a force of  $F = 0.45$  N upon the spring (note: a negative force would mean pulling instead of pushing).



This interpretation of forces in 20-sim is only valid when a positive velocity defined from the left to the right, and from the bottom to the top!

## Through Variables in Submodels

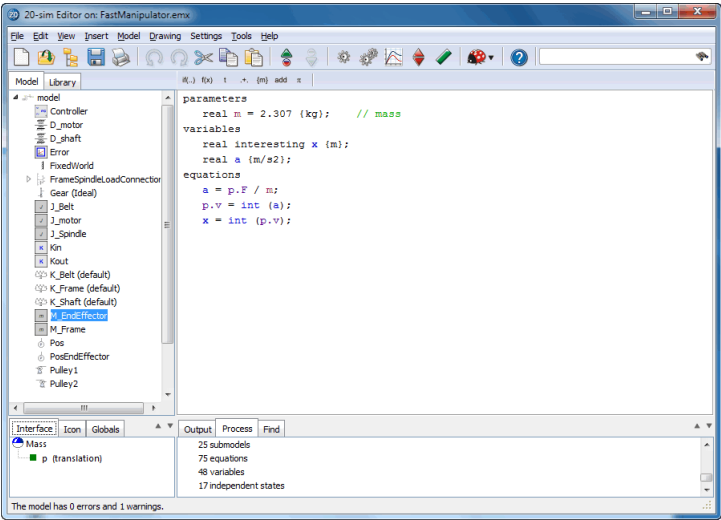
In submodels, you have to use the Type Editor to find out how through variables are defined. For example an ideal mass (see next figure) uses the option any number of terminals for its port (inspect the port in the Type Editor). The port equations are:

$$\begin{aligned} p.F &= p1.F + p2.F \\ p.v &= p1.v = p2.v; \end{aligned}$$

The internal equations are:

$$\begin{aligned} p.v &= (1/m) * \text{int}(p.F); \\ x &= \text{int}(p.v); \end{aligned}$$

where  $p1$  and  $p2$  are the ports to the connections at both sides of the mass.  $p1.v$  and  $p2.v$  are velocities defined with respect to the global reference. However,  $p.F$  (see also in the figure below) is the sum of the forces applied on both sides.



The definition of through variables depends on the definition of number of terminals of a port, which is shown in the Type Editor. To inspect the ports, put the mouse pointer on top of the Interface tab and select *Edit* from the right mouse menu.

**Note**

- The geometrical layout of the iconic diagram does not have a meaning. If a resistor is drawn upside down, its current is still defined with respect to the resistor (flowing towards or from). If a mass is drawn upside down, its force is still defined with respect to that mass (pulling or pushing).
- To show or hide the orientation of an Iconic Diagram select or deselect the *Orientation Info* option of the View menu.

**Global Reference**

20-sim iconic diagram models do not contain geometrical information. It is not important how a model is drawn, but how the elements are connected. To make a correct interpretation of the simulation results, the definition of references has to be known.

**Across**

Across variables in the top level of a model are always defined with respect to a single global reference. For all domains this global reference is equal to 0. The interpretation of this reference is up to the user. For example a zero pressure could be the absolute vacuum or the air pressure at ground level. For most physical domains, unless specified otherwise, a standard interpretation is used. This is shown in the table below.

Domain	Across (a)	Global Reference
power	across <i>a</i>	zero
mechanical (translation)	velocity <i>v</i> [m/s]	zero velocity
mechanical (rotation)	angular velocity <i>omega</i> [rad/s]	zero angular velocity

pneumatic	pressure $p$ [Pa]	air pressure at ground level
thermal	temperature $T$ [K]	absolute minimum temperature
electric	voltage $u$ [V]	<i>zero voltage</i>
hydraulic	pressure $p$ [Pa]	air pressure at ground level
magnetic	magnetomotoric force $i$ [A]	zero
pseudothermal	temperature $T$ [K]	absolute minimum temperature

**Through**

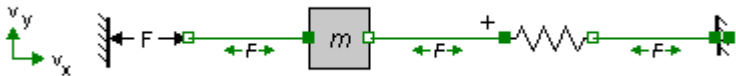
Through variables in connections are always defined with respect to the components they are connected with.

**Non-Mechanical**

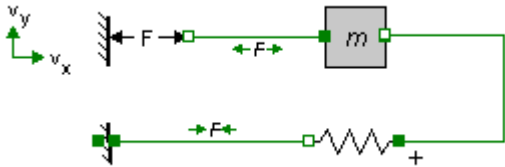
Through variables that are not of the mechanical domain are always shown with an arrow indicating the direction of the positive flow.

**Mechanical**

Through variables of the mechanical domain are always shown with two arrows indicating the direction of the positive force. Since mechanical variables are often geometrically interpreted, these arrows assume a positive velocity from the left to the right and from the bottom to the top.



See for example the system shown above. Look at the connection between the spring and the fixed world. Most users will correctly interpret a positive force as one that "makes the mass slow down". The same model is shown below. To prevent an incorrect interpretation such as a positive force "makes the mass accelerate", the arrows are pointing inwards.



This interpretation is only valid when you assume that a positive velocity is from the left to the right and from the bottom to the top!

**Causality**

The connection between two components describes the flow of power from one to the other. This power flow is always described by across and through variables. For example an electrical connection can be described by the variables voltage  $u$  and current  $i$  ( $u \cdot i = \text{power}$ ). Each Iconic Diagram component creates a causal relation between these variables. E.g. an electric resistor can be described by the equation:

$$u = i \cdot R;$$

where  $R$  is the resistance. Here the voltage is a function of the current. In 20-sim we say the component has a voltage out causality. This causality is not fixed. We can easily invert the equation:

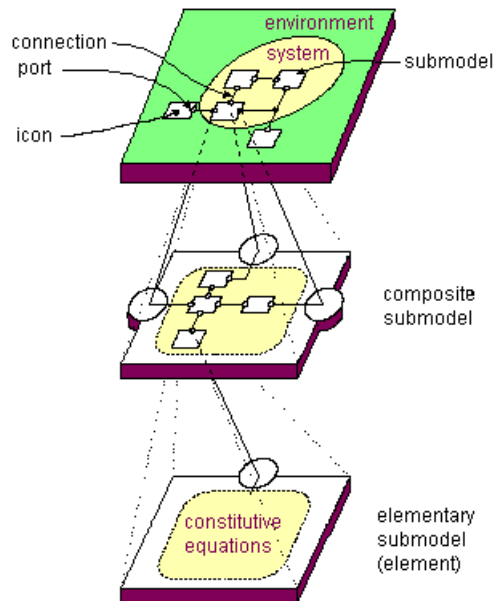
$$i = u/R;$$

Now the component has a current out causality. Which of the two equations will be used for the simulation depends on the other components.

In 20-sim an advanced algorithm detects the possible causalities of each model and tries to combine these in such a way, that optimal simulation code will be generated.

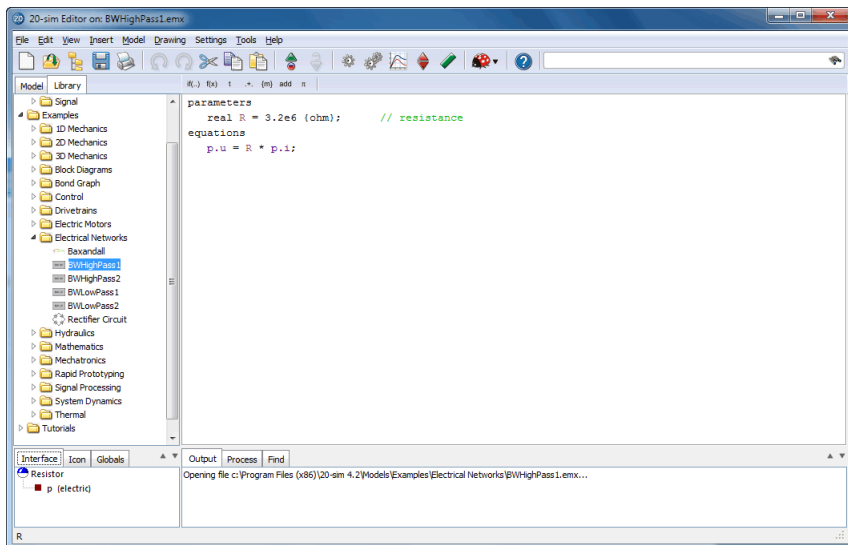
## Ports

A port is a location where a component can exchange information (in case of a signal port) or power (in case of a power port) with its environment. So, it is the port that defines the connection with a component. A port is an important concept, as it allows you to describe the properties of the connection that can be made to the component, i.e., its direction, size, domain, etc. Ports can be defined in 20-sim using the Type Editor.



## Port Variables

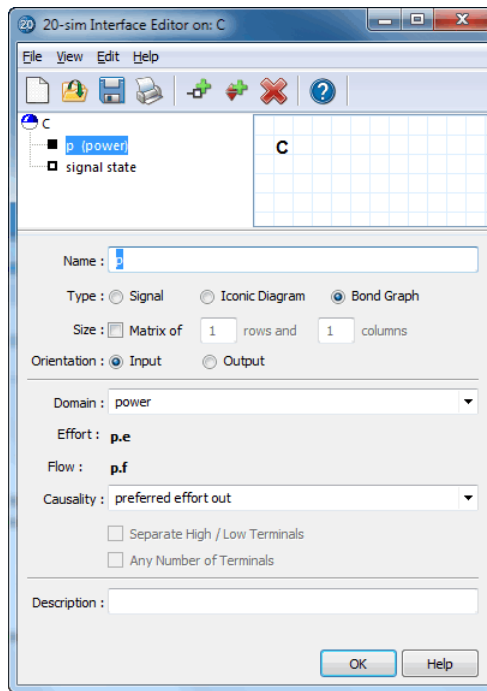
All ports of a submodel are shown in the Type window of the 20-sim Editor. In the figure below an electrical Resistor is shown with one power port  $p$ . Each port has an across and through variable. In 20-sim these variables are denoted with the extensions  $.a$  and  $.t$ . You can also use the names that are specific for a certain domain. For the electrical domain the extensions  $.u$  and  $.i$  are used. You can see an example in the figure below (Implementation section) where equations are defined using the variables  $p.u$  and  $p.i$ .



## Port Properties

Ports can be added and defined in the 20-sim Type Editor. You can open the *Interface Editor* in the Interface tab (right mouse menu). The *Interface Editor* of the Resistor is shown below.





## Port Properties

Iconic Diagram Ports have several properties:

- **Name:** The name of the port.
- **Type:** Next to Iconic diagram ports, 20-sim also knows bond graph ports and signal ports.
- **Size:** The standard size of a port and corresponding connection is 1 but you can also define ports with larger sizes.
- **Orientation:** The orientation of a port defines how the through variable is connected.
  - **Input:** A positive through variable will act upon a component in the positive direction (mechanical domain) or flows into the component (non-mechanical domain).
  - **Output:** A positive through variable will act upon a component in the negative direction (mechanical domain) or flows from the component (non-mechanical domain).

Note: The port orientation and the orientation of the corresponding connection can be made visible in 20-sim by arrows.

- **Domain:** The physical domain of the port.
- **Causality:** The causality of the port variable (across and through). You have to define here what should be the input variable (across or through) and what should be the output variable (across or through).

By default, an iconic diagram port is a port where power can be exchanged between a component and its environment in terms of an across variable and a through variable. Such a port is represented by one terminal. However, there are two special cases where it is desirable to define an iconic diagram port that has more than one terminal. These are the Separate High / Low Terminals port and the Any Number of Terminals port. These options are only for advanced users!

- **Separate High / Low Terminals:** Select the port to have two terminals. Only for experienced users!
- **Any Number of Terminals:** Select the port to have any number of terminals. Only for experienced users!

## Ports with more than one Terminal

By default, an iconic diagram port is a port where power can be exchanged between a component and its environment in terms of an across variable and a through variable. Such a port is represented by one terminal (connection point). However, there are two special cases where it is desirable to define an iconic diagram port that has more than one terminal.

### Separate High / Low Terminals

Consider, as an example, an mechanical spring. The power that flows into such a component is uniquely determined by the velocity difference between the two terminals of the component and the common force that acts upon both ends. Because of this one could say that there is one port, whose power is determined by one across value (the velocity difference) and one through value (the common force), but is represented by two terminals. To support this, 20-sim allows you to define a special type of iconic diagram port by indicating that it has Separate High / Low Terminals. The two terminals of the connection are named high and low. If the port is named p, the formal equations are:

#### fixed in orientation

$$\begin{aligned} p.t &= p1.t = p2.t \\ p.a &= p\_high.a - p\_low.a \end{aligned}$$

#### fixed out orientation:

$$\begin{aligned} p.t &= p1.t = p2.t \\ p.a &= - p\_high.a + p\_low.a \end{aligned}$$

In 20-sim these equations are automatically derived.

### Any Number of Terminals

Consider, as an example, a mass. A characteristic of this component is that you can connect many springs and dampers to it. Implicitly, one expects that the net force (i.e., the summation of the forces applied by the connected components) will be applied to the mass, and that it will have a single velocity. To support this, 20-sim allows you to define a special type of iconic diagram port by indicating the kind to be Any Number of Terminals. The terminals of the connection are named 1, 2, 3 etc.. If the port is named p, the formal equations are:

$$\begin{aligned} p.a &= p1.a = p2.a = p3.a = ..... \\ p.t &= sign(p1)*p1.t + sign(p2)*p2.t + sign(p3)*p3.t + .... \\ sign &= 1 \text{ when } p1 \text{ has a fixed in orientation etc.} \\ sign &= -1 \text{ when } p2 \text{ has a fixed out orientation etc.} \end{aligned}$$

In 20-sim these equations are automatically derived.

## Creating Iconic Diagrams

When you understand the concepts of across and through, including orientation, constructing an iconic diagram is easy:

1. Create an ideal physical model.
2. Select the components that represent the various parts of the ideal physical model and drag and drop them to the 20-sim editor. Iconic Diagram components can be found in the model library. Some standard components are shown in the tables of this tutorial.
3. Connect the components according to the ideal physical model.
4. Compile the model and run a simulation. For a good interpretation of the plots, you must know that across variables are always defined with respect to a global reference and through variables are always defined with respect to the components.

## Creating your own Components

In 20-sim you can easily create your own components. The process of creation consists of three parts:

1. For any connection an internal port has to be defined. For each port you have to specify some data:
  - The physical domain.
  - The size.
  - The orientation.
  - The causality.
2. Create the icon for the component. This can be done with a specialized drawing editor.
3. Create the component description. This can be done by (differential) equations or by an iconic diagram.

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20-sim is a modeling and simulation program that runs under Microsoft Windows. With 20-sim you can simulate the behavior of dynamic systems, such as electrical, mechanical and hydraulic systems or any combination of these.

20-sim fully supports graphical modeling, allowing to design and analyze dynamic systems in a intuitive and user friendly way, without compromising power. 20-sim supports the use of components. This allows you to enter models as in an engineering sketch: by choosing components from the library and connecting them, your engineering scheme is actually rebuilt, without entering a single line of math!

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